ALDERON IRON ORE CORP.



AMENDMENT TO THE ENVIRONMENTAL IMPACT STATEMENT VOLUME 3 APPENDICES – INFORMATION REQUEST RESPONSES

Appendix Q

NRCAN 07 Response and Supporting Documents

Information Request No. NRCan 07 (Labrador)

- a) A careful numerical or analytic estimation of the drawdown cone should be carried out because this drawdown estimate is of major importance. NRCan recommends that a long-term pumping test be performed at least in one of the two wells drilled down to 300 m, using many of the boreholes/wells as observation wells. These observation wells should be selected so as to obtain a good spatial coverage 1) in all directions and 2) at a large distance (2 km) to properly estimate the drawdown cone. Measurements of the water level of Lakes Gleeson and Daviault should also be carried out during pumping tests. The flow rate should be chosen so as to cause a large drawdown at the well, keeping in mind that the objective is to predict the dewatering effect of the 400 m-deep open pit.
- b) NRCan recommends that accurate estimates of hydraulic conductivity (K) in the vicinity of Rose Pit be calculated.
- c) It is recommended that the cross-section of Appendix A (of Appendix G) be improved so as to integrate geological formations, as well as existing wells and boreholes. Its location should be shown on one of the maps.
- d) Slug tests performed need to be re-analysed, because only straight lines, not curves, can be analyzed with the Bouwer and Rice (1976) method. Butler (1998) suggests a way for analysing these data: first normalize observed data, and then use data around a certain value. This method is summarized on the AqteSolv website: http://www.agtesolv.com/slu g-tests/recommended-normalized-head-ranges.htm. The K values might decrease slightly. The slug test in borehole BH-GE-06 should not be interpreted, as there is not enough data.

As mentioned earlier, the two lakes that are to the north and south of Rose pit (hydraulically connected to the one in the center) might be affected or dry up if they are not dammed.

Reference:

Butler, J.J., Jr., 1998. The Design, Performance, and Analysis of Slug Tests, Lewis Publishers, New York, 252p

Alderon Response to IR No. NRCan 07 (Labrador)

General Response

Since submission of the EIS, additional geological assessment, map creation, and geotechnical work has been completed which has advanced the understanding of the hydrogeological environment, as represented in this response. The current understanding of the existing and future hydrogeological environment is based on exploration geological data, geotechnical investigations, and hydrogeological testing and monitoring that have been completed to date and this has served to confirm and further support the hydrogeological model presented in the EIS.

The hydrologic and hydrogeological assessments completed to date indicate that the groundwater drawdown around the open pit development will not impact water levels in adjacent lakes. As part of the ongoing Project design process, Alderon will continue the field work and analyses necessary to update and refine the current model of the existing hydrogeological environment around the proposed open pit, and the potential impacts of the open pit development. The results will serve as key input planning, design, and operation of the open pit.

Response to IR No. NRCan 07 "a"

Part 1: Drawdown Cone Prediction

The conceptual cross section provided in the EIS showing the predicted drawdown from the open pit (now updated to show geology and attached as Drawing No. 121614000-306-GE-06; REV. 1) was developed on the basis of the limited hydrogeological information that was available at the time. It was assumed that the hydraulic conductivities from the packer testing were an indication of the bulk hydraulic conductivity of the bedrock. Since submission of the EIS, additional hydrogeological information has been obtained in the open pit area. This data supports the previous work and findings and includes:

- 11 additional rising head response tests performed on overburden or the till-overburden interface zone in the vicinity of open pit;
- Block geological model showing inferred orientation of faults based on core logs and core recovery;
- Falling head permeameter analysis of selected overburden materials; and
- Additional estimates of overburden hydraulic conductivity based on grain size distribution from sieve/hydrometer analysis.

The assessment of the existing and future hydrogeological environment presented in the EIS remains unchanged based on the review and incorporation of this additional data. The additional work outlined in Part 3, below, will update and refine the current model as part of the Project detailed engineering and design process.

Part 2: Long-term Pumping Test

To date, Alderon's field work and subsequent analyses have been constrained by requirements imposed on the project by the Newfoundland and Labrador Department of Environment and Conservation in relation to the activities in the Pike Lake South Habitat Management Unit. Alderon has been informed that no further permits will be provided for work required in the Management Unit, where the open pit will be located, until the project is released from the Environmental Assessment process.

The two geotechnical / exploration bedrock boreholes (RBR-12-01 and RBR-12-02) referenced, shown on Drawing A2-1 (attached), were drilled as follows:

• 208 m and 300 m deep, respectively;

- inclined at 60°; and
- at 96 mm in diameter (HQ drill core).

These boreholes were drilled to investigate structural features such as fault systems and weathering zones that were identified from exploration borehole logging which are discussed in the structural geology response to NRCan 06. The diameter of the boreholes (RBR-12-01 and RBR-12-02) are not large enough to accommodate a pump that could produce the flow rates that would be required to induce a substantial hydraulic response in nearby observation wells (typically more than 100 m apart). Therefore, pumping of these holes would generate a limited area of drawdown influence which would not provide the information needed to predict the dewatering effect of the proposed pit. Alderon is planning to carry out further assessment and field work as outlined in Part 3, below, and part of this work will be to refine the modelling and measurement of the pit draw-down cone

Part 3: Detailed Design Phase

As part of the normal progression of the Kami Project through the detailed design and engineering phase of the Project, further hydrogeological assessment will be conducted including:

- Compilation and input of the data collected to date to create a preliminary numerical groundwater flow model (using MODFLOW or FEFLOW) that would generate a number of possible scenarios regarding the effects of the proposed open pit mine on the regional groundwater flow system.
- Comparison of the flow model scenarios with the structural geology data available from the exploration program to determine: 1) what additional data is required to advance/confirm the model; 2) what field work is required to obtain that data; and 3) what field work location(s) are strategic with respect to potential environmental and operational impacts.
- Carry out the necessary field and assessment work determined in the previous stage, once permission is granted to re-enter the Pike Lake South Habitat Management Unit. This work is expected to include additional boreholes, packer tests, large-scale pump tests, and possibly other work including geophysics, and other test work as determined to be required.
- Finalization of the hydrogeological model and design and development of detailed management plan with respect to environmental or operational impacts.

The results of the advanced hydrogeological work will be presented in support of Alderon's development and operation permit documentation for review by regulators.

Response to IR No. NRCan 07 "b"

Hydraulic conductivity test data on the overburden soils collected from boreholes completed in the area surrounding the Rose Pit and throughout the site have been modified since the submission of the EIS and these updated results, as well as the results of further testing completed in existing boreholes in the Rose Pit area in August 2012, are presented in Table 1. Estimates of hydraulic conductivity were also derived from grain size distribution curves of soil samples collected from the overburden material in the pit area as presented in Table 2. These grain size based estimates agree quite closely with the test results shown in Table 1. For reference, Drawing A1-2 (attached) presents the overburden thickness across the open pit area.

Estimates of hydraulic conductivity of the bedrock units are based on packer injection tests completed in two geotechnical / exploration bedrock boreholes (RBR-12-01 and RBR-12-02). Packer Test Reports for these boreholes are attached to this response and the results are presented in Table 1.

As shown in Table 1, below, the re-evaluated data, and additional data collected since the EIS was issued are generally consistent with that presented in the EIS. As a result, the conclusions presented in the EIS are maintained. These hydraulic conductivity estimates will be further refined/updated as additional investigation of soil and bedrock hydraulic properties is carried out during the detailed engineering and design phase of the Project.

Table 1 Summary of Hydraulic Conductivity Testing

Well ID	Test Date	MW Location	Screened In	% of sand pack in Till	MW Depth (mbg)	WL (mbg)	Sand pack		Corrected	Previously
							Depth (mbg)	Length (m)	K (m/s)	Reported K (m/s)
BH-GE-03	31-Jan-12	Main Plant East	Silty Sandy Till	100.0%	15.47	1.34	6.4-15.5	9.1	1.1E-06	6.78E-07
BH-GE-06	25-Mar-12	Access Road - Waldorf R.	Sandy Till	100.0%	15.25	3.14	3.1-15.8	12.7	2.6E-05	2.60E-05
BH-GE-09	25-Mar-12	Process Plant Area	Silty Sandy Till	100.0%	9.25	1.71	3.4-9.4	6	1.3E-04	7.26E-07
BH-GE-10	26-Mar-12	Process Plant Area	Silty Sandy Till	100.0%	9.15	0.20	2.4-9.2	6.8	5.2E-07	2.55E-07
BH-GE-15	12-Aug-12	Tailings Area	Silty Sandy Till	100.0%	8.95	-0.07	2.95-8.75	6.8	7.0E-07	
BH-GE-18	29-Mar-12	Kami Rail Spur	Silty Sandy Till	100.0%	12.2	3.21	2.4-12.2	9.8	2.3E-07	2.41E-07
ROB-11-01B	7-Aug-12	Rose Pit Perimeter	Silty Sandy Till	100.0%	47.56	-0.60	3.05-46.53	43.48	8.7E-08	
ROB-11-13B	26-Mar-12	Rose Pit Perimeter	Silty Sandy Till	100.0%	10.67	4.78	1.4-10.7	9.3	1.7E-06	1.92E-06
ROB-11-05B (run1)	23-Mar-12	Rose Pit Perimeter	Silty Sandy Till	100.0%	13.72	1.54	3.1-13.7	10.6	3.2E-06	1.81E-06
ROB-11-05B (run2)	23-Mar-12	Rose Pit Perimeter	Silty Sandy Till	100.0%	13.72	1.54	3.1-13.7	10.6	1.0E-06	5.06E-07
ROB-11-02	22-Mar-12	Rose Pit Perimeter	till/rock	71.0%	25.90	-0.33	3.1-25.9	22.8	1.9E-07	9.48E-08
ROB-11-03	8-Aug-12	Rose Pit Perimeter	till/rock	73.6%	23.60	-0.95	2.74-23.6	20.86	1.8E-06	
ROB-11-04	8-Aug-12	Rose Pit Perimeter	till/rock	84.7%	21.30	0.20	2.45-21.3	18.85	2.2E-07	
ROB-11-06	9-Aug-12	Rose Pit Perimeter	till/rock	54.8%	13.72	5.05	2.44-13.72	7.53	1.0E-07	

Well ID	Test Date	MW Location	Screened In	% of sand pack in Till	MW Depth (mbg)	WL (mbg)	Sand pack		Corrected	Previously
							Depth (mbg)	Length (m)	K (m/s)	Reported K (m/s)
ROB-11-07	9-Aug-12	Rose Pit Perimeter	till/rock	82.2%	60.05	5.62	3.05-60.05	57	9.7E-08	
ROB-11-14	10-Aug-12	Rose Pit perimeter	till/rock	26.5%	9.15	-0.01	2.4-9.15	6.75	1.7E-06	
ROB-11-15	9-Aug-12	Rose Pit perimeter	till/rock	16.5%	8.98	0.94	2.82-8.98	6.16	1.3E-06	
ROB011-16	10-Aug-12	Rose Pit perimeter	till/rock	55.8%	16.41	-0.67	3.05-16.41	13.36	1.8E-07	
ROB-11-17	23-Jan-12	Rose Pit Interior	till/rock	81.1%	47.9	1.91	4.6-47.8	43.2	5.8E-08	
ROB-11-18	11-Aug-12	Rose Pit interior	till/rock	79.2%	30.50	0.11	2.44-30.38	27.94	7.9E-07	3.17E-08
ROB-11-19	11-Aug-12	Rose Pit interior	till/rock	48.2%	14.95	0.14	2.1-14.95	12.85	5.5E-07	
ROB-11-20	31-Jan-12	Rose Pit Interior	till/rock	57.9%	15.1	4.44	1.5-15.0	13.5	3.8E-07	1.16E-06
ROB-11-11	12-Aug-12	Rose Pit Perimeter	bedrock	0.0%	5.8	0.85	2.2-5.8	3.6	1.1E-07	
RBR-12-02	27-Mar-12	Rose Pit Interior	bedrock	0.0%	245.2 (Vert)	4.87	33.1-290.0	256.9	1.2E-06	
RBR-12-01	13-Mar-12	Rose Pit Interior	bedrock	0.0%	185.8 (Vert)	-0.90	16.4-300.0	283.6	2.6E-06	
Geomean Silty Sandy Till (m/sec)								1.6E-06	8.80E-07	
Geomean till/rock (m/sec)								3.5E-07	4.29E-07	
Geomean Bedrock (m/sec)								6.9E-07	1.88E-06	

Note: all MW with rrising head within the sand pack were corrected for 25% porosity (clean silica sand). Method: Bouwer & Rice, 1976 (ATESOLV).

Area	Well	Sample	Depth (m)	d ₁₀ (mm)	K (cm/s)	K (m/s)
	ROB -11-11	SS2	0.6-1.0	0.01	1.0E-04	1.0E-06
	ROB -11-12	SS4	3.0-3.6	0.04	1.6E-03	1.6E-05
Eastern	ROB -11-12	SS3	1.4-2.0	0.06	3.6E-03	3.6E-05
	ROB -11-16	SS16	11.1-11.7	0.009	8.1E-05	8.1E-07
	ROB -11-16	SS2	0.6-1.0	0.017	2.9E-04	2.9E-06
	ROB -11-07	SS2	1.2-1.6	0.0066	4.4E-05	4.4E-07
	ROB -11-08	SS9	7.6-8.0	0.0085	7.2E-05	7.2E-07
	ROB -11-08	SS21	17.4-17.8	0.059	3.5E-03	3.5E-05
	ROB -11-08	BS26	22.0	0.0098	9.6E-05	9.6E-07
Southern	ROB -11-09	SS7	4.5-5.1	0.002	4.0E-06	4.0E-08
Southern	ROB -11-09	SS11	7.6-8.2	0.17	2.9E-02	2.9E-04
	ROB -11-09	SS16	12.1-12.7	0.25	6.3E-02	6.3E-04
	ROB -11-09	SS17	12.7-13.3	0.0072	5.2E-05	5.2E-07
	ROB -11-09	SS18	16.8-17.4	0.04	1.6E-03	1.6E-05
	ROB -11-20	SS11		0.025	6.3E-04	6.3E-06
	ROB -11-03	SS9	9.5-10.1	0.0068	4.6E-05	4.6E-07
	ROB -11-05	SS2	1.8-2.4	0.018	3.2E-04	3.2E-06
	ROB -11-17	SS40	31.0-31.6	0.0032	1.0E-05	1.0E-07
	ROB -11-18	SS4	2.1-2.7	0.04	1.6E-03	1.6E-05
Western	ROB -11-18	SS6	3.6-4.2	0.016	2.6E-04	2.6E-06
	ROB -11-18	SS10	6.7-7.3	0.005	2.5E-05	2.5E-07
	ROB -11-18	SS12	8.2-8.8	0.038	1.4E-03	1.4E-05
	ROB -11-18	SS18	13.7-13.9	0.07	4.9E-03	4.9E-05
	ROB -11-19	SS9	7.6-8.2	0.0075	5.6E-05	5.6E-07
Northern	ROB -11-01	SS34	26.0-26.4	0.0045	2.0E-05	2.0E-07
Northern	ROB -11-01	SS29	21.8-22.4	0.017	2.9E-04	2.9E-06

Table 2 – Hydraulic Conductivity Estimates from Grain Size Distribution

Area	Well	Well Sample Depth (m)		d ₁₀ (mm)	K (cm/s)	K (m/s)
	ROB -11-01	SS51	44.7-44.8	0.0025	6.3E-06	6.3E-08
	ROB -11-17	SS11	8.2-8.6	0.0098	9.6E-05	9.6E-07
	ROB -11-17	SS25	18.1-19.5	0.0098	9.6E-05	9.6E-07
	ROB -11-17	BS46	39.5-39.6	0.0005	2.5E-07	2.5E-09
	2.5E-07	2.5E-09				
				Maximum	6.3E-02	6.3E-04
	1.9E-04	1.9E-06				
	893). $K = A[d_{10}]^2$; where $A = 1$. hydrometer data reaching 909			1979).		

Source: Appendix A: Geotechnical Investigations; Figures A1-5 to A1-8.

Response to IR No. NRCan 07 "c"

The cross section presented in Drawing No. 121614000-306-GE-06; REV. 1, has been revised and updated as requested with information on bedrock geology and the location of the cross section through the pit is depicted in the inserted plan view. Drawings showing the geological data and locations of the existing wells and boreholes that were used to generate this cross section are attached to this response (Drawing Nos. A1-1, A1-2, A2-1, and A3-1).

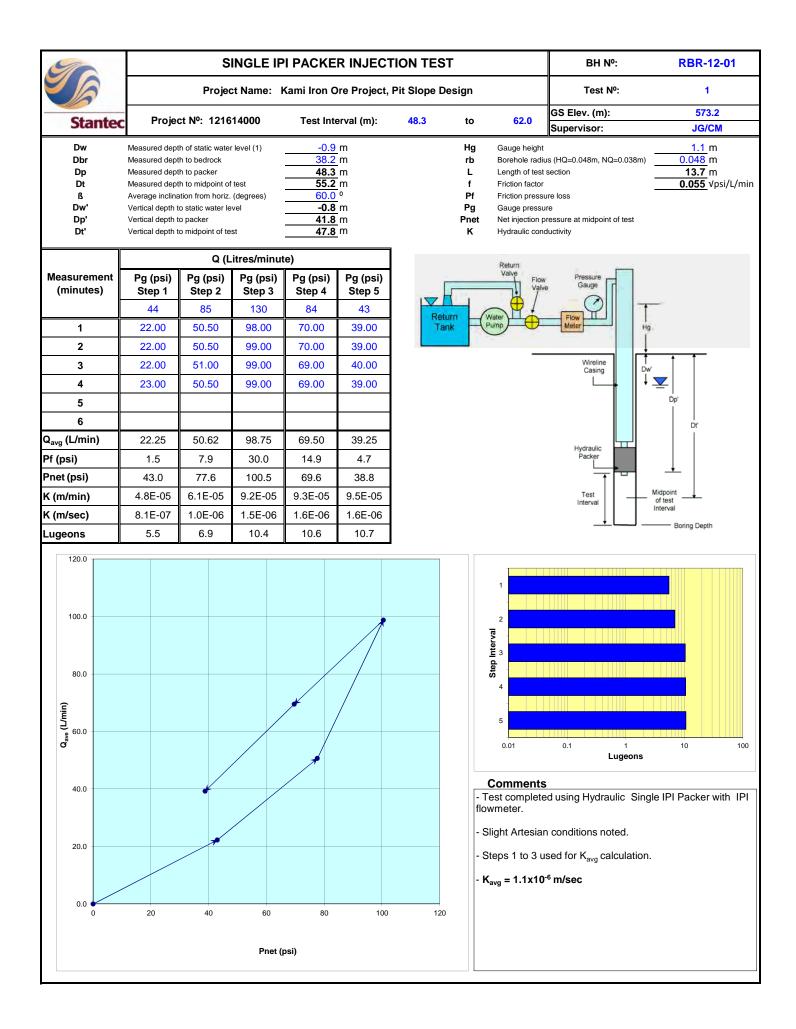
Response to IR No. NRCan 07 "d"

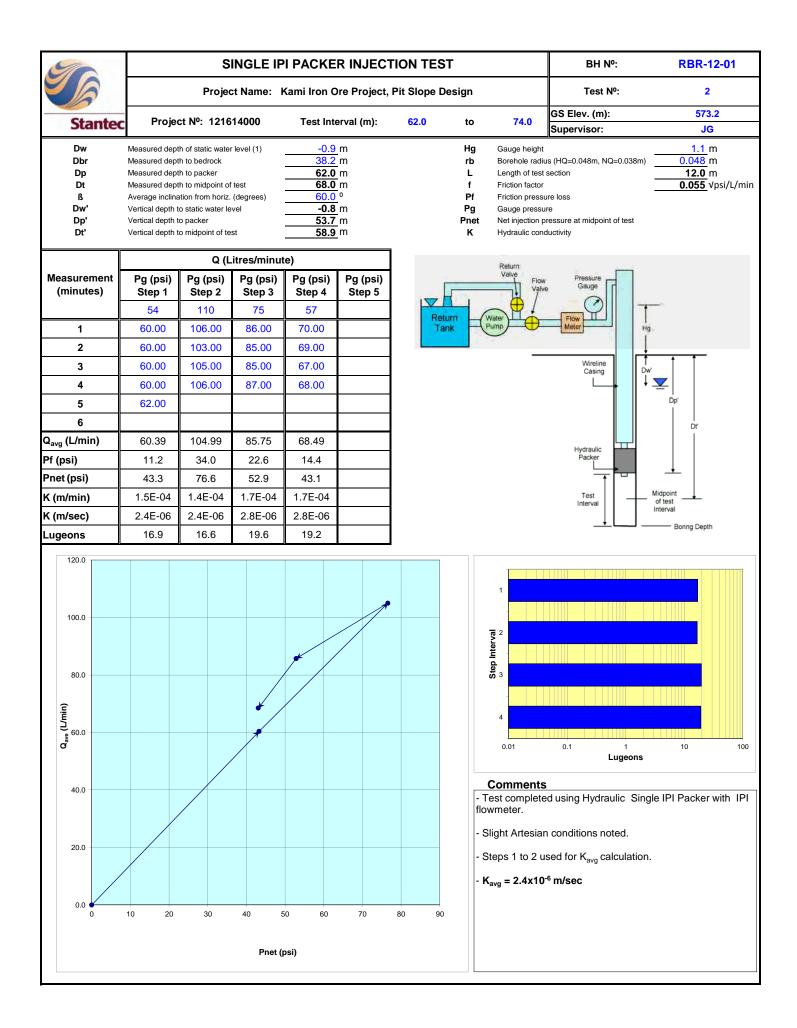
Hydraulic test data collected from boreholes completed in the area surrounding the Rose Pit and throughout the site was re-evaluated as recommended by NRCan and the revised results are presented in Table 1, above. As shown in the table by direct comparison with the data reported in the EIS provided in the last column, the revised data did not vary significantly from the estimates presented in the EIS.

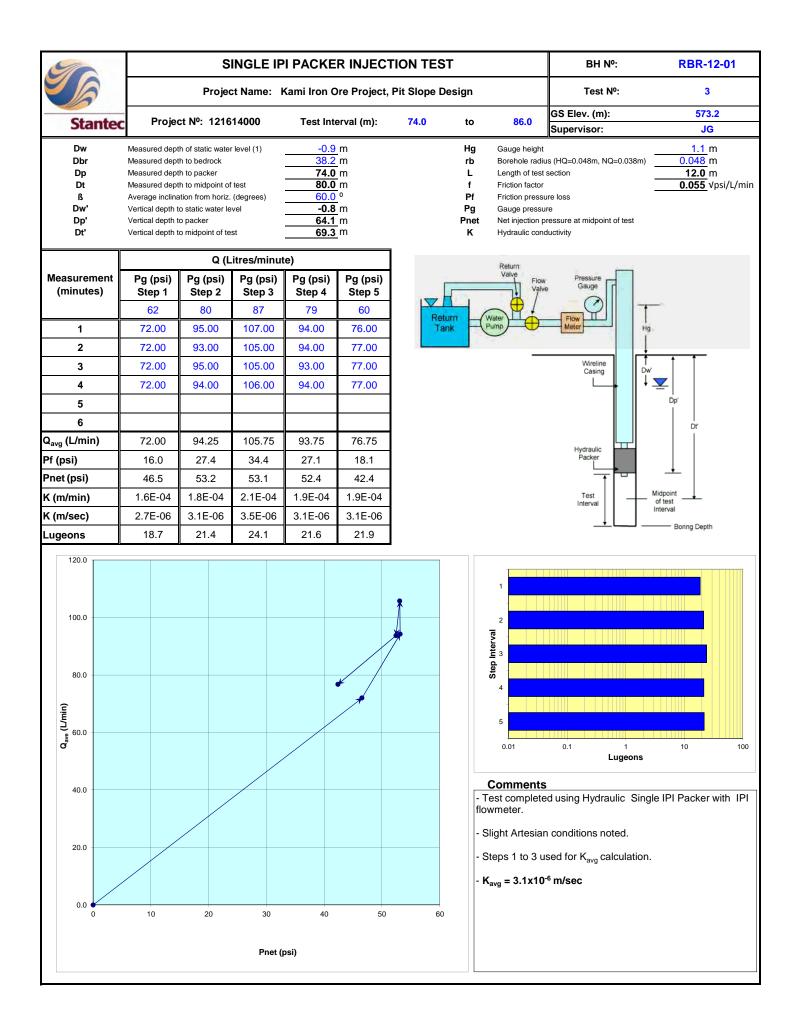
BH-GE-06 was included as it is the only well screened in apparent permeable sand (e.g., response almost too fast to measure; 90 percent in 15 sec); and is intended to show that such strata are locally present.

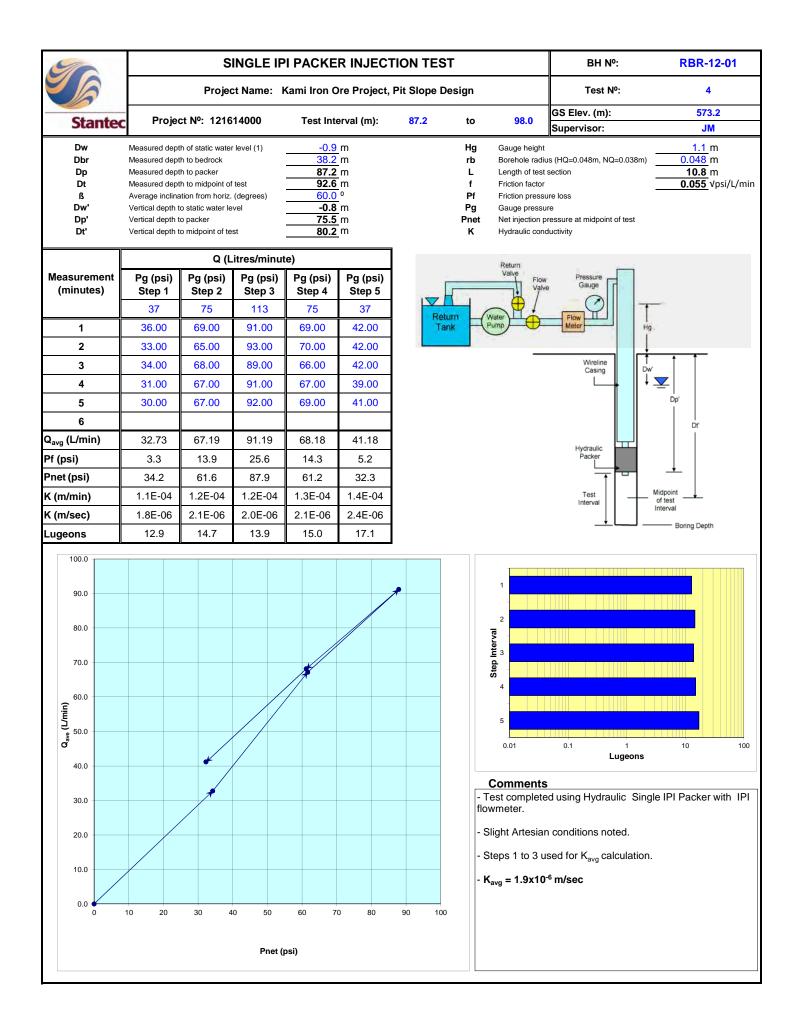
Additional Comment by NRCan

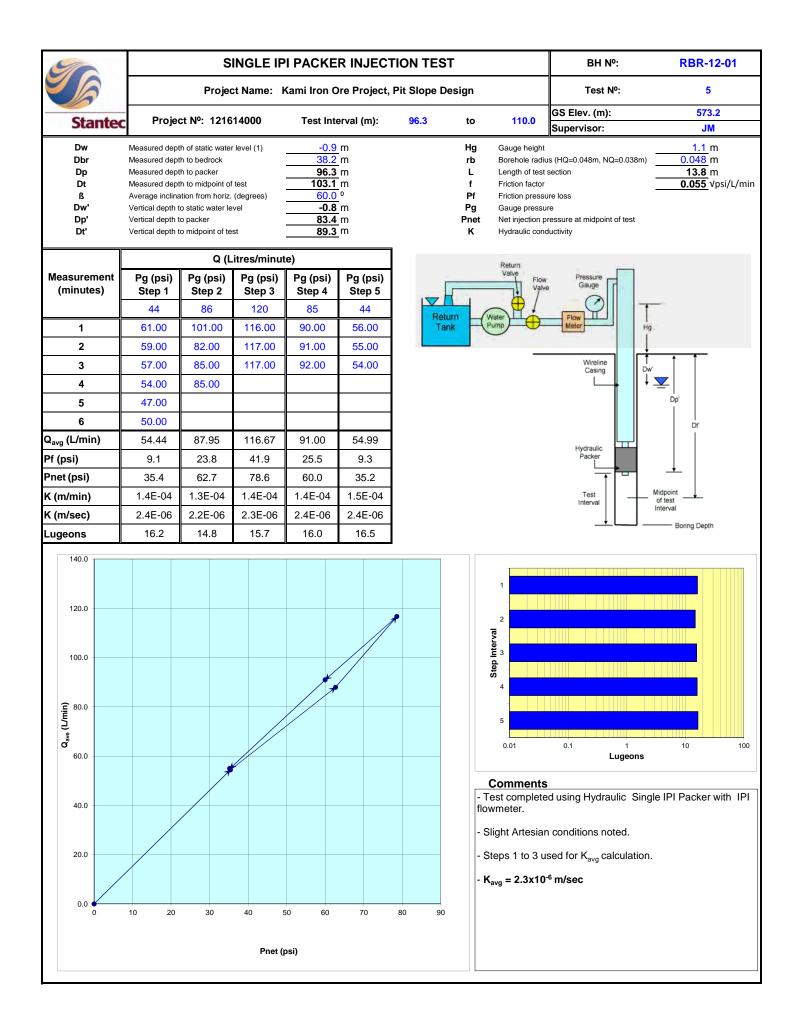
The two lakes located to the north (Pike Lake) and south (Mid Lake) of Rose Pit have been, and will continue to be considered in the hydrological and hydrogeological assessment of the open pit area. Currently, the design for control of surface water includes a small diversion dam at the downstream end of Mid Lake to allow surface water flow to be captured and piped around the pit and then discharged to the upstream end of Pike Lake. There is no "dam" currently designed for the upstream end of Pike Lake adjacent to the open pit as the assessment of topography, pit slope design, and water levels within Pike Lake shows that a dam is not required to control surface water. The current design for the crest of the proposed open pit adjacent to Pike Lake will incorporate a small diversion berm to address any surface water that might flow towards the open pit, and the design of the pit slope in overburden (greater than 30 m in thickness at this location) will incorporate slope stability and to minimize sedimentation. All collected water from precipitation and groundwater seepage will be pumped to a sedimentation pond and released back to Pike Lake to ensure the natural lake water levels are maintained.

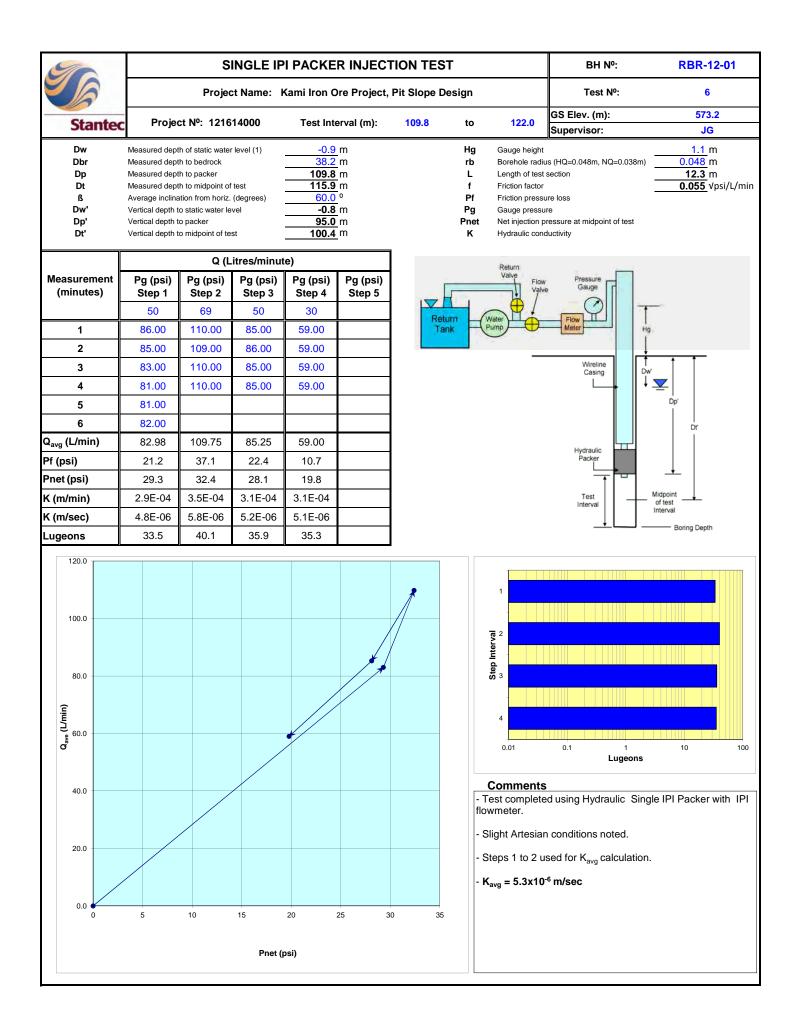


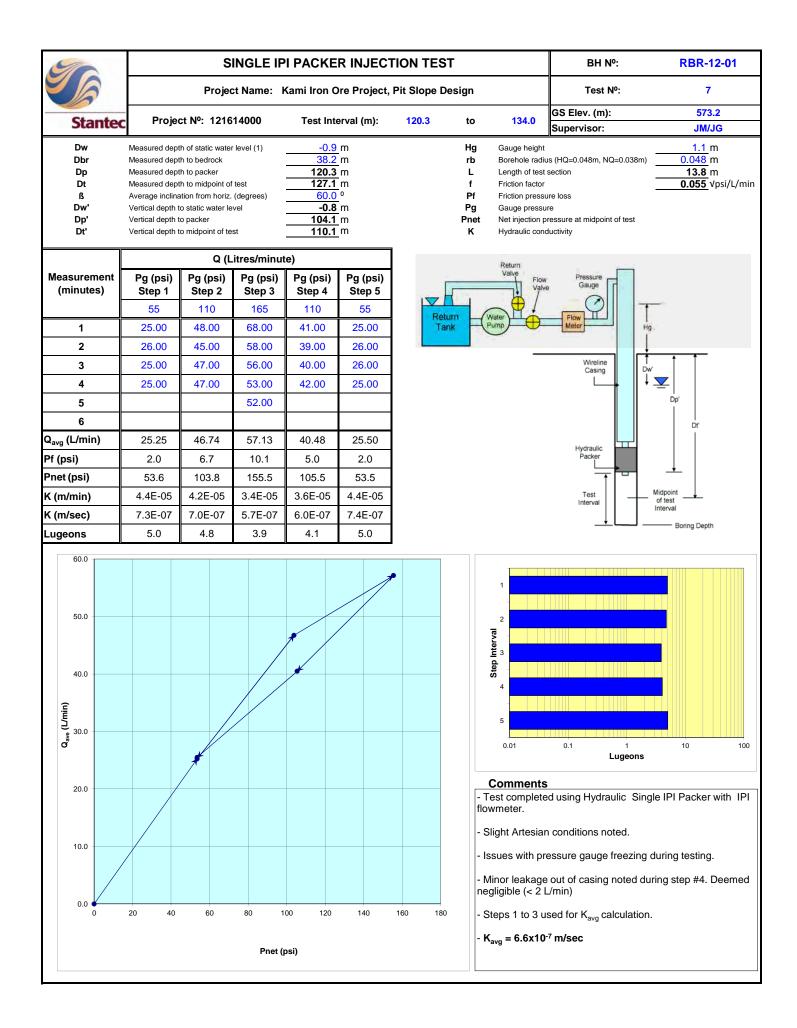


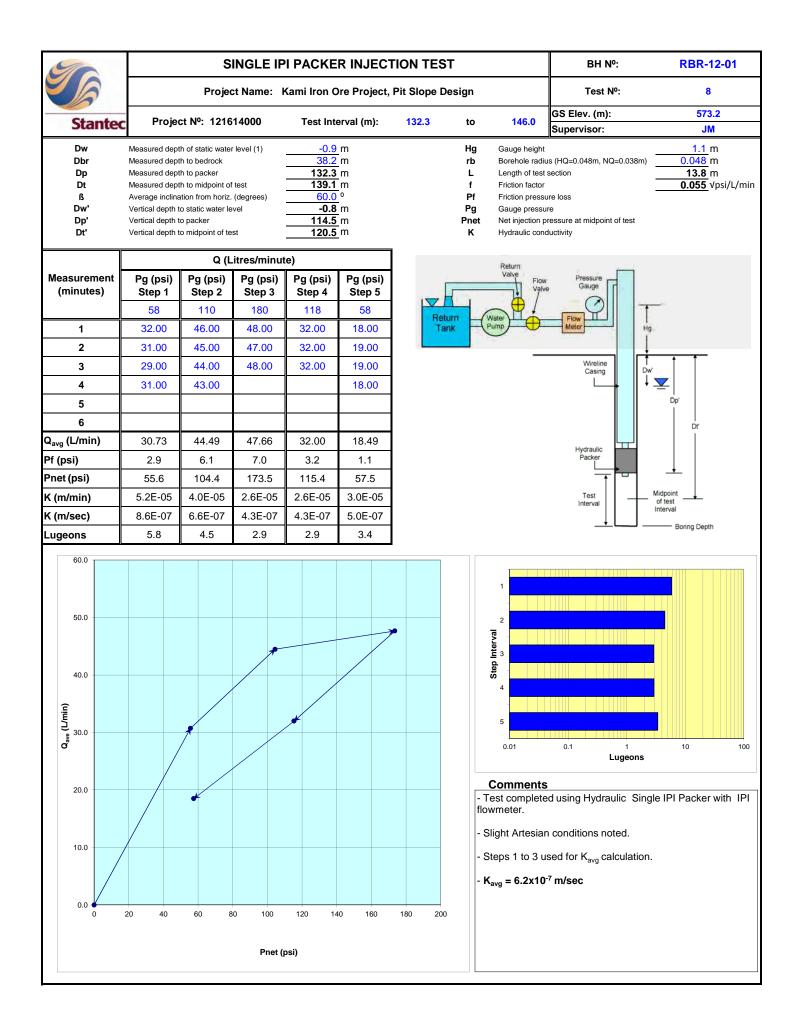


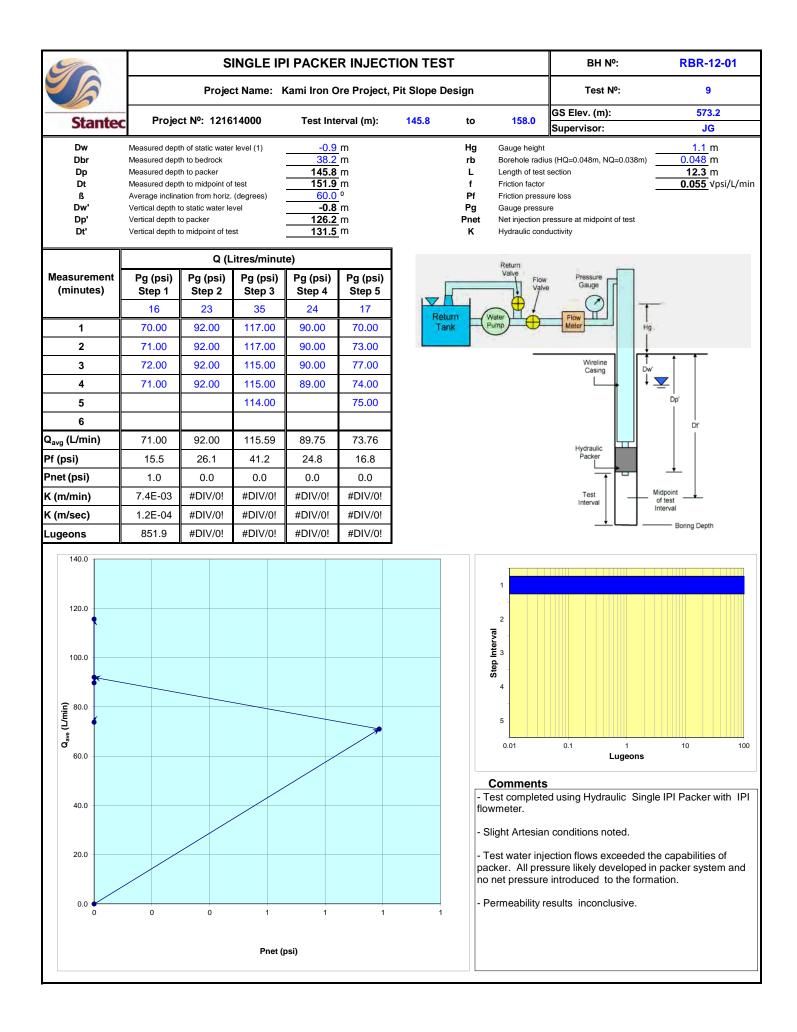


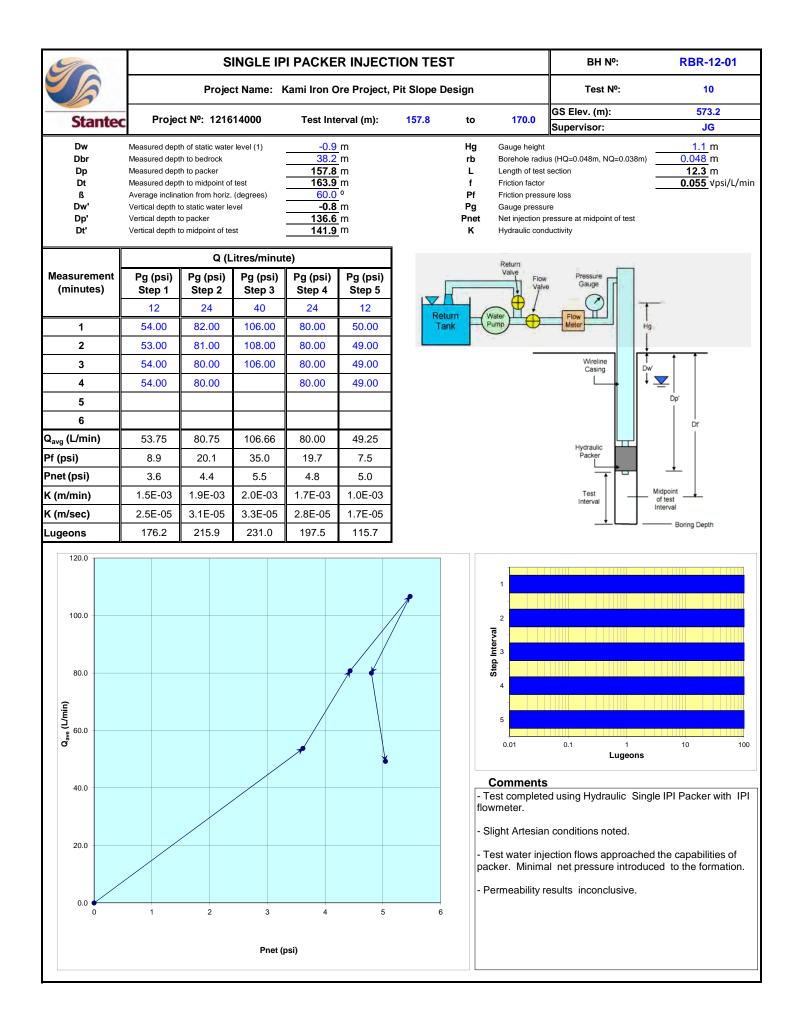


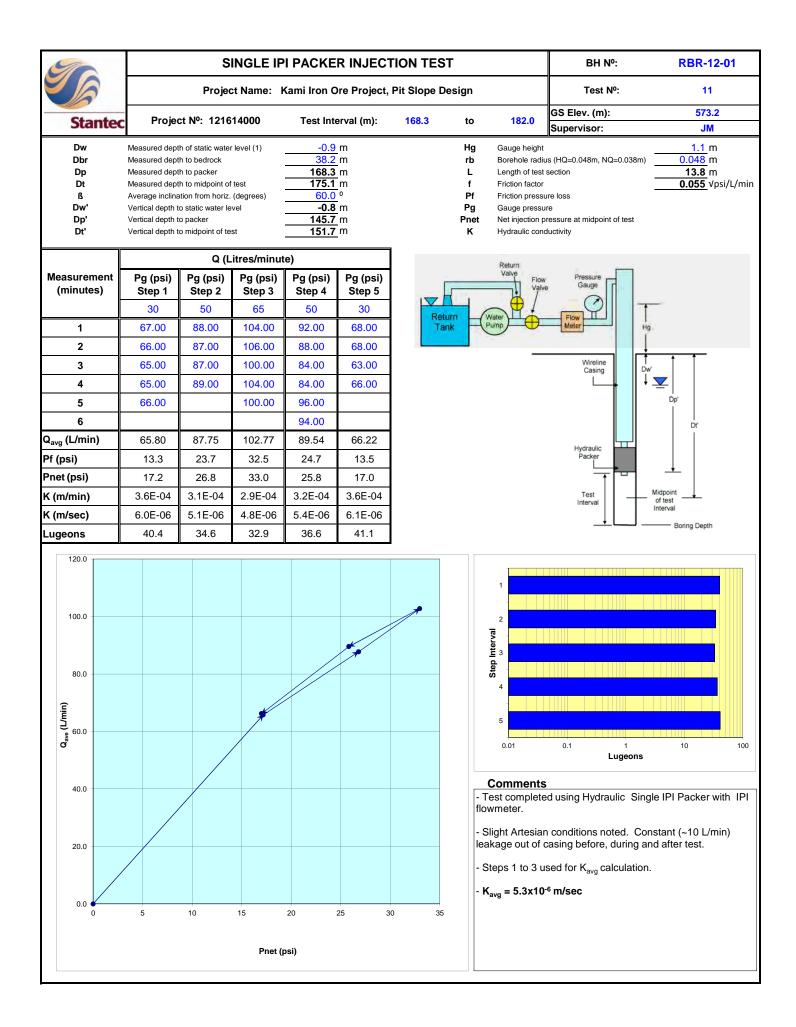


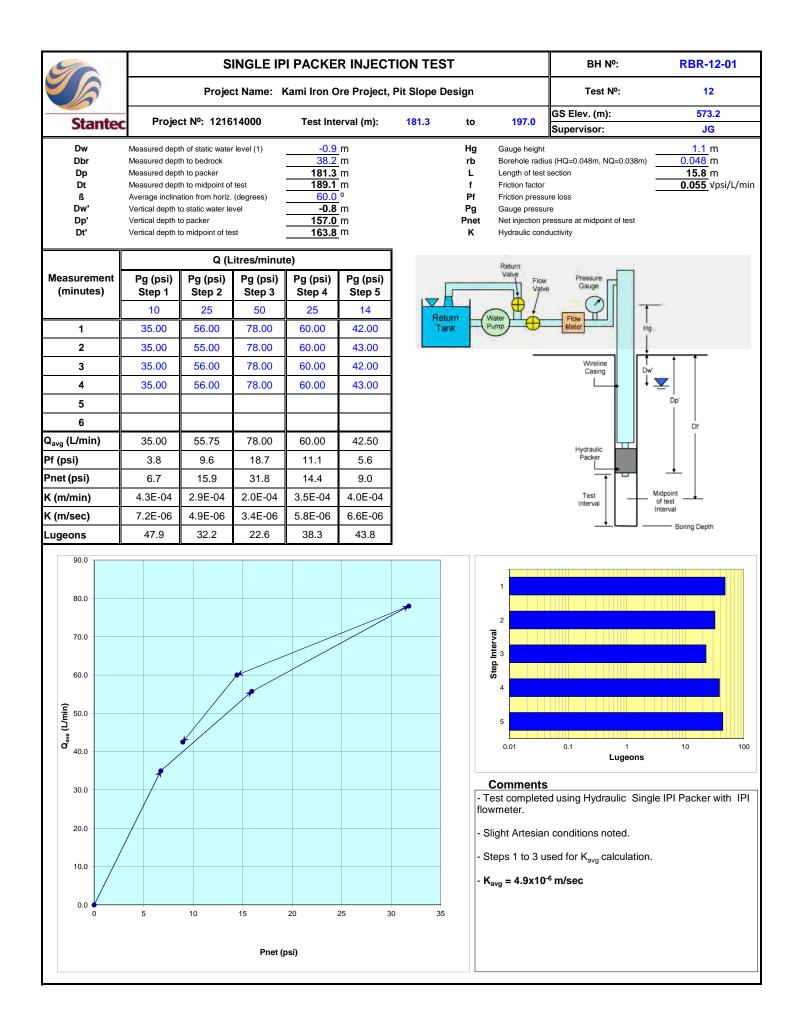


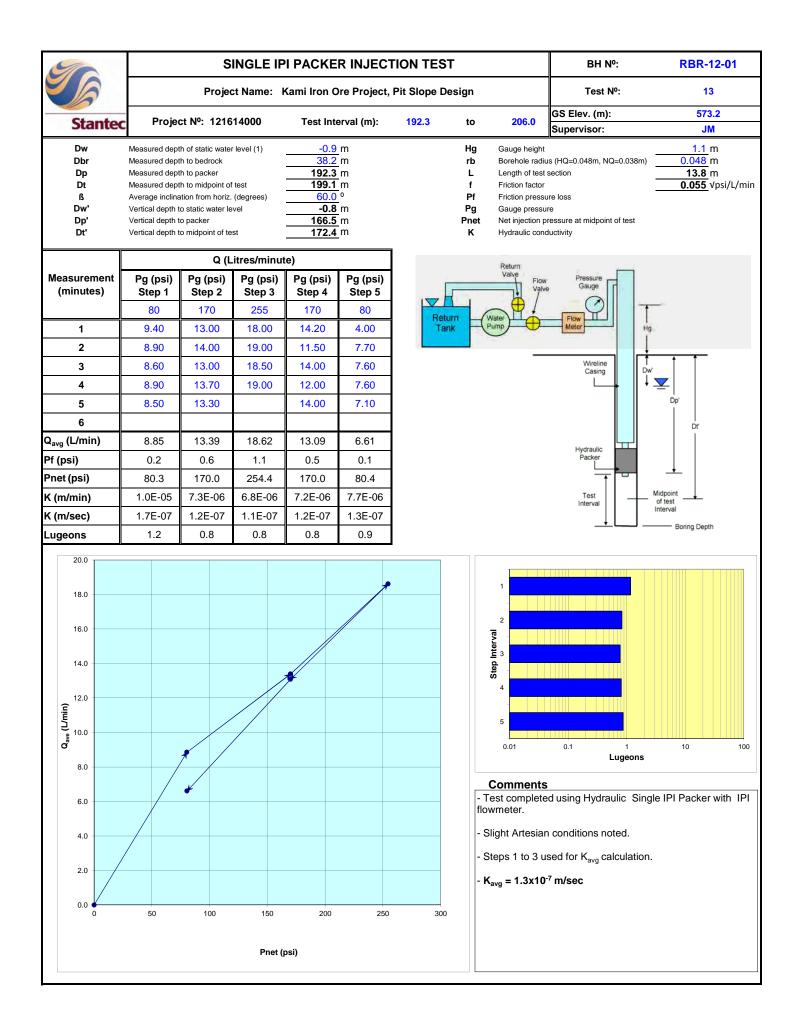


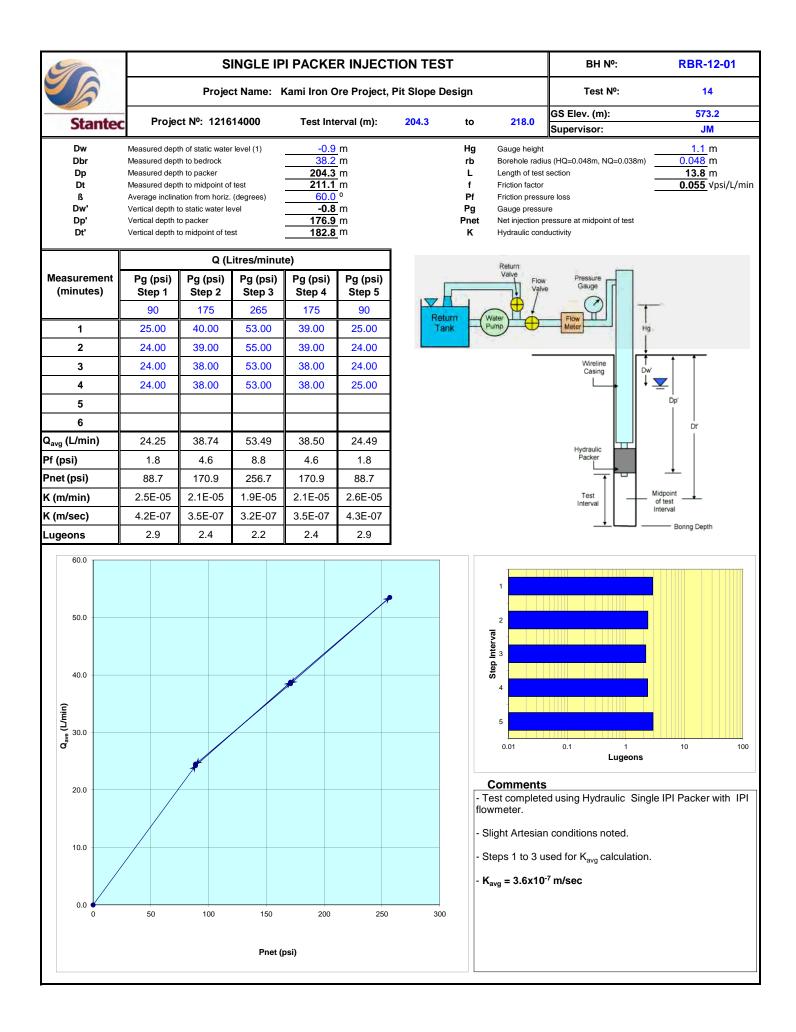


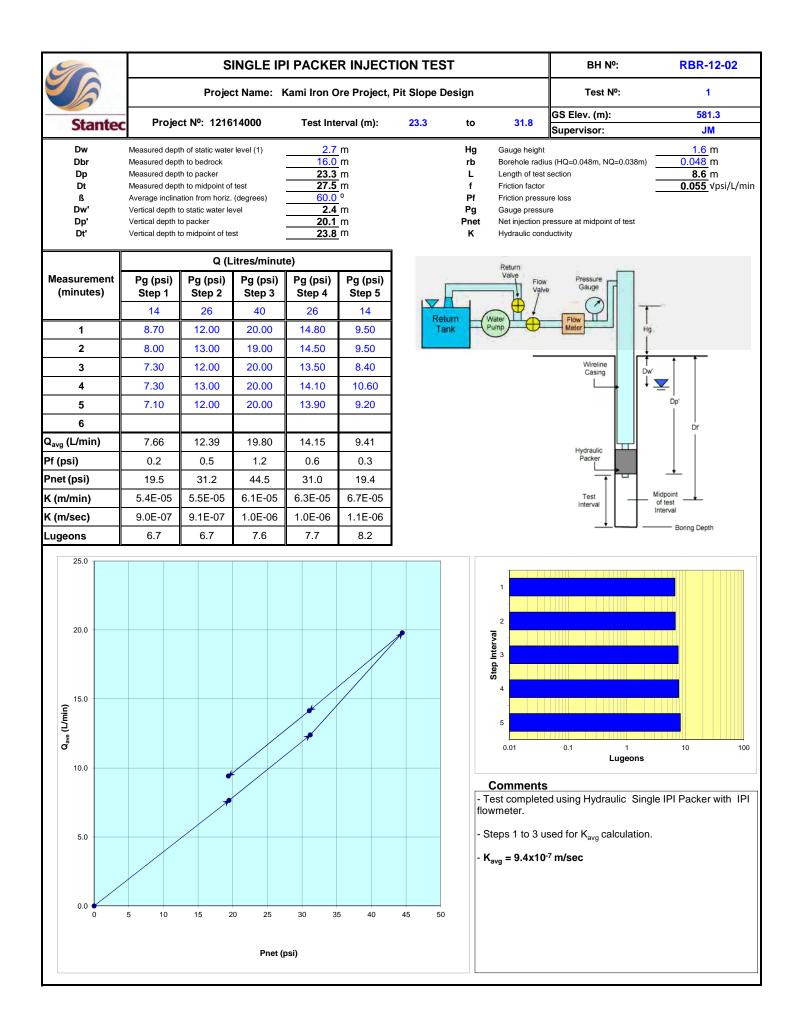


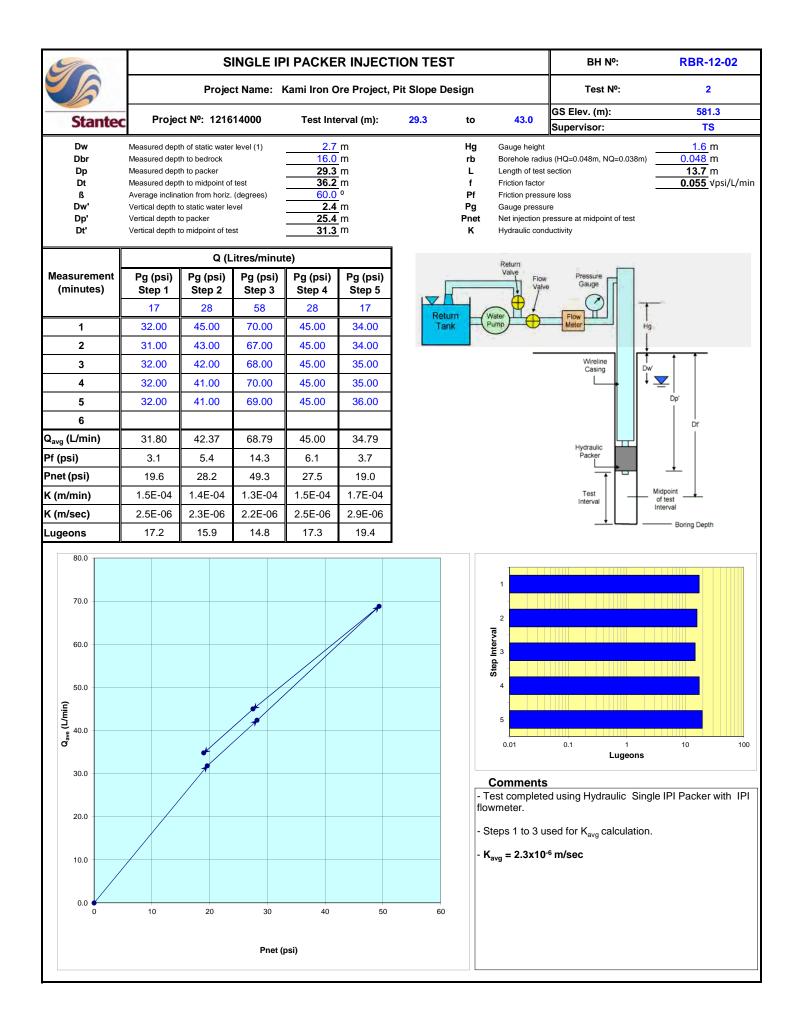


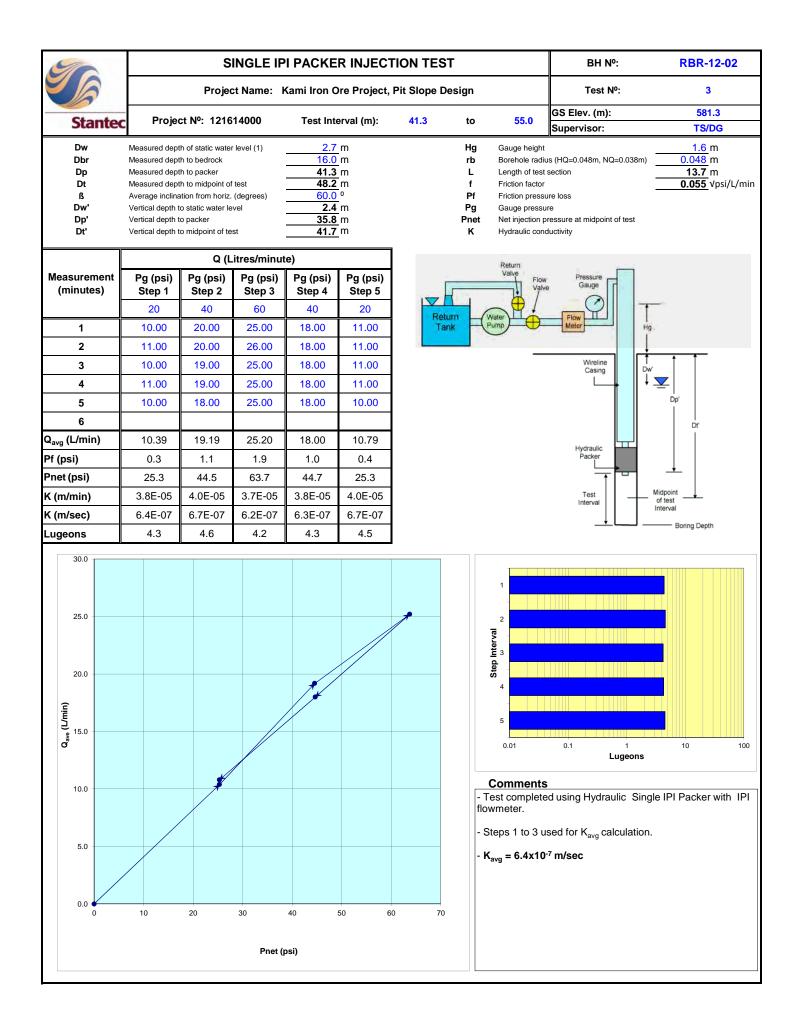


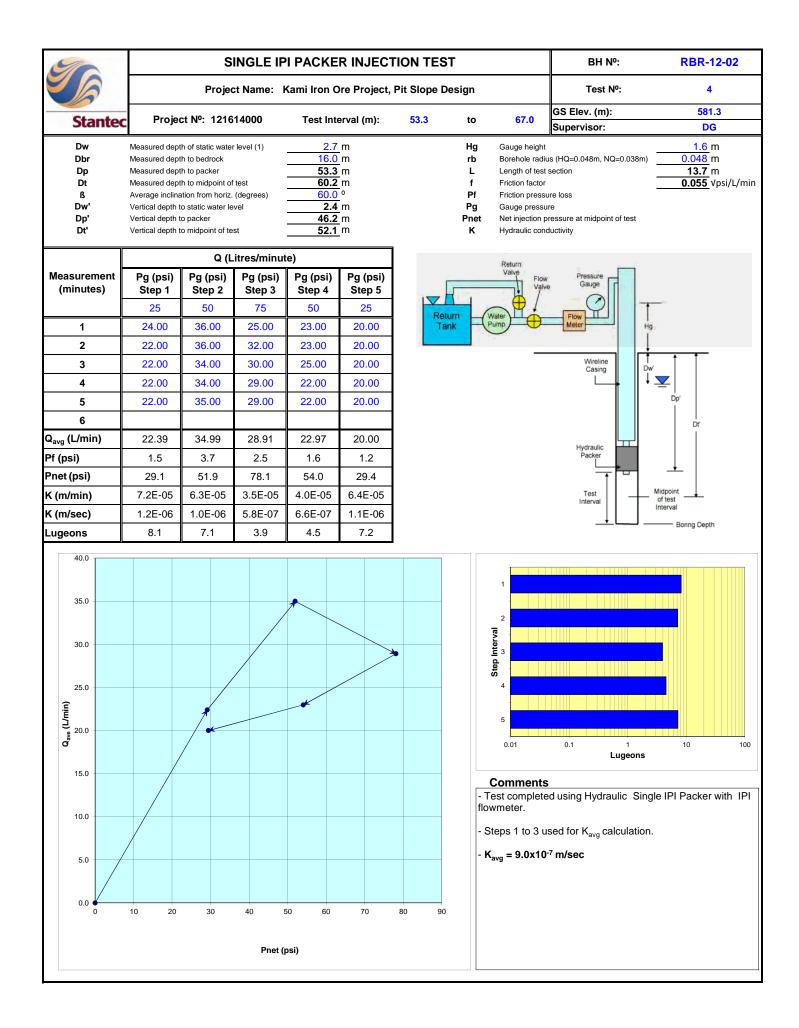


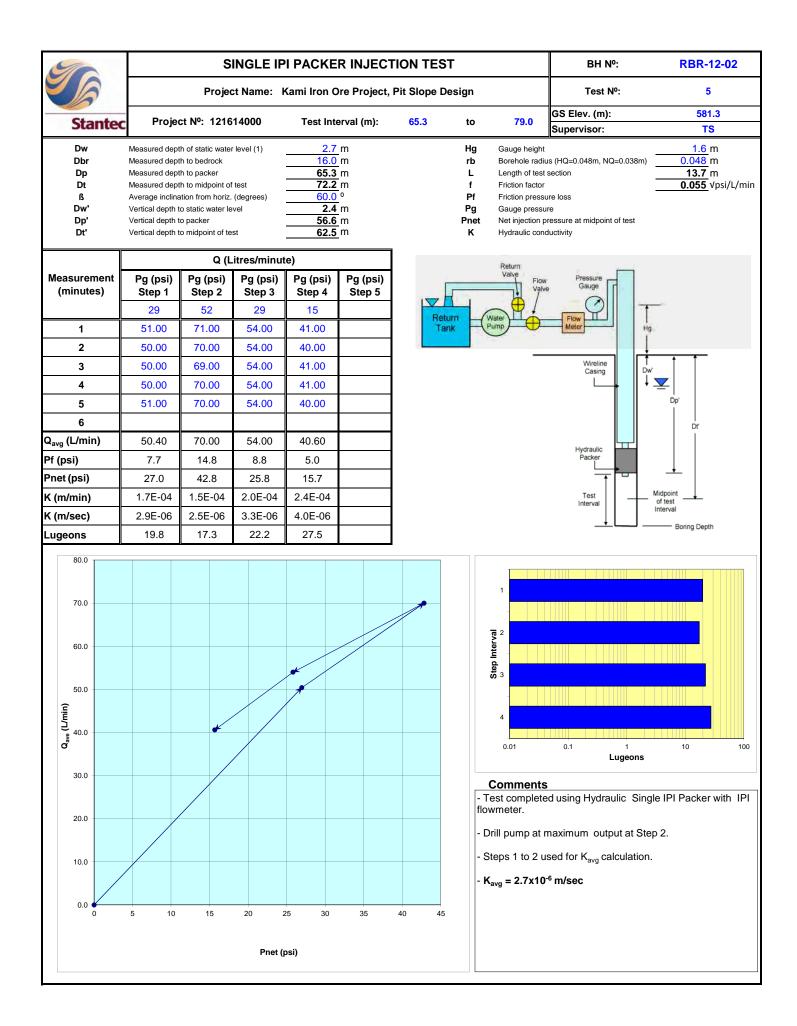


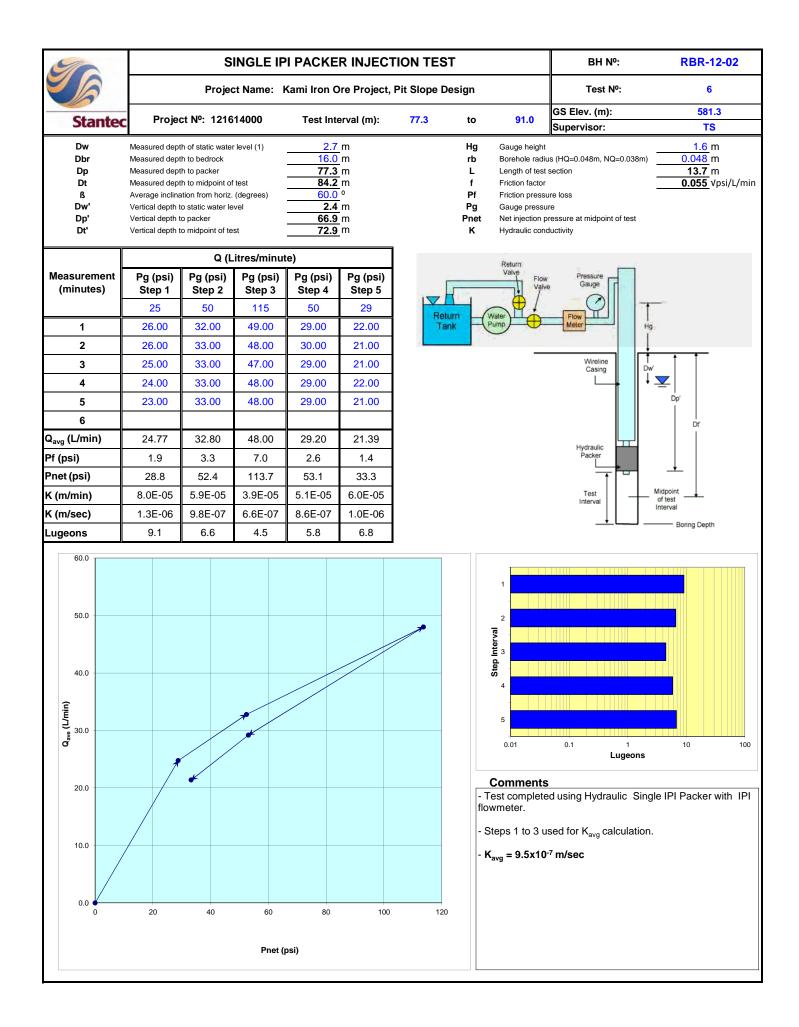


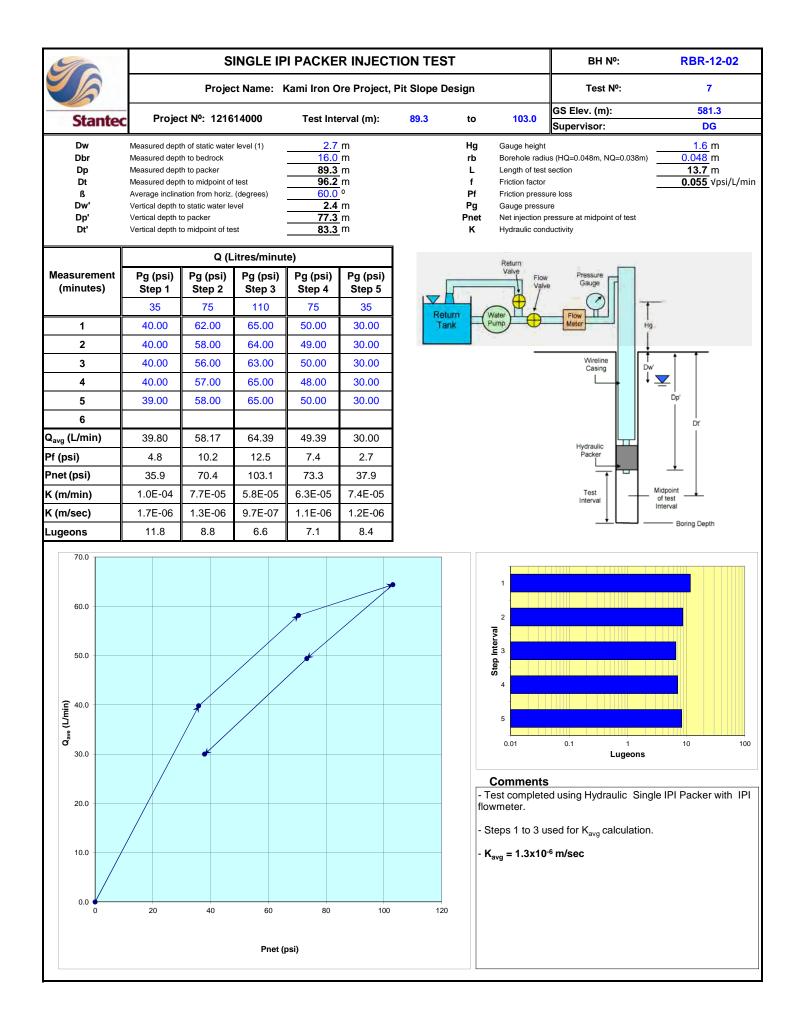


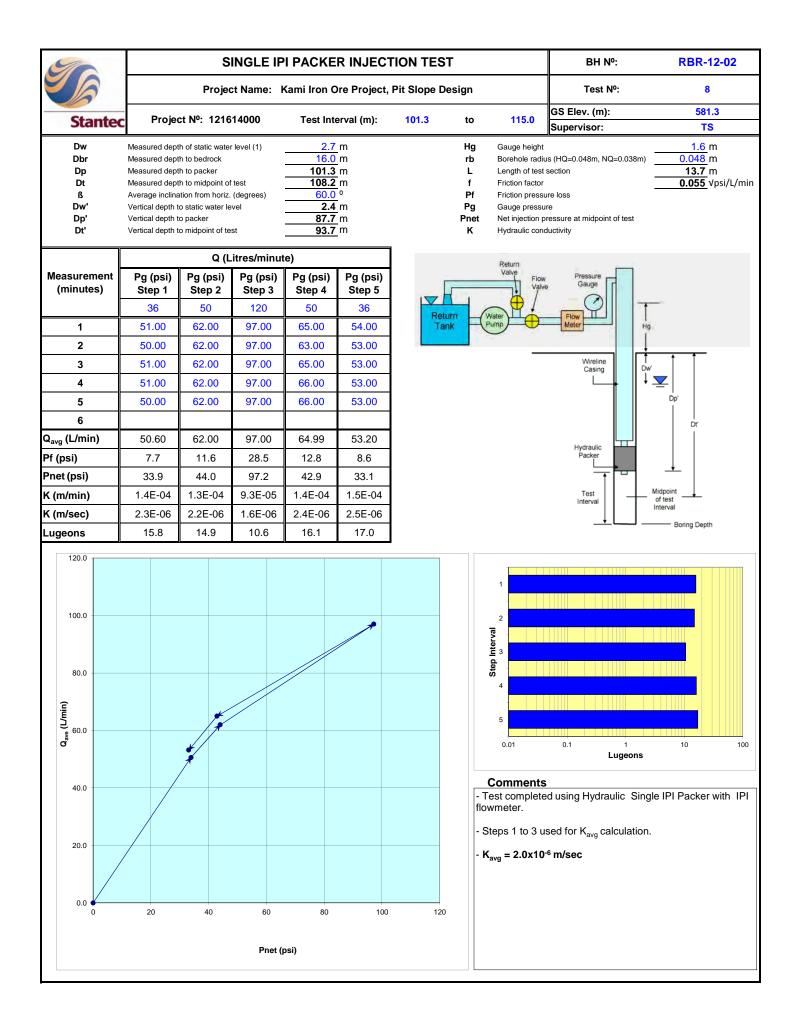


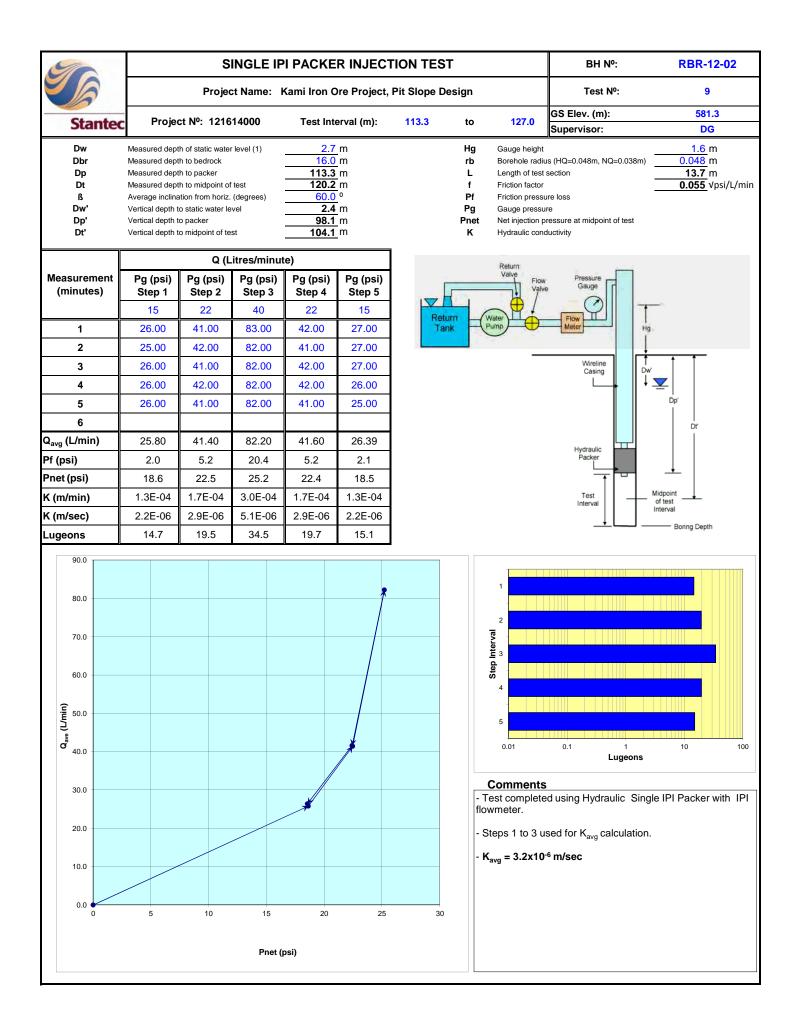


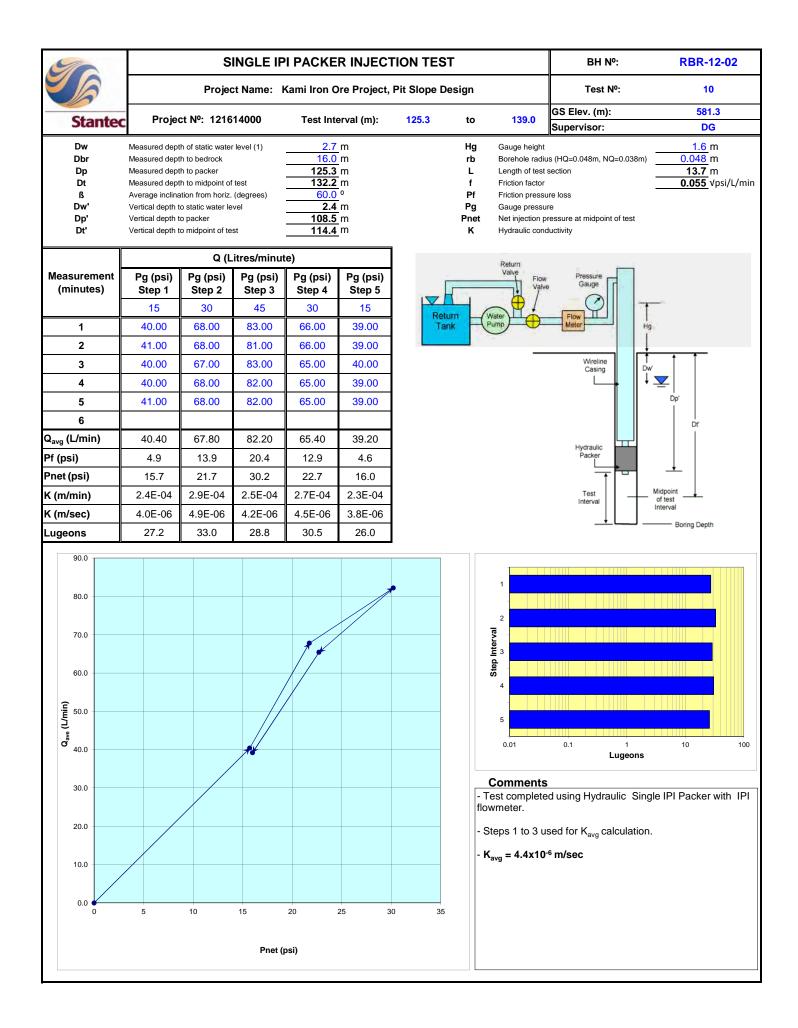


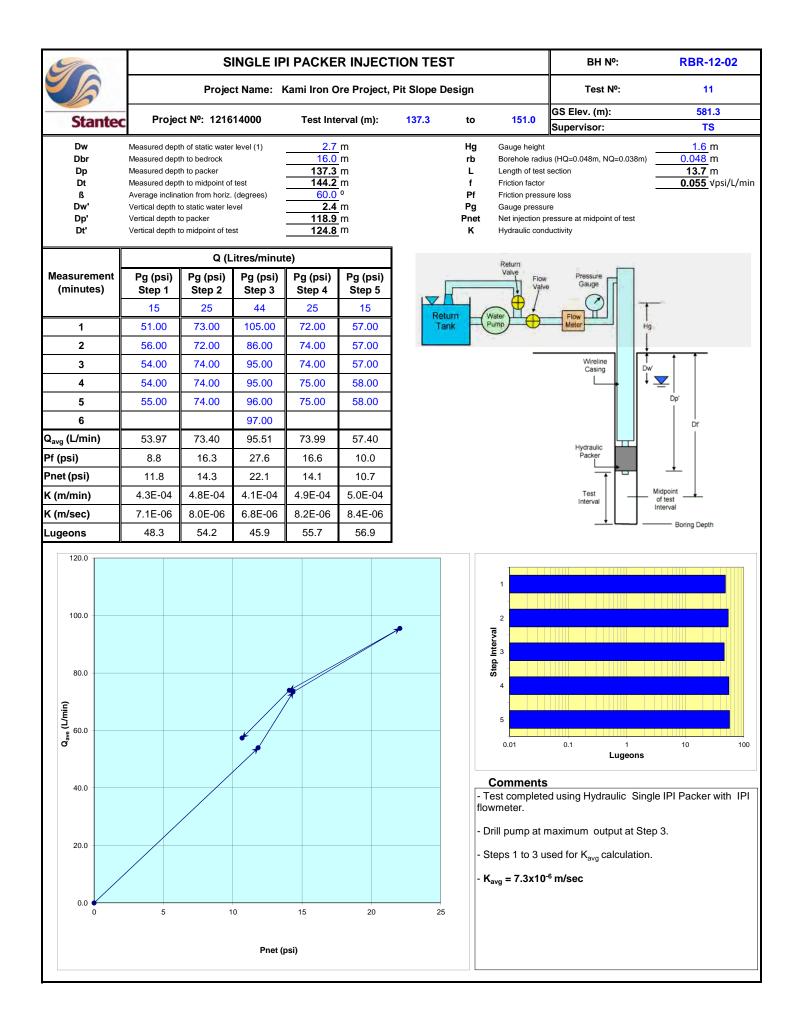


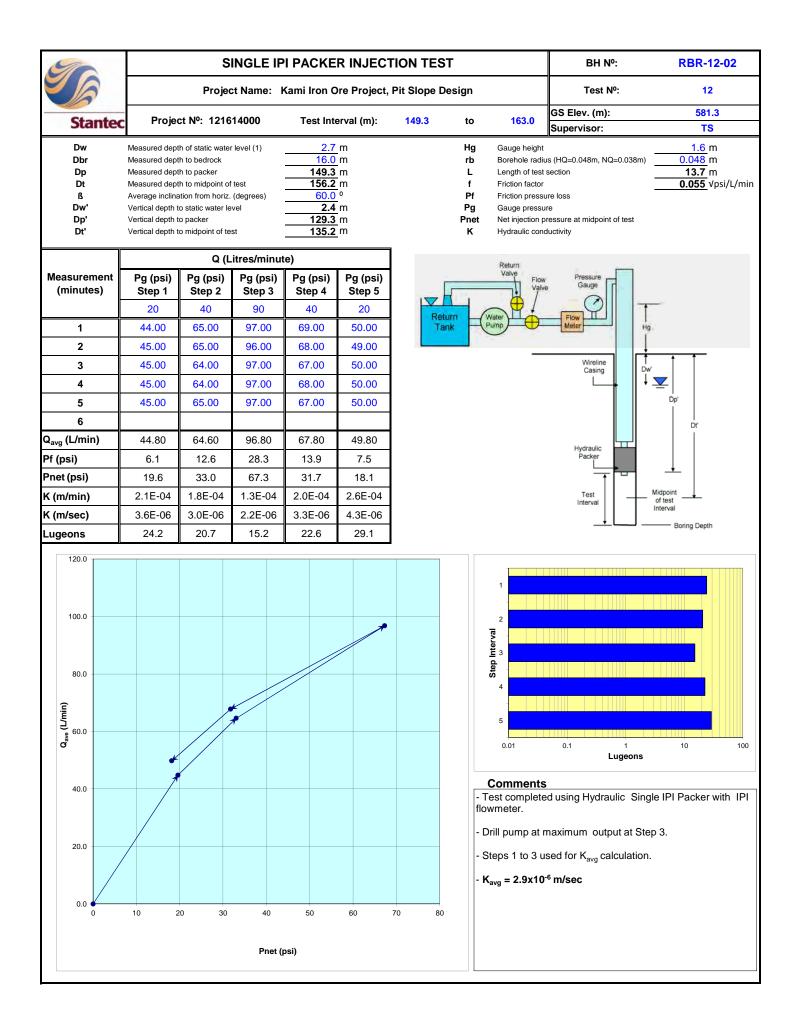


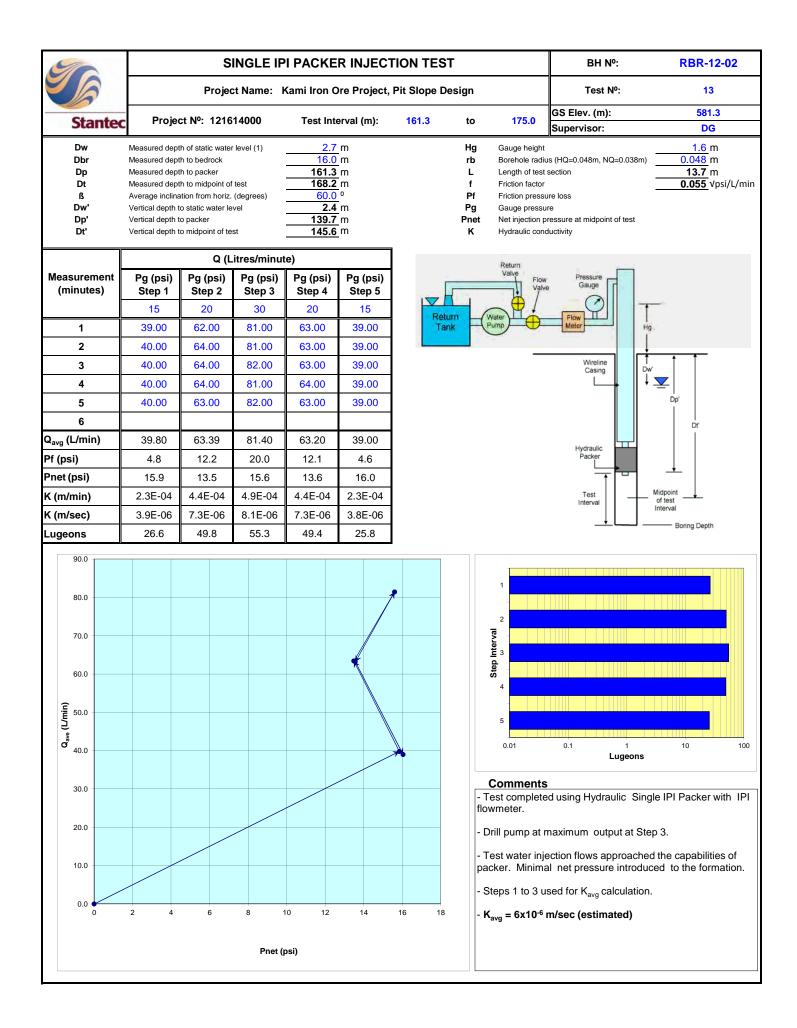


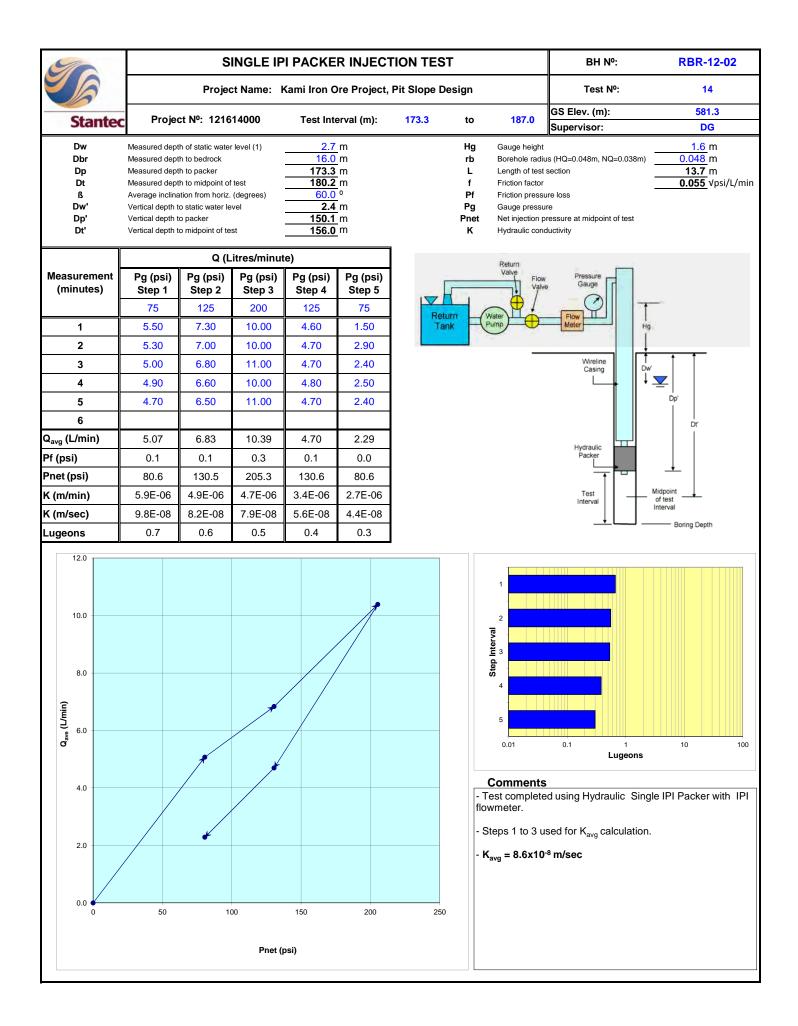


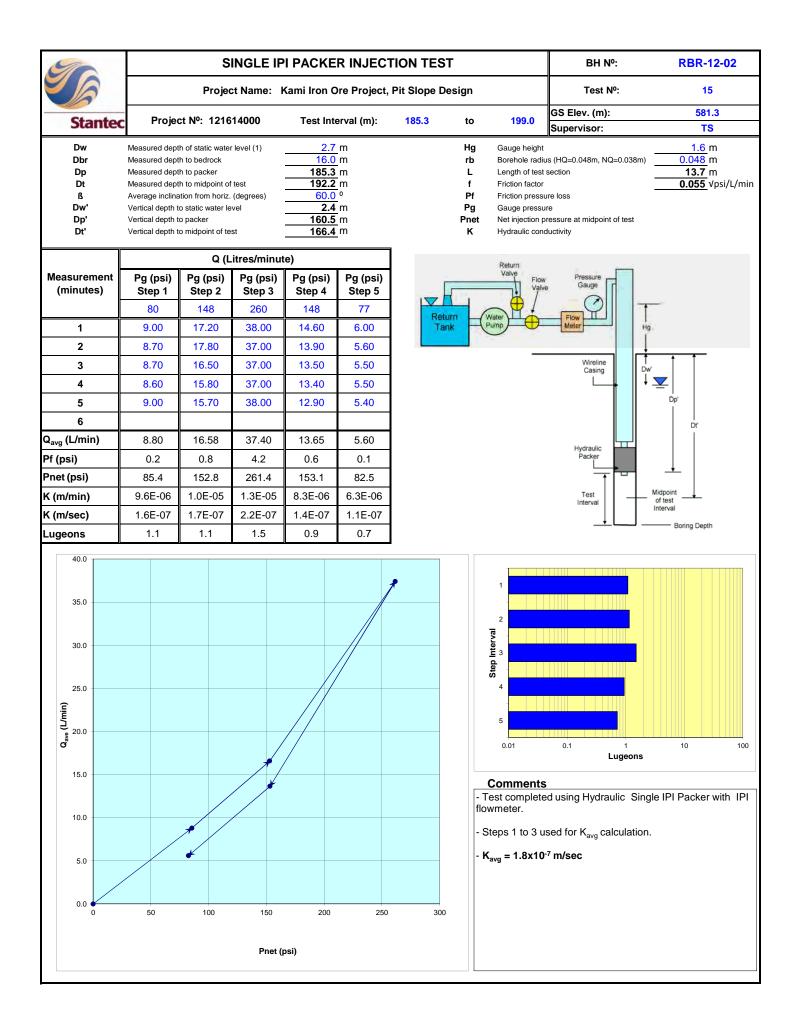


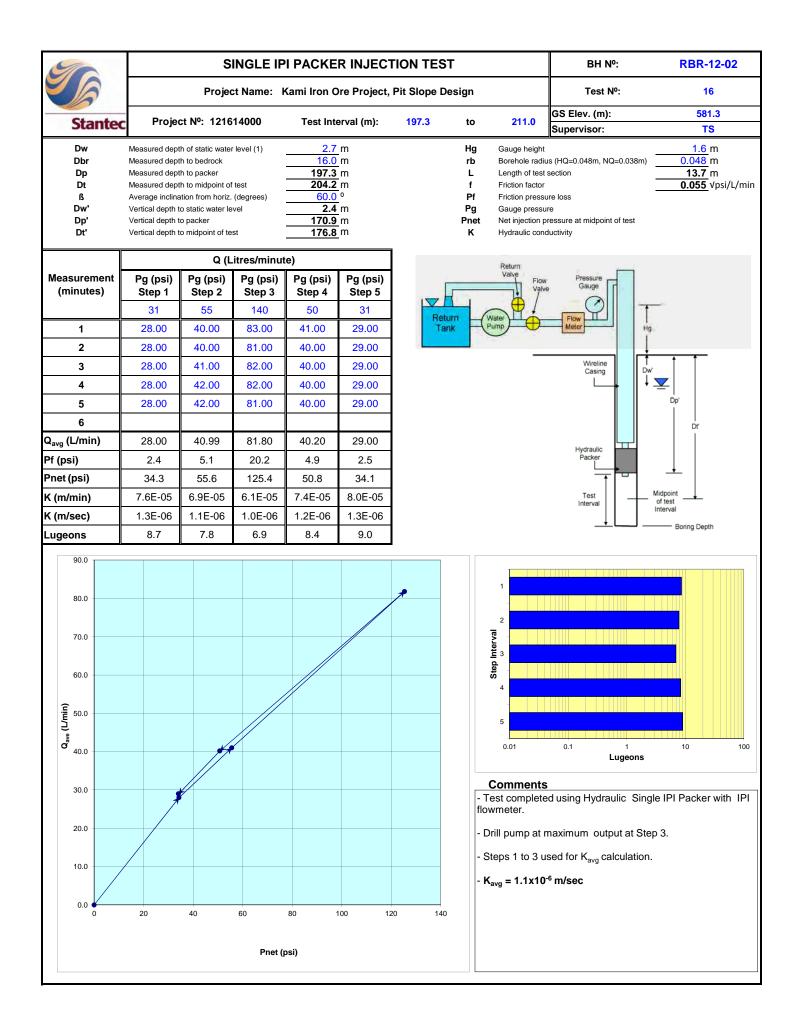


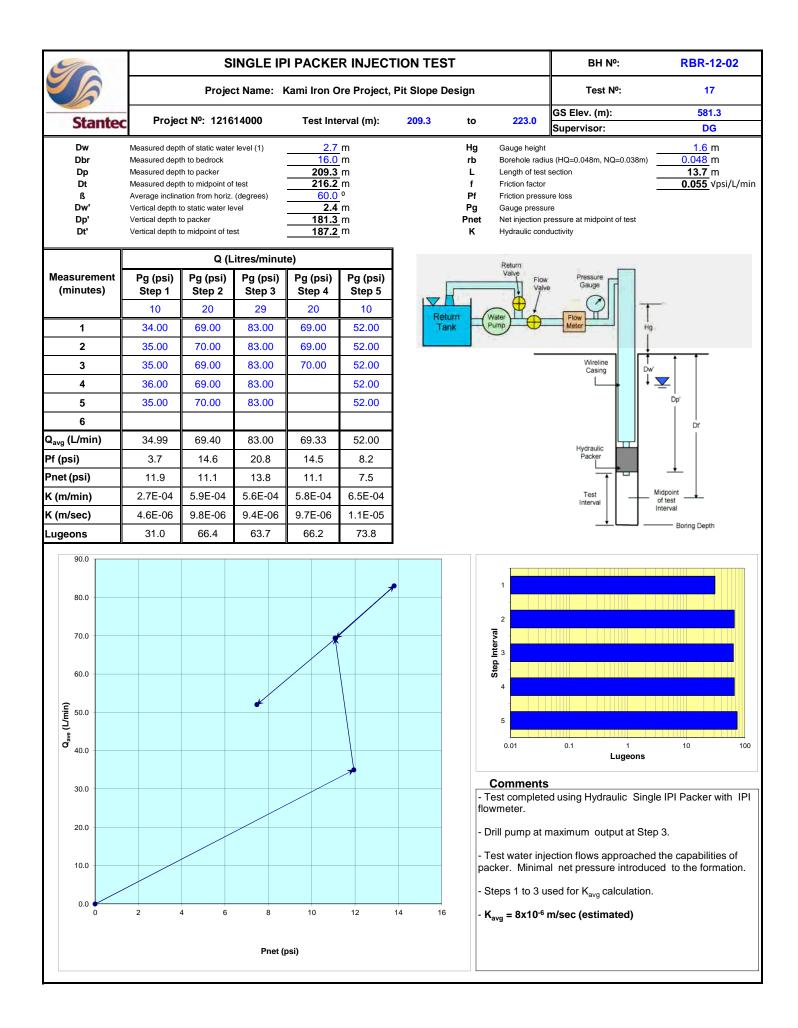


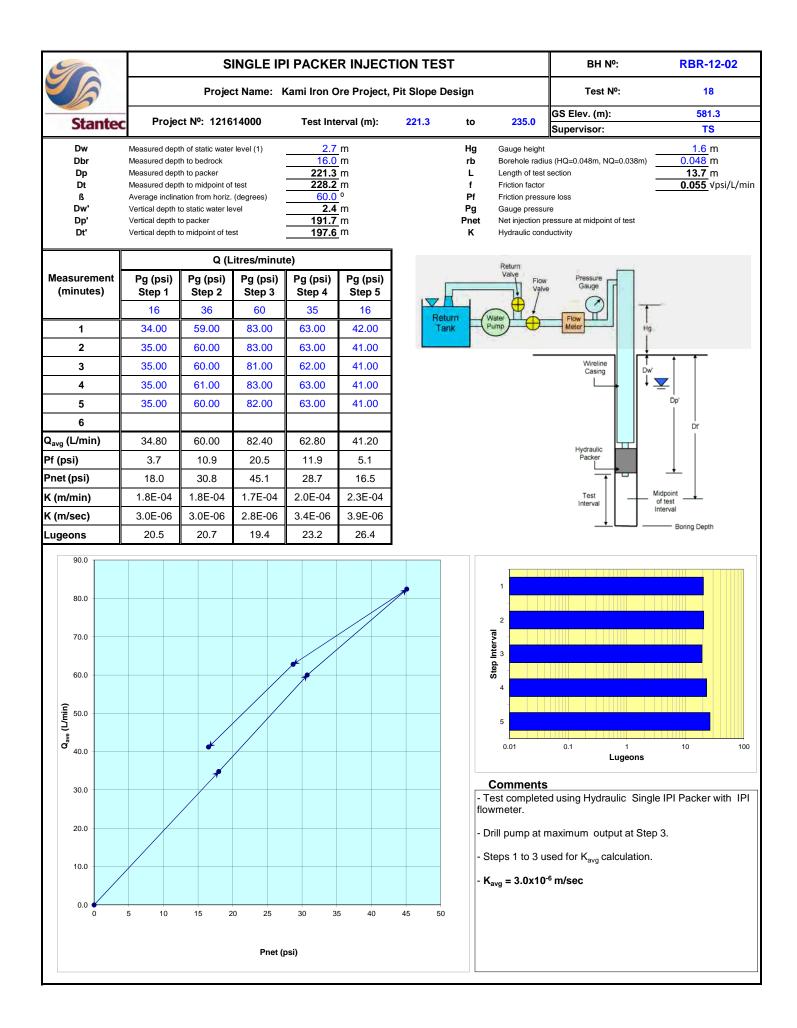


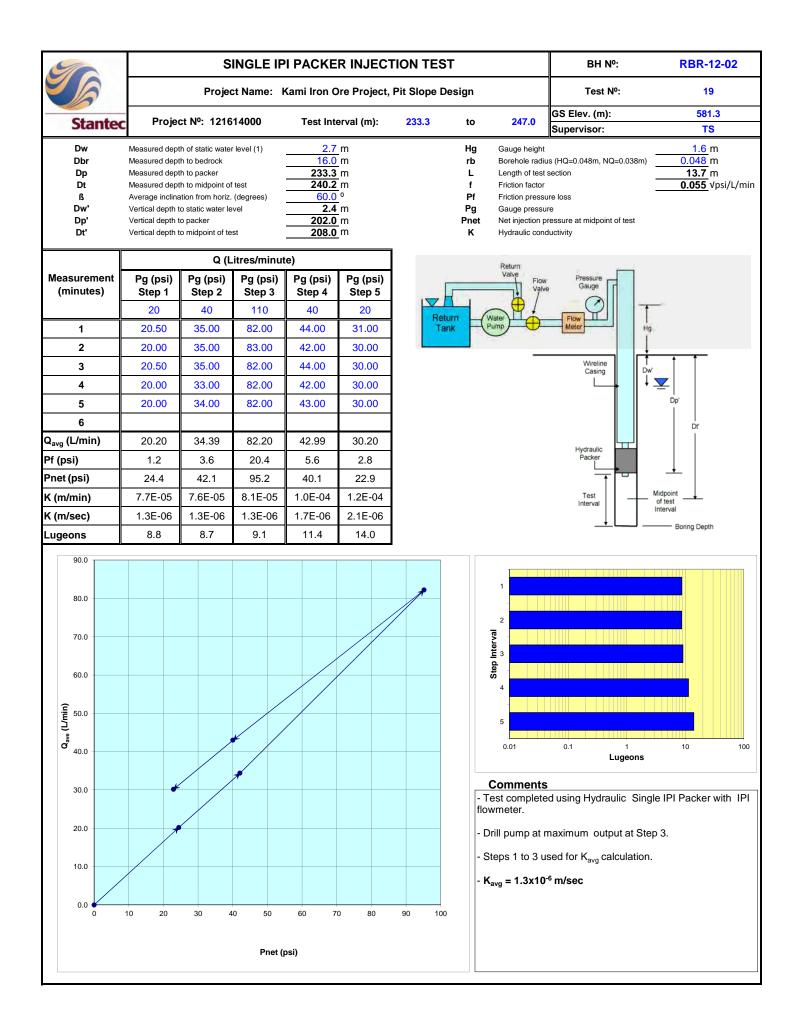


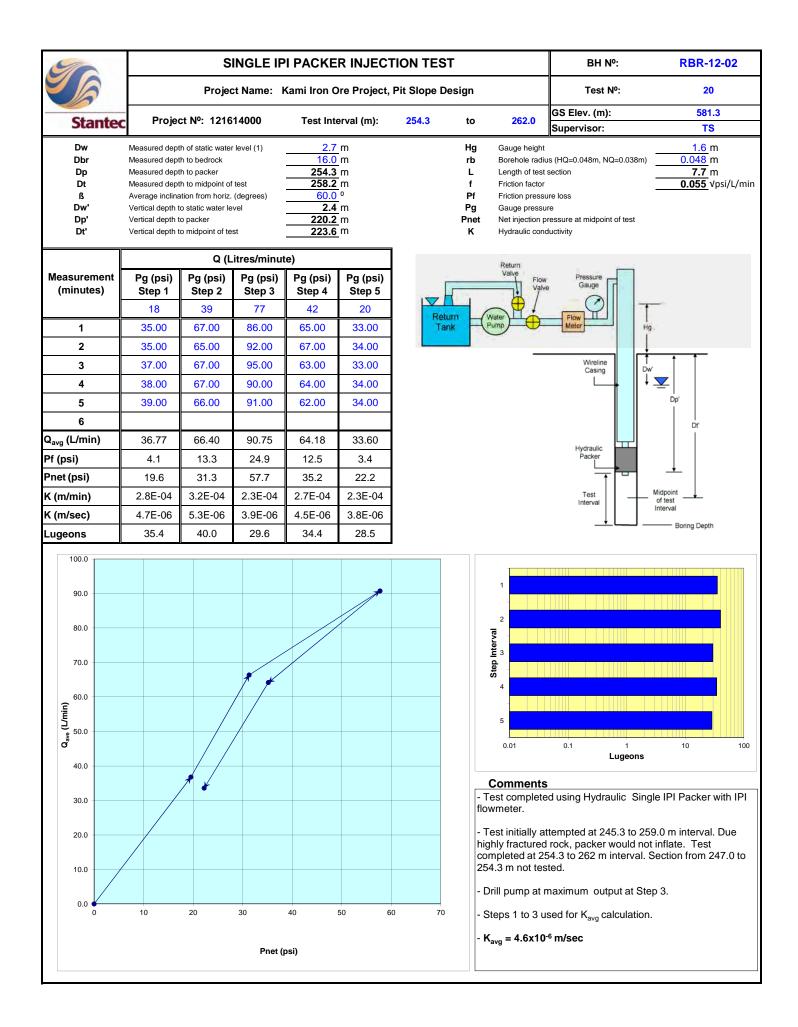


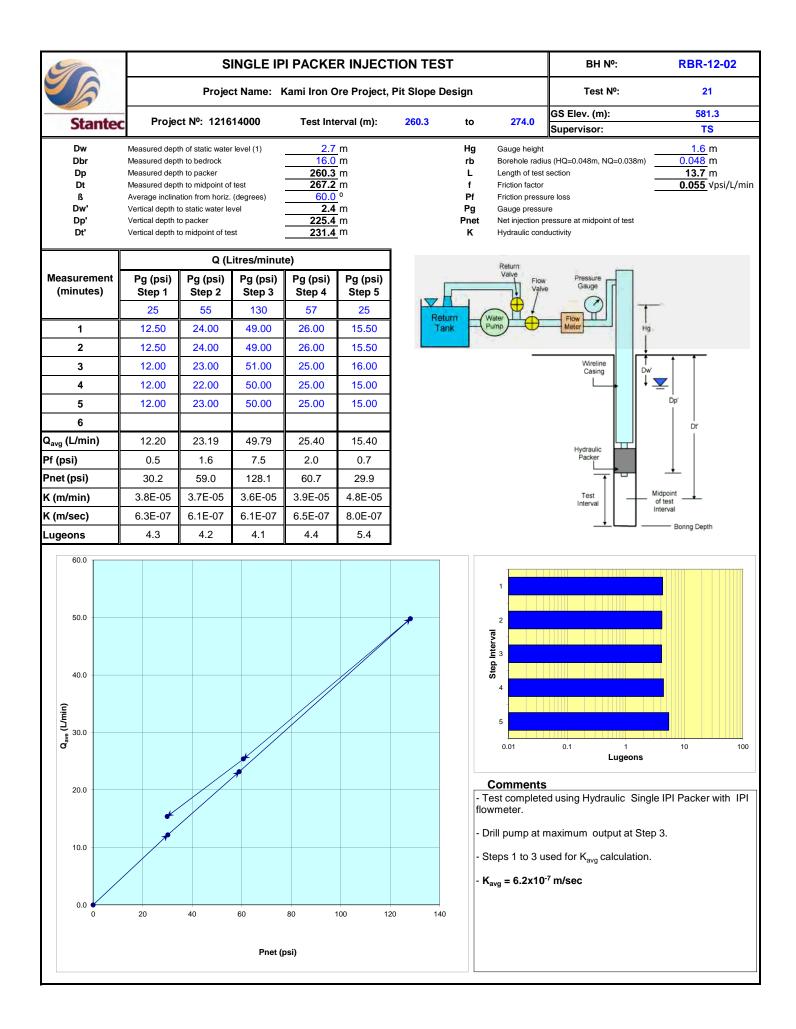


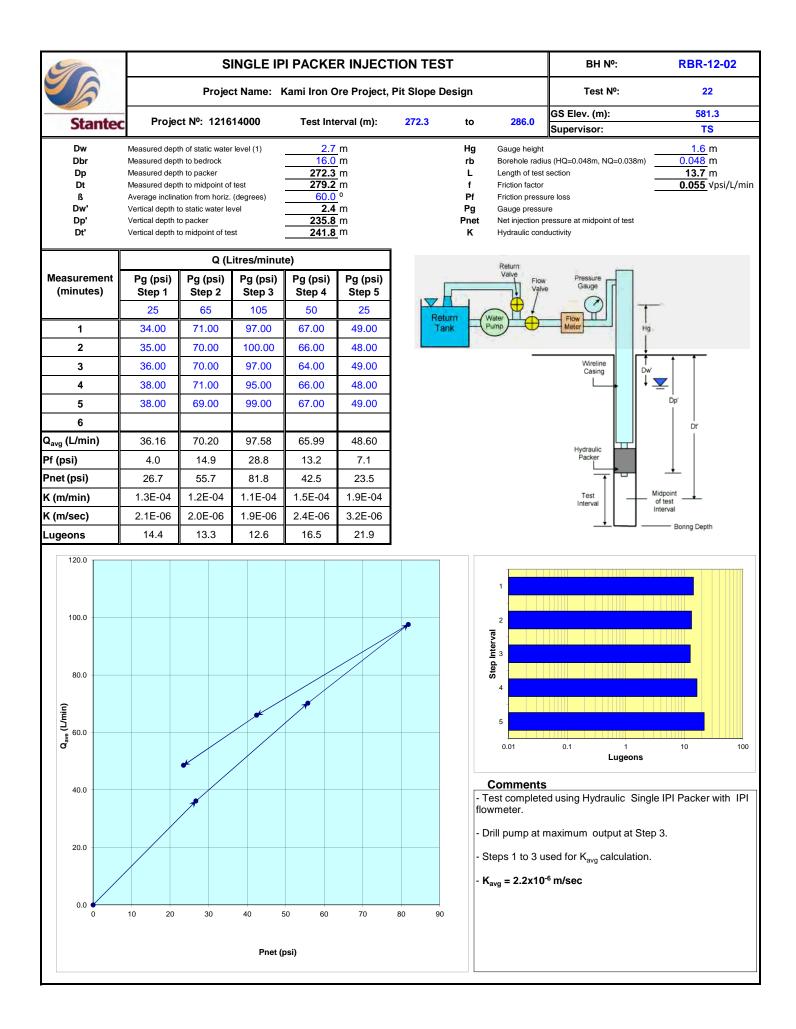


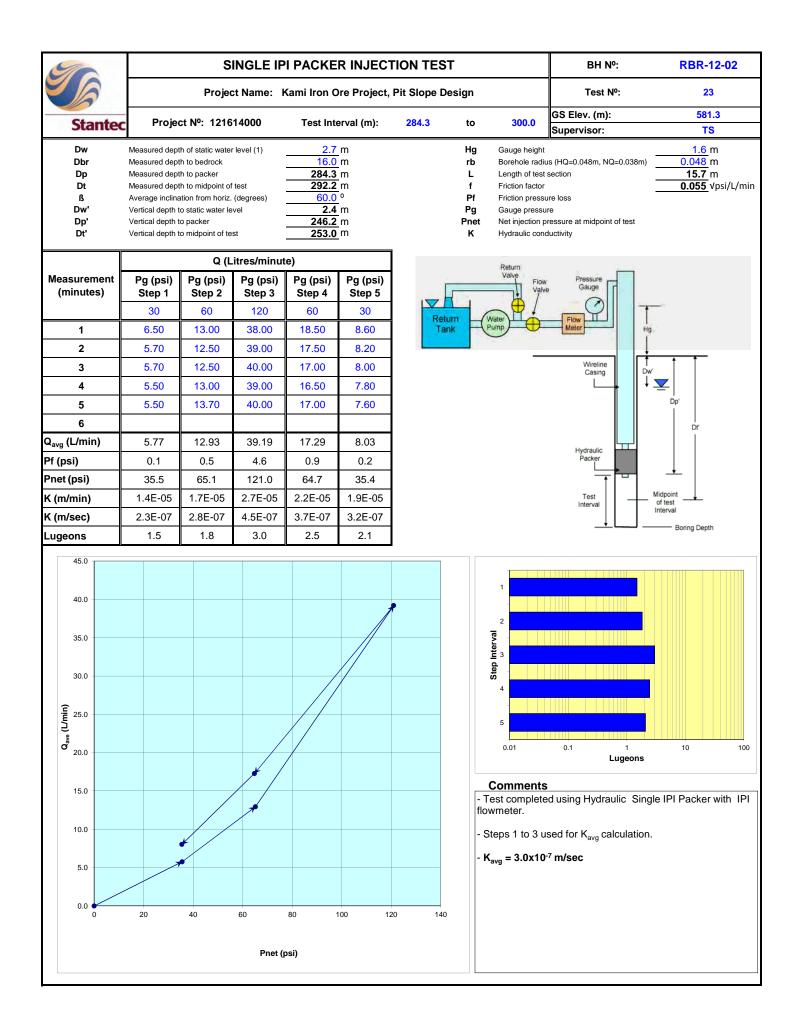


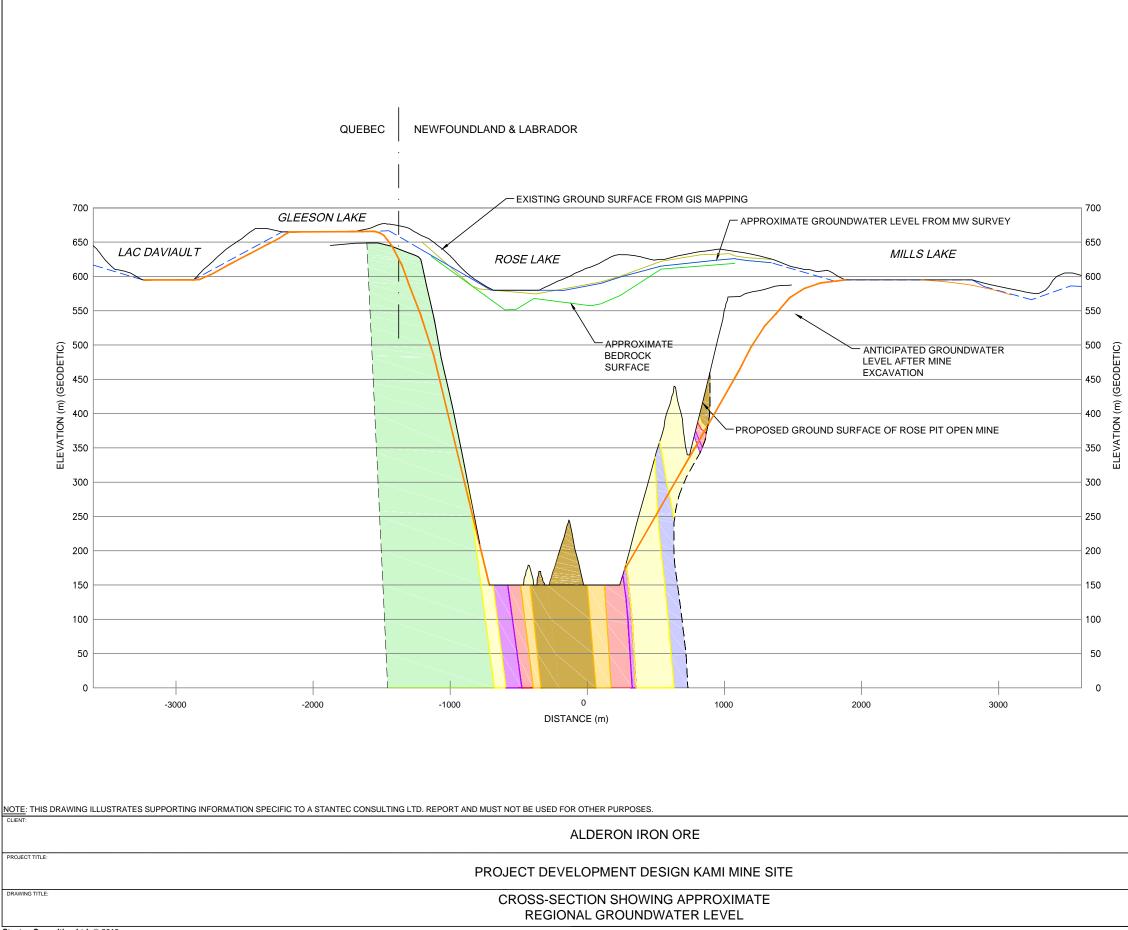


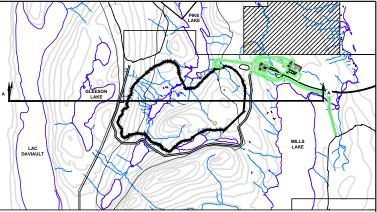






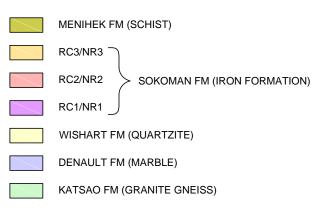




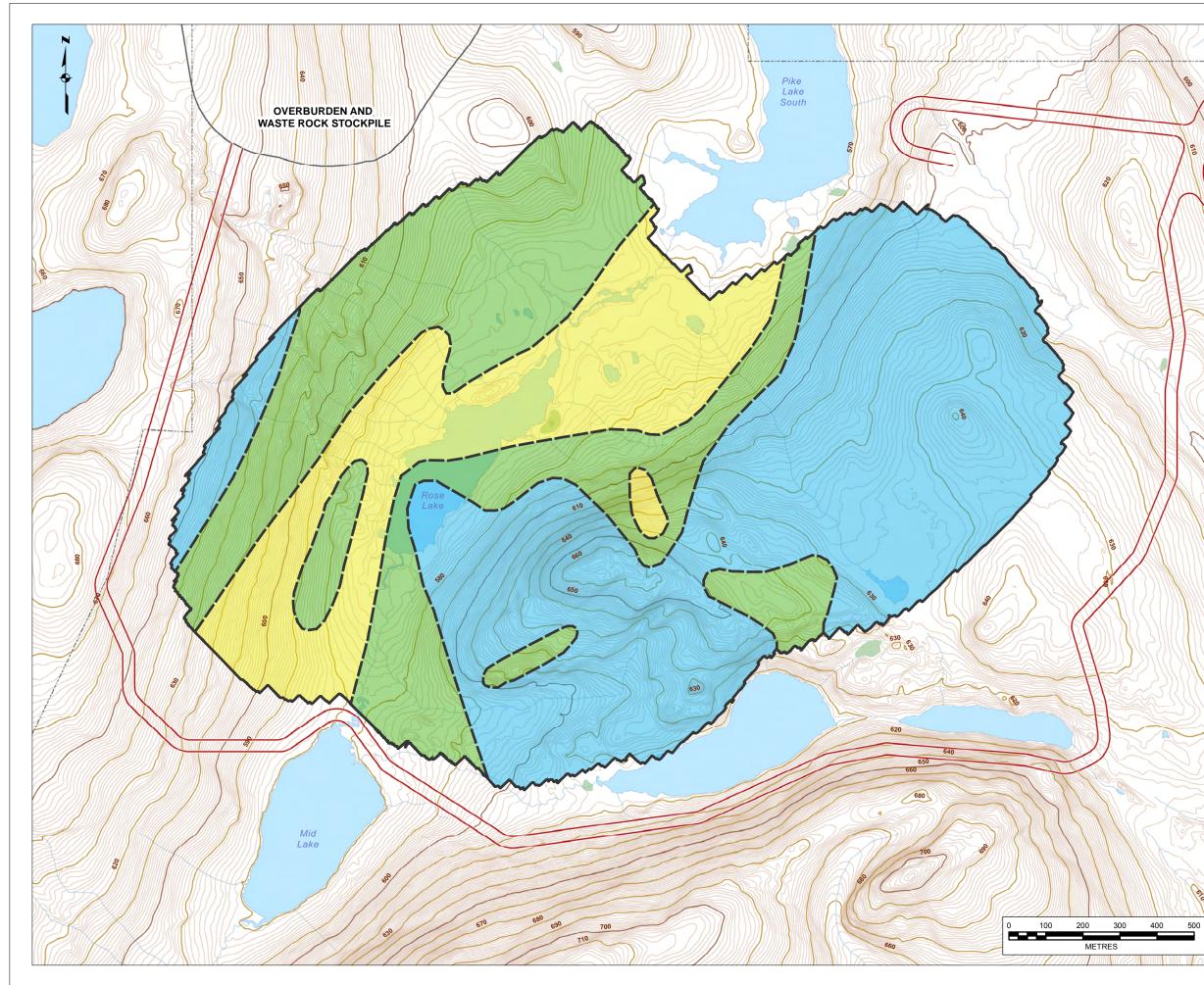


CROSS SECTION A'-A'

LEGEND



SCALE: AS SHOWN	DATE: JAN. 7, 2013	
DRAWN BY: R.L.	CHECKED BY: R.M.	
EDITED BY:	REV. No. 1	
DRAWING No: 1216140	00-306-GE-06	<u> </u>
CAD FILE: 12161400	0-306-GE-06.dwg	Stantec



Interrec		0		
	d Overburden Thickness	Cont		
) to 15 metres		10m Interval	
	15 to 30 metres		50m Interval	
	> 30 metres		Wetland	
•	ed Kami Project Features		Waterbody	
F	Proposed Project Features			
F	Proposed Access Road			
A	Alderon Licenses			
F NOTE	Rose Pit Boundary			
 Final bo were co understi 19U and Interpre complet (K- serie lengths collar az collar lo topogra Estimati encount 		ar azim) and w I was re m. R- and on of ex using t ectories are sho ole orie rs on ir ased of ations,	uths, and collar in ere provided to St eferenced to NAD ROB- series hole: ploration holes the recorded drille orientated at the wn plotted at the p entation, variations inclined boreholes. n subsurface conc and can only be e	clinations antec. It is 27 Zone s was d overburde provided provided s in litions xtrapolated
1. Base D 2. Site pla ACAD-305 Rose Pit fo (5/07/2012 * Scoping the origina	ata provided by Forbes West: K an and infrastructure (except Ros 54001-000000-41-D20.0001-RA potprint: ACAD-3054001-000000 2) level Rose Pit footprint was the l pit outline, provided in May 20 on: Transverse Mercator	e Pit fo -dwg, p -41-D2	potprint): provided by BBA (0.0001.dwg, provi f this assessment,	ided by BBA
1. Base D 2. Site pla ACAD-305 Rose Pit fo (5/07/2012 * Scoping the origina 3. Projectio Datum:	an and infrastructure (except Ros 54001-00000-41-D20.0001-RA 500tprint: ACAD-3054001-000000 2) level Rose Pit footprint was the al pit outline, provided in May 20	e Pit fo -dwg, p -41-D2	potprint): provided by BBA (0.0001.dwg, provi f this assessment,	ided by BBA
1. Base D 2. Site pla ACAD-305 Rose Pit fo (5/07/2012 * Scoping the origina 3. Projectio Datum:	an and infrastructure (except Ros 54001-000000-41-D20.0001-RA potprint: ACAD-3054001-000000 2) level Rose Pit footprint was the l pit outline, provided in May 20 on: Transverse Mercator NAD 83	e Pit fc F.dwg, p -41-D2 focus of I2, is sh	potprint): provided by BBA (0.0001.dwg, provi f this assessment,	ided by BBA
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1. Base D 2. Site pla ACAD-305 Rose Pit fc (5/07/2012 * Scoping the origina 3. Projectic Datum: Coordin DATE Sept. 2012	an and infrastructure (except Ros 54001-000000-41-D20.0001-RA 500tprint: ACAD-3054001-000000 2) level Rose Pit footprint was the al pit outline, provided in May 20 on: Transverse Mercator NAD 83 late System: UTM Zone 19N DESCRIP 2 Final Rep	E Pit fc -dwg, r -41-D2 focus of 12, is sh TION ort E P	otprint): provided by BBA (0.0001.dwg, provi f this assessment, nown herein.	ided by BB/ , therefore REVISION 0
1. Base D 2. Site pla ACAD-305 Rose Pit fc (5/07/2012 * Scoping the origina 3. Projectic Datum: Coordin DATE Sept. 2012 clieNT: PROJECT TITLE PROJECT TITLE	An and infrastructure (except Ros 54001-000000-41-D20.0001-RA 54001-000000-21-D20.0001-RA 500tprint: ACAD-3054001-000000 2) level Rose Pit footprint was the al pit outline, provided in May 20 500 cm: Transverse Mercator NAD 83 late System: UTM Zone 19N DESCRIP 2 Final Rep CALLON I R O N CON KAMI IRON OR	E Pit fc -dwg, p -41-D2 focus of 12, is st TION ort E P DE EN T	Provided by BBA (0.0001.dwg, provided by BBA (0.0001.dwg, provided by BBA (1.00001.dwg, pr	ided by BBA , therefore REVISION 0
1. Base D 2. Site pla ACAD-305 Rose Pit fc (5/07/2012 * Scoping the origina 3. Projectic Datum: Coordin DATE Sept. 2012 clieNT: PROJECT TITLE PROJECT TITLE	an and infrastructure (except Ros 54001-000000-41-D20.0001-RA bootprint: ACAD-3054001-000000 level Rose Pit footprint was the al pit outline, provided in May 20 on: Transverse Mercator NAD 83 late System: UTM Zone 19N DESCRIP Pinal Rep CONCERSION KAMI IRON OR PIT SLOPE TIMATED OVERBURD	E Pit fc -dwg, p -41-D2 focus of 2, is st TION ort E P DE EN T Sulti	Provided by BBA (0.0001.dwg, provided by BBA (0.0001.dwg, provided by BBA (0.0001.dwg, provided by BBA (1.0001.dwg, provid	ided by BBA , therefore REVISION 0
1. Base D 2. Site pla ACAD-305 Rose Pit fc (5/07/2012 * Scoping the origina 3. Projectic Datum: Coordin DATE Sept. 2012 clieNT: PROJECT TITLE PROJECT TITLE	an and infrastructure (except Ros 54001-000000-41-D20.0001-RA 54001-000000-41-D20.0001-RA 54001-000000(2) level Rose Pit footprint was the al pit outline, provided in May 20 on: Transverse Mercator NAD 83 late System: UTM Zone 19N DESCRIP 2 Final Rep 7 KAMI IRON OR FINATED OVERBURD Stantec Cons ISCALE:	E Pit fc -dwg, p -41-D2 focus of 2, is st TION ort E P DE EN T Sulti	Provided by BBA (0.0001.dwg, provided by BBA (0.0001.dwg, provided by BBA (0.0001.dwg, provided by BBA (1.0001.dwg, provid	Interefore REVISION 0
1. Base D 2. Site pla ACAD-305 Rose Pit fc (5/07/2012 * Scoping the origina 3. Projectic Datum: Coordin DATE Sept. 2012 client: PROJECT TITLE PROJECT TITLE	an and infrastructure (except Ros 54001-000000-41-D20.0001-RA bootprint: ACAD-3054001-000000 level Rose Pit footprint was the al pit outline, provided in May 20 on: Transverse Mercator NAD 83 late System: UTM Zone 19N DESCRIP Pinal Rep CONCERSION KAMI IRON OR PIT SLOPE TIMATED OVERBURD Stantec Cons SCALE: 1:10,00 DRAWN BY:	E Pit fc -dwg, p -41-D2 focus of 2, is st TION ort E P DE EN T Sulti	ADDEDTINESS ADDITIONAL SECTIONS ADDITIONAL SECTIO	MAP
1. Base D 2. Site pla ACAD-305 Rose Pit fc (5/07/2012 visor visor visor batum: Coordin DATE Sept. 2012 CLIENT: PROJECT TITLE PROJECT TITLE EST	an and infrastructure (except Ros 54001-000000-41-D20.0001-RA bootprint: ACAD-3054001-000000 level Rose Pit footprint was the all pit outline, provided in May 20 on: Transverse Mercator NAD 83 late System: UTM Zone 19N DESCRIP 2 Final Rep Final Rep CONCERSION KAMI IRON OR PIT SLOPE TIMATED OVERBURD Stantec Cons SCALE: 1:10,00 DRAWN BY: AB EDITED BY:	E Pit fc -dwg, p -41-D2 focus of 2, is st TION ort E P DE E P DE EN T Sulti 0	ADDEDTINESS ADDITIONAL SECTIONS ADDITIONAL SECTIO	MAP

