

**ENVIRONMENTAL PREVIEW REPORT
PURSUANT TO THE NEWFOUNDLAND
AND LABRADOR *ENVIRONMENTAL
PROTECTION ACT***

**AGS Fluorspar Project
St. Lawrence, NL
Volume 2, Appendix E-1**

Submitted to:

Newfoundland and Labrador Department of Environment
and Conservation, Environmental Assessment Division

Submitted by:

Canada Fluorspar (NL) Inc.



September 2015



APPENDIX E-1

Phase 1 Hydrogeology Program





January 2015

PROPOSED AGS MINE PROJECT

Phase 1 Hydrogeology Study Canada Fluorspar Inc. St. Lawrence, NL (Rev 0)

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REPORT



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Executive Summary

This report presents the results of an initial phase (Phase 1) of hydrogeological and hydrological site investigations to provide the data necessary to support an Environmental Impact Assessment (EIA) for the AGS Mine Project (the Project), a proposed fluorite mine to be located on the Burin Peninsula 1 km south of the Town of St. Lawrence, Newfoundland (Figure 1), owned by Canada Fluorspar (NL) Inc. (CFI).

The mining concept being developed will likely comprise:

- Shallow surface mining with the later development of an underground mine; or
- Underground mining only

Given that the hydrogeological program to assess inflows and environmental effects will be quite different for these two mining concepts, Phase 1 program focused on information requirements generally applicable to both mining concepts with a later phase of the program tailored more specifically the proposed mining plan when developed.

The study area targeted an assumed general outline of the surface mine as shown on Figure 2, considering a project footprint in which Grebes Nest pond would be removed during mining and John Fitzpatrick Pond to the north and Upper Island Pond to the east would not be disturbed.

The scope of work can be summarized as follows:

- Limited hydrological measurements and limited sampling of surface water and groundwater including
 - Test pit excavation and shallow upper bedrock borehole drilling completed with monitoring well installations;
 - Monitoring well development, groundwater sampling and in-situ hydraulic conductivity testing;
 - Staff gauge stream flow measurements and surface water sampling;
 - Collection of relevant climate data and the locations of nearby municipal water wells sources; and
 - General geology information.

The report text presents the results of these investigations including with limited interpretations. Supporting factual data are provided in Appendices A through I.



Table of Contents

1.0 INTRODUCTION..... 4

2.0 SCOPE OF WORK 4

3.0 BACKGROUND 4

4.0 FIELD INVESTIGATION 5

 4.1 Rationale 6

 4.2 Methodology 6

 4.2.1 Test pit Excavation and Borehole Drilling..... 6

 4.2.2 Monitoring Well Installation 7

 4.2.3 Well Development..... 8

 4.2.4 Groundwater Sampling 8

 4.2.5 Monitoring Well Coordinates 8

 4.2.6 Hydraulic Conductivity Testing..... 9

 4.2.7 Surface Water Monitoring (Staff Gauges and Stream Flow Measurements)..... 9

 4.2.7.1 Staff Gauge 9

 4.2.7.2 Stream Flow Measurements 10

 4.2.8 Surface Water Sampling 10

 4.2.9 Long Term Groundwater Monitoring 11

5.0 RESULTS 11

 5.1 Physiography..... 11

 5.2 Climate 12

 5.3 Water use 14

 5.4 Geology 14

 5.4.1 Regional Geology..... 14

 5.4.2 Site Geology 14

 5.4.3 Borehole Stratigraphy 15

 5.4.4 Hydraulic Response Testing 16

 5.4.5 Groundwater Elevations..... 18

 5.4.6 Groundwater Flow Directions..... 19



5.4.7	Surface Water Flow Monitoring.....	19
5.4.8	Shallow groundwater-surface water interaction	19
5.4.9	Groundwater Quality	21
5.4.10	Surface water Quality.....	22
6.0	CLOSURE.....	24
7.0	REFERENCES.....	25

TABLES

Table 1: Monitoring Well Details Summary

Table 2-1: Monthly Mean Total Precipitation for the Environment Canada meteorological station near St.Lawrence, NL

Table 2-2: Monthly Mean Total Precipitation (mm) for the Environment Canada meteorological Station

Table 3: Hydraulic Conductivity Estimates based upon single well response tests and pumping tests

Table 4: Input Parameters and Hydraulic Conductivity Estimates

Table 5: Hydraulic Conductivity Estimates based upon Hazen methos for grain size results

Table 6: Groundwater Elevations

Table 7: Measured Water Level and Stream flow

Table 8: Groundwater Quality Field Measurements

Table 9: Surface Water Quality Field Measurements

FIGURES

Figure 1 Site Plan

Figure 2 Phase 1 Hydrogeological Work Plan

Figure 3 Surficial Geology

Figure 4 Municipal Water Sources

Figure 5 Bedrock Geology

Figure 6 Geological Cross-Section

Figure 7 Watershed Boundaries

APPENDICES

APPENDIX A

Borehole Record; Rock Core Images; Geophysics Borehole Survey

APPENDIX B

Test pit Record and Images; Gradation Curves

APPENDIX C

Monitoring Well Installation Record; Monitoring Well Completion Images; Monitoring Well/Stream Gauge Survey Data



APPENDIX D

Water Quality Analysis Report

APPENDIX E

Hydraulic Conductivity Analysis

APPENDIX F

Staff Gauge Completion Images

APPENDIX G

Surface Water and Groundwater Hydrographs

APPENDIX H

Stream Flow Transect Images and Discharge Profile

APPENDIX I

Surface Water Sampling Locations Images



1.0 INTRODUCTION

This report presents the results of an initial phase of hydrogeological and hydrological site investigations to provide the data necessary to support an Environmental Impact Assessment (EIA) for the AGS Mine Project (the Project), a proposed fluorite mine located on the Burin Peninsula 1 km south of the Town of St. Lawrence, Newfoundland (Figure 1), owned by Canada Fluorspar (NL) Inc. (CFI).

2.0 SCOPE OF WORK

CFI retained Golder Associates Ltd (Golder) to carry out these investigations. The scope of work is outlined in Golder's Hydrogeology field work – Memorandum dated October 1, 2014 and can be summarized as follows.

- Limited hydrological measurements and limited sampling of surface water and groundwater.
- For the purpose of developing this program we have assumed a general outline of the surface mine as shown on Figure 2; wherein Grebes Nest pond would be removed during mining and John Fitzpatrick Pond to the north and Upper Island Pond to the east would not be disturbed.
- Thus the focus of this program is the hydrogeological and hydrological conditions in the vicinity of these ponds located immediately down gradient of the assumed surface mine footprint.

3.0 BACKGROUND

The granite hosted veins have been operated by several owners over the past seven decades; before 1957 by the St. Lawrence Corporation and between 1940 and 1978 by Alcan. During the period 1979 to 1984 the mine was idle until operation was resumed in 1986 by St. Lawrence Fluorspar Limited, a subsidiary of Minworth. The mine has been out of operation since 1991 (Scott, 2009).

The site is a former Aluminum Company of Canada (ALCAN) fluorspar mine which closed down its operations in 1977. Limited production was reported between 1986 and 1991 by St. Lawrence Fluorspar.

The mineralized rock at the AGS vein is hosted in meta-sediments and rhyolites, in a ratio of approximately 70:30 meta-sediments to rhyolite that are variably fractured with some fine-grained intrusive(s) of granitic composition (i.e. rhyolites). The mineralized zone is subvertical with thicknesses ranging from about 3 to 25 metres (m). Groundwater levels are reported to be close to ground surface and drill water circulation is lost close to surface in many boreholes. Drillers report some indication of drill water reporting to surface at nearby boreholes prior to these being grouted. Further east, the previously mined deposits comprising the Tarefare, Director and Blue Beach veins, are hosted predominantly in granites with limited occurrences of meta-sedimentary rocks. These mines were each reported to have groundwater inflows of about 2,000 to 3,000 gallons per minute (gpm).

In parallel, Golder has completed water quality sampling at various water courses and streams at the Project site. Several of the groundwater monitoring installations were completed to integrate the assessment of groundwater / surface water interactions.



4.0 FIELD INVESTIGATION

This phase of the program comprises the limited assessment of baseline hydrogeological, limited hydrological conditions and baseline water quality. It can be summarized as follows.

- Four (4) test pit excavation of overburden materials, completed with 38.1 millimetres (mm) Inner diameter (ID) standpipes placed in the backfill.
 - Soil sampling for grain size analysis from test pit samples.
- Borehole drilling and rock core logging at four (4) locations adjacent to the test pits completed with ID 38.1 mm standpipe shallow bedrock monitoring wells.
- Well development, water level measurements, hydraulic response (slug) testing at all 8 monitoring wells.
- Hydraulic response (slug) testing and pumps testing at two existing exploration boreholes.
- Completion of three river staff gauge installations.
- Water quality sampling at 8 streams and 4 ponds.
- Groundwater sampling from 4 monitoring wells and two exploration boreholes (open holes).

Monitoring well, staff gauge locations along with surface water sampling locations are shown on Figure 1. A summary of monitoring well details is provided in Table 1. Borehole logs are provided in Appendix A.

The test pit and borehole locations were selected according to the assumed footprint of a possible open pit. The test pits were excavated to refusal. The shallow drilling depths of 3 m into rock was with specific purpose to compare overburden and near surface bedrock water levels and water quality for hydraulic connection and gradients.

Table 1: Monitoring Well Summary Details

Well ID	GPS Easting WGS84	GPS Northing WGS84	Hole Diameter (mm) Or test pit	Well Depth (mbgs)	Screen Top (mbgs)	Top of Bedrock	Screened Geologic Unit	Water Level (mbgs)	Vertical Gradient (m/m)
MW14-01A	617,458	5,195,561	96	6.4	4.9	6.8	Overburden	0.28	-0.03
MW14-01B	617,465	5,195,550	Test pit	1.9	0.4	-	Overburden	0.41	
MW14-02A	617,096	5,196,293	75.7	8.5	7.0	4.8	Meta-sediments	2.90	0.32
MW14-02B	617,101	5,196,293	Test pit	1.8	0.3	-	Overburden	0.74	
MW14-03A	616,285	5,196,552	75.7	5.5	4.0	2.4	Meta-sediments	0.60	0.12
MW14-03B	616,284	5,196,552	Test pit	1.8	0.3	-	Overburden	0.14	
MW14-04A	615,673	5,196,695	75.7	6.4	4.9	2.0	Meta-sediments	0.49	0.10
MW14-04B	615,671	5,196,693	Test pit	1.6	0.1	-	Overburden	0.03	

Note: "A" denotes well in borehole and "B" refers to well in test pit

The following subsections provide details on the rationale, methodology, and results of the field investigation.



4.1 Rationale

The field investigation was developed to support the estimate of groundwater inflows to the proposed AGS mine and the assessment of effects on the surface environment.

We understand the mining concept being developed will likely comprise:

- Shallow surface mining with the later development of an underground mine; or
- Underground mining only.

Given that the hydrogeological program to assess inflows and environmental effects will be quite different for these two mining concepts, we have proposed a staged program with the Phase 1 program focusing on information requirements generally applicable to both mining concepts with a later phase of the program tailored more specifically the proposed mining plan when developed.

The Phase 1 program was established to assess baseline hydrogeological conditions generally at the assumed perimeter of the surface mine footprint, the limited hydrogeology studies were conducted in the following areas:

- At the assumed perimeter of the surface mine footprint (MW14-4, MW-14-3, PGS-93b, PGS-124). See Figure 2.
- In the vicinity of John Fitzpatrick Pond and Upper Island Pond located immediately down-gradient of the assumed surface mine footprint (MW14-1, MW14-2).

In order to assess the interaction of the surface water features with the shallow table and to augment the bioscience work program, we have included:

- The installation of three staff gauges and collection of flow measurements in local streams at locations shown on Figure 1.
- Limited hydrological sampling of surface water bodies WQ STA-1, WQ STA-7, WQ STA-3, WQ STA-4, WQ STA-8, and WQ STA-9, shown on Figure 1.
- Due to overlapping aquatic and water quality programs with this Phase 1 program, additional sampling was carried out at the following locations: WS-2, WS-5, WS-10, WQ STA-5, WQ STA-6, and WQ STA-2.

In order to assess these areas, a total of four well clusters consisting of two monitoring wells (“deep” – A-series and “shallow” – B-series) were completed, resulting in total of 8 wells (Figure 1). Table 1 provides a specific location and construction detail for each well cluster. Prior to drilling, each location was first visited and approved by CFI staff.

4.2 Methodology

4.2.1 Test pit Excavation and Borehole Drilling

Test pit and borehole drilling activities occurred between October 20, 2014 and October 24, 2014. Excavation and drilling was undertaken by Springdale Diamond Drilling contractor, an affiliate of Springdale Forest Resources, Inc. Test pit excavation of overburden materials and adjacent borehole drilled to approximately 3 m



into rock were completed; for a total of four test pits and four adjacent boreholes. All test pit excavation and drilling activities were overseen by a Golder field geologist.

Test pit locations were selected in the field to avoid shallow depths to rock so as to characterize the overburden materials below the organic soil cover. Test pits were excavated by Springdale Drilling using a CAT 320B backhoe. The pits ranged in depth from 1.6 to 2.0 m and were in back filled with cutting the same day. Overburden samples were recovered from the excavator bucket and examined at surface and one sample of granular material from each excavation submitted for grain size analysis.

Boreholes were drilled by Springdale Drilling using a track mounted, Duralite 800 diamond drill. The boreholes ranged in depth from 5.5 m to 8.8 m with a total of 27.8 m drilled. Borehole was drilled with NQ rods with a nominal hole diameter of approximately 76 mm. A continuous core of bedrock was obtained by Springdale Drilling. After drilling, the core was stored in CFI core shack and logged and photographed by Golder.

Springdale Drilling used a biodegradable drilling additive, called Poly-Plus, while drilling the boreholes to raise drill cuttings and to maintain stability of borehole wall during drilling. Immediately after drilling to depth, fresh and clean water was circulated for about 30 minutes to wash any additive out of the borehole.

Borehole logs are presented in Appendix A. Test pit logs and images are presented in Appendix B.

4.2.2 Monitoring Well Installation

All well installations were completed by Springdale Drilling and overseen by a Golder field geologist. A total of four monitoring well clusters consisting of two holes (“deep” – A-series and “shallow” – B-series) were completed, resulting in a total of eight monitoring well standpipe piezometers.

A typical well installation involved the following procedure:

Following the excavation of the test pit a standpipe piezometer was placed into the excavation backfilled with nominal compaction of the excavated materials. The “shallow” – B-series monitoring well consists of a 1.5m long PVC well screen (number 10 slot size, 38.1 mm diameter), with riser pipe extending about 1 m above ground surface.

At the completion of the drilled borehole, the NQ rods were removed and a 1.5 m long PVC well screen (number 10 slot size, 38.1 mm diameter), was lowered down the borehole. About 1 m of riser pipe was left extending above ground surface. Silica filter sand was used to fill the annular space to a selected depth above the screen, followed by bentonite pellets (hole plug) and completed with an above ground protective steel casing. With the exception of MW14-01, the HQ surface casing was left in the borehole to provide an anchor for the protective surface casing.

Monitoring well installation record along with photos of completed well installations is presented in Appendix C.



4.2.3 Well Development

The screened intervals in each of the B-series monitoring well were developed by air-lifting for about one hour to improve the hydraulic connection between the well intake screen and the surrounding host unit by removing sediment and residual materials from drilling and well installation activities.

The water level in the well was allowed to rise to a static condition following to well development (air lift), whereupon a depth to water measurement was recorded.

A full round of stabilized groundwater levels were manually measured by Golder on November 1, 2014. Water levels are presented in Table 1. A water level probe was utilized for all water level measurement events.

4.2.4 Groundwater Sampling

Groundwater samples were collected from the 4 monitoring wells installed in bedrock and the 2 exploration boreholes for a total of six groundwater sample suites. With the exception of MW14-04A which was sampled with a disposable bailer, samples were collected using air lift techniques.

Groundwater quality sample were collected from monitoring wells:

- MW14-01A, MW14-02A, MW14-03A, immediately following well development on October 24, 2014.
- MW14-04A, on November 4, 2104. The following day after well was purged dry.
- PGS-93b, and PGS-124, immediately following constant rate pump test on October 25 and 26, 2014.

Field measurements were collected at the time the sample was taken with a pH/temperature metre and a conductivity/temperature metre. The results are outlined in section 5.

Sampling was conducted in accordance with standard practices to obtain a representative sample and to avoid cross contamination between monitoring locations. Chemical analysis was carried out by Maxxam and one blind duplicate sample was taken for QA/QC purposes.

The groundwater samples were analyzed for a general suite of inorganic parameters including pH, conductivity, major ions and heavy metals, TDS, TSS, nitrates, nitrites and ammonia following the same suite as for surface water. The test results were compared to the Summary of Guidelines for Canadian Drinking Water Quality (SGCDWQ), Health Canada, 2014. These analytical results will provide a limited and general characterization of the bulk hydrogeological conditions of the rock encountered over the length of each borehole.

Maxxam's Laboratory water quality analysis report can be found in Appendix D.

4.2.5 Monitoring Well Coordinates

Well locations were obtained Golder using a hand-held Garmin Geographical positioning Device Model No 60Sx. The average accuracy of this device is within 3 m (Garmin, 2014). Well locations were surveyed on November 19, 2014, by Edward and Associates Ltd. under contract with Canada Fluorspar Inc. Well coordinates are presented in Table 1 and Appendix C and well locations shown in Figure 1.



4.2.6 Hydraulic Conductivity Testing

Hydraulic conductivity testing is used to characterize groundwater flow through soil or rock. Hydraulic conductivity (K) describes the ease with which groundwater can move through pore spaces or fractures. Localized estimates of hydraulic conductivity may be obtained through the analysis of in-situ hydraulic response tests or pumping tests of groundwater wells.

In-situ rising or falling head tests were completed at each well by Golder to estimate the hydraulic conductivity of screened units at the site. In some cases multiple (confirmatory) tests were performed. The hydraulic testing involved establishing a static water level depth and then instantaneously removing or adding a known volume (a “slug”) to the well to observe the hydraulic head response over time. Recovering water levels were measured using automatic groundwater data loggers set to record time, pressure and temperature at a time interval selected based on the rate of recovery during well development. Water levels were measured manually to determine the end of the test and the data logger removed and downloaded. The hydraulic response data was processed in the software package Aqtesolv Pro (HydroSOLVE Inc., 2014) and interpreted using the Hvorslev mathematical solution (Hvorslev, 1951). Details of these tests are presented in Appendix E.

The open hole pumping tests were conducted in two exploration holes that were at least 150m deep, with the pump set no deeper than 15m downhole. Exploration hole pGS-93b (GS-14-113) was pumped at approximately 2 L/min for about 75 minutes. While exploration hole pGS-124 (GS-14-94) was pumped at approximately 9 L/min for about 140 minutes. These short-term pumping tests were evaluated using the Thiem (1906) solution for steady-state flow to a well, which is a high-level hydrogeological method used to provide preliminary quantitative characterization. Details of these tests are presented in Appendix E.

4.2.7 Surface Water Monitoring (Staff Gauges and Stream Flow Measurements)

The surface water monitoring program was undertaken to assess the interaction of the surface water features with the shallow groundwater table and to augment the bioscience work program. The limited baseline surface water program consisted of two components:

- 1) Water level monitoring at the outlet from each pond (Fitzpatrick Pond, Upper Island Pond, and un-named pond) via periodic staff gauge measurements.
- 2) Field stream surveys for stream characterization.

The locations of the surface water monitoring have been selected to coincide with the monitoring locations in the aquatics program as appropriate.

4.2.7.1 Staff Gauge

Three staff gauges SW-1, SW-2, and SW-3 with locations coinciding with surface monitoring stations WQ STA-1, WQ STA-3, and WQ STA-9 were installed on October 29, 2014, by Golder field staff in local streams at locations shown on Figure 1. A data logger was installed in the stream, adjacent to each staff gauge to develop a continuous record of water levels and water temperatures at these locations. Data loggers were installed on October 29th and removed on November 20, 2014, before streams begin freezing.



Each station involved stakes (T-Posts) installed at the approximate channel mid-point with a pressure transducer data logger (Schlumberger DIVER DI501) attached near the base of the T-Posts using a karabiner and eye bolt, and a stainless steel cable, to secure the data logger at a fixed position above the channel bed. A level survey was completed to reference these stations. A removable acrylonitrile butadiene styrene (ABS) plastic casing was fitted to the T-Posts at both stations to prevent water level disturbance (by turbulence and/or debris).

Photographs of staff gauge completion are presented in Appendix F and surface water hydrographs are shown in Appendix G.

4.2.7.2 Stream Flow Measurements

Stream surveys were carried out by Golder field staff, with the assistance of CFI personnel on October 31, 2014.

The stream flow surveys were carried out the following surface monitoring stations, which were established downstream of the corresponding Ponds (Figure 1):

- WQ STA-1: The surface monitoring station is located about 86 m downstream of Upper Island Pond. One transect, or cross-section, located 13 m downstream of staff gauge SW-1 was surveyed.
- WQ STA-3: The surface monitoring station is located about 36 m downstream of John Fitzpatrick Pond. Two transects, were surveyed: One transect positioned at staff gauge SW-2 and the second transect at approximately 18 m downstream of staff gauge SW-2.
- WQ STA-9: The surface monitoring station is located about 41 m downstream of the pond inlet. Two transects, were surveyed: One transect positioned at staff gauge SW-3 and the second transect at approximately 3.4 m downstream of staff gauge SW-2.

Streamflow measurements were estimated using the velocity-area method. A tape measure was extended the length of a representative cross-section during measurement. Streamflow velocities and corresponding water depths were collected at various intervals along the cross-section (0.1 m to 0.2 m). Current velocities were recorded using a Flo-Mate2000 Electromagnetic Flow Meter (EM Flow Meter) at 60% of the total water depth (for water depths less than 0.50 m) or at the 20% and 80% depths and then averaged (for water depths greater than 0.50 m). The sum of the flows in all segments yields the total flow at the station at the time of each measurement. Stream flow transect photos and discharge calculations are presented in Appendix H.

4.2.8 Surface Water Sampling

Surface water quality sampling was conducted from November 3 to 4, 2014 to provide a limited baseline of the existing surface water quality against future potential impacts to the surface water as a result of the proposed mining operations. As part of the hydrogeological phase 1 investigation, sampling occurred at six locations: WQ STA-1, WQ STA-7, WQ STA-3, WQ STA-4, WQ STA-8, and WQ STA-9. Due to overlapping aquatic and water quality programs, additional sampling was carried out at the following locations: WS-2, WS-5, WS-10, WQ STA-5, WQ STA-6, and WQ STA-2. Sampling locations are shown on Figure 1 and sampling location images are presented in Appendix I.



Field measurements were collected at the time sample was taken with a pH/temperature metre and a conductivity/temperature metre. The results are outlined in Section 5.

Sampling was conducted in accordance with standard practices to obtain a representative sample and to avoid cross contamination between monitoring locations. As with the groundwater sampling, chemical analysis was carried out by Maxxam.

The surface water samples were analyzed for a broad suite of inorganic parameters including pH, conductivity, major ions and heavy metals, TDS, TSS, nitrates, nitrites and ammonia following the same suite as for groundwater. The test results were compared to the Summary of Guidelines for Canadian Drinking Water Quality (SGCDWQ), Health Canada, 2014.

Maxxam's Laboratory water quality analysis report can be found in Appendix D.

4.2.9 Long Term Groundwater Monitoring

Golder installed pressure transducer data logger (Schlumberger DIVER DI502) in four monitoring wells completed in bedrock and two exploration boreholes to collect a continuous record of water levels: MW14-01A, MW14-02A, MW14-03A, MW14-04A PGS-93a and PGS-124. Loggers were installed in their corresponding wells on November 1, 2014, and then removed from the well on November 20, 2015, the data uploaded and then placed back in the corresponding wells the following day. A barometric pressure data logger (Schlumberger DIVER DI500) was installed inside the protective casing of MW14-01A to provide atmospheric pressure compensation for the water level loggers.

The loggers were set to record data every hour, which allows for more than a year data collection between data logger downloads. Given that loggers can sometimes fail, it is advisable to download the loggers quarterly as access allows.

Daily precipitation and temperature records for the monitoring period were obtained from the Environment Canada meteorological station, which is located approximately 1 km east of the town of St. Lawrence. Results are presented along with the hydrographs in Appendix G.

5.0 RESULTS

5.1 Physiography

The Project topography is generally controlled by underlying bedrock geology and the effects of glaciation and associated soil deposits, ranging from 80 m above sea level (masl) to over 150 masl (Figure 3). The majority of the area is hummocky with small ponds and drainage systems with relatively low gradients over much of their lengths.

The area surrounding the Site is covered with hummocks of grasses, many ponds and drainage brooks. There are abundant outcrops and peat bogs in the low lying areas.

With the exception of the Project access road and exploration drill roads, the surrounding countryside is accessible only by footpaths and/or All-Terrain Vehicle (ATV).



5.2 Climate

The Project area climate is marked by foggy, cool summers and short relatively moderate winters. The mean annual temperature is approximately 5.5°C. The mean summer temperature is 11.5°C and the mean winter temperature is -1°C. The mean annual precipitation ranges 1200 to over 1600 mm (Transport Canada, 2010).

Environment Canada meteorological station, which is located approximately 1 km east of the town of St. Lawrence, and assumes to be the nearest source of suitable precipitation data. Meteorological records are available-online:

http://climate.weather.gc.ca/climateData/dailydata_e.html?timeframe=2&Prov=NL%20%20&StationID=45567&dlyRange=2006-12-01|2014-09-18&Year=2014&Month=7&Day=18

The monthly mean precipitation normal for St. Lawrence are provided in Table 2-1. Based on 2014 precipitation data, a total of 1350.3 mm of precipitation fell up to November 23rd. Precipitation occurs all year round as rain with some snow in winter. The long term average rainfall (1971-2000) over the area was 1564.1 mm ranging between 1000 mm and 1650 mm per year (Scott, 2009).

Table 2-1: Monthly Mean Total Precipitation for the Environment Canada meteorological station near St. Lawrence, NL

Month	Total Precip. (mm)	Days Missing
Jan-14	227.9	1
Feb-14	118.3	0
Mar-14	148.8	0
Apr-14	91.3	1
May-14	143.2	0
Jun-14	131.1	0
Jul-14	86.3	0
Aug-14	108.7	0
Sep-14	31	0
Oct-14	119	1
Nov-14	144.7	8
Dec-14	0	31



Table 2-2: Monthly Mean Total Precipitation (mm) for the Environment Canada Meteorological Station

Station	Code ¹	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Mean Annual
St. Lawrence	A	140.2	121.6	122.7	118.9	118.5	133.1	109.4	106.1	157.4	157.4	146.4	132.4	1564.0

Note:

1. The minimum number of years used to calculate normals are indicated by a "code" defined as:

- "A": No more than 3 consecutive or 5 total missing years between 1971 to 2000.

Source: Environment Canada Meteorological Data website, date modified 08/08/14.



5.3 Water use

The St. Lawrence potable water supply system draws from the intake (WS-S-0699) in the St. Lawrence River located approximately 7 km northeast of the AGS Site, as shown on Figure 4. The nearby communities of Lawn and Little St. Lawrence obtain their potable water from intakes at Brazil Pond and Butler’s Brook, respectively. Brazil Pond intake (WS-S-0406) is located approximately 9 km northwest of the AGS Site while two intakes exists for Butler’s Brook (WS-S-0421) located about 7 km east of the AGS Site (refer to Figure 4).

Source data

Community	LGP Number	Serviced A	SA Number	Source Name	WS Number
Little St. Lawrence	2885	Little St. Lawrence	Sa-0433	Butler’s Brook	WS-S-0421
Little St. Lawrence	2885	Little St. Lawrence	Sa-0433	Butler’s Brook	WS-S-0421
Lawn	2745	Lawn – PWDU	SA-0936	Brazil Pond	WS-S-0406
Lawn	2745	Lawn – PWDU	SA-0936	Brazil Pond	WS-S-0406
Little St. Lawrence	4435	Little St. Lawrence – PWDU	SA-0910	St. Lawrence River	WS-S-0699
Little St. Lawrence	4435	Little St. Lawrence	SA-0724	St. Lawrence River	WS-S-0699

5.4 Geology

5.4.1 Regional Geology

The St. Lawrence fluorspar deposits are situated within the Avalonian belt of the Appalachian mountain system which is more than 200 km wide on land and extends more than 400 km offshore. The bedrock is characterized by widespread sections of thick volcanic rocks and marine to terrestrial clastic sedimentary rocks of Pre-Cambrian age. These are locally overlain by predominantly shallow marine sedimentary rocks of Cambrian age. Both sequences are locally overlain with angular unconformity by Carboniferous age sedimentary and volcanic rocks. There are several Late Precambrian and Late Devonian to Carboniferous granite intrusions throughout the Avalonian belt system in eastern Newfoundland (Scott, April 2009).

The geology of the area is described in detail by the Mineral Development Division of Newfoundland and Labrador’s Department of Mines and Energy (Scott, 2009).

5.4.2 Site Geology

Geological reports and maps indicate that the Site is underlain by gravel and sand deposits of glacial outwash and fluvial origin and Till veneer (refer to Figure 3). The geological sequence in the overburden typically consists of a thin layer (~1m) of surficial organic soils, underlain by glacial till comprised of silty sand and gravel with varying percentages of cobbles and boulders. Based on the results of the subsurface investigation, superficial material is observed to be up to 5 metres in thickness and absent in places where the bedrock is exposed.

Shallow rock types observed at the AGS Site are typically meta-sedimentary rocks and some fine-grained intrusive(s) of granitic composition (i.e. rhyolites). These rocks form part of the Pre-Cambrian Burin Group which is comprised of sedimentary and meta-sedimentary rocks and subordinate volcanic flows consisting of pillowed and massive basaltic and andesitic flows and aquagene tuffs (Howse A, et all, 1983).





Outcrops of felsic rocks of the intrusive St. Lawrence batholith were observed at the AGS Site but only metasediments were intercepted in the investigation boreholes. The St Lawrence batholith is comprised of leucocratic granites (Scott, Oct. 2009). Figure 5 shows the bedrock geology which includes a 200 to 500 m wide belt of Plutonic Felsic rock consisting mainly of rhyolite of the St. Lawrence batholith, trending northwest through Gerbes Nest Pond and flanked by siliciclastic marine shale or meta-sediments of the Burin Group.

Geological cross section along NE-SW direction is presented in Figure 6. The fluorite veins at the AGS Site are hosted in meta-sediments and are genetically and spatially associated with the rhyolite sills which form part of the St. Lawrence batholith (refer to Figure 6) As shown in Figure 6, the mineralized zone, veins, are subvertical and tend to follow fault system.

St. Lawrence Fluorspar occurs as a hydrothermal deposit in the fissures in the fine-grained intrusives of granitic composition. The veins were reported to persist for many hundreds of metres with lengths ranging from less than 100 m to over 2,100 m and thicknesses of several metres, averaging 11 m (Harris A, et al. 1999).

5.4.3 Borehole Stratigraphy

Test pit log records (including test pit images) and gradation curves are provided in Appendix B.

Surficial soil conditions observed during excavation of test pits are summarized as follows:

- A layer of organic soil ranging in thickness from 0.5 to 1.0 m was encountered in all four test pits. The organic soil comprised of dark brown silty clay with rootlets, moss and/or peat. Test pit, TP-01, also contained some cobbles and sparse boulders.
- This was underlain by glacial outwash deposits (observed in TP-03 and TP-04) composed of varying proportions of sand and gravel (~30% to 90% gravel), with less than 10% silt. The unit thickness varied between 1 to 1.5 m.
- In test pits, TP-01 and TP-02, a compact till was encountered underlying the organic soil. The till layer is at least 1 m thick and contains 30% to 80% matrix (sand size or finer), and 80% to 20% clasts (greater than sand size).

Gradation analysis carried out on 4 representative samples generally confirmed the interpretation of the main stratigraphic units. Laboratory testing used the Unified Soils Classification System (USCS) to label the soil. The till material obtained from TP-01 and TP-02 labelled SM contained 32.6% to 40.4% gravel, 40.8% to 41.6% sand and 18.8% to 25.8% fines (silt/Clay). The till material obtained from TP-03 and TP-04, labelled GP-GM and GW respectively, contained 67.4% to 68.9% gravel, 23.8% to 29.6% sand and 1.5% to 8.5% fines (silt/Clay).

It should be noted that both TP-03 and TP-04 had a visually estimated larger rate of groundwater seepage into the pit than TP-01 and TP-02. This can be attributed to the coarser grained material exposed.

Borehole log records, including rock core photos and geophysical logs of selected exploration wells are provided in Appendix A.

The bedrock geology at the four new monitoring wells consisted of Grey-green, fresh, medium strong, Meta-sediment rock with weak chlorite alteration. The depth to top of bedrock ranges from 2.0 m to 6.8 m below ground surface.



At borehole BH14-01, large cobbles and boulders in the surficial material made drilling difficult and drilling was terminated after drilling 20 centimeters (cm) into bedrock. Bedrock was observed to contain numerous fractures within the first 2 m with fractures becoming less frequent with depth. The Rock Quality Designation (RQD) presented in the borehole field logs is a quantitative index of the rock quality with 100% RQD representing the highest quality (little to no fractures). The RQD values for the first 1.5 metre run in boreholes BH14-02, BH14-03, and BH14-04 are 50%, 77%, and 88%, respectively.

The geophysical log results for PGS-93b and PGS-124 are provided on the borehole records in Appendix A. The logs generally confirmed the stratigraphy and identified depth of large fractures along with fracture frequency. There significant rock fractures effect on the caliper and televiwer log response at 6.06 and 7 metres below surface and in the very near surface in borehole PGS-93b. Similarly, log shows significant rock fractures in borehole PGS-124, from 5.6 to 13.6 metres below surface.

5.4.4 Hydraulic Response Testing

This section provides a summary of the shallow overburden and bedrock hydraulic conductivity in the area of the AGS mine. These hydraulic conductivities are from 8 single well response tests and also from 4 grain size analysis which were completed that were also used to determine the hydraulic conductivity via the Hazen method.

The hydraulic parameter used to characterize groundwater flow through soil or rock is hydraulic conductivity. Hydraulic conductivity (K) describes the ease with which groundwater can move through pore spaces or fractures. Localized estimates of these parameters may be obtained through the analysis of in-situ hydraulic response tests, or slug tests, of groundwater monitoring wells.

In-situ rising and falling head tests were completed at each monitoring well to estimate the hydraulic conductivity of screened units at the site. In some cases multiple (confirmatory) tests were performed. The hydraulic testing involved establishing a static water level and then instantaneously removing or adding a known volume (a “slug”) to the well to observe the water level response over time. Recovering water levels were measured using data loggers set to record pressure at a 0.5 or 10 second time interval. In addition, water levels were manually measured to determine the end of the test; afterwards the data logger was removed and the data uploaded to a computer. Golder conducted slug testing on the four monitoring wells installed in October 2014 and in two existing exploration boreholes. The hydraulic response data was processed in the software package Aqtesolv Pro (HydroSOLV Inc., 2014) and interpreted using the Hvorslev Solution.

The pumping test was conducted for the two exploration holes PGS-93b and PGS-124. Short-term pumping tests were evaluated using the Thiem (1906) solution for steady-state flow to a well, which is a high-level hydrogeological method used to provide preliminary quantitative characterization. To account for uncertainties in the length of the borehole that contributes flow (b) and the radius of influence from pumping (R), these parameters were varied in a sensitivity analysis. Corrections for borehole inclination were also used to test the sensitivity of the results. Estimates of hydraulic conductivity were corrected for input parameters and associated estimates of K for PGS-93b and PGS-124 are presented in Table 3.



Table 3: Input Parameters and Hydraulic Conductivity Estimates

Parameter	Borehole PGS-93b	Borehole PGS-124
Flow Rate (Q), in m ³ /s	3.3*10 ⁻⁵	1.5*10 ⁻⁴
Constant Head Drawdown (s), in m	0.93	4.8
Radius of Well (R _w), in m	0.03785	0.03785
Borehole Length Contributing Flow (b), in m	10 – 20	10 – 20
Radius of Influence (R), in m	1 – 100	1 – 100
Hydraulic Conductivity (K), in m/s	8*10 ⁻⁷ – 4*10 ⁻⁶	7*10 ⁻⁷ – 4*10 ⁻⁶

After cessation of airlifting / pumping, there were several occasions where water was heard to be entering the borehole from above, possibly at the base of the surface casing. If this is the case, and water was recharging the borehole from the bedrock / overburden interface, the above hydraulic conductivity estimates would be invalid.

The core logging and geophysics records shown in Appendix A, indicate that the permeability of the bedrock is primarily related to open, near surface, bedding/joint partings within the rock. Therefore, the hydraulic conductivity values determined during slug tests are considered to primarily reflect a secondary permeability along the open bedding/joint partings.

Table 4 summarizes the hydraulic conductivities estimated from the results of the rising and falling head tests, the pumping test of the two exploration holes. Table 5 summarizes the Hazen method hydraulic conductivities estimated from the results of the grain size analysis. The complete pumping test and rising head test results can be found in Appendix E.

Table 4: Hydraulic Conductivity Estimates

Borehole ID	Screened Material	Single well response test Estimated Hydraulic Conductivity (m/s)	Pumping test Estimated Hydraulic Conductivity (m/s)
MW14-01a	Gravel and cobbles	2 x 10 ⁻⁵	-
MW14-02a	Bedrock	2 x 10 ⁻⁵	-
MW14-03a	Bedrock	5 x 10 ⁻⁵	-
MW14-04a	Bedrock	6 x 10 ⁻⁹	-
PGS-93b	Bedrock	-	8 x 10 ⁻⁷ to 4 x 10 ⁻⁶
PGS-124	Bedrock	-	7 x 10 ⁻⁷ to 4 x 10 ⁻⁸



Table 5: Hydraulic Conductivity Estimates based upon Hazen Method

Borehole ID	Screened Material	Hazen Method Estimated Hydraulic Conductivity (m/s)
MW14-01b	SAND & GRAVEL; some silt (SM)	3×10^{-6}
MW14-02b	Gravelly; silty SAND (SM)	2×10^{-7}
MW14-03b	Sandy GRAVEL; trace silt (GP-GM)	2×10^{-4}
MW14-04b	Sandy GRAVEL; trace silt (GW)	6×10^{-3}

5.4.5 Groundwater Elevations

Top of standpipe at each groundwater monitoring well location were surveyed and ground surface elevation calculated. Water levels in each monitoring well were recorded on November 1, 2014 after well installation and well development.

The reference and ground surface elevations of the monitoring wells are listed in Table 9. These elevations were used, along with depths to water measured by Golder, to calculate groundwater elevations.

Table 6: Groundwater Elevations

Monitoring Well ID	Top of Pipe Elevation (m asl)	Ground Surface Elevation (m asl)	Sample Date (dd/mm/yy)	Water Level (m bgs)	Groundwater Elevation (m asl)
MW14-1A	113.534	112.924	1/11/14	0.28	112.644
MW14-1B	113.918	112.768	1/11/14	0.41	112.358
MW14-2A	111.874	111.074	1/11/14	2.90	108.174
MW14-2B	111.976	110.726	1/11/14	0.74	109.986
MW14-3A	119.554	118.564	1/11/14	0.06	118.504
MW14-3B	119.554	118.304	1/11/14	0.14	118.164
MW14-4A	94.857	93.887	1/11/14	0.49	93.397
MW14-4B	94.915	93.515	1/11/14	0.03	93.485
PGS-93b	123.190	122.80	1/11/14	3.43	119.761
PGS-124	123.347	122.567	1/11/14	1.76	120.807

Note:
m asl = metres above sea level



m btop = metres below top of pipe

Groundwater levels in monitoring wells were observed to be near ground surface and groundwater levels of the ponds likely represent groundwater levels to a certain extent.

5.4.6 Groundwater Flow Directions

Insufficient data were collected to determine the deep ground water flow directions. The working assumption is that shallow bedrock flow directions are same as surface water flows (Figure 7).

5.4.7 Surface Water Flow Monitoring

Limited surface water flow monitoring was conducted at a total of 3 locations as described in Section 4 and shown on Figure 1. The instantaneous flow measurements were compiled to provide a baseline characterization of the stream flows at the AGS Site.

Stream flow survey data is contained in Appendix H which includes discharge estimates at five transects locations. Table 7 presents field measured water level at staff gauge and flow at the monitoring stations, during the October 31, 2014 monitoring period.

Table 7: Measured Water Level and Stream flow

Station	Staff Gauge (m)	Flow (L/s)
WQ STA-1	0.44	30
WQ STA-3	0.38	77
WQ STA-9	0.32	3

Note: 1. Water Flows based on October 31, 2014, survey.

Monitoring locations WQ STA-1, WQ STA-3 and WQ STA-9 are all located downstream of a lake or water body. A lake/water body can cause a decrease (attenuation) in flow from upstream to downstream depending on the available storage within the water body; therefore, the flows measured at WQ STA-1, WQ STA-3 and WQ STA-9 may be influenced by the upstream lakes.

5.4.8 Shallow groundwater-surface water interaction

The majority of the bedrock within the study area contains little if any primary permeability. In crystalline rock, the primary porosity may be as low as 0.05% while a typical sand aquifer usually has a porosity of 30% or greater (Novakowski, 2000). Therefore, bedrock with secondary permeability through fracture systems generally predominates. Water levels shown in Table 1 indicate a downward gradient from the shallow groundwater system (overburden) to the fractured bedrock groundwater system.

Groundwater levels are fairly close to ground surface in both the bedrock and overburden (refer to Table 1). The shallow aquifer system will be largely controlled by surface runoff and local recharge.



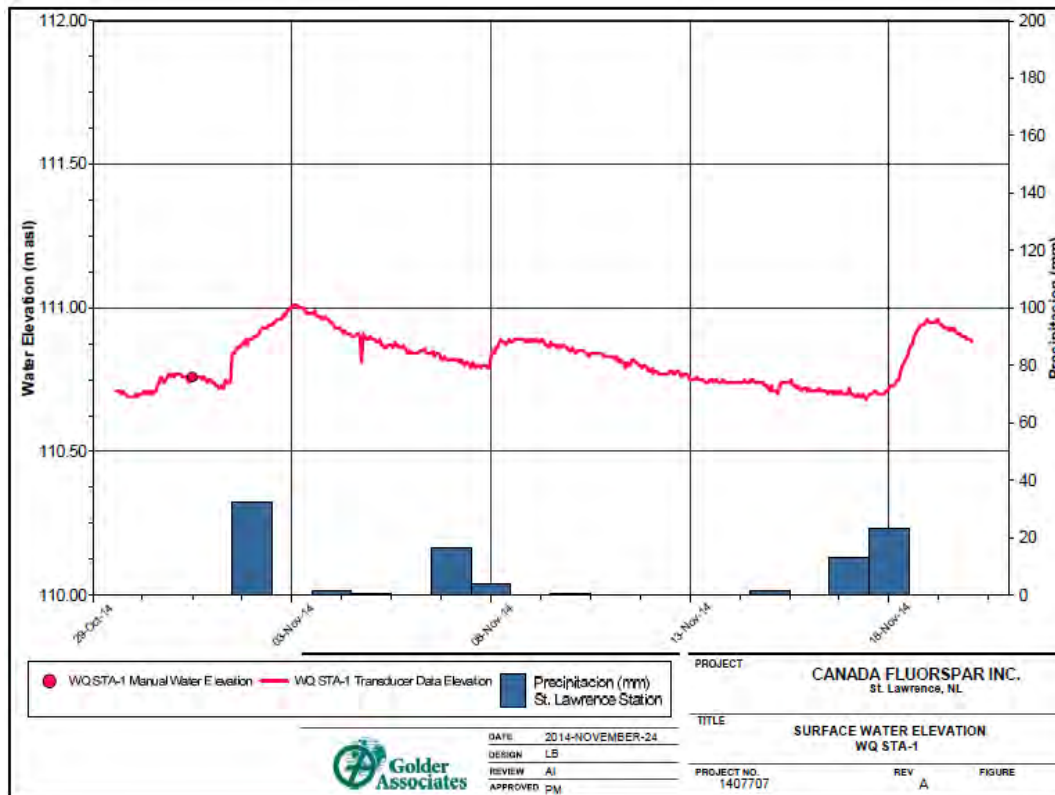
Hydrographs for the groundwater monitoring wells (MW14-01A, MW14-02A, MW14-03A, and MW14-04A) and surface water stations (WQ STA-7, WQ STA-3, and WQ STA-9) are presented in Appendix G for the period of November 1 to 20, 2014. Data loggers were re-installed in their corresponding wells on November 21, 2014, in continuation with monitoring program. The graph also plots daily precipitation, using data provided by the Environment Canada meteorological station.

With reference to groundwater hydrograph figures in Appendix G, the following is noted:

- Groundwater fluctuations generally reflect climatic conditions suggesting hydraulic connection between systems. Three rain events on November 2, 7, and 17 had a direct correlation with peaks in the groundwater system. Further evidence of the hydraulic connectivity between shallow bedrock aquifer and highly permeable overburden aquifer system is likely the result of the abundant fractures from the shallow bedrock observed within the top 10 m of the geophysics logs (refer to Appendix A). In order to quantify the magnitude of the hydraulic gradient on the bedrock groundwater system, further testing is necessary through pump test.
- The highest influence occurred in monitoring well PGS-124 with a groundwater elevation spike of about 0.75 m and lowest groundwater elevation spike in MW-02A. Topography may be driving groundwater flows in which groundwater flows from higher-elevation recharge to lower-elevation discharge areas resulting in higher groundwater spikes following a storm event.
- The exception of MW14-02A, all hydrographs for monitoring wells show that there is a slight downward groundwater trend during non-rain events.
- Large rhythmic fluctuations was observed in the hydrograph fro well PGS-93b (Figure G-2). These groundwater fluctuations are not observed in any of the other monitoring wells and are likely due to a malfunction of the data logger.
- Based on the observed groundwater elevations at the monitoring wells located near ponds where water elevation in the pond is near that of the groundwater, the pond appears to provide a moderate hydraulic buffer that can influence local groundwater levels.

With reference to surface water hydrograph figures in Appendix G, the following is noted:

- Surface water level fluctuations are reflective of climatic conditions.
- Water levels at WQ STA-1, WQ STA-3 and WQ STA-9 showed similar responses to precipitation events. Following a 32.7 mm rainfall event on November 2, 2014 water levels at STA-1, STA-3, and STA-9, increased by 0.30m, 0.30m, and 0.24m following the start of the rain event, peaking at elevations 111.01 masl, 108.25 masl, and 116.18 masl, respectively. A smaller peak occurred on November 8, 2014, following a rainfall of 16.7 mm, resulting in water levels at STA-1, STA-3, and STA-9 peaking at 110.89 masl, 108.12 masl, and 116.11 masl. A large peak occurred on November 18, 2014, following a two day rainfall of 23.5 mm, resulting in water levels at STA-1, STA-3, and STA-9 peaking at 110.96 masl, 108.14 masl, and 116.15 masl.
- An example from Appendix G illustrating this response is shown below:



- Following precipitation events, water levels at STA-1 returned to an elevation of approximately 110.7 masl. Likewise, water levels at STA-3 typically returned to an elevation of approximately 108 masl. Water levels at STA-09 returned to an elevation of approximately 116 masl.
- 16.7 mm rainfall event on November 7 and a 23.5 mm rainfall event on November 18
- Surface water level fluctuations mirrors that of the groundwater indicating that groundwater flow systems in the study area are closely tied to surface water systems.
- The close connection between surface water and groundwater, with lack of substantial storage, make groundwater levels very sensitive to dry periods.

5.4.9 Groundwater Quality

Water quality results are provided below and compared to Summary of Guidelines for Canadian Drinking Water Quality (SGCDWQ). Under Aesthetic Objectives (AO), water quality results showed elevated concentrations of colour, aluminium, iron and total manganese in deep bedrock wells. Shallow wells screened in the overburden were not sampled.

Groundwater sample collected from MW14-04A has a pH value of 6.22 which is below the guideline for drinking water of 6.5-8.5 pH units (Health Canada, 2014).

Field measurements were collected at the time the sample was taken with a pH/temperature metre and a conductivity/temperature metre. The results are shown in Table 8 and compared to laboratory results.



Table 8: Groundwater Quality Field Measurements

Station	Field Measurements		Laboratory Results	
	pH	Conductivity (mS)	pH	Conductivity (mS)
MW14-01A	7.38	0.10	7.36	0.12
MW14-02A	7.69	0.17	7.63	0.18
MW14-03A	6.65	0.07	6.51	0.08
MW14-04A	6.22	0.22	6.22	0.25
PGS-93b	8.05	0.16	8.02	0.18
PGS-124	6.50	0.12	6.80	0.13

The physical quality of the water with regards to colour exceeded (SGCDWQ) acceptable concentrations of 15 true colour units (TCU) in MW14-03A and PGS-124. Colour value recorded for MW14-03A and PGS-124 is 160 TCU and 95 TCU, respectively.

Samples from all monitoring wells exceeded the 0.3 mg/L drinking water guideline for iron. Bedrock wells MW14-02A, MW14-03A and MW14-04A, open in the Meta-sediment rock, showed elevated iron concentrations above SGCDWQ, ranging from 0.49 to 15.0 milligrams per liter (mg/L). Deep exploration bedrock boreholes PGS-93a and PGS-124 showed elevated concentrations of iron of 0.58 mg/L and 39 mg/L, respectively. Iron concentrations are primarily an aesthetic objective and do not present a health concern unless in excessive concentrations.

With the exception of MW14-01A and PGS-93b, all monitoring wells exceeded the 0.05 mg/L drinking water guideline for manganese. Elevated manganese concentrations range from 0.12 mg/L to 1.1 mg/L. Manganese concentrations are primarily an aesthetic objective and do not present a health concern unless in excessive concentrations.

Samples from all monitoring wells exceeded the 0.1 mg/L drinking water guideline for aluminium. Elevated aluminum concentrations range from 0.18 mg/L to 39.0 mg/L.

5.4.10 Surface water Quality

Water quality results are provided below and compared to Summary of Guidelines for Canadian Drinking Water Quality (SGCDWQ). Under Aesthetic Objectives (AO), water quality results showed elevated concentrations of colour, aluminium, iron and total manganese.

Field measurements were collected at the time the sample was taken with a pH/temperature metre and a conductivity/temperature metre. The results are shown in Table 9 and compared to laboratory results.



Table 9: Surface Water Quality Field Measurements

Station	Field Measurements		Laboratory Results	
	pH	Conductivity (mS)	pH	Conductivity (mS)
WS-2	6.00	0.10	7.29	0.099
WS-5	6.23	0.13	7.28	0.110
WS-10	6.11	0.06	6.50	0.055
WQ STA-1	5.92	0.04	5.88	0.056
WQ STA-2	5.95	0.04	6.15	0.054
WQ STA-3	4.69	0.04	5.65	0.092
WQ STA-4	4.76	0.02	5.65	0.052
WQ STA-5	5.53	0.01	6.03	0.039
WQ STA-6	5.68	0.01	6.02	0.040
WQ STA-7	5.94	0.04	5.92	0.054
WQ STA-8	3.94	0.04	4.98	0.053
WQ STA-9	3.70	0.04	5.16	0.054

Note: Highlighted results were collected as part of the Phase 1 Hydrogeological Investigation. The remainder, collected at the same time for the concurrent surface water program, are also presented for completeness.

Nine of the thirteen surface water samples collected had pH values below the guideline for drinking water of 6.5-8.5 pH units (Health Canada, 2014). Low pH values are typical of surface waters in Newfoundland and Labrador, due to large amounts of organic materials produced by bogs, swamps and boreal forest (Amec 2013). Low pH values can also be attributed to granitic rocks that tend to make groundwater slightly acidic and the lack of limestone to buffer the acidity.

The physical quality of the water with regards to colour exceeded (SGCDWQ) acceptable concentrations of 15 TCU in all surface water samples. Concentration values ranged from 31 to 160 TCU. High colour values are typical of surface waters near wetlands in Newfoundland. High levels of colour to surface runoff is contributed by wetland drainage; whereas exposed bedrock in a basin or less organic soils contribute little to no colour.

Surface samples from WQ STA-1 and WQ STA-7 out of the six WQ stations in the phase 1 study have iron concentrations of exceeded the 0.3 mg/L drinking water guideline for iron ranging from 0.52 to 0.66 mg/L. With the exception of W2, surface samples collected outside the phase 1 program showed elevated iron concentrations above SGCDWQ, ranging from 0.13 to 0.62 mg/L.

Only two surface samples from outside the phase 1 program, W5 and W10, showed elevated manganese concentrations of 0.64 mg/L and 0.75 mg/L , above the 0.05 mg/L drinking water guideline.

All surface water samples exceeded the 0.1 mg/L drinking water guideline for aluminium. The results for aluminum ranged from 0.17 mg/L to 0.61 mg/L for samples collected within the phase 1 program. The remainder of the samples showed aluminum concentrations ranging from 0.13 mg/L to 0.43 mg/L.



6.0 CLOSURE

The report presented the factual results of the Phase 1 hydrogeological investigation. We trust that this report meets your requirements. If you have any questions, please do not hesitate to contact the undersigned.



Report Signature Page

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7.0 REFERENCES

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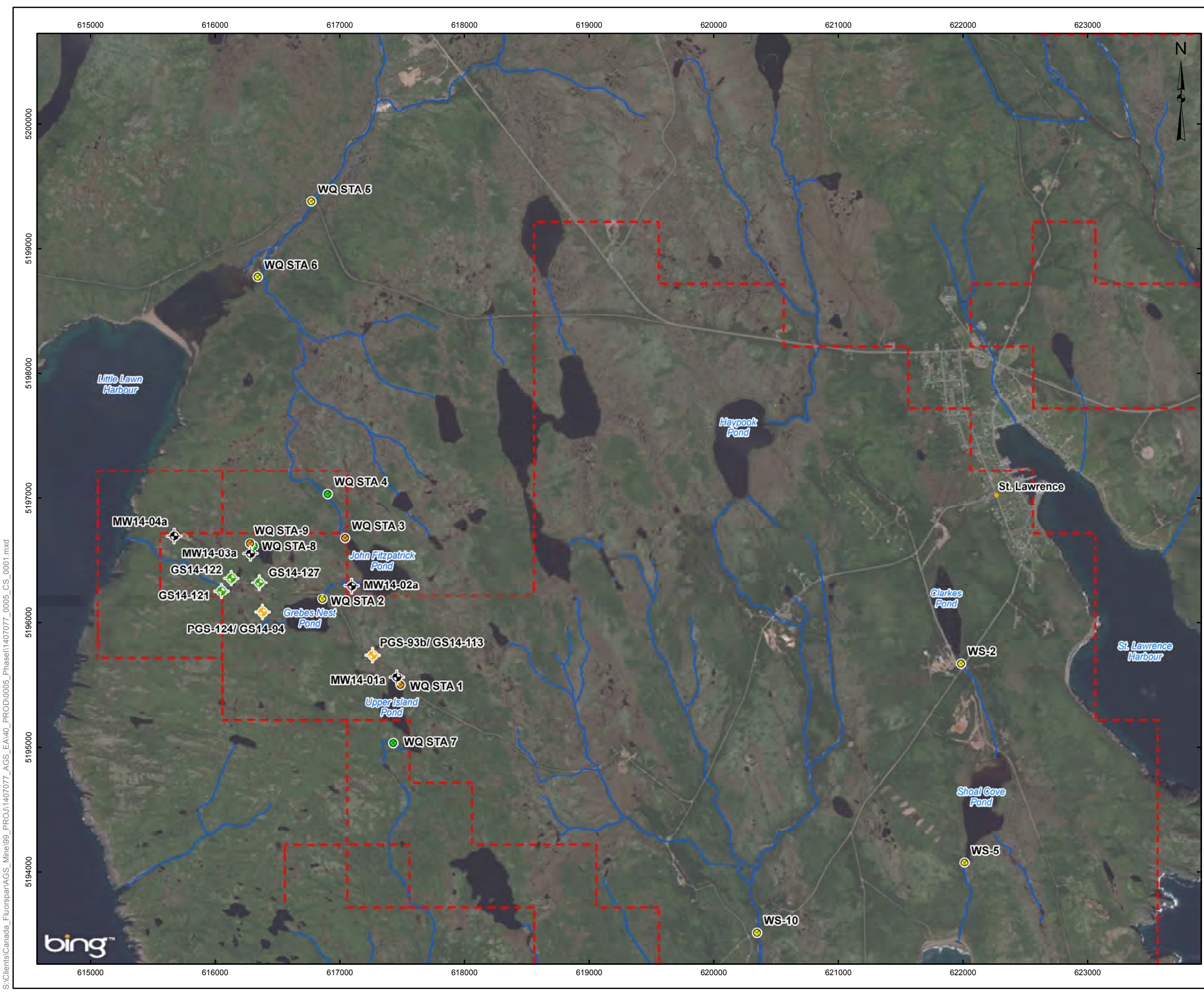
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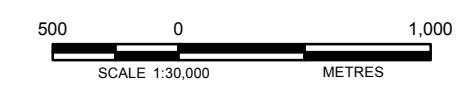
FIGURES



- LEGEND**
- Town
 - Sampling Locations**
 - Surface Water Gauge
 - Water Quality
 - Water Quality and Aquatic
 - ⊕ Vertical Borehole, Test Pit and Monitoring Well
 - ◆ Exploration Hole for Groundwater Sampling and Geophysics Hole
 - ◆ Geophysics Hole
 - - - Mineral Licenses Existing
 - River/Stream



REFERENCE
 Surface Plan provided by the Client (August 2014)
 Projection: Transverse Mercator Datum: NAD 83 Coordinate System: UTM Zone 21N



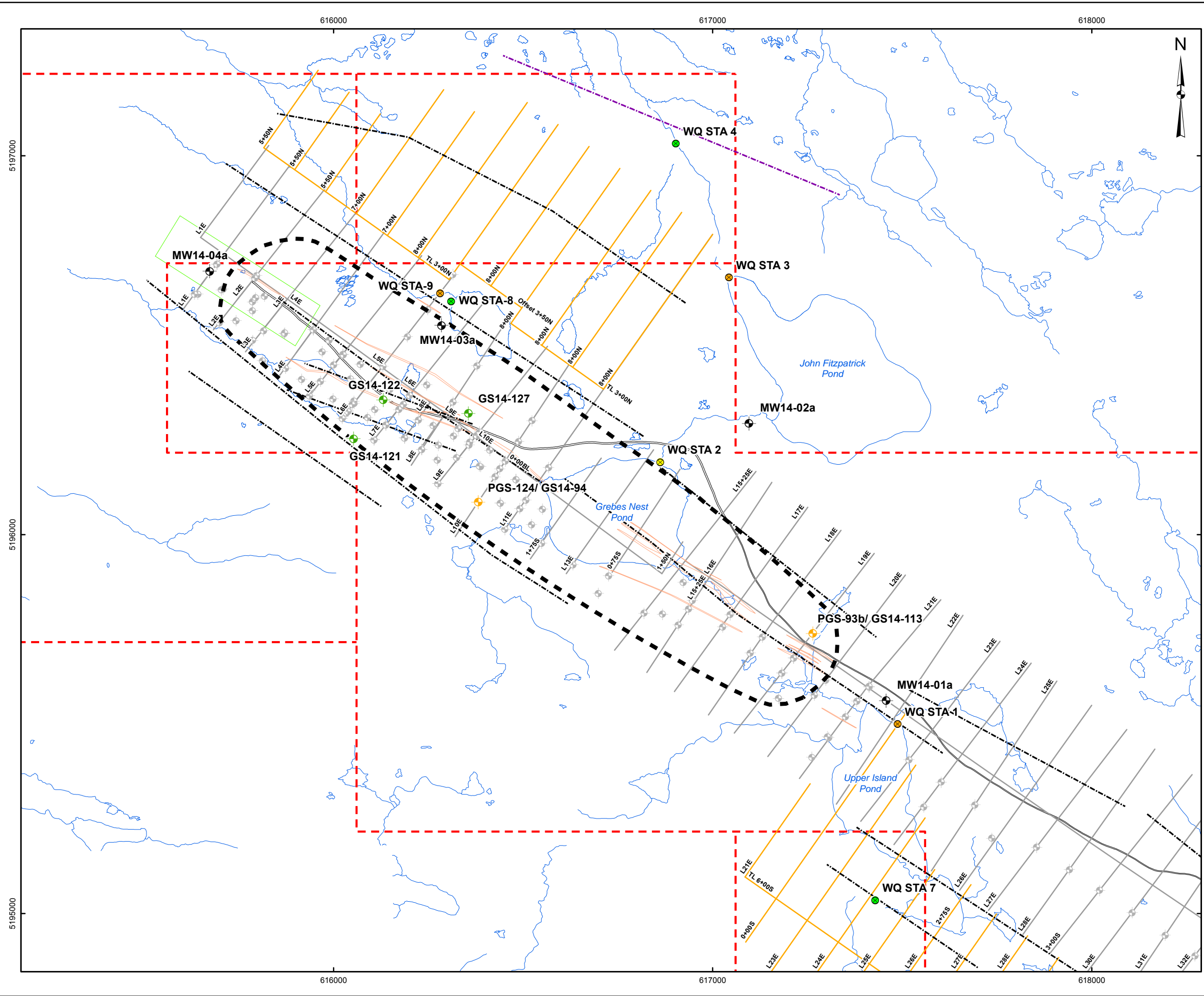
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	GIS	SO 10 Dec. 2014	
	CHECK	PM 10 Dec. 2014	
	REVIEW	PM 10 Dec. 2014	

FIGURE: 1

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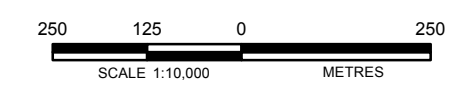
LEGEND

Sampling Locations

- Surface Water Gauge
- Water Quality
- Water Quality and Aquatic
- ⊕ Vertical Borehole, Test Pit and Monitoring Well
- ⊕ Exploration Hole for Groundwater Sampling and Geophysics Hole
- ⊕ Geophysics Hole
- ⊕ Drillhole Other
- AGS 2013 Grid Extension
- - - AGS Magnetic Linears Targets 2014
- GN Field Grid
- GN Veins Surface
- Mine Cove Vein Linear
- Mine Lease Boundary
- - - Mineral Licenses Existing
- Road
- Water Feature
- ▭ Assumed Surface Mine Footprint

REFERENCE

Surface Plan provided by the Client (August 2014)
 Projection: Transverse Mercator Datum: NAD 83 Coordinate System: UTM Zone 21N




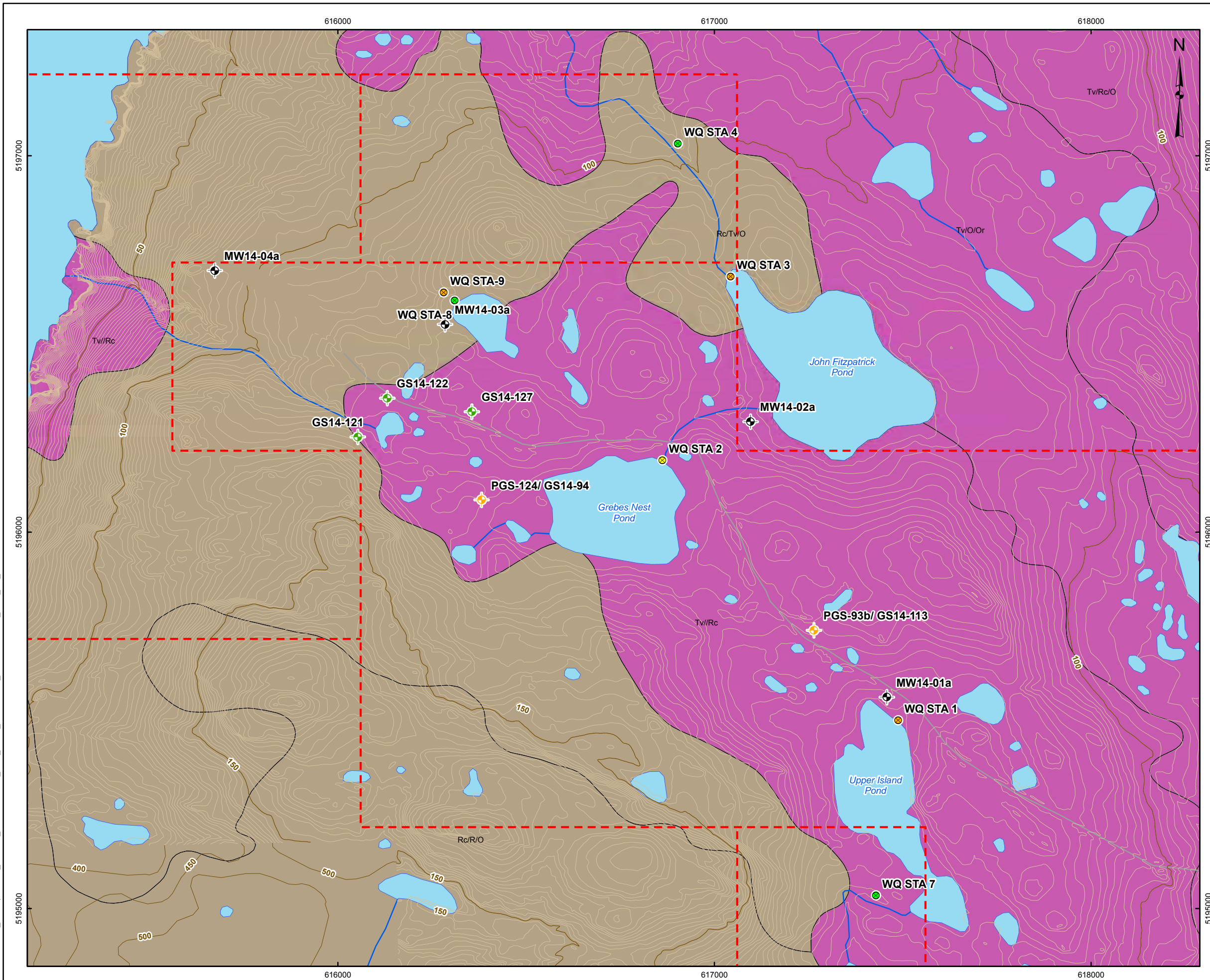
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FIGURE: 2

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LEGEND

Sampling Locations

- Surface Water Gauge
- Water Quality
- Water Quality and Aquatic
- ⊕ Vertical Borehole, Test Pit and Monitoring Well
- ⊕ Exploration Hole for Groundwater Sampling and Geophysics Hole
- ⊕ Geophysics Hole

Surficial Geology

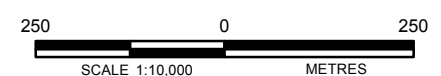
- RC, Rock Concealed
- TV, Till Veneer

Other Features:

- - - Mineral Licenses Existing
- Roads
- Contour - 50m Interval
- Contour - 2m Interval
- River/Stream
- Waterbody

REFERENCE

Basedata - CanVec 2009, Government of Newfoundland Geoscience Atlas (<http://geoatlas.gov.nl.ca/Default.htm>)
 Contours (2m Interval) provided by the CIF
 (Filename: St.Lawrence property map_v14.dwg)
 Projection: Transverse Mercator Datum: NAD 83 Coordinate System: UTM Zone 21N




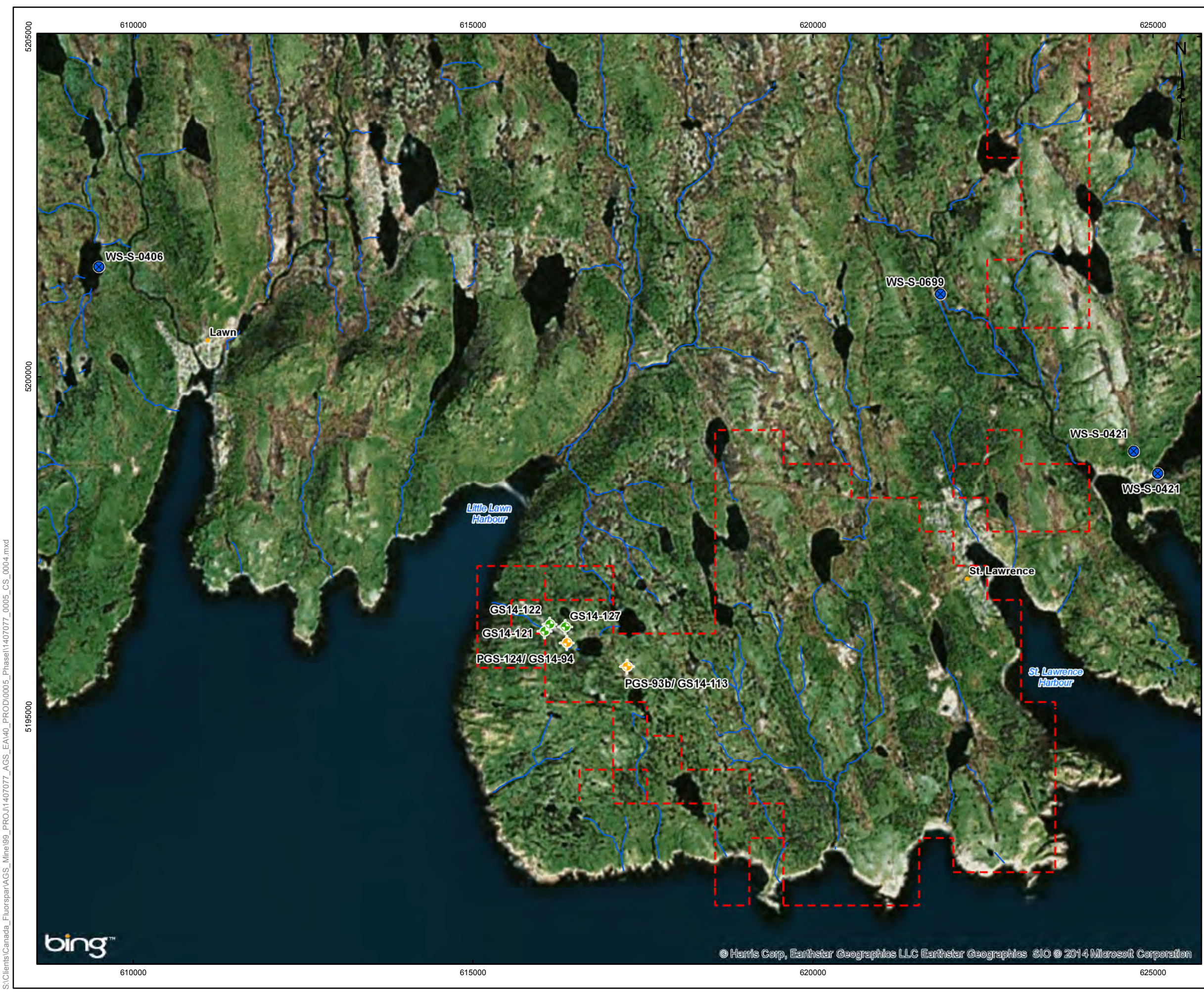
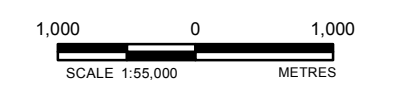
PROJECT	AGS PROPERTY NEWFOUNDLAND		
TITLE	SURFICIAL GEOLOGY		
 Mississauga, Ontario	PROJECT NO.	1407707	SCALE AS SHOWN
	DESIGN	SO 2 Sep. 2014	REV. 0.0
	GIS	SO 10 Dec. 2014	
	CHECK	PM 10 Dec. 2014	
	REVIEW	PM 10 Dec. 2014	


FIGURE: 3



- LEGEND**
- Town
 - ⊗ Public Water Intakes/Wellheads
 - ⊗ Exploration Hole for Groundwater Sampling and Geophysics Hole
 - ⊗ Geophysics Hole
 - - Mineral Licenses Existing
 - River/Stream

REFERENCE
 Surface Plan provided by the Client (August 2014)
 Projection: Transverse Mercator Datum: NAD 83 Coordinate System: UTM Zone 21N



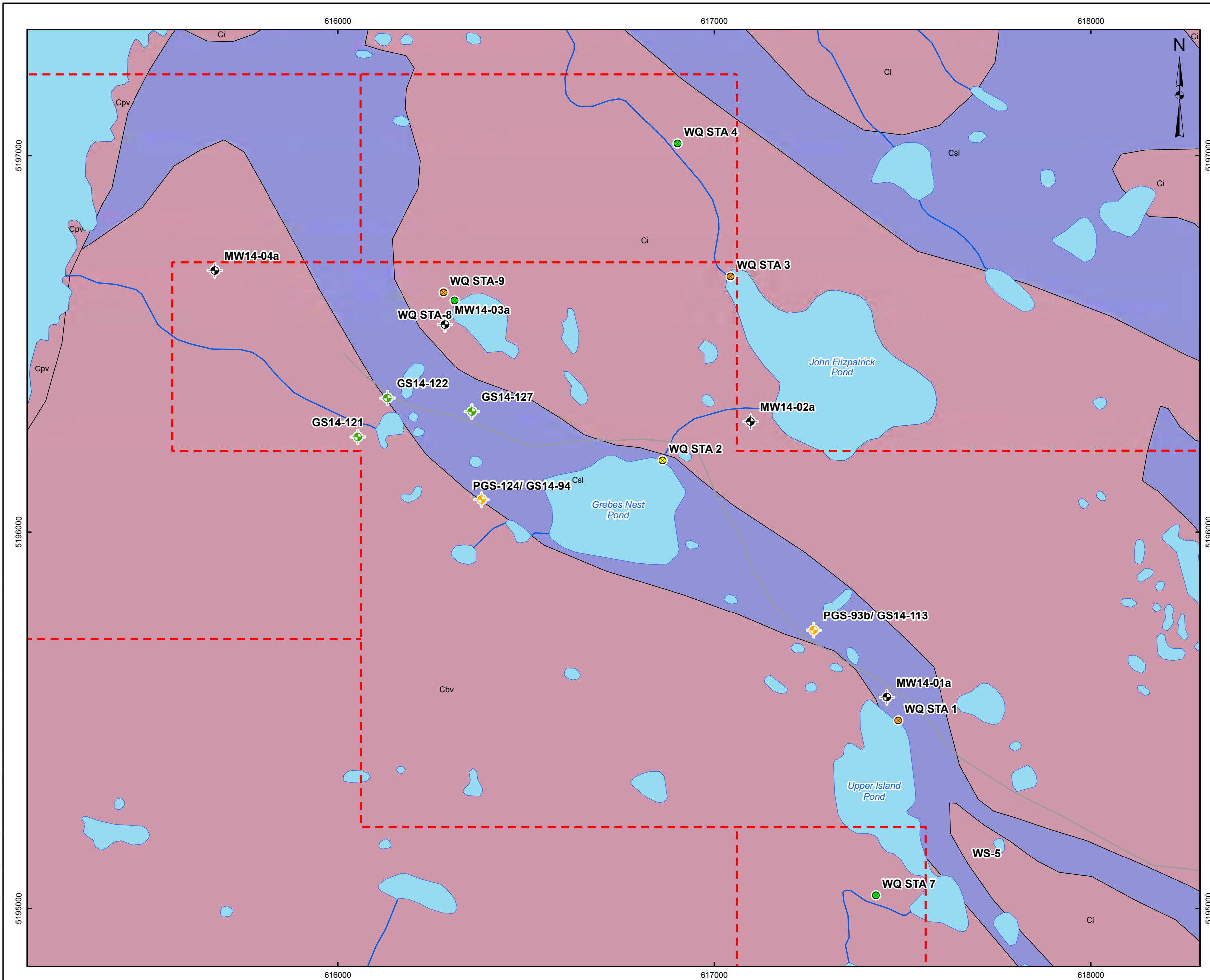
PROJECT	AGS PROPERTY NEWFOUNDLAND		
TITLE	MUNICIPAL WATER SOURCES		
 Mississauga, Ontario	PROJECT NO.	1407707	SCALE AS SHOWN
	DESIGN	SO 2 Sep. 2014	REV. 0.0
	GIS	SO 10 Dec. 2014	FIGURE: 4
	CHECK	PM 10 Dec. 2014	
	REVIEW	PM 10 Dec. 2014	

S:\Clients\Canada_Florispar\AGS_Mime\99_PROJ\1407077_AGS_EA\40_PROD\0005_Phase\1407077_0005_CS_0004.mxd



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LEGEND

Sampling Locations

- Surface Water Gauge
- Water Quality
- Water Quality and Aquatic
- Vertical Borehole, Test Pit and Monitoring Well
- Exploration Hole for Groundwater Sampling and Geophysics Hole
- Geophysics Hole

Mineral Licenses Existing

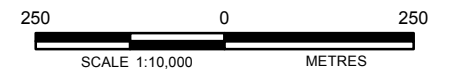
- Roads
- River/Stream
- Waterbody


Bedrock Geology

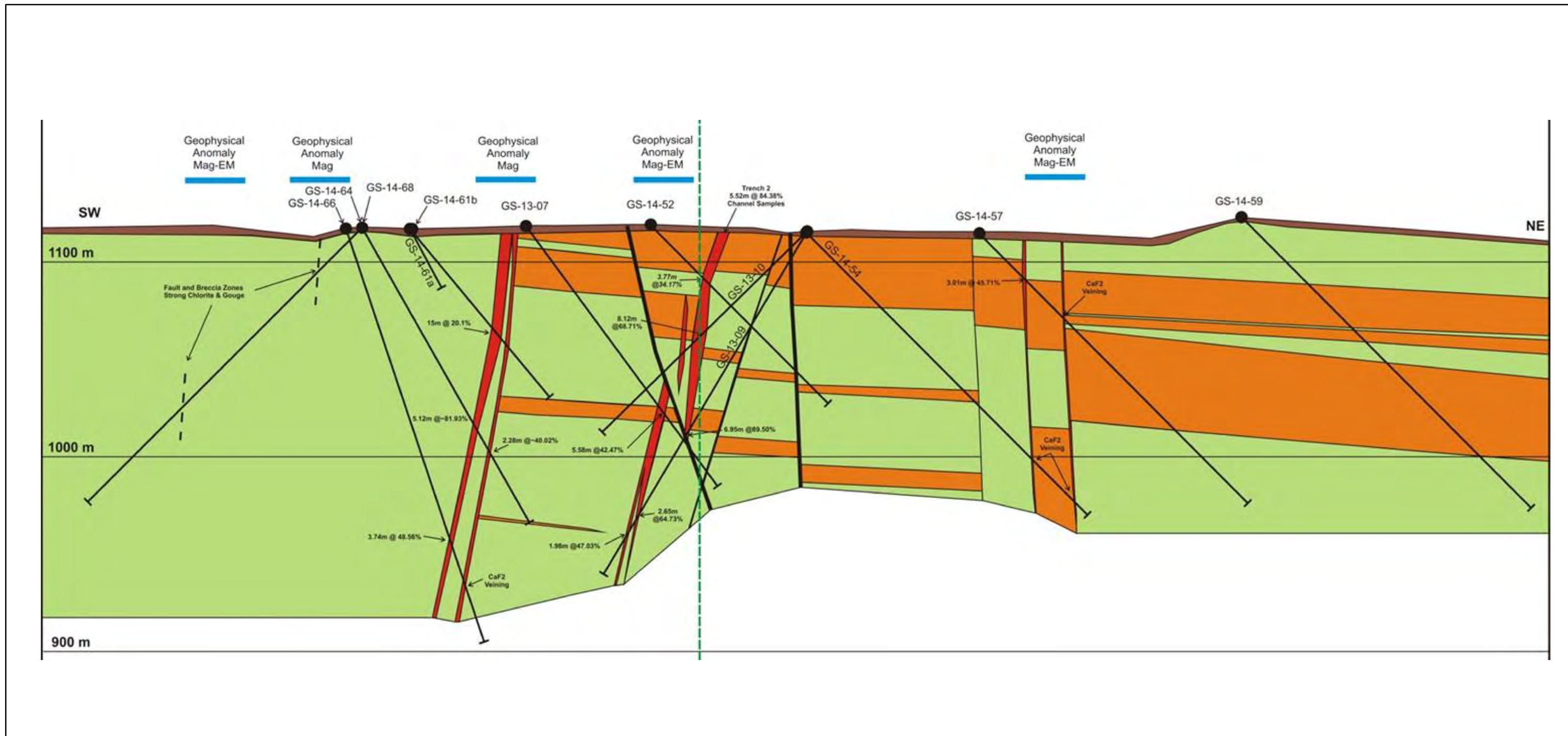
- Plutonic felsic (includes rhyolitic rock of the St. Lawrence batholith)
- Siliciclastic marine shale (includes meta-sediments)

REFERENCE

Basedata - CanVec 2009, Government of Newfoundland Geoscience Atlas (<http://geoatlas.gov.nl.ca/Default.htm>)
 Projection: Transverse Mercator Datum: NAD 83 Coordinate System: UTM Zone 21N



PROJECT	AGS PROPERTY NEWFOUNDLAND			
TITLE	BEDROCK GEOLOGY			
 Golder Associates Mississauga, Ontario	PROJECT NO.	1407707	SCALE AS SHOWN	REV. 0.0
	DESIGN	SO	2 Sep. 2014	FIGURE: 5
	GIS	SO	10 Dec. 2014	
	CHECK	PM	10 Dec. 2014	
REVIEW	PM	10 Dec. 2014		



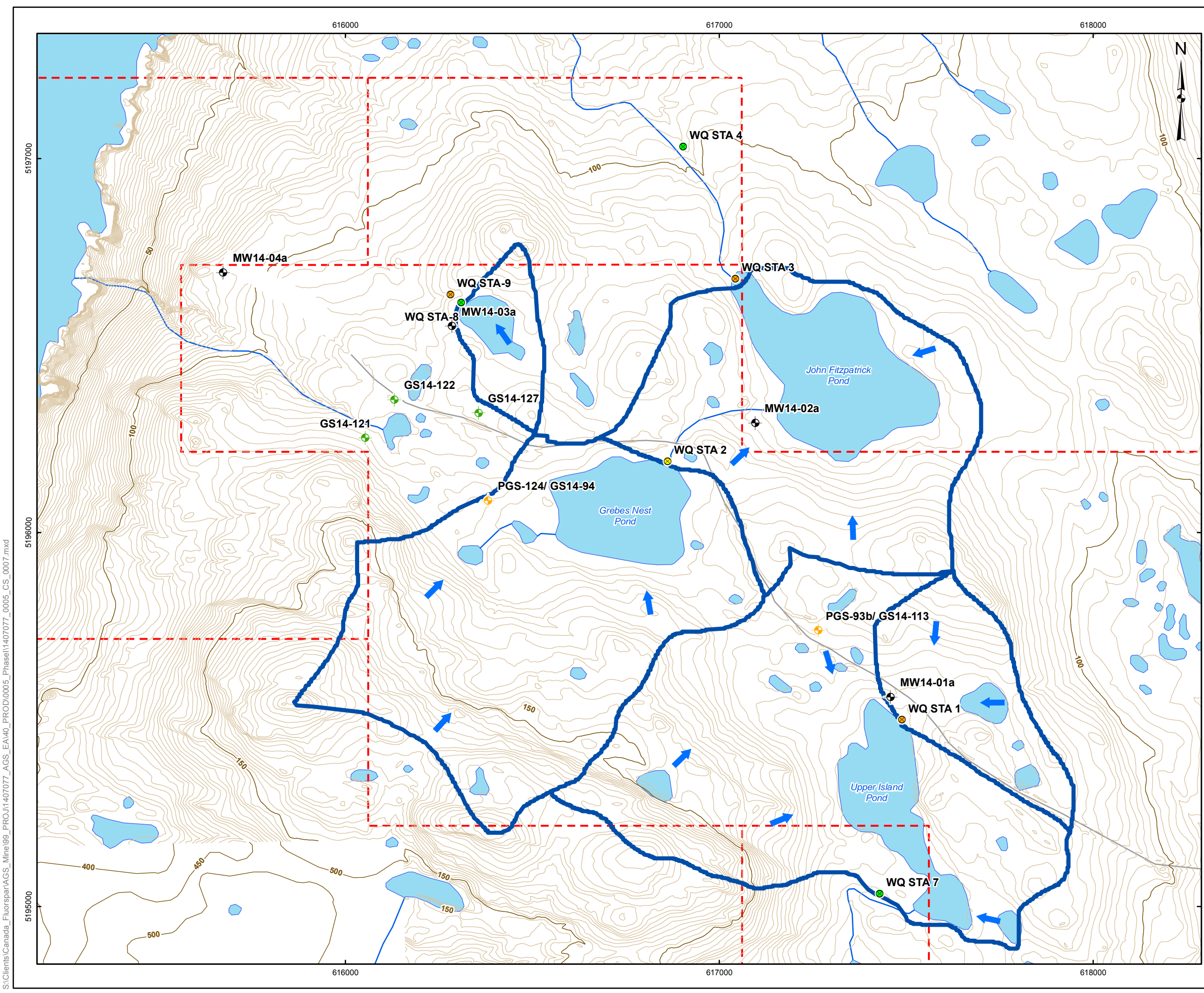
LEGEND

- Diamond Drill Hole (Complete)
- Diamond Drill Hole (Planned)
- Geophysical Anomaly
- Rhyolite Sills
- Fluorite Veins
- Meta-sediments
- Fault Zones

REFERENCE

Cross-section of line 6 received via email from CFI October 8, 2014

PROJECT	AGS PROPERTY NEW FOUNDLAND																						
TITLE	GEOLOGICAL CROSS-SECTION																						
<p style="font-size: 8px; margin-top: 5px;">Mississauga, Ontario</p>	<table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td colspan="2">PROJECT No. 1407707</td> <td>NOT TO SCALE</td> <td>REV. 0.0</td> </tr> <tr> <td>DESIGN</td> <td>SO</td> <td>26 Nov. 2014</td> <td></td> </tr> <tr> <td>GIS</td> <td>SO</td> <td>4 Dec. 2014</td> <td></td> </tr> <tr> <td>CHECK</td> <td>PM</td> <td>4 Dec. 2014</td> <td></td> </tr> <tr> <td>REVIEW</td> <td>PM</td> <td>4 Dec. 2014</td> <td></td> </tr> </table>	PROJECT No. 1407707		NOT TO SCALE	REV. 0.0	DESIGN	SO	26 Nov. 2014		GIS	SO	4 Dec. 2014		CHECK	PM	4 Dec. 2014		REVIEW	PM	4 Dec. 2014		FIGURE: 6	
PROJECT No. 1407707		NOT TO SCALE	REV. 0.0																				
DESIGN	SO	26 Nov. 2014																					
GIS	SO	4 Dec. 2014																					
CHECK	PM	4 Dec. 2014																					
REVIEW	PM	4 Dec. 2014																					



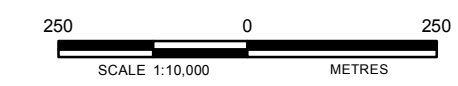
LEGEND


Sampling Locations

- Surface Water Gauge
- Water Quality
- Water Quality and Aquatic
- ⊕ Vertical Borehole, Test Pit and Monitoring Well
- ⊕ Exploration Hole for Groundwater Sampling and Geophysics Hole
- ⊕ Geophysics Hole
- ➔ Flow Direction
- - - Mineral Licenses Existing
- Roads
- Contour - 50m Interval
- Contour - 2m Interval
- River/Stream
- Waterbody
- ▭ Watershed Boundary

REFERENCE

Basedata - CanVec 2009, Government of Newfoundland Geoscience Atlas (<http://geoatlas.gov.nl.ca/Default.htm>)
 Contours (2m Interval) provided by the CIF
 (Filename: St.Lawrencece property map_v14.dwg)
 Projection: Transverse Mercator Datum: NAD 83 Coordinate System: UTM Zone 21N



PROJECT	AGS PROPERTY NEWFOUNDLAND		
TITLE	WATERSHED BOUNDARIES		
 Mississauga, Ontario	PROJECT NO. 1407707	SCALE AS SHOWN	REV. 0.0
	DESIGN SO 2 Sep. 2014		
	GIS SO 10 Dec. 2014		
	CHECK PM 10 Dec. 2014		
	REVIEW PM 10 Dec. 2014		

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APPENDIX A

Borehole Record; Rock Core Images; Geophysics Borehole Survey

FIELD DRILLHOLE LOG

Job No. 1407707 Job Name Canada Fluorspar Inc Phase I Date Oct 20/14 Drillhole No. BH14-01
 DH Location Elevation (Obtained From) Datum WGS-84
 Inclination 90° Azimuth Along Hole Total Length
 Type of Drilling Diamond Type of Rig Duralite 300 Flush water Feed
 Type of Core Barrel Snake Tube Bit Design Bit No.
 Drillhole Dia. NQ - 76mm Drillcore Dia. 60mm Casing Dia. 89mm
 Contractor Springdale Drilling Driller [Signature]
 Temperature ~8°C Weather overcast Engineer A. Ivanoff

- | | | | |
|---|------------------------------------|--------------------------------|---------------------|
| R.Q.D. - Rock Quality Designation
(% Core Run > 0.1m Long) | F.R. - Fracture (Undifferentiated) | B. - Bedding | P. - Polished |
| S.C.R. - Solid Core Recovery
(% Cylindrical) | S.A. - Sample | F.O. - Foliation / Schistosity | S. - Slickensided |
| T.C.R. - Total Core Recovery | C.A. - Casing | CL. - Cleavage | SM - Smooth |
| F.I. - Fracture Index (Fractures / ...) | W.L. - Water Level | SH. - Shear Plane / Zone | R. - Ridged / Rough |
| | B.C. - Broken Core | VN. - Vein | CO. - Contact |
| | | F. - Fault | J. - Joint |
| | | | ST. - Stepped |
| | | | PL. - Planar |
| | | | F.L. - Flexured |
| | | | UE. - Uneven |
| | | | W. - Wavy |
| | | | C. - Curved |

Date / Time Core Ø, Depth	Date / Time Casing Ø, Depth	Water Levels am & pm	Penetration Percent Flush Return	Time For Run, min	Rate (/ min)	Depth	Drilling Run No. & Length	RECOVERY				Core Quality	Fractures Per	DISCONTINUITIES			FORMATION	CORE DESCRIPTION DEPTH FROM : TO - Weathering ; Structure (Bedding Foliation, Jointing) Colour ; Grain Size & Texture ; Alteration State ; Cementation ; Rock Name ; Rock Formation		
								T.C.R.		S.C.R.				R.Q.D.		DIP ° W.R.T. Core Axis			Type & Surface Description	
								LENGTH	%	LENGTH	%			LENGTH	%					
	<u>Ground Surface</u>					0														
						1											<u>0-1m dark brown organic soil.</u>			
						2											<u>1 TO 6.8m.</u>			
						3											<u>Silty sand and gravel with varying percentages of cobbles and boulders.</u>			
						4											<u>from 4 to 6.8m cased through cobbles and boulders composed of metasediments and rhyolite (volcanics)</u>			
						5											<u>very unstable borehole wall.</u>			
						6											<u>overburden</u>			
						6.8m											<u>overburden</u>			
						7											<u>Bedrock from 6.8 to 7.0m.</u>			
																	<u>RQD = 100% SCR = 85% TCR = 100% } 20cm section.</u>			
																	<u>Rock Type Grey Metasediment fresh, medium strong rock.</u>			
																	<u>EOH 7.0m</u>			

SPECIAL NOTES / SKETCHES

CONSUMABLE MATERIALS USED

Monitoring Well Construction details found in Excel document.

RESULTS OF IN SITU TESTING

No.	TIME	DATE	DEPTHS	RESULTS

DEPTH - From to Dates TIME - Moving & Set-Up hrs.

Drilling hrs. Testing etc. hrs. Delayed Stand-by hrs. Productive hrs.



JOB No. 1407707
 DRILLHOLE No. BH 14-01
 DEPTH 0 TO 7m.

FIELD DRILLHOLE LOG

Job No. 1407707 Job Name Canada Fluorspar Inc. Phase I Date Oct 21, 2014 Drillhole No. BH14-02
 DH Location..... Elevation..... (Obtained From.....) Datum WGS 82
 Inclination..... 90 Azimuth..... Along Hole Total Length.....
 Type of Drilling Diamond Type of Rig Duralite 800 Flush water Feed 1.5m
 Type of Core Barrel single tube Bit Design..... Bit No.....
 Drillhole Dia. NQ - 76mm Drillcore Dia. 76mm Casing Dia. 89mm
 Contractor Springdale Drilling Driller.....
 Temperature 6 C. Weather overcast Engineer A. IVANOFF

R.Q.D. - Rock Quality Designation (% Core Run > 0.1m Long)
S.C.R. - Solid Core Recovery (% Cylindrical)
T.C.R. - Total Core Recovery
F.I. - Fracture Index (Fractures /)
F.R. - Fractures (Undifferentiated)
S.A. - Sample
C.A. - Casing
W.L. - Water Level
B.C. - Broken Core
B. - Bedding
F.O. - Foliation / Schistosity
CL. - Cleavage
SH. - Shear Plane / Zone
VN. - Vein
F. - Fault
P. - Polished
S. - Slickensided
SM - Smooth
R. - Ridged / Rough
ST. - Stepped
PL. - Planar
F.L. - Flexured
UE. - Uneven
W. - Wavy
C. - Curved

Date / Time Core Ø, Depth	Date / Time Casing Ø, Depth	Water Levels am & pm	Percent Flush Return	Penetration		Depth ()	Drilling Run No. & Length	RECOVERY				Core Quality		DISCONTINUITIES			CORE DESCRIPTION
				Time For Run, min.	Rate (/ min)			T.C.R. LENGTH	S.C.R. %	R.Q.D. LENGTH	Fractures Per 0.25	DIP ° W.R.T. Core Axis	Type & Surface Description	Formation	DEPTH FROM : TO - Weathering ; Structure (Bedding Foliation, Jointing) Colour ; Grain Size & Texture ; Alteration State ; Cementation ; Rock Name ; Rock Formation		
																%	%
						0-4.8m										Overburden	
						4.8-5.2										Lost core -> Damaged	
						5.23-5.75										BC	
						6.0m										JN, UN, RO, PC - 3mm silt.	
						7.07										JN, IR	
						8.0										HVN, IR, R, CC JN - crystals with	
						8.16										JN, IR, RO, PC grey with silt.	
						4.8											
						5.2	5	①					10		PL		
						6.0	6	②	1.5 / 1.5	100%	1.5 / 1.5	47%	1.5 / 1.5	50%	60m	14°	
						6.7											
						7.0	7	③	1.5 / 1.5	100%	1.5 / 1.5	69%	1.5 / 1.5	68%	1-7.07	35°	
						8.2	8								1-8.0	14°	
								④	0.6 / 0.6	100%	0.6 / 0.6	100%	0.6 / 0.6	100%	1-8.16	65°	
						8.8											EoH 8.8m

SPECIAL NOTES / SKETCHES
 CONSUMABLE MATERIALS USED
 DEPTH - From.....to..... Dates..... TIME - Moving & Set-Up..... hrs.
 Drilling..... hrs, Testing etc..... hrs, Delayed..... Stand-by..... hrs, Productive..... hrs.

RESULTS OF IN SITU TESTING

No.	TIME	DATE	DEPTHS	RESULTS.....



JOB No. 1407707
 DRILLHOLE No. BH14-02
 DEPTH 0 TO 8.8m

FORM CREATED BY R.S. COOPER, SCORP, DMFCPV G-6-10

FIELD DRILLHOLE LOG

Job No. 1407707 Job Name Canada Fluorspar Inc - Phase 1 Date Oct 22, 2014 Drillhole No. BH14-03
 DH Location Elevation (Obtained From Garmin - GPS) Datum WGS 84
 Inclination 90° Azimuth Along Hole Total Length
 Type of Drilling Diamond Type of Rig Duralite 800 Flush Water Feed
 Type of Core Barrel Single Tube Bit Design Bit No.
 Drillhole Dia. NQ - 76mm Drillcore Dia. 76mm 60mm Casing Dia. 89mm
 Contractor Springdale Drilling Driller
 Temperature -6° C Weather overcast Engineer A. IVANOFF

R.Q.D. - Rock Quality Designation (% Core Run > 0.1m Long) S.C.R. - Solid Core Recovery (% Cylindrical) T.C.R. - Total Core Recovery F.I. - Fracture Index (Fractures /)	F.R. - Fracture (Undifferentiated) S.A. - Sample C.A. - Casing W.L. - Water Level B.C. - Broken Core	B. - Bedding F.O. - Foliation / Schistosity CL. - Cleavage SH. - Shear Plane / Zone VN. - Vein F. - Fault	P. - Polished S. - Slickensided SM - Smooth R. - Ridged / Rough ST. - Stepped PL. - Planar	F.L. - Flexured UE. - Uneven W. - Wavy C. - Curved
---	--	--	---	---

Date / Time Core Ø, Depth	Date / Time Casing Ø, Depth	Water Levels am & pm	Percent Flush Return	Penetration		Depth (m)	Drilling Run No. Length	RECOVERY				Core Quality	DISCONTINUITIES			CORE DESCRIPTION	
				Time For Run, min.	Rate (/ min)			T.C.R. LENGTH	S.C.R. LENGTH	R.Q.D. LENGTH	Fractures Per m		DIP W.R.T. Core Axis	Type & Surface Description	Formation		DEPTH FROM : TO - Weathering ; Structure (Bedding Foliation, Jointing) Colour ; Grain Size & Texture ; Alteration State ; Cementation ; Rock Name ; Rock Formation
Ground Surface																	
						0										0 - 2.44 Overburden	
						1										Run @ 2.44 - 4.0m	
						2										2.81m JN, JN, RO, PC - silt	
						3	①	1.36 100%	1.08 100%	1.20 100%	77%	2.81 45°				2.92m JN, IR, RO, CC - salt - white	
						4		1.5 100%	1.25 100%	1.47 100%	77%	2.92 40°				2.98 70°	
						5	②	1.5 100%	1.25 100%	1.47 100%	77%	3.05 60°				3.05 JN, IR, RO, CC - salt - white with lim	
						6						3.20 32°				3.20 JN, JN, PL, PC	
						7						3.48 90°				3.48 F, JN, RO, JN - clay/silt	
						8						3.82 28°				3.82 JN, PL, RO, JN - 1mm silt	
						9						4.25 28°				4.25 JN, PL, RO, JN - 1mm silt powder	
						10						4.42 75°				4.42 JN, PL, SM, SA, ST - red clay	
						11										Rock Type	
						12										Grey-green Metasediment fresh, medium strong rock	
						13										ROH 5.54m	
						14										Monitoring Well Construction details found in Excel document	

SPECIAL NOTES / SKETCHES 	CONSUMABLE MATERIALS USED 	RESULTS OF IN SITU TESTING <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th>No.</th> <th>TIME</th> <th>DATE</th> <th>DEPTHS</th> <th>RESULTS</th> </tr> </thead> <tbody> <tr><td> </td><td> </td><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td><td> </td><td> </td></tr> </tbody> </table>	No.	TIME	DATE	DEPTHS	RESULTS																									
No.	TIME	DATE	DEPTHS	RESULTS																												
DEPTH - From to Dates TIME - Moving & Set-Up hrs. Drilling hrs. Testing etc. hrs. Delayed Stand-by hrs. Productive hrs.																																



JOB No. 1407707
 DRILLHOLE No. BH14-03
 DEPTH 0 TO 5.54m

FORM CREATED BY R.P.O. 10/11/10 PER 2010. REVISED FOR 2014-10-10

FIELD DRILLHOLE LOG

Job No. 1407707 Job Name Canada Fluorspar Inc - Phase I Date Oct 23, 2014 Drillhole No. BH14-04
 DH Location 615673mE / 5196695mN Elevation (Obtained From Garmin-GPS) Datum WGS 84
 Inclination 90° Azimuth Along Hole Total Length
 Type of Drilling diamond Type of Rig Duralite 800 Flush Water Feed
 Type of Core Barrel Single Tube Bit Design Bit No.
 Drillhole Dia. NQ - 76 mm Drillcore Dia. 76 mm Casing Dia. HR - surface casing - 89 mm
 Contractor Springdale Drilling Driller
 Temperature -6 °C Weather overcast / windy Engineer A. IVANOFF

R.Q.D. - Rock Quality Designation (% Core Run > 0.1m Long)	F.R. - Fracture (Undifferentiated)	B. - Bedding	P. - Polished	F.L. - Flexured
S.C.R. - Solid Core Recovery (% Cylindrical)	S.A. - Sample	F.O. - Foliation / Schistosity	S. - Slickensided	UE. - Uneven
T.C.R. - Total Core Recovery	C.A. - Casing	CL. - Cleavage	SM - Smooth	W. - Wavy
F.I. - Fracture Index (Fractures / m)	W.L. - Water Level	SH. - Shear Plane / Zone	R. - Ridged / Rough	C. - Curved
	B.C. - Broken Core	VN. - Vein	CO. - Contact	ST. - Stepped
		F. - Fault	J. - Joint	PL. - Planar

Date / Time Core Ø, Depth	Date / Time Casing Ø, Depth	Water Levels am & pm	Penetration		Depth (m)	Drilling Run No. & Length	RECOVERY				Core Quality		DISCONTINUITIES			FORMATION	CORE DESCRIPTION <small>DEPTH FROM: TO - Weathering; Structure (Bedding Foliation, Jointing) Colour; Grain Size & Texture; Alteration State; Cementation; Rock Name; Rock Formation</small>
			Time For Run, min.	Rate (m/min)			T.C.R.	S.C.R.	R.Q.D.	Fractures Per	DIP ° W.R.T. Core Axis	Type & Surface Description	ROCK MATERIAL				
							LENGTH	%	LENGTH					%	LENGTH		
					0m											0-2.0m overburden.	
					2.14											overburden.	
					2.14											RUN#1 (2m to 3.5m)	
					3	1	1.36	91%	0.51	1.36	88%	1	2.17m 14° UN/SM	R3		2.17m JN UN/SM; SA J _r =2.0 J _a =2 JCR=16	
					3	2	1.36	91%	0.51	1.36	88%	1	2.42m 40°	R3		2.42m JN UN/SM; SA J _r =2.0 J _a =2 JCR=16	
					3	3	1.36	91%	0.51	1.36	88%	1	2.82m 30°	R3		2.82m JN UN/SM; SA J _r =2.0 J _a =2 JCR=16	
					3	4	1.36	91%	0.51	1.36	88%	1	3.36m 45°	R3		3.36m JN UN/SM; SA J _r =2.0 J _a =2 JCR=16	
					4	1	1.5	100%	1.5	1.5	100%	1	3.67m 14°	R3		3.67m JN PL, SM, ST - reddish-brown. J _r =1.0, J _a =1, JCR=16	
					4	2	1.5	100%	1.5	1.5	100%	1	2.82m JN PL, SM, ST - chlorite	R3		2.82m JN PL, SM, ST - chlorite J _r =1.0, J _a =1, JCR=16	
					5	1	1.5	100%	1.5	1.5	100%	1	3.36m JN ST, RO, CL	R3		3.36m JN ST, RO, CL J _r =3, J _a =1, JCR=25	
					5	2	1.5	100%	1.5	1.5	100%	1	3.67m JN PL, SM, PC - chlorite	R3		3.67m JN PL, SM, PC - chlorite J _r =1.0, J _a =2, JCR=16	
					5	3	1.5	100%	1.5	1.5	100%	1	5.20m JN, PL, RO, PC - chlorite	R3		5.20m JN, PL, RO, PC - chlorite J _r =3, J _a =2, JCR=20	
					6	1	1.5	100%	1.5	1.5	100%	1	5.25m 83°	R3		5.25m JN, PL, RO, PC - chlorite J _r =3, J _a =2, JCR=20	
					6	2	1.5	100%	1.5	1.5	100%	1	6.17m 14°	R3		6.17m UN, RO, ST - yellowish-brown. J _r =1.5, J _a =1, JCR=25	
					6	3	1.5	100%	1.5	1.5	100%	1	6.28m 14°	R3		6.28m UN, RO, ST - yellowish-brown. J _r =1.5, J _a =1, JCR=25	
					7	1						1	6.17m UN, RO, ST - yellowish-brown. J _r =1.5, J _a =1, JCR=25	E0H		6.17m UN, RO, ST - yellowish-brown. J _r =1.5, J _a =1, JCR=25	
					7	2						1	6.28m JN, PL, SM, PC - green chlorite	E0H		6.28m JN, PL, SM, PC - green chlorite J _r =1.0, J _a =2, JCR=16	
					7	3						1	6.28m same as above.	E0H		6.28m same as above.	

SPECIAL NOTES / SKETCHES 	CONSUMABLE MATERIALS USED 	RESULTS OF IN SITU TESTING <table border="1" style="width: 100%; border-collapse: collapse; font-size: x-small;"> <thead> <tr> <th>No.</th> <th>TIME</th> <th>DATE</th> <th>DEPTHS</th> <th>RESULTS</th> </tr> </thead> <tbody> <tr><td> </td><td> </td><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td><td> </td><td> </td></tr> </tbody> </table>	No.	TIME	DATE	DEPTHS	RESULTS																				
No.	TIME	DATE	DEPTHS	RESULTS																							
DEPTH - From to Dates TIME - Moving & Set-Up hrs. Drilling hrs. Testing etc. hrs. Delayed Stand-by hrs. Productive hrs.																											




JOB No. 1407707
 DRILLHOLE No. BH14-04
 DEPTH 0 TO 6.5m




PROJECT
CANADA FLUORSPAR INC. PROJECT


TITLE
MW14-01 ROCK CORE

	PROJECT # 1407707		SCALE: N/A	REV. 1
	DESIGN	ADI	NOVEMBER 2014	<p>FIGURE A1</p>
	CHECK	PM	NOVEMBER 2014	
REVIEW	JMP	NOVEMBER 2014		




PROJECT		CANADA FLUORSPAR INC. PROJECT	
TITLE		MW14-02 ROCK CORE	
	PROJECT #: 1407707		SCALE: N/A
	DESIGN	ADI	NOVEMBER 2014
	CHECK	PM	NOVEMBER 2014
	REVIEW	JMP	NOVEMBER 2014
			REV. 1
			FIGURE A2



PROJECT		CANADA FLUORSPAR INC. PROJECT	
TITLE		MW14-03 ROCK CORE	
	PROJECT # 1407707		SCALE: N/A
	DESIGN	ADI	NOVEMBER 2014
	CHECK	PM	NOVEMBER 2014
	REVIEW	JMP	NOVEMBER 2014
			REV. 1
			FIGURE A3



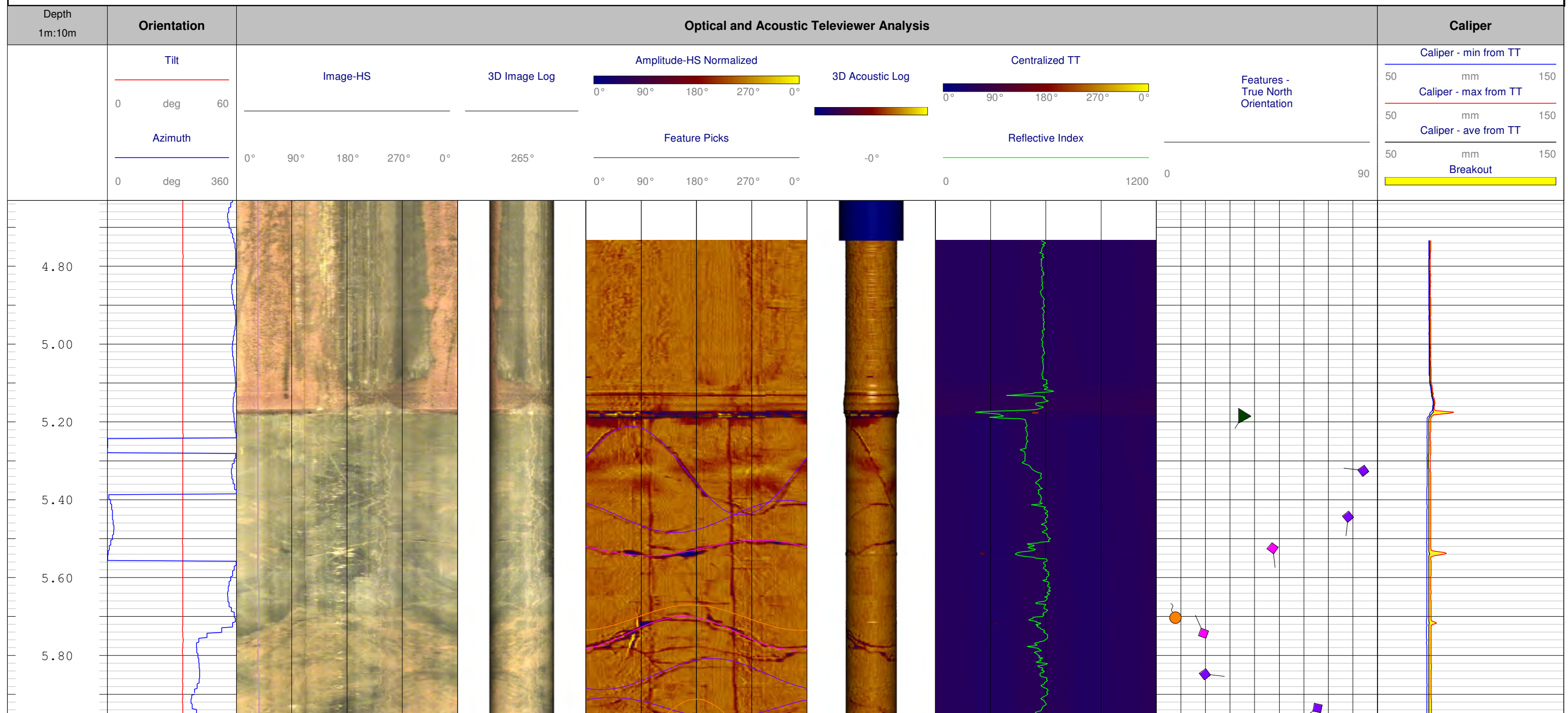
PROJECT		CANADA FLUORSPAR INC. PROJECT		
TITLE		MW14-04 ROCK CORE		
	PROJECT #: 1407707		SCALE: N/A	REV. 1
	DESIGN	ADI	NOVEMBER 2014	
	CHECK	PM	NOVEMBER 2014	
	REVIEW	JMP	NOVEMBER 2014	
			FIGURE A4	

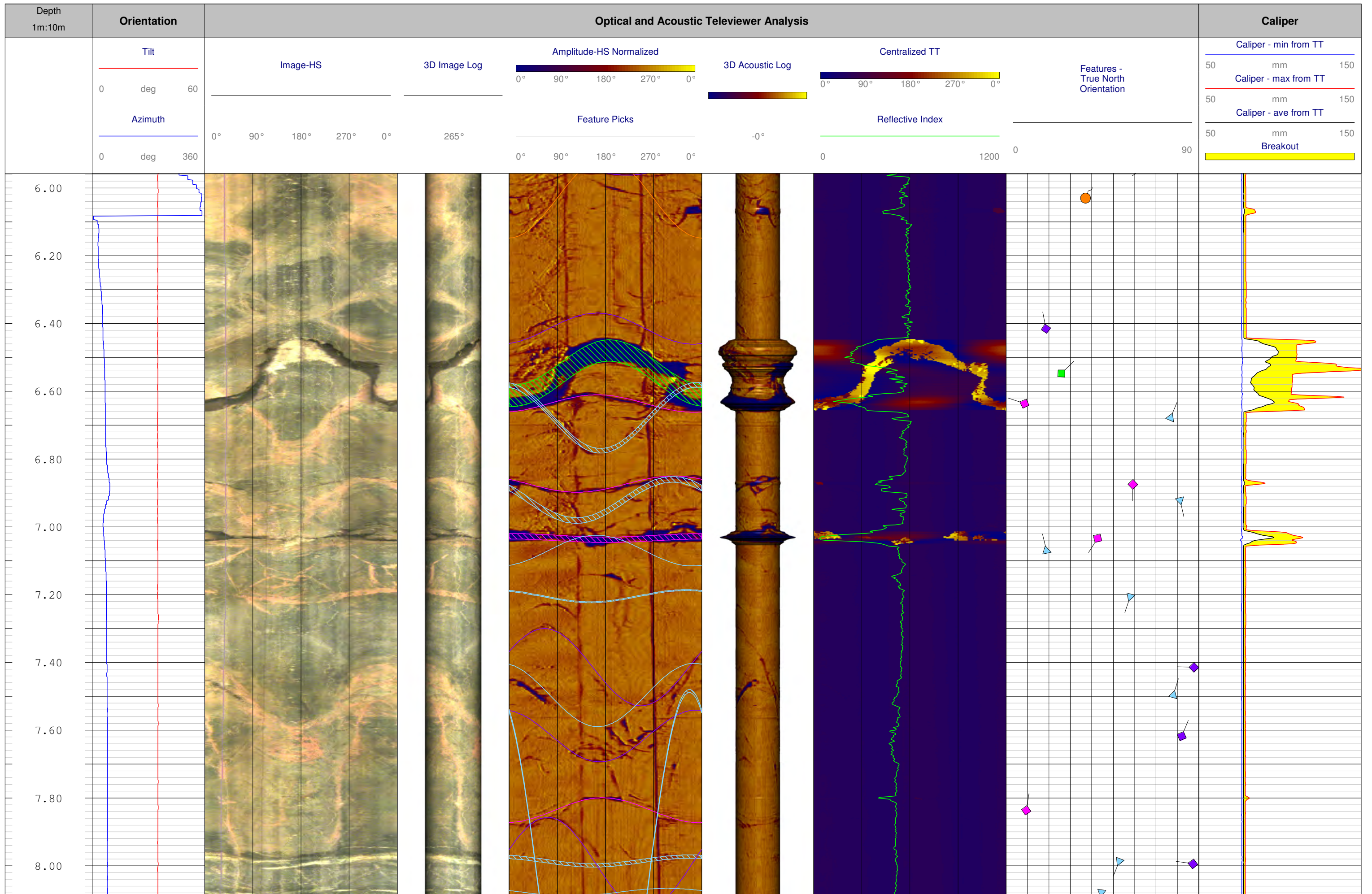
ACOUSTIC and OPTICAL TELEVIEWER PLOT

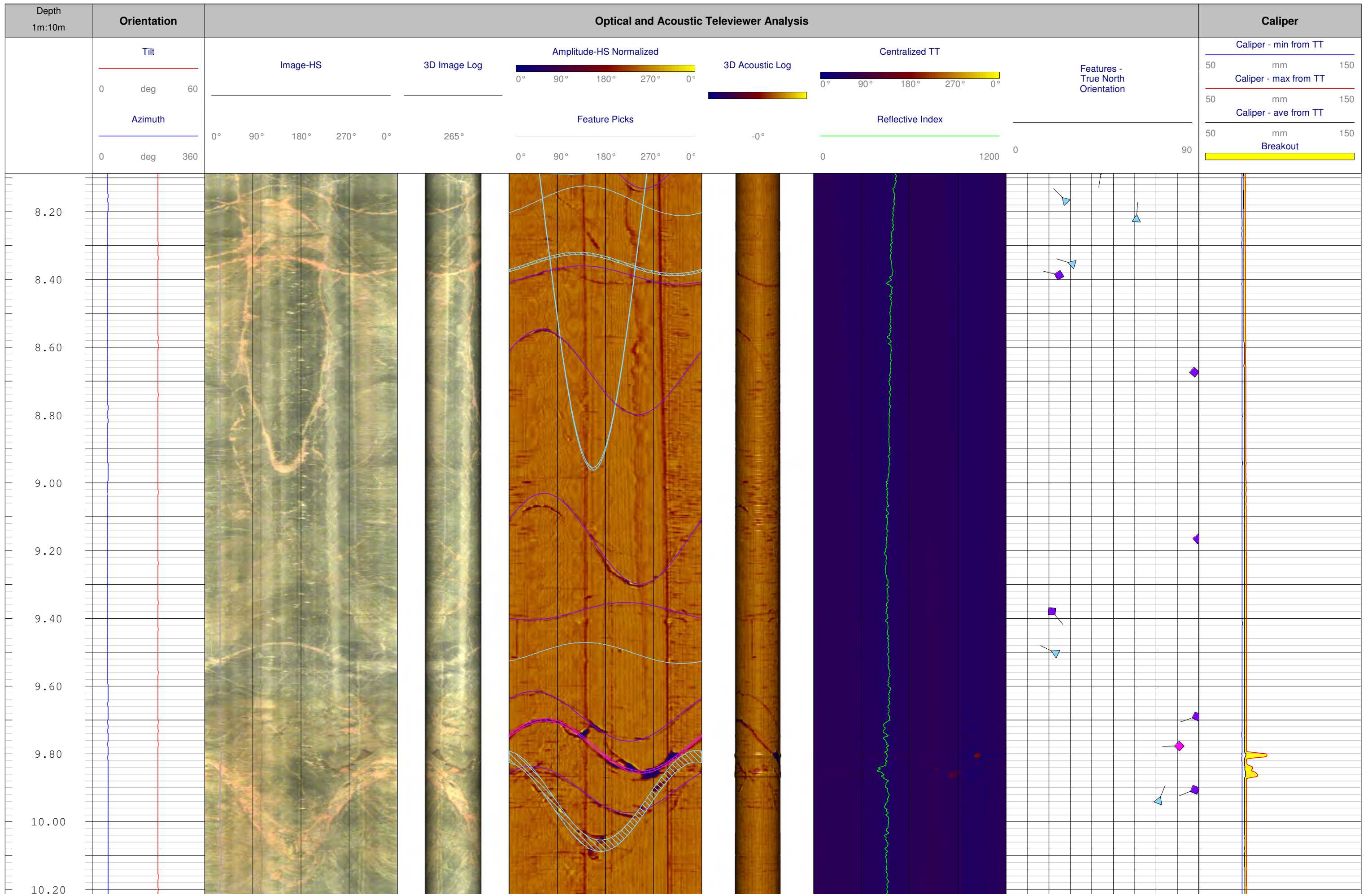
Company:	Canada Fluorspar	Total Depth:	110 m	UTM X (Easting):	N/A	Notes: DGI Geoscience Inc. 119 Spadina Avenue, Suite 405 Toronto, Ontario Canada, M5V 2L1 416.361.3191
Hole ID:	GS-14-94	Surveyed Depth:	108 m	UTM Y (Northing):	N/A	
Acquisition date(s):	Nov. 05, 2014	Hole Diameter:	NQ	UTM Z (Elevation):	N/A	
Field Personnel:	J. Smith, R. Morrison	Hole Type:	Core			
Legal Location:	Saint Lawrence, NFLD	Casing Depth:	5 m			
Survey Day(s):	1	Fluid Type:	Water			

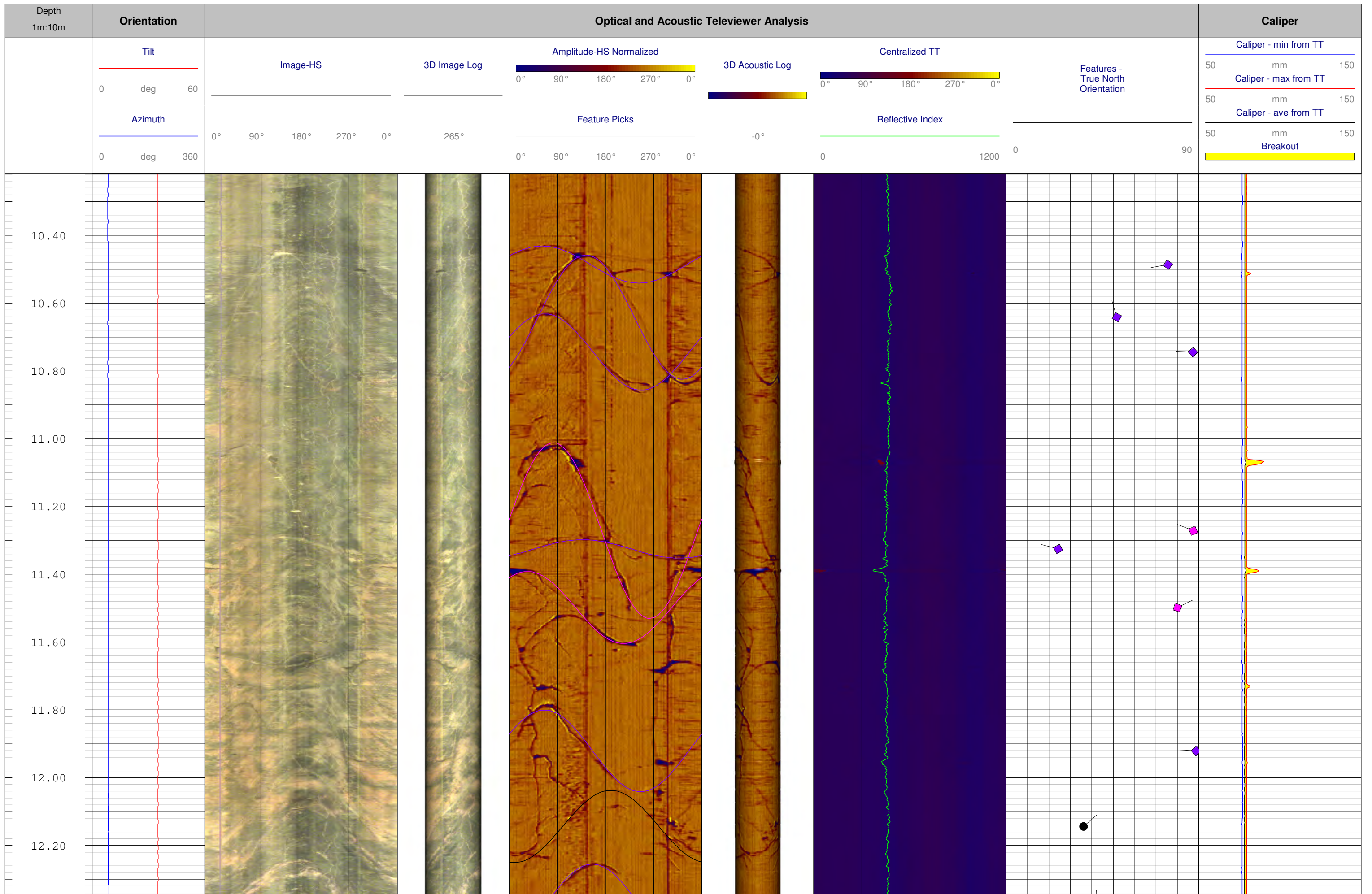
LEGEND - STRUCTURE TYPE

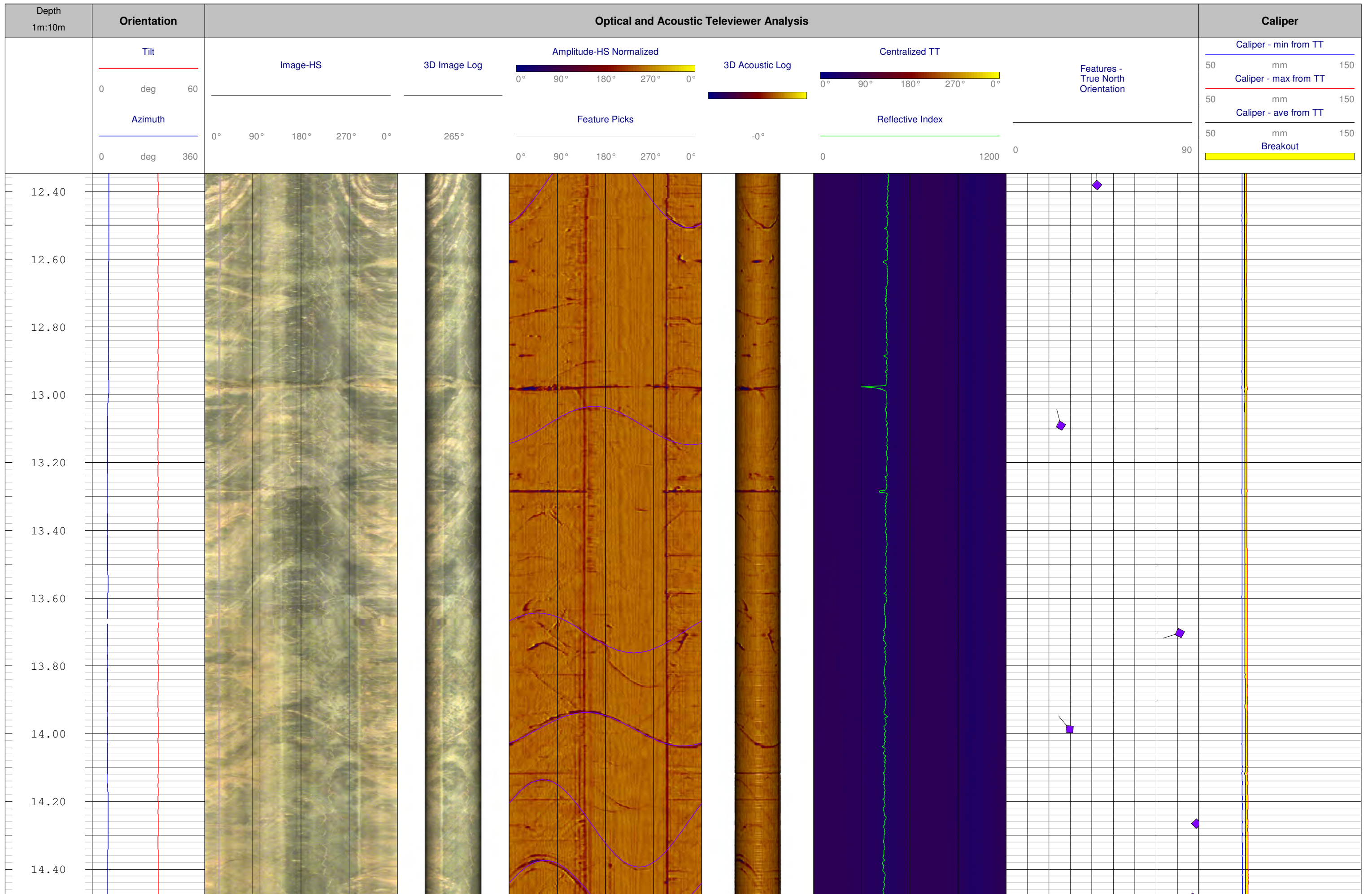
- Btm of Casing
- Major Open Joint/Fracture
- Partially Open Joint/Fracture
- Minor Joint/Fracture
- Bedding/ Banding/ Foliation
- Vein - Group 1
- Lithology Contact

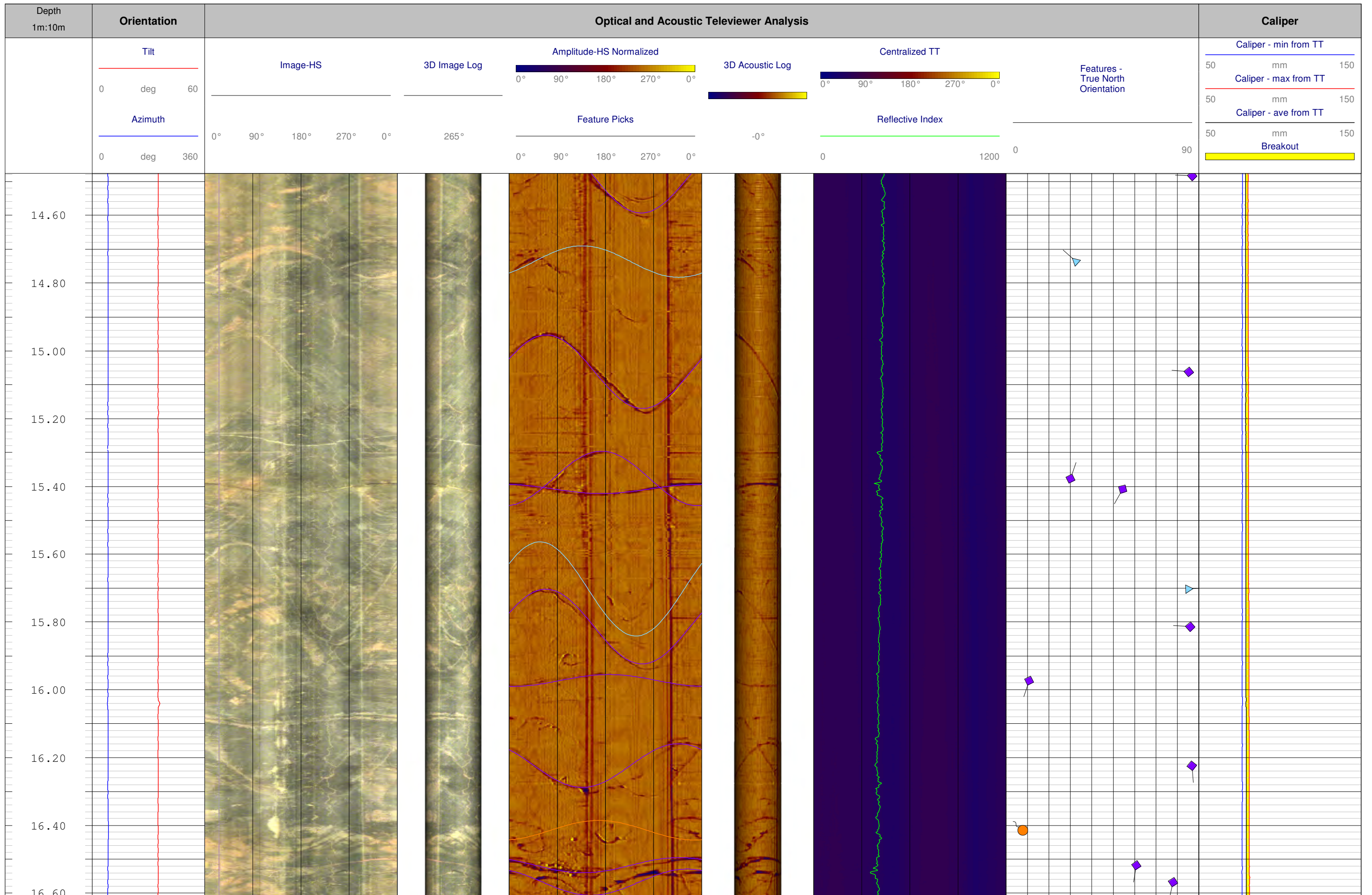


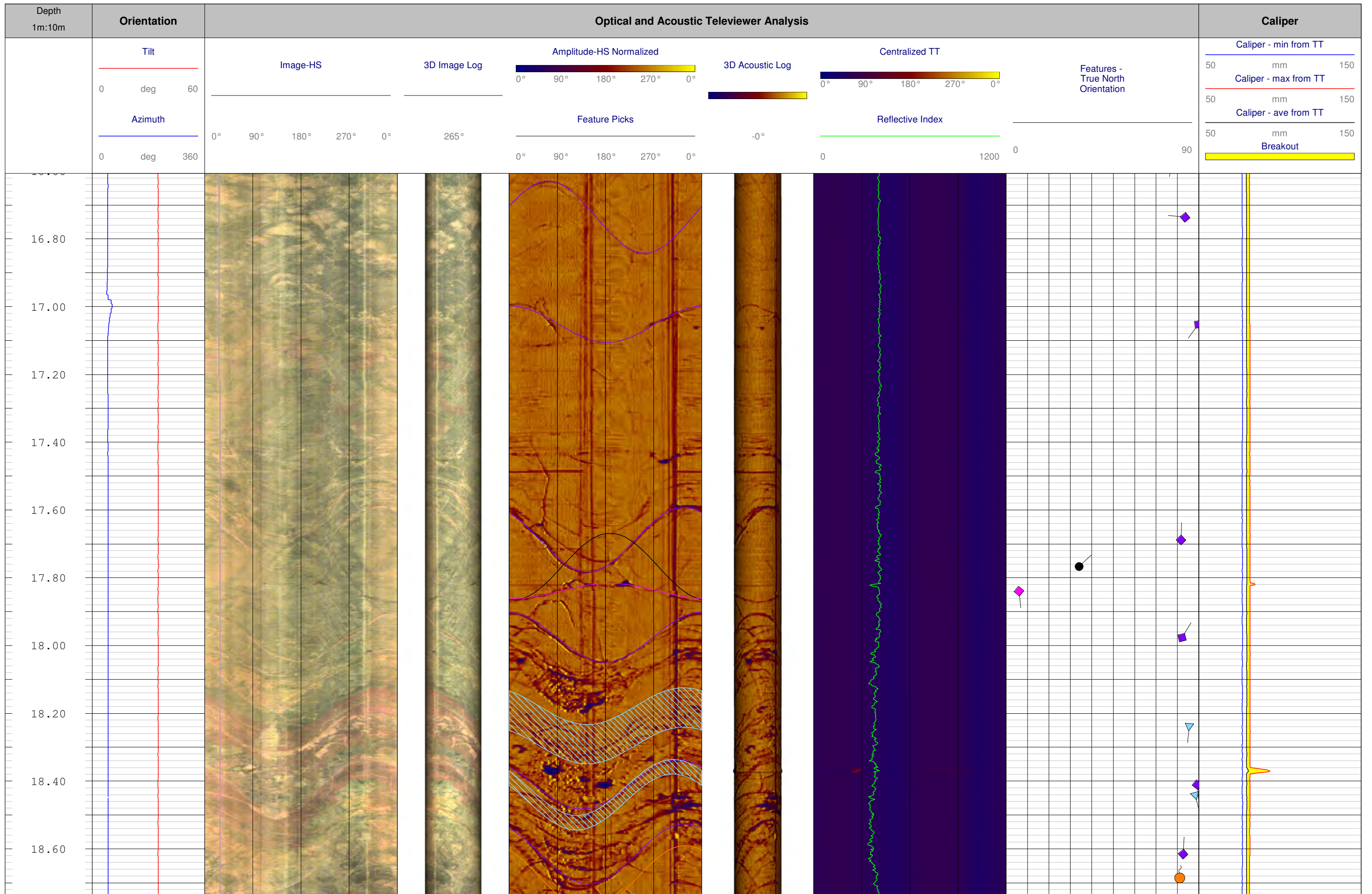


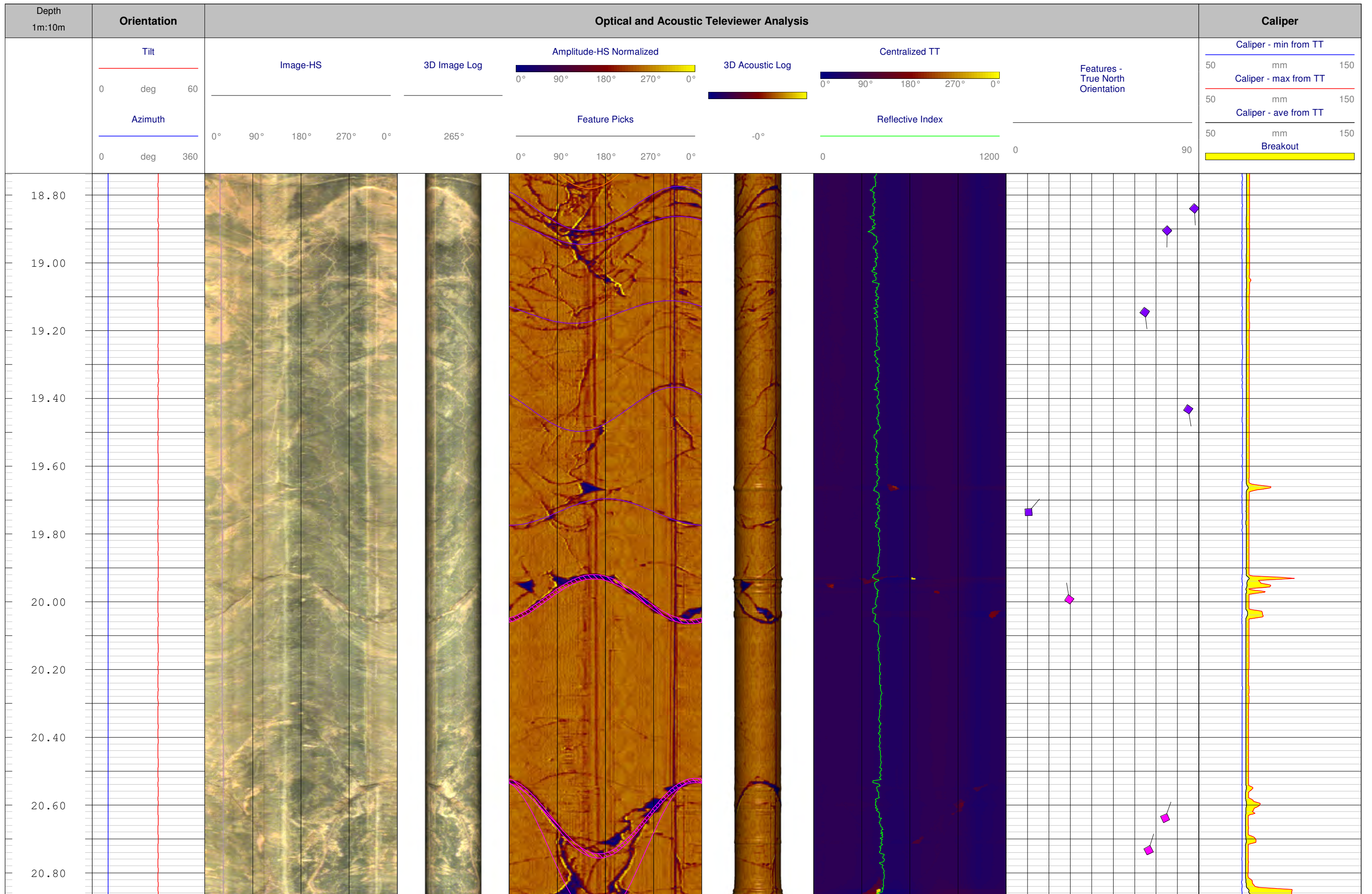


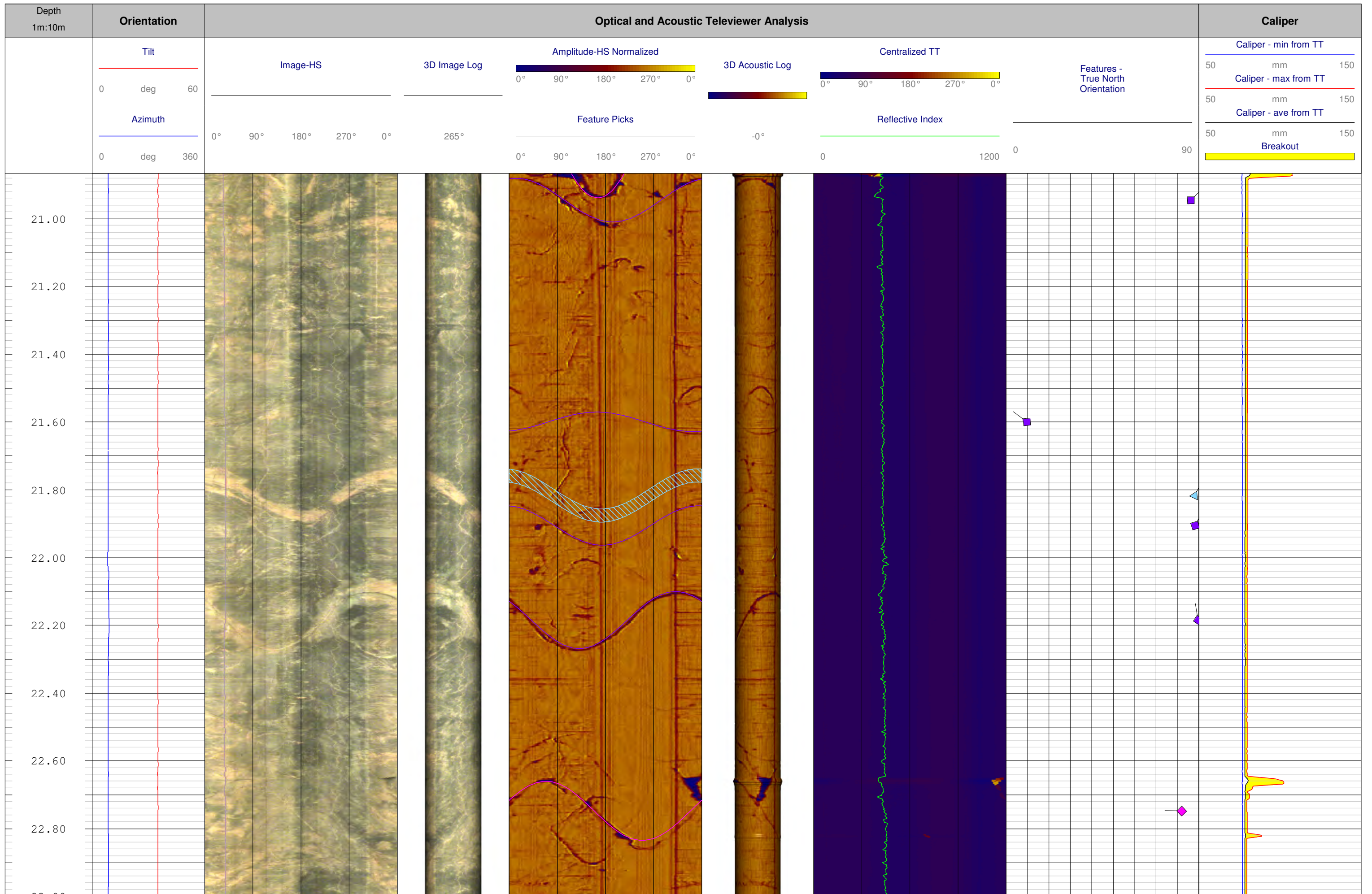


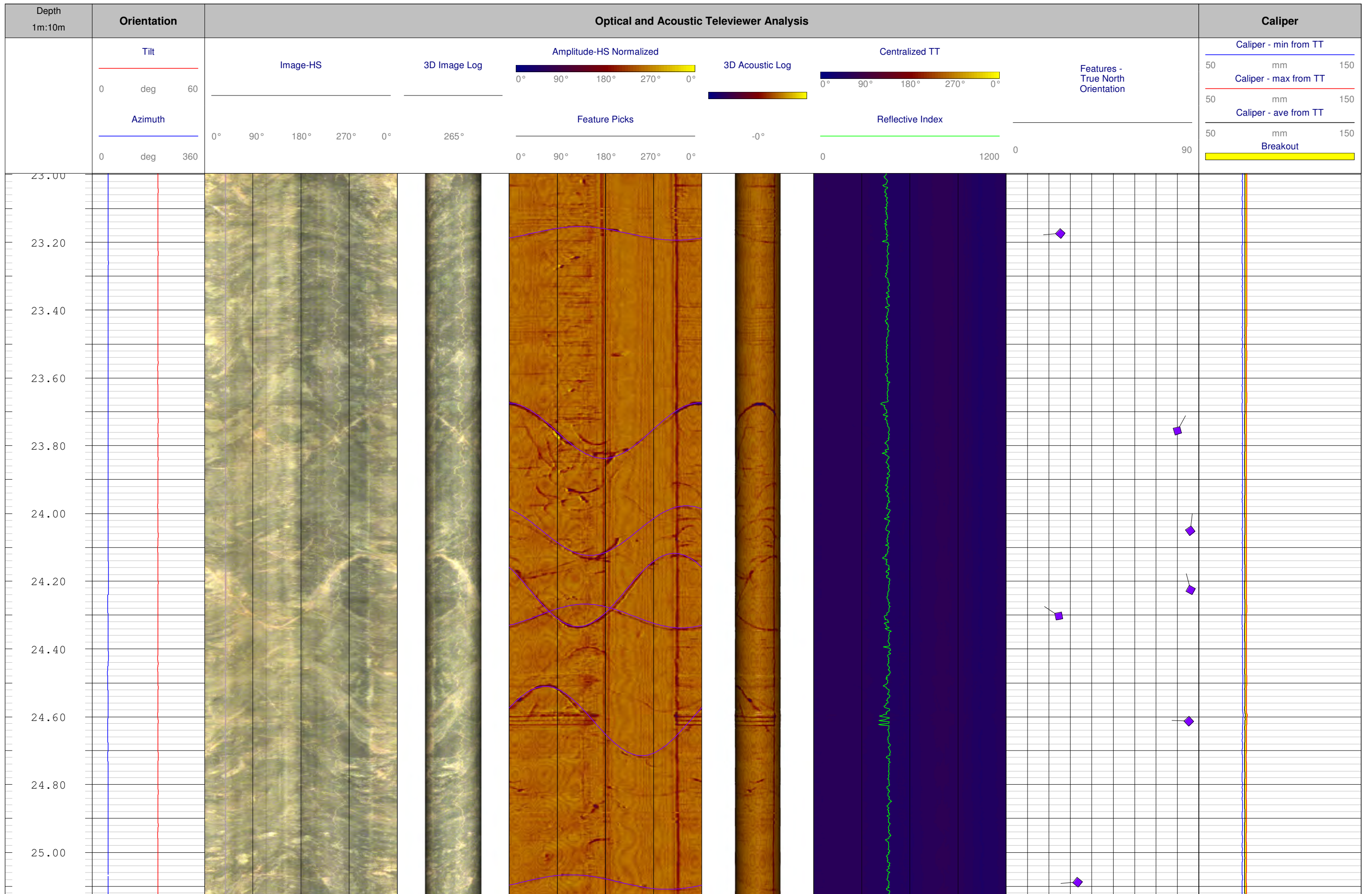


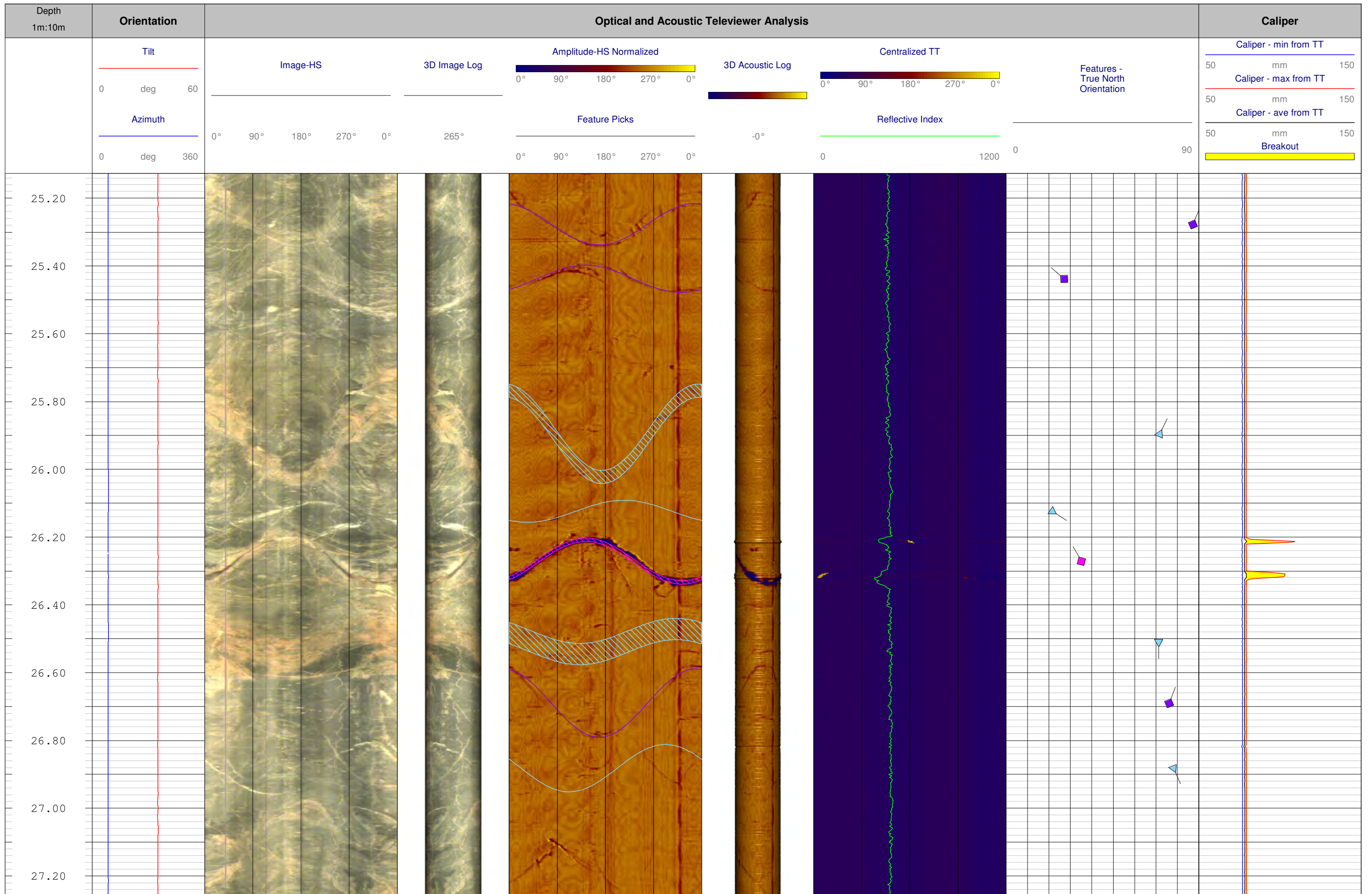


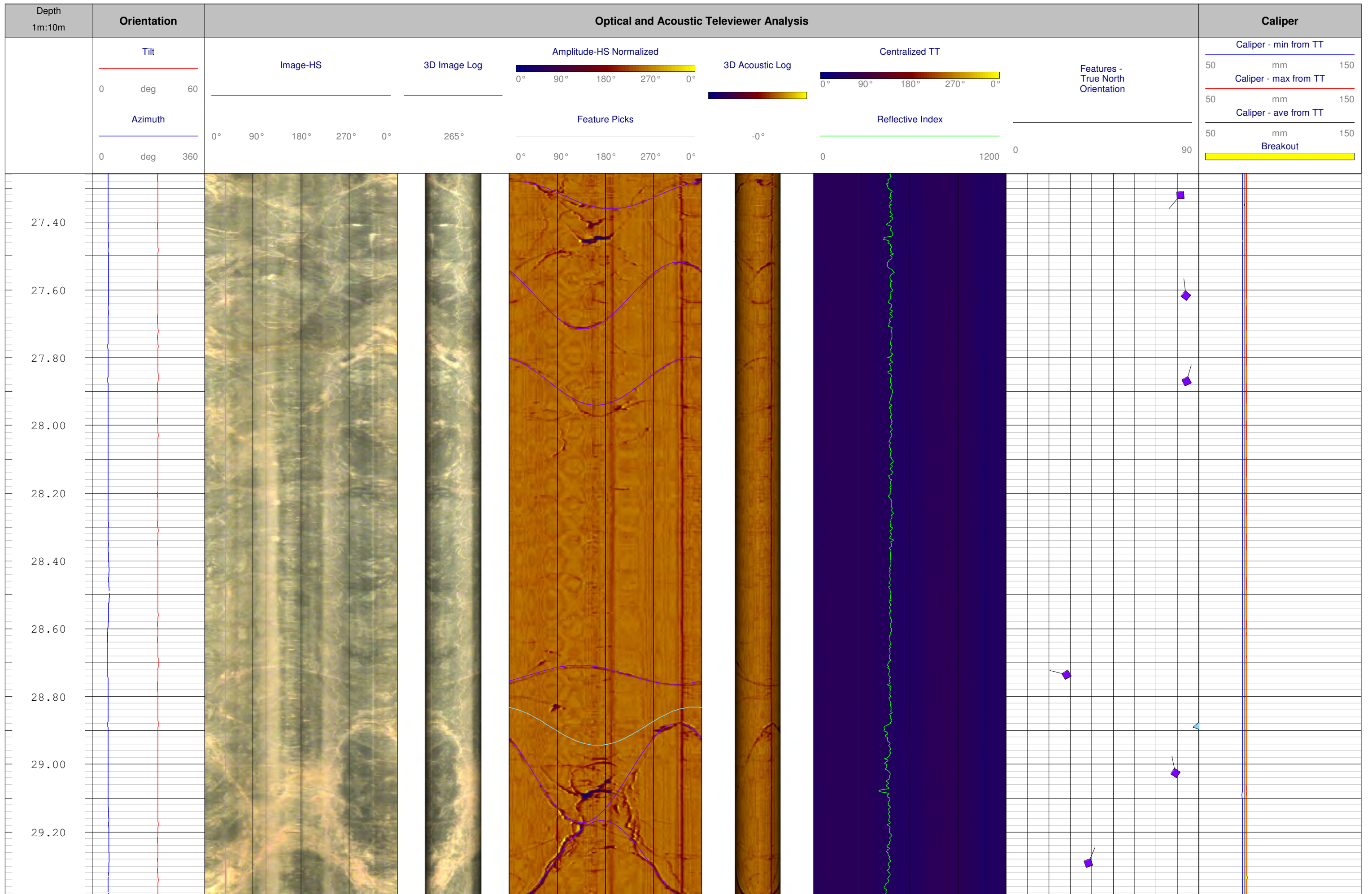


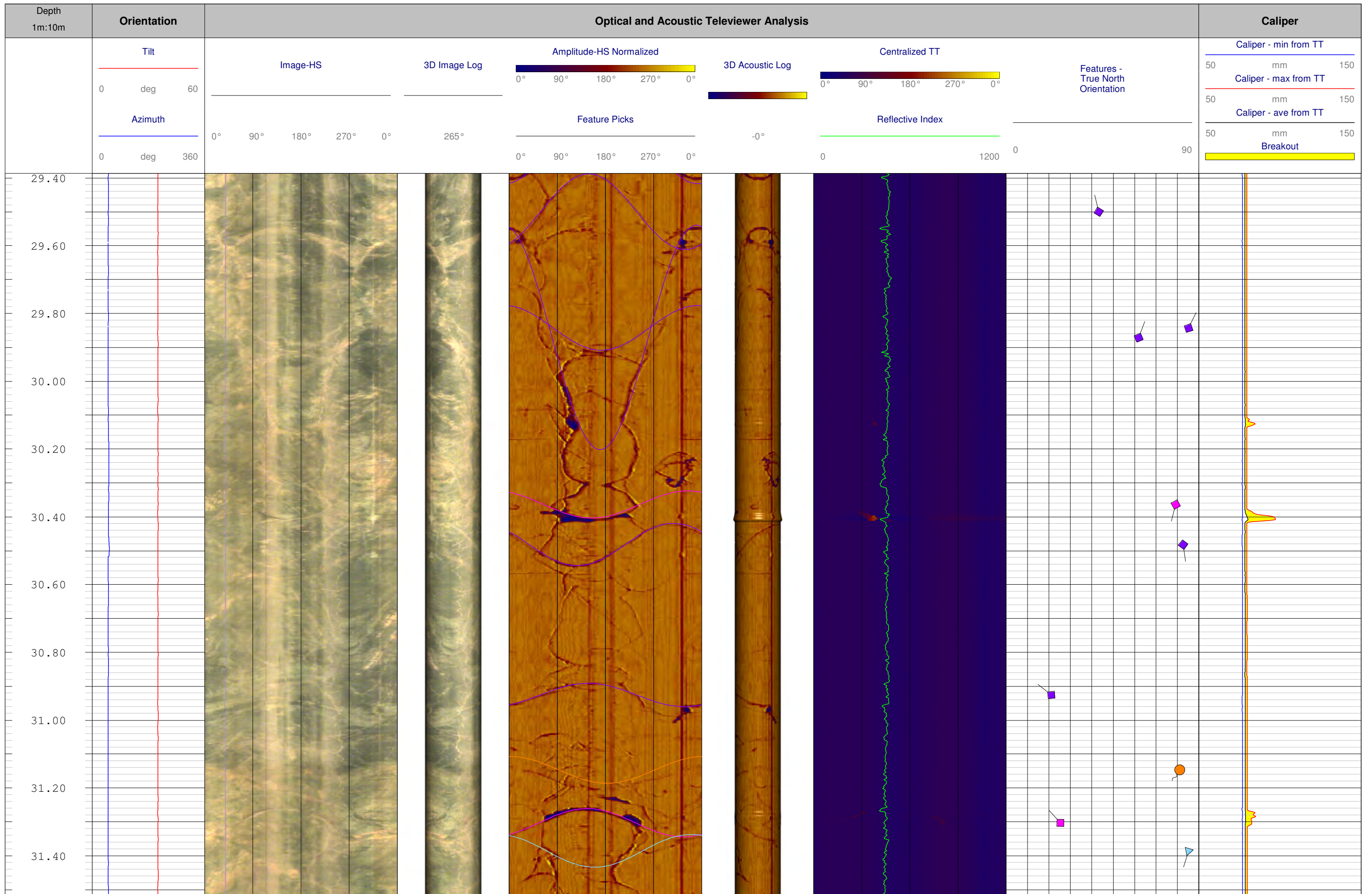


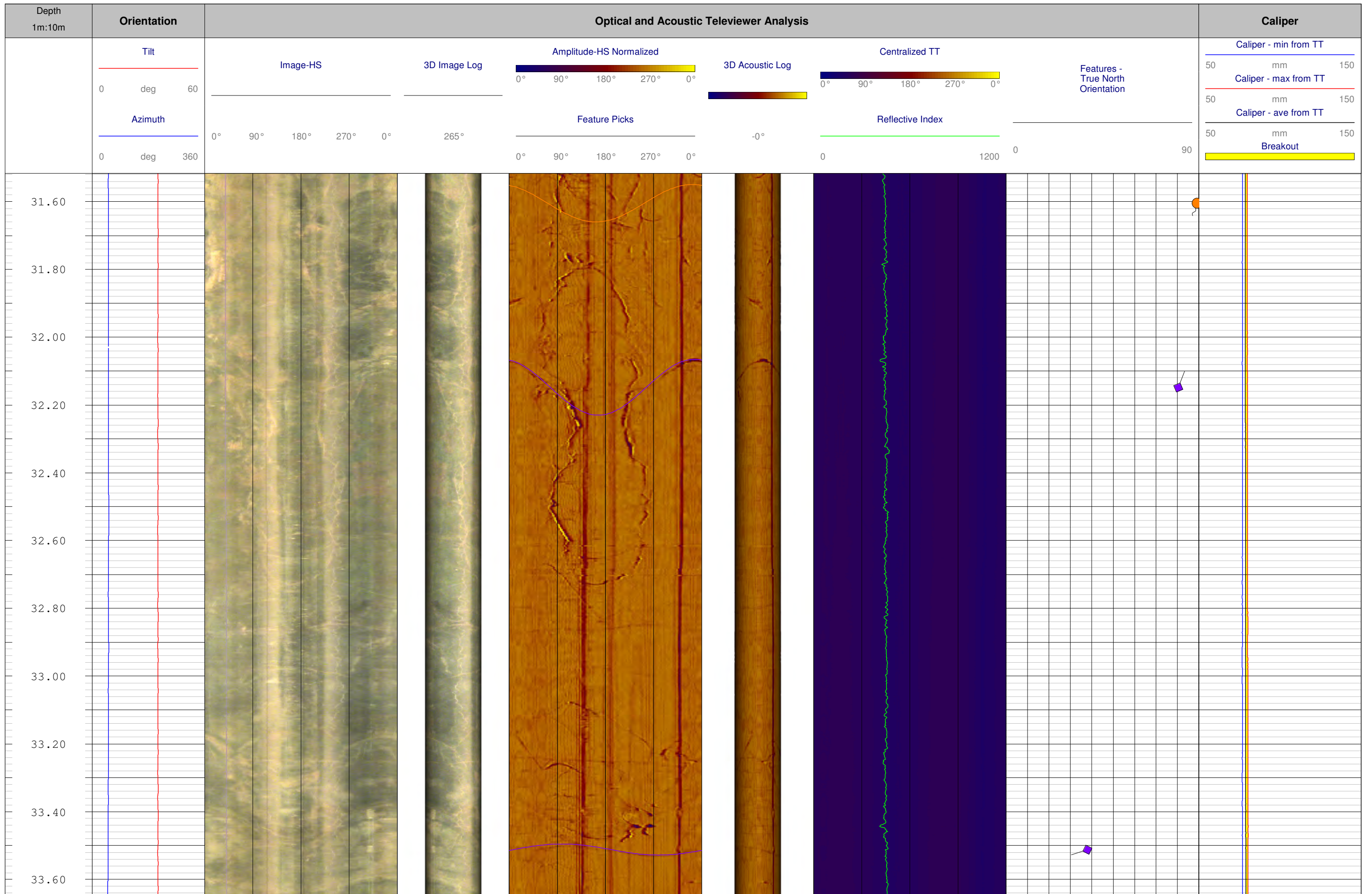


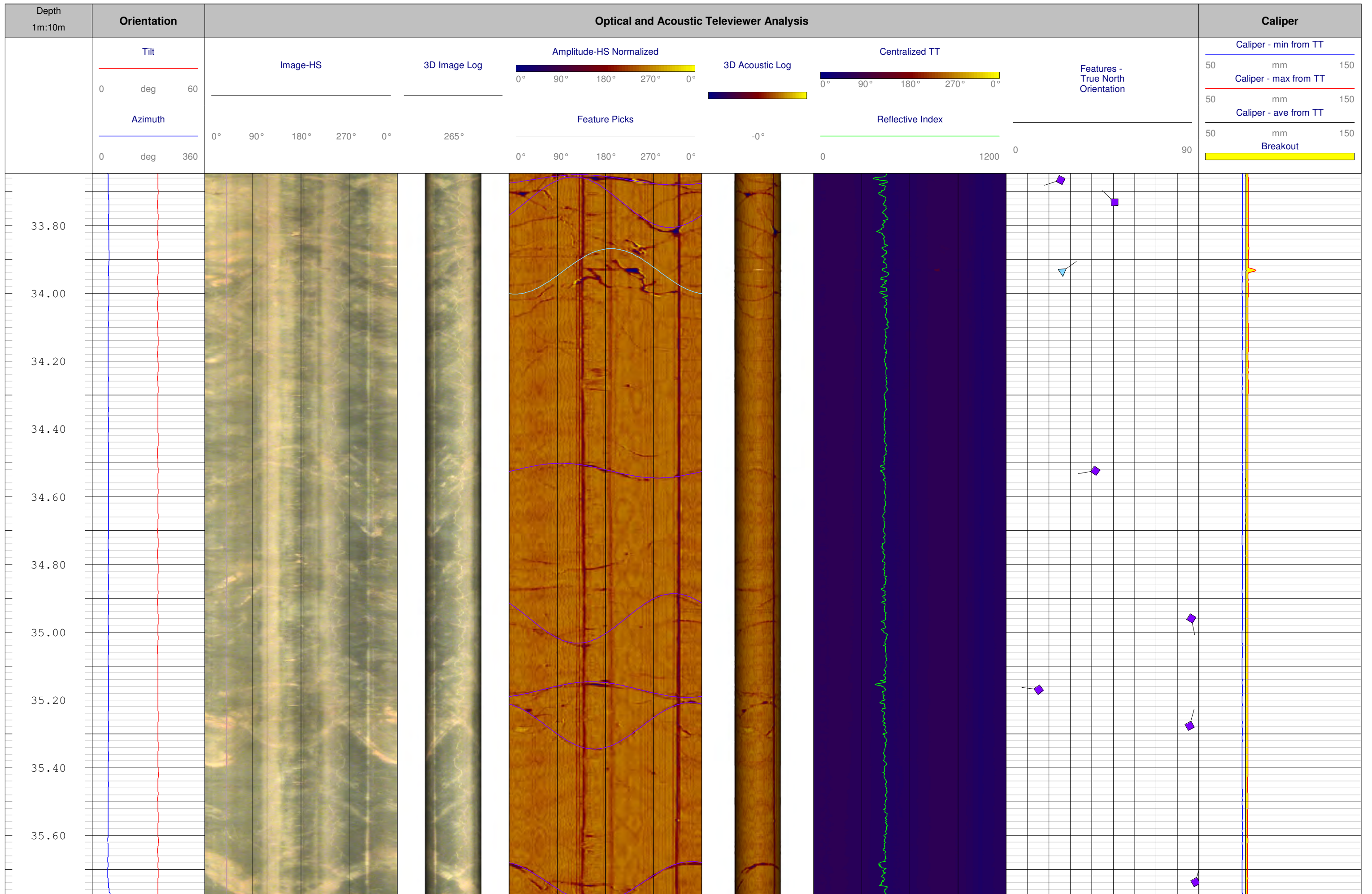


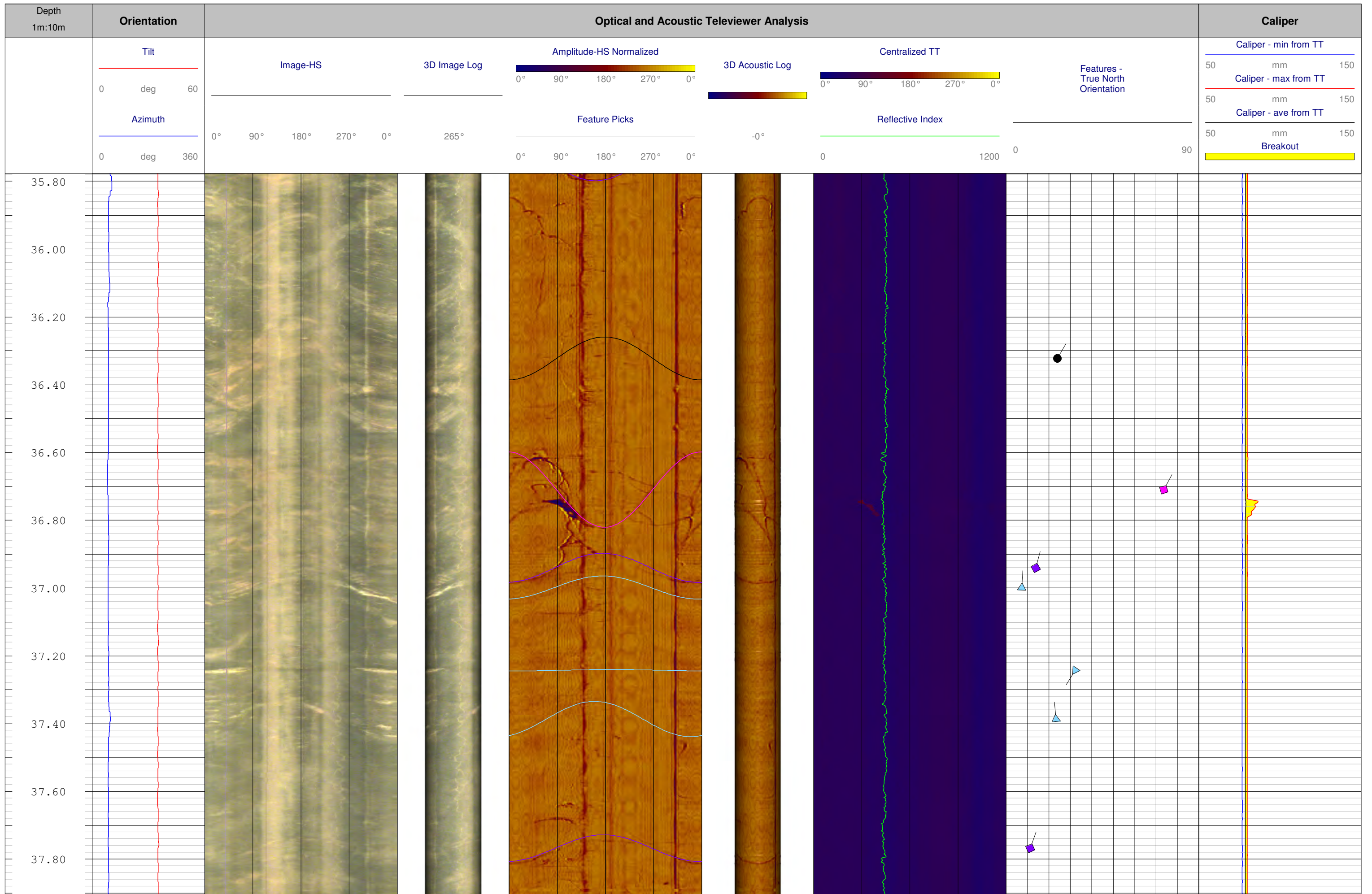


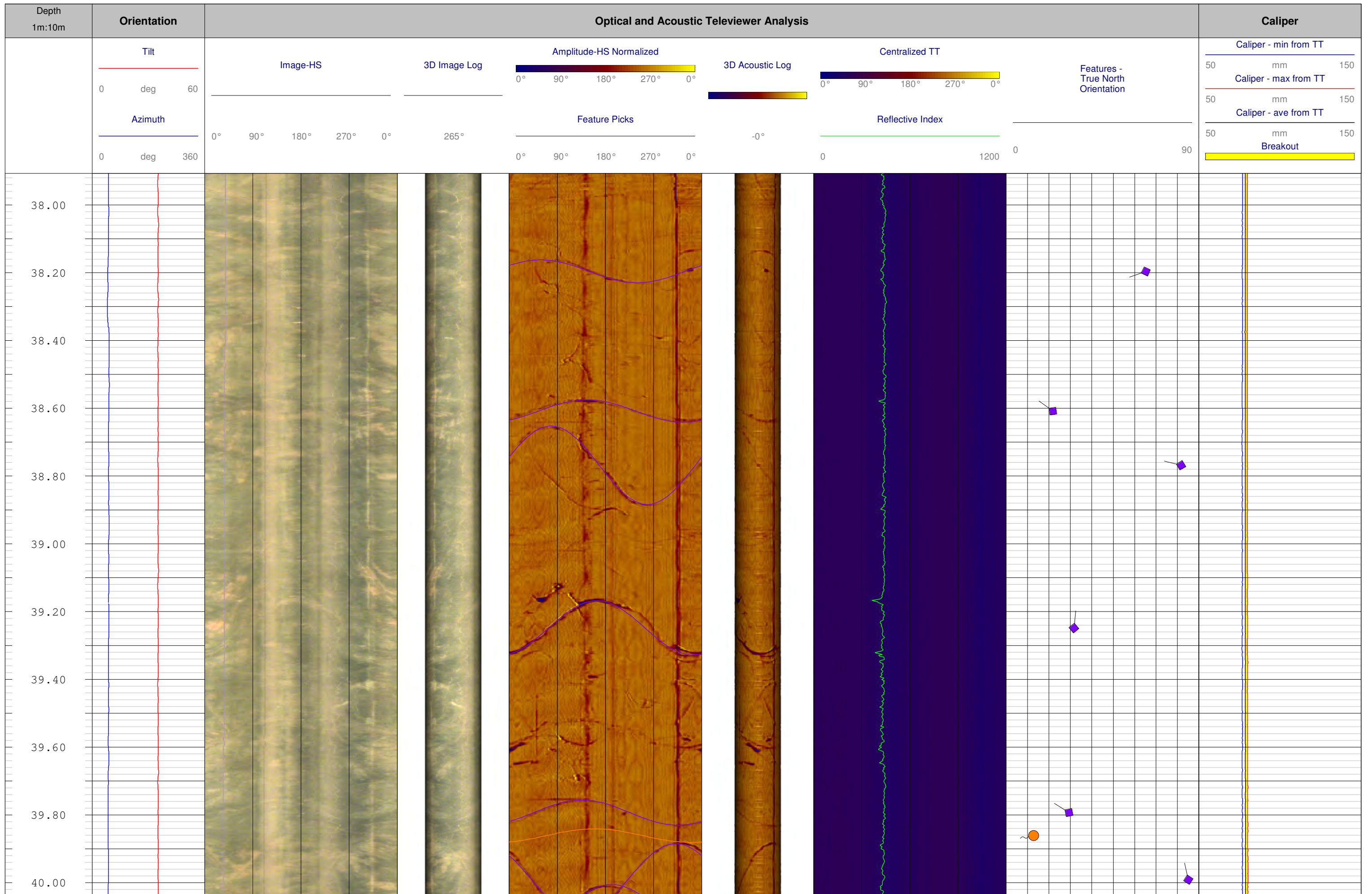


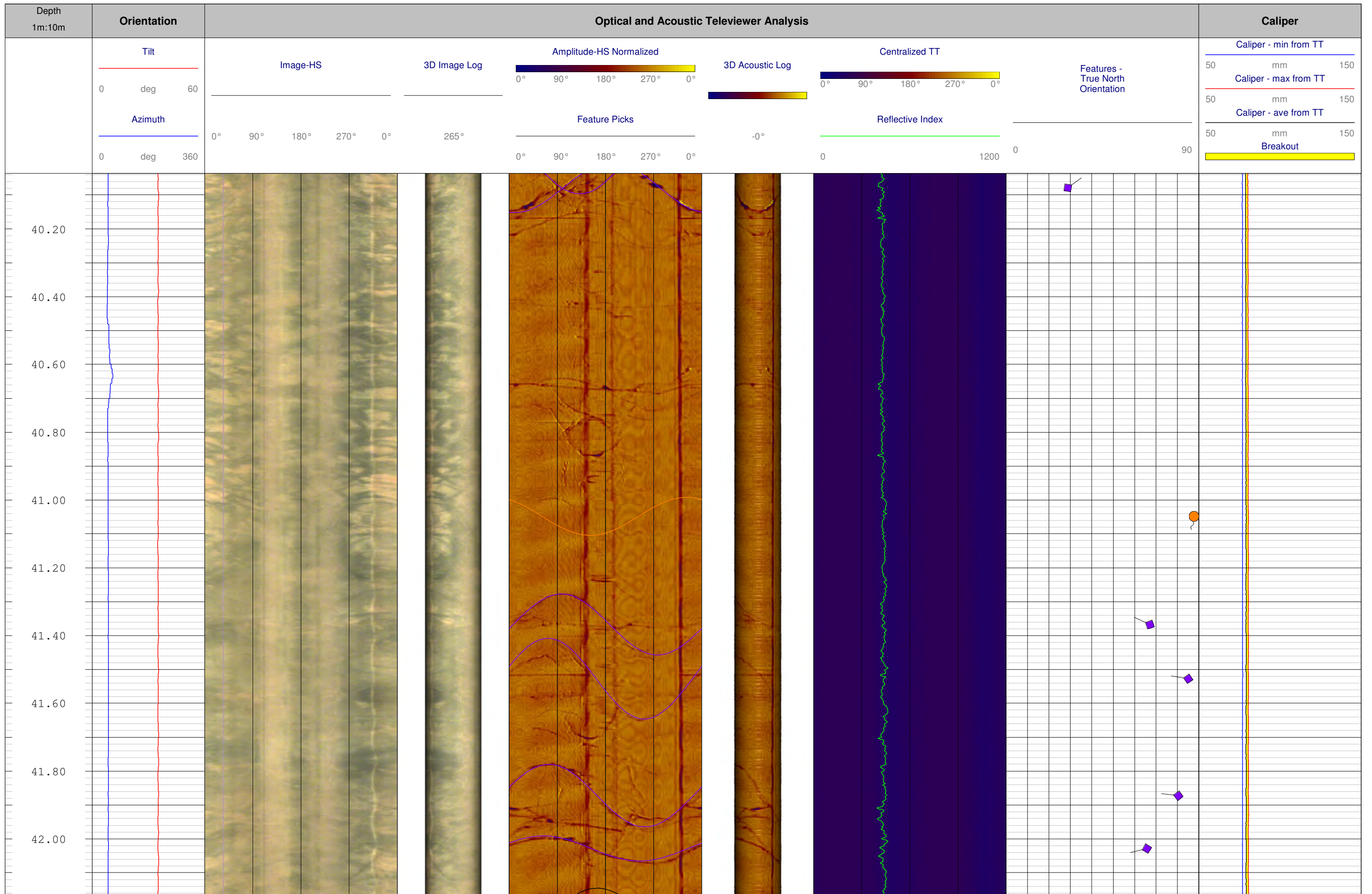


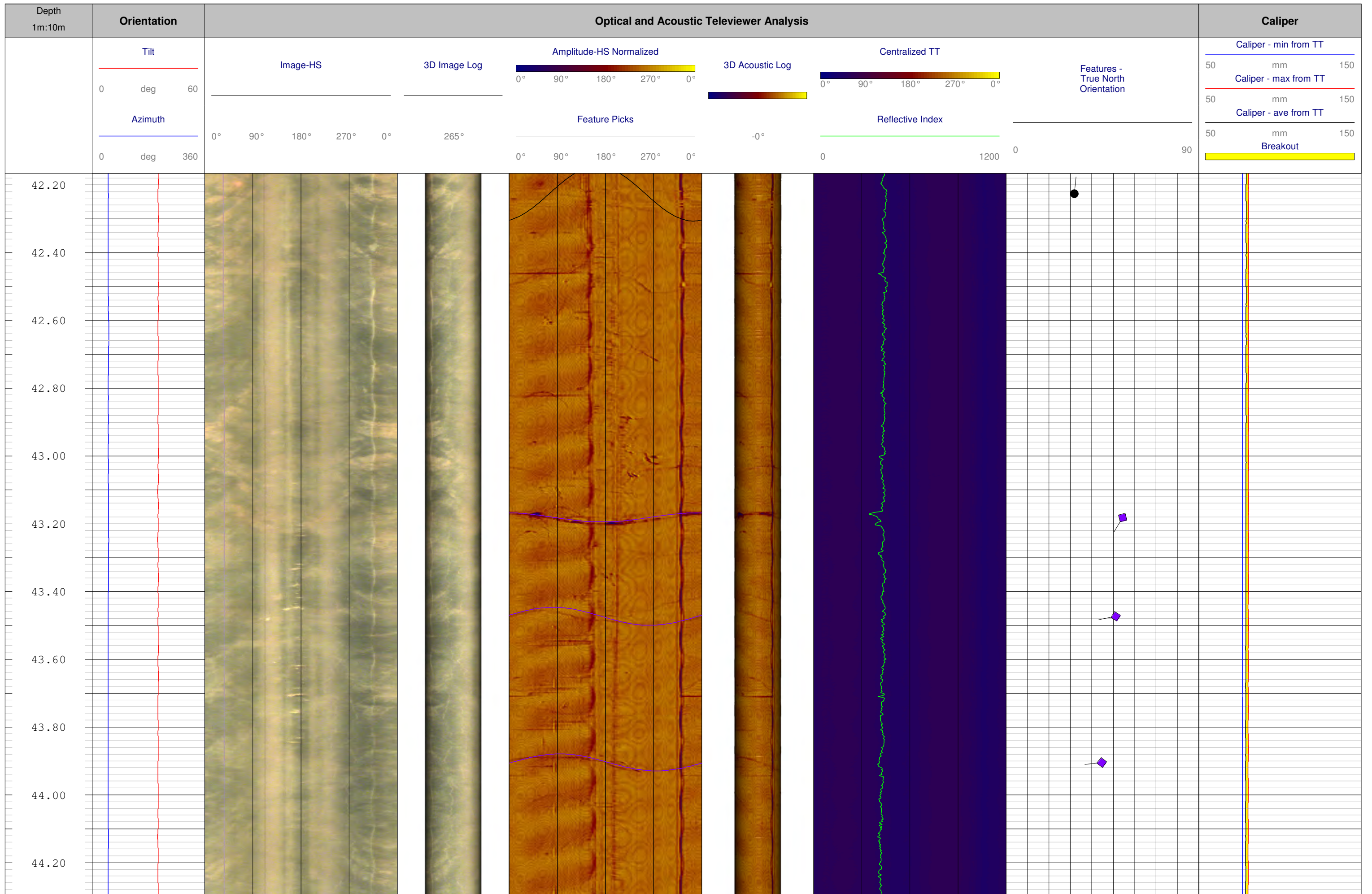


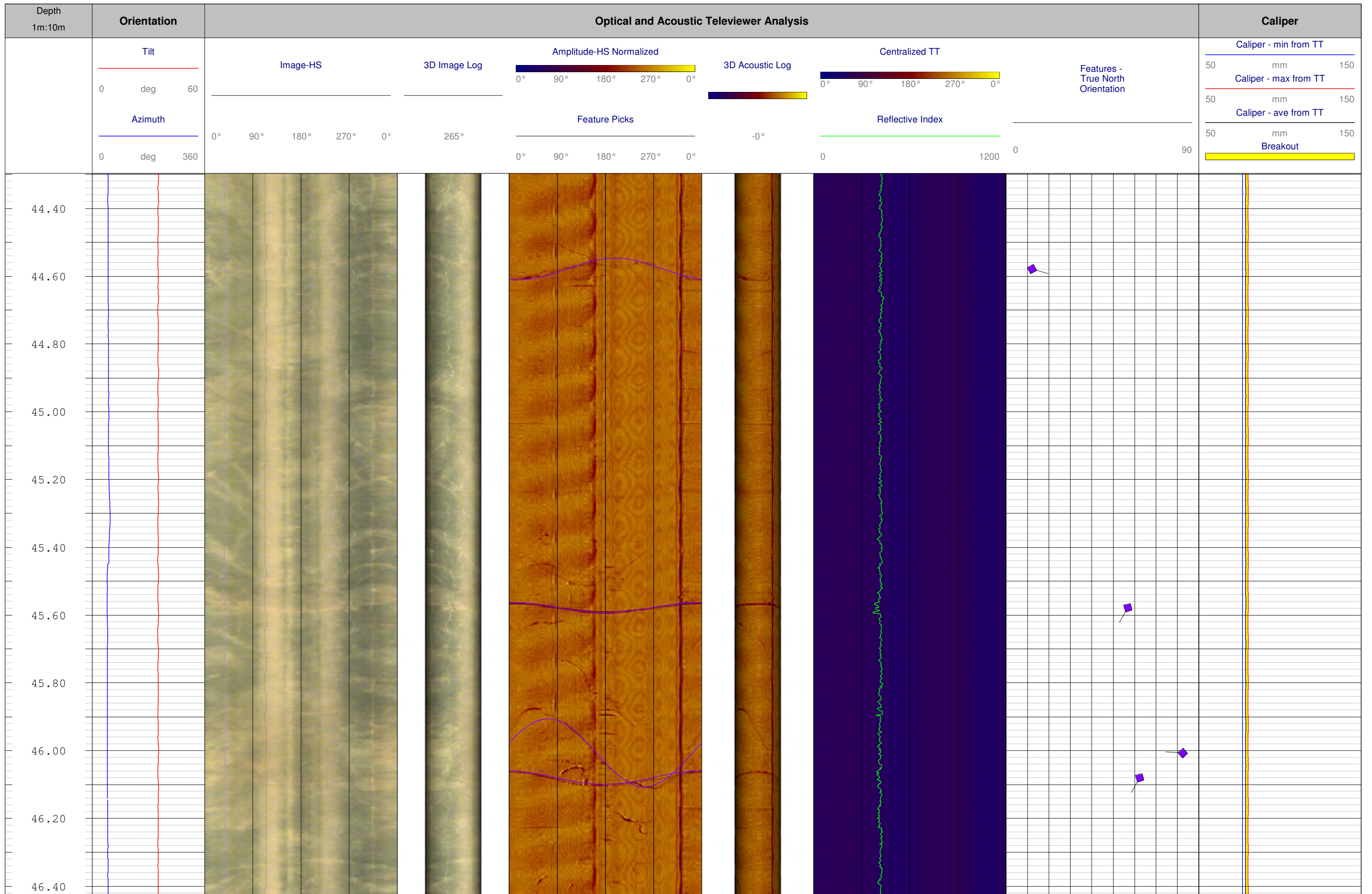


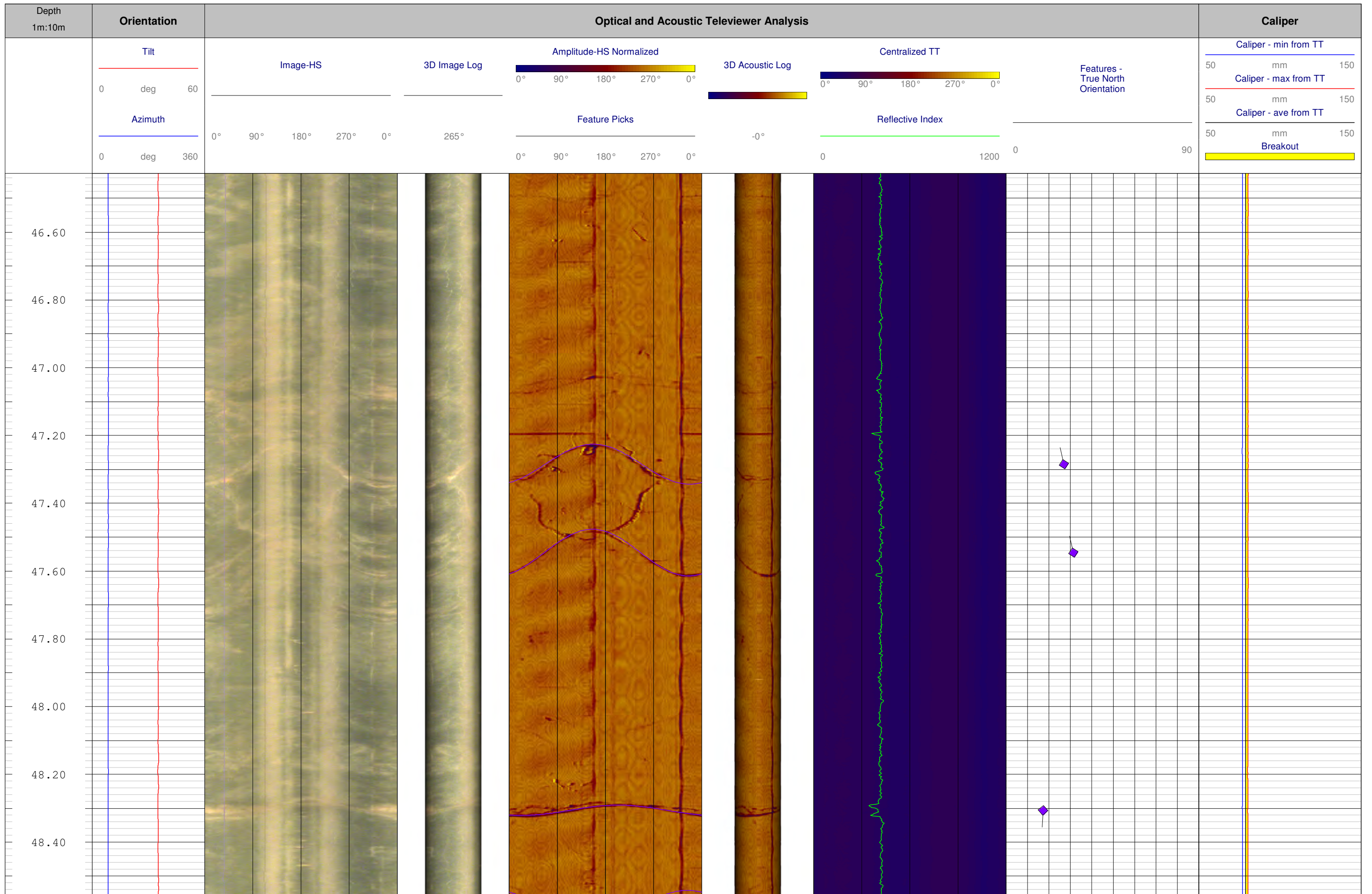


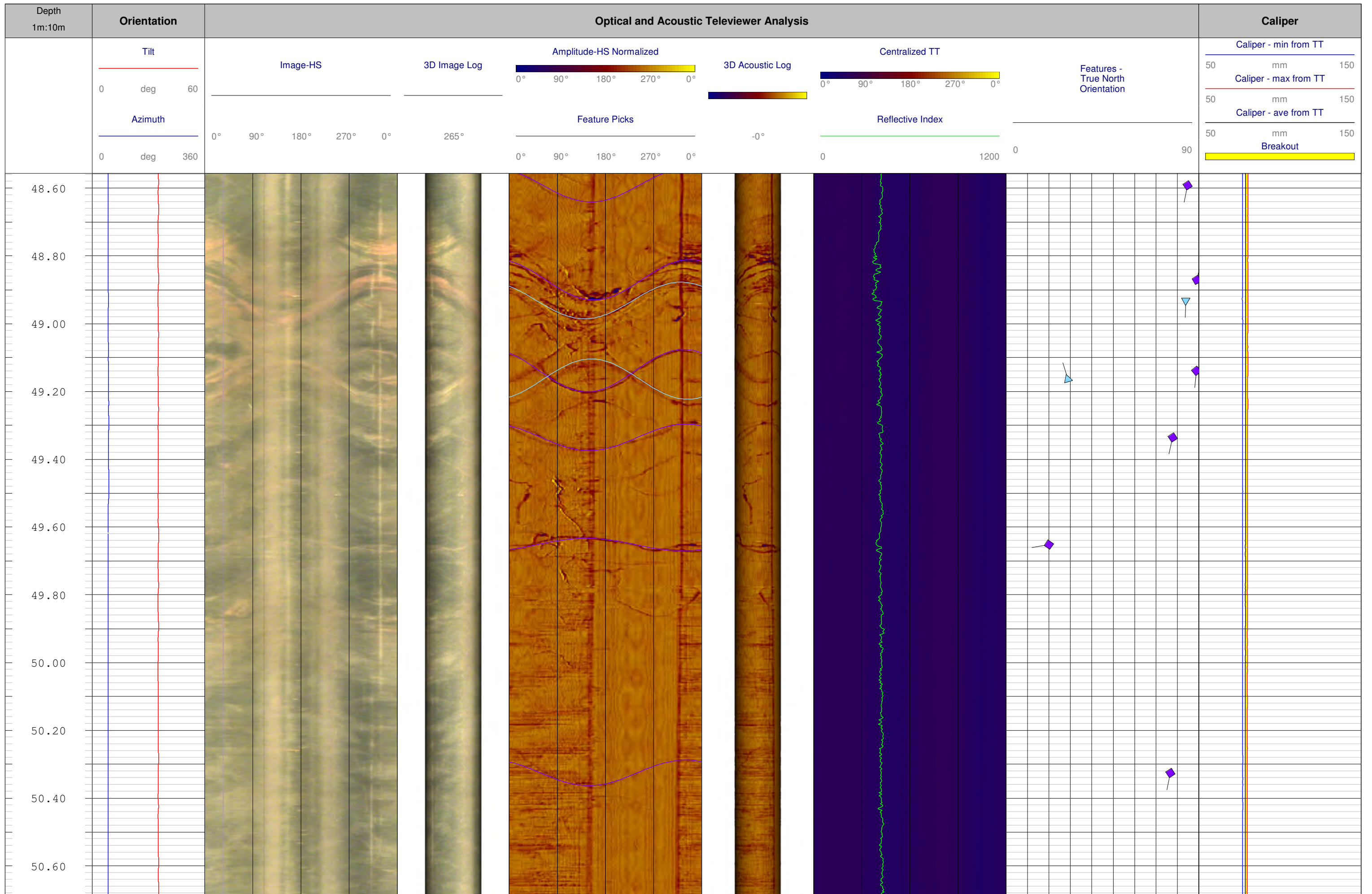


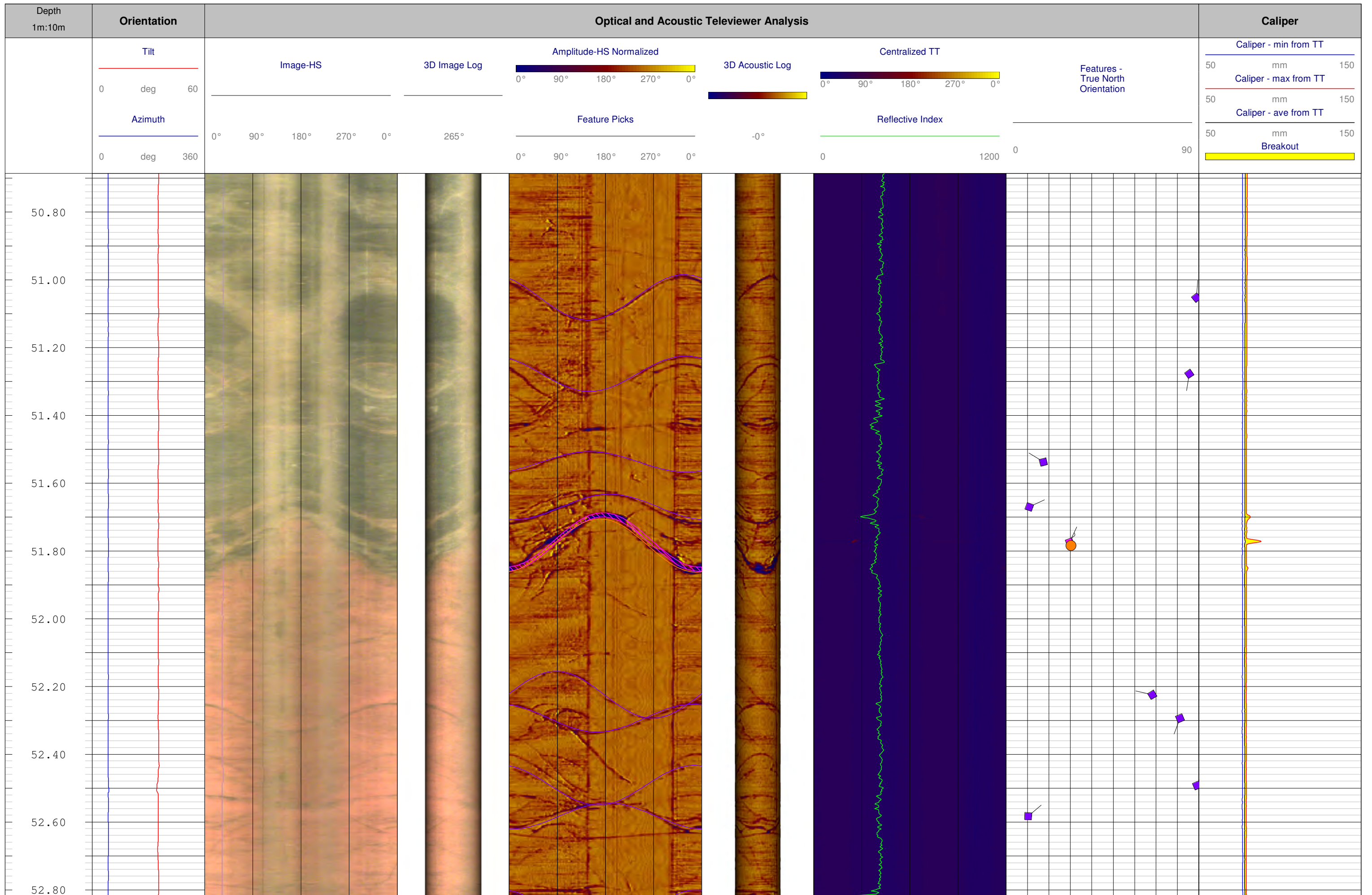


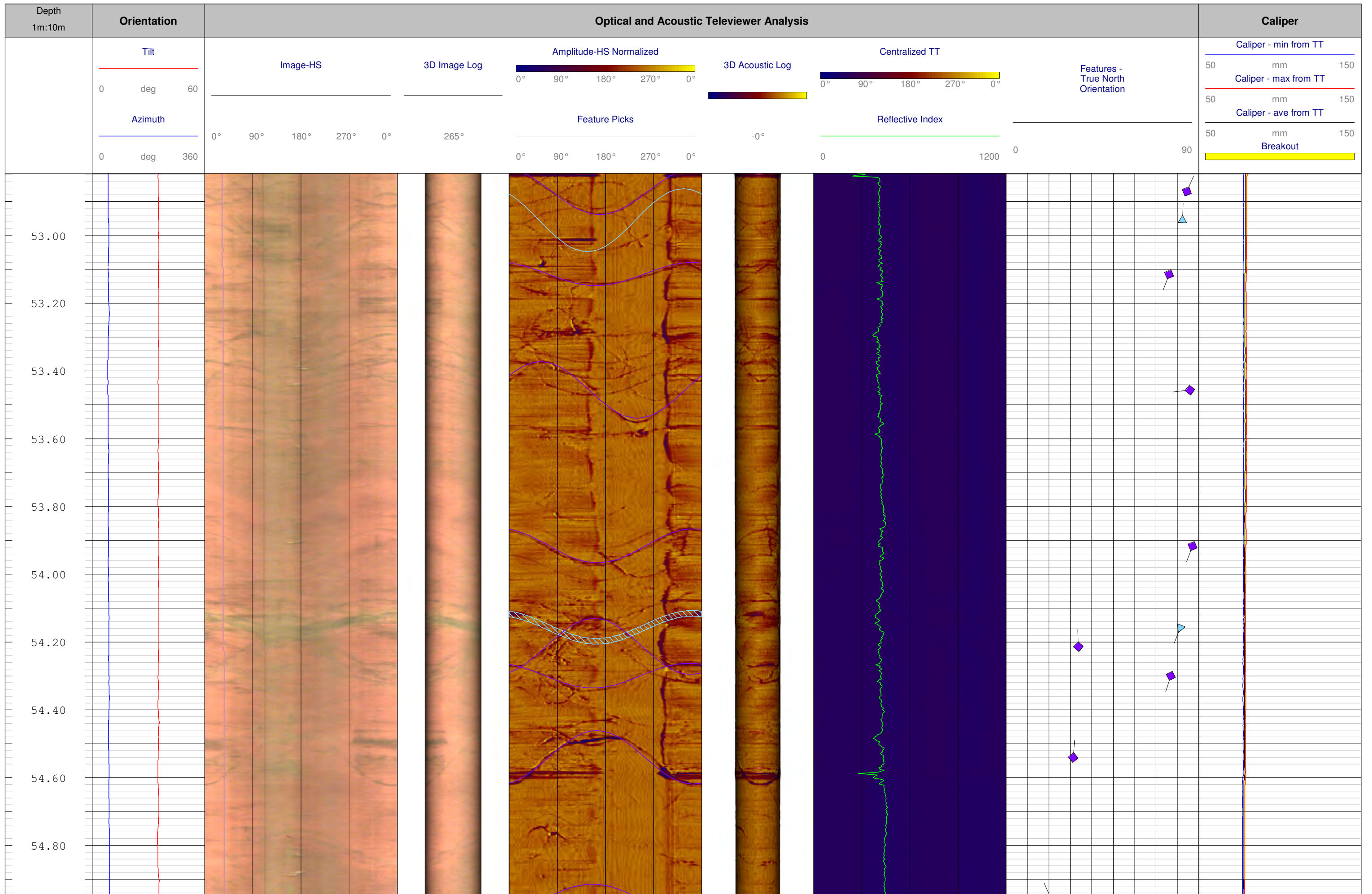


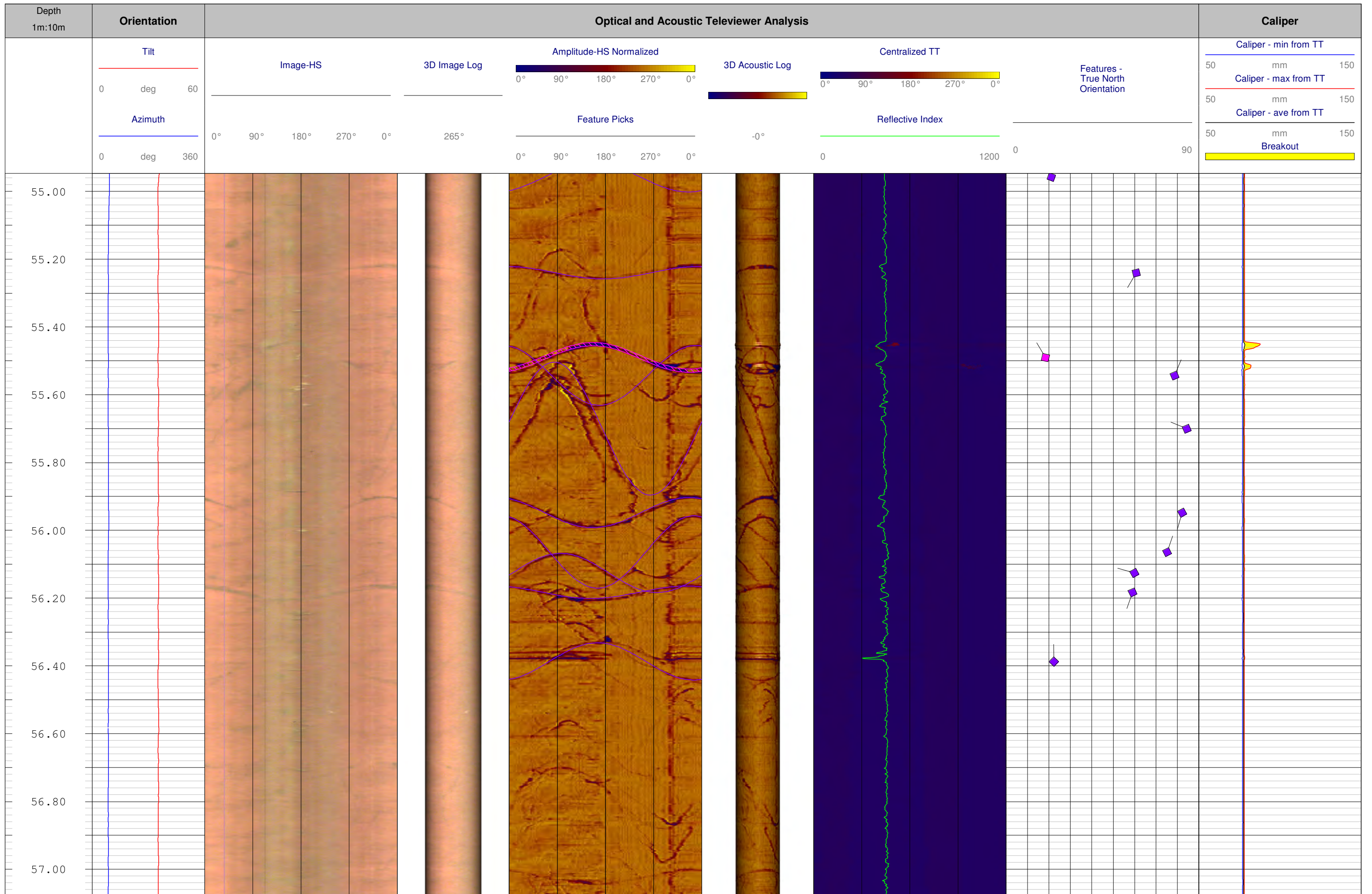


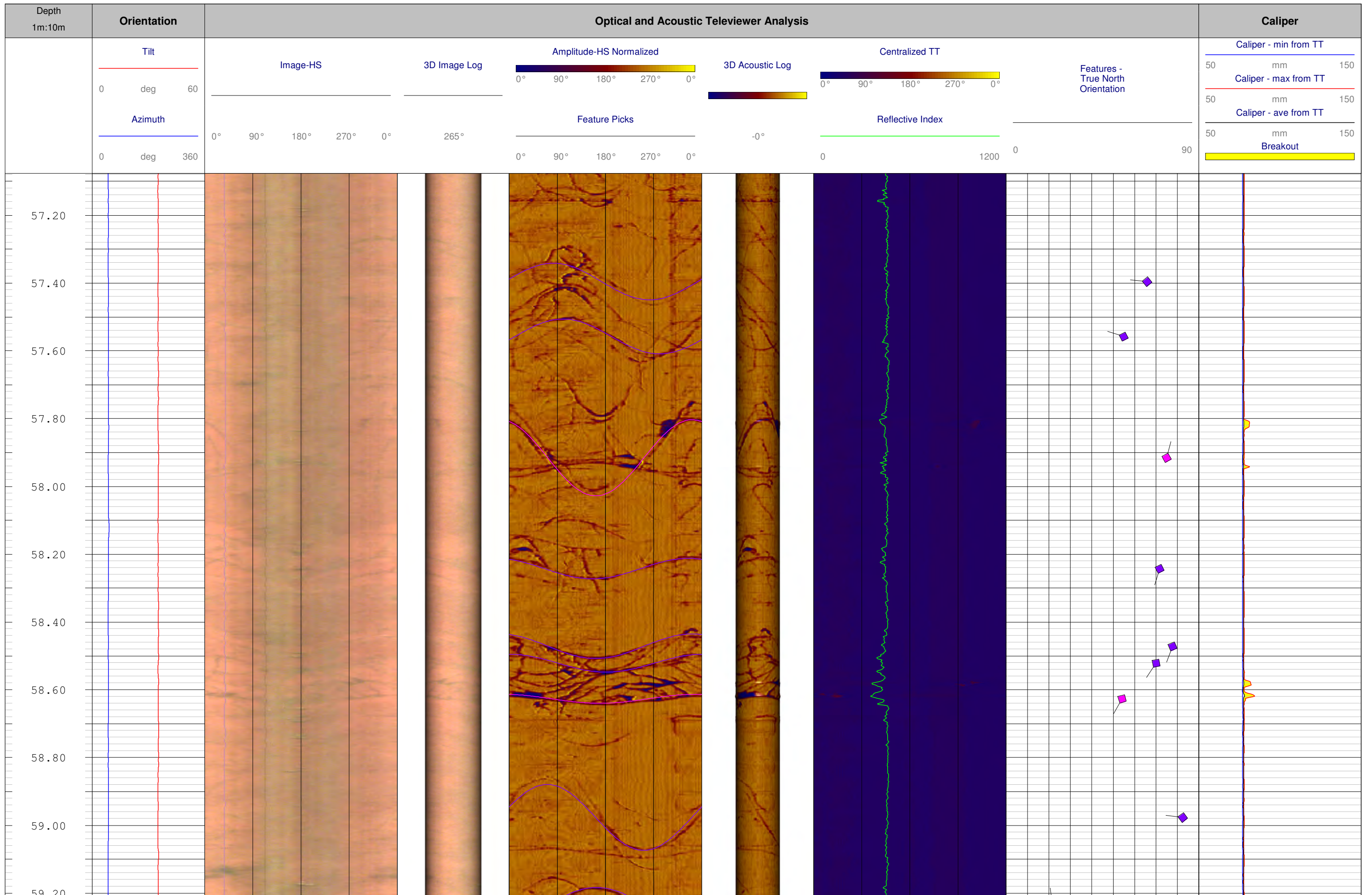


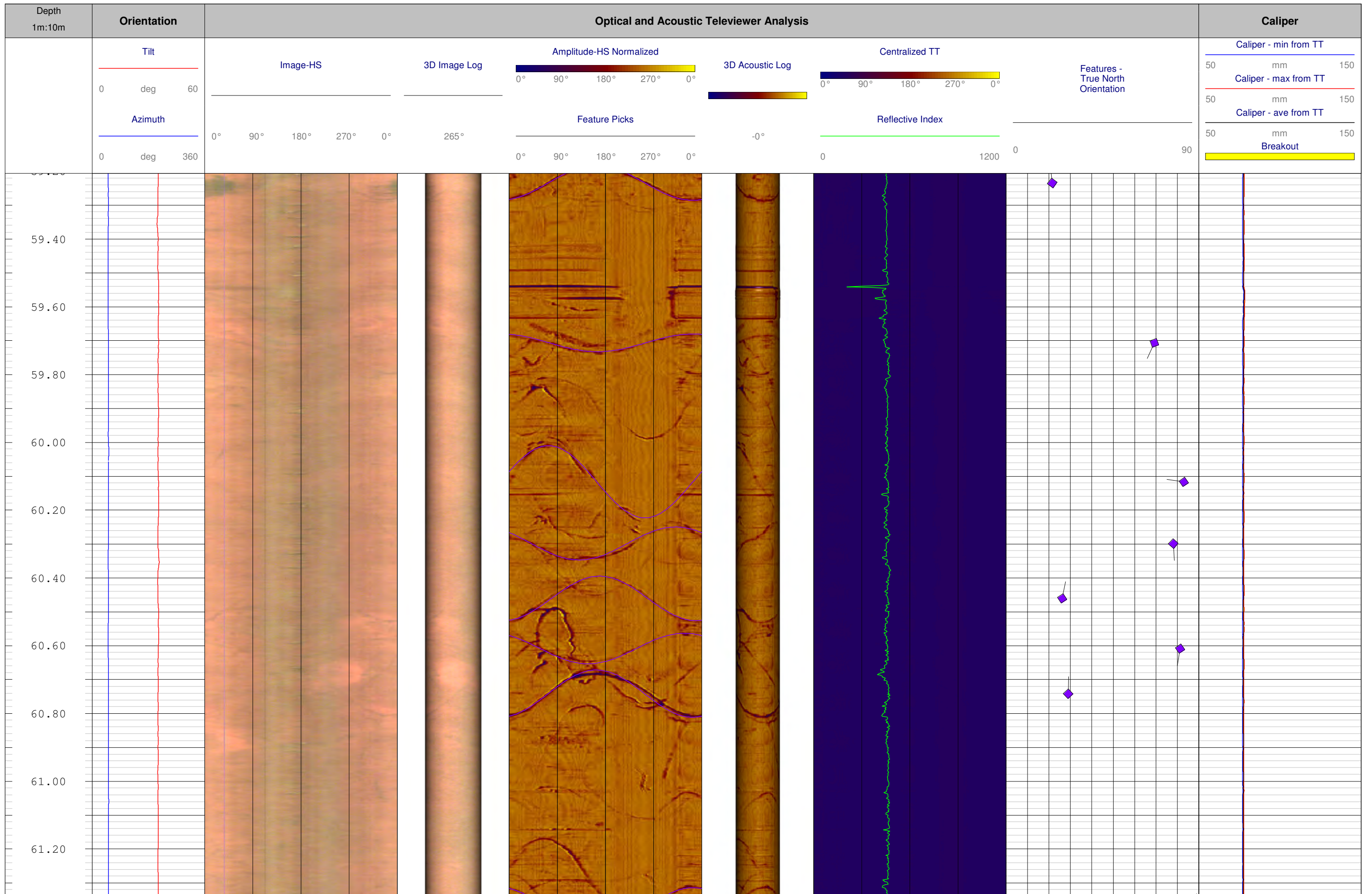


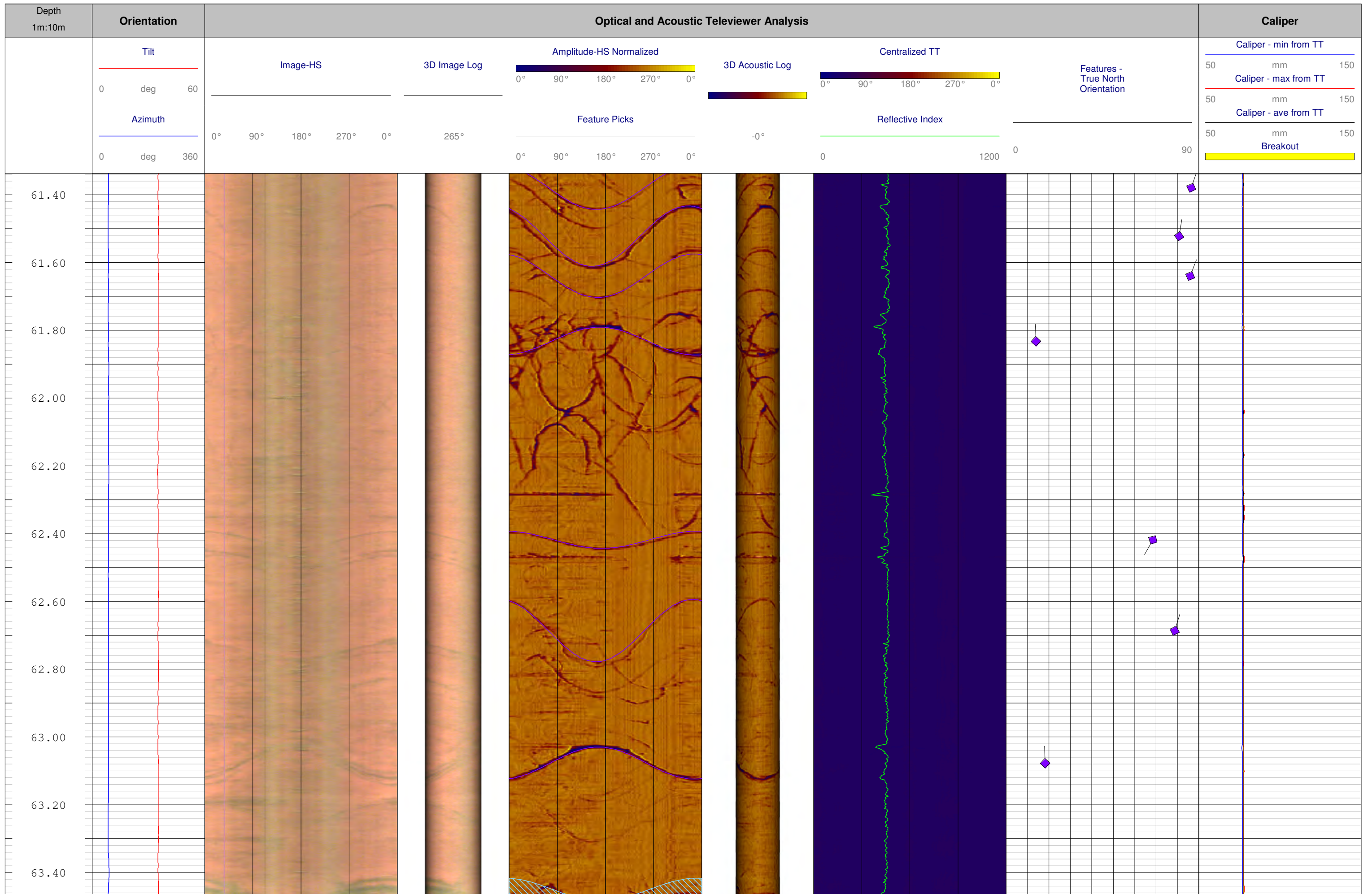


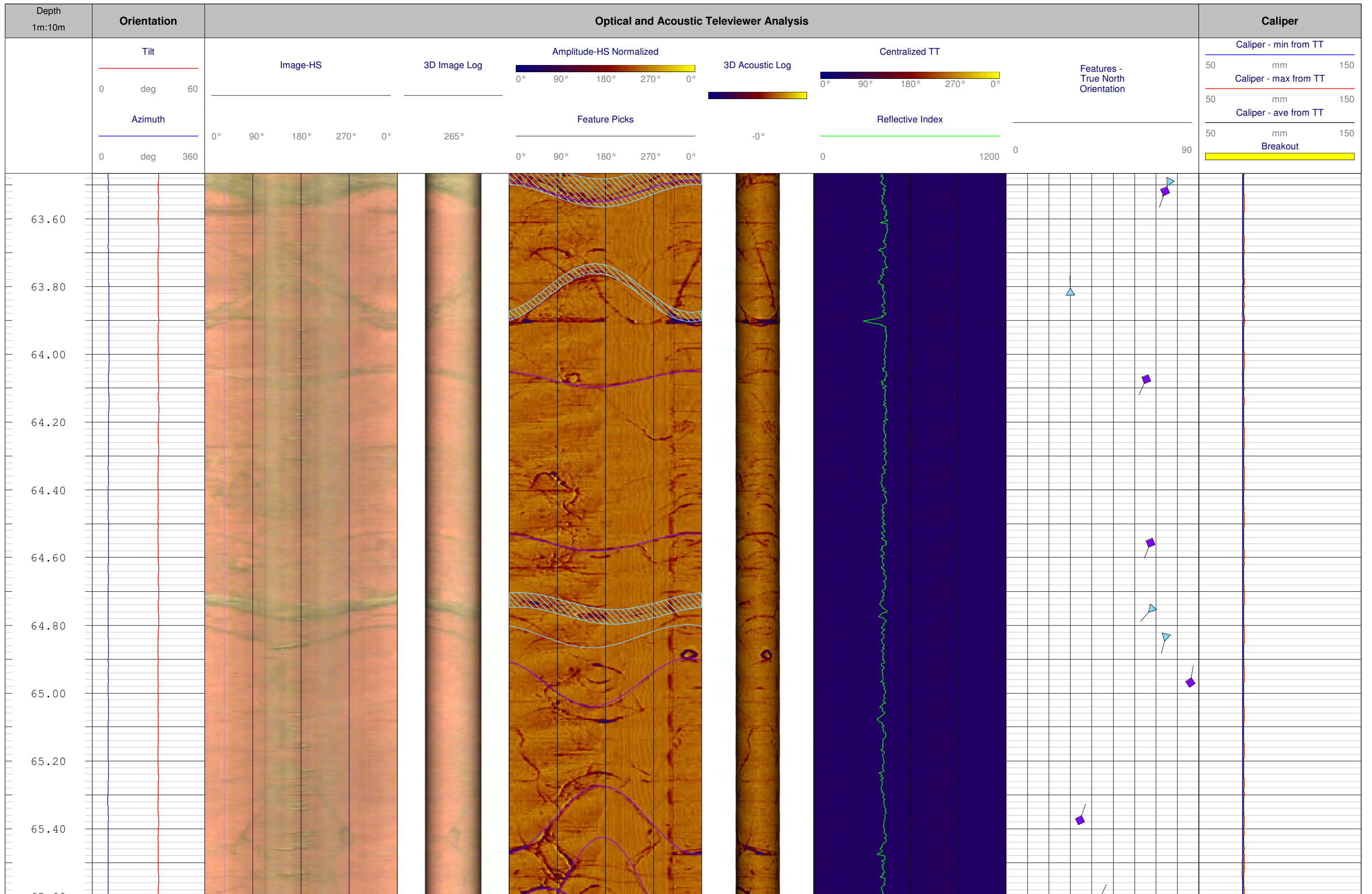


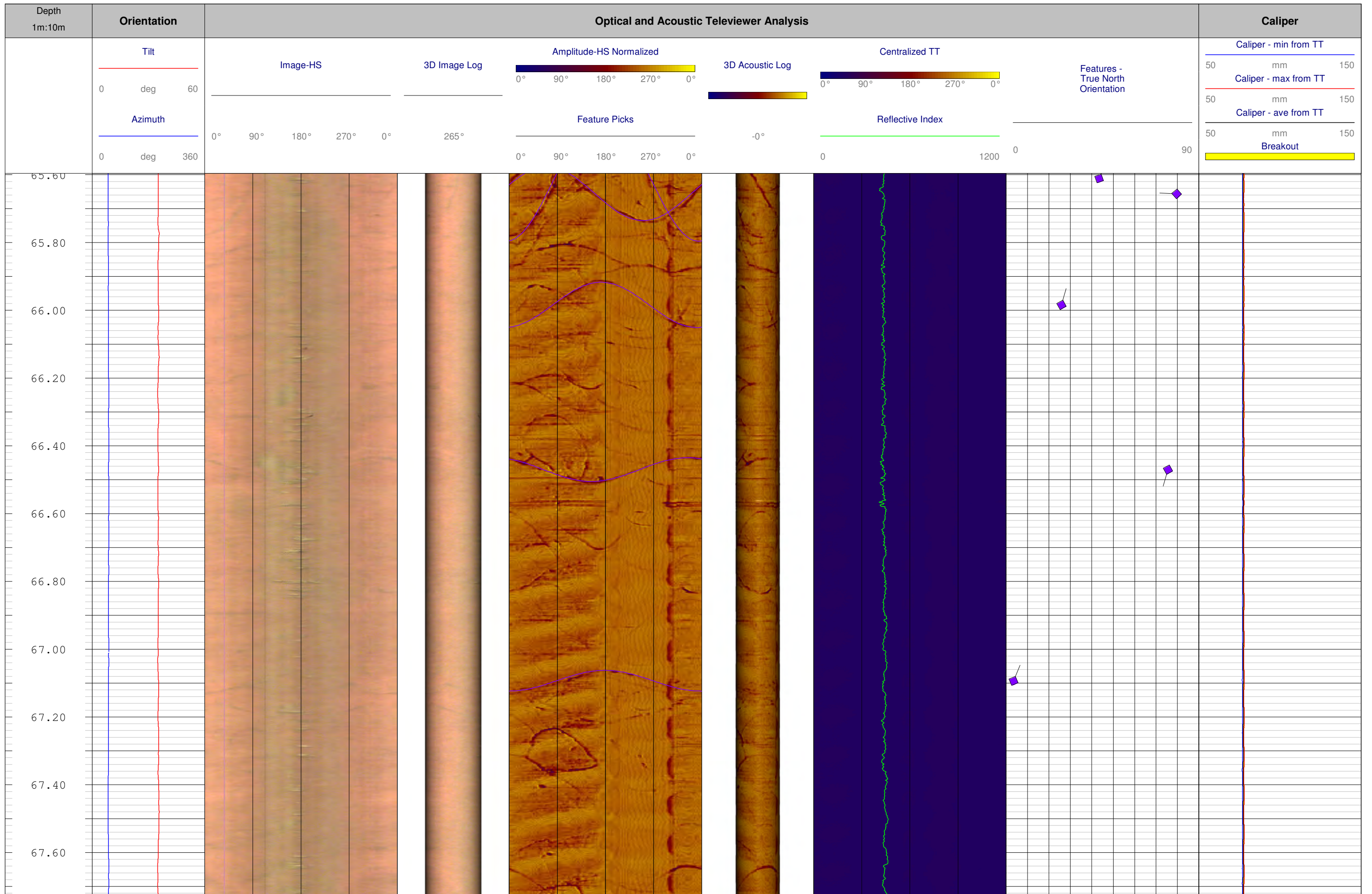


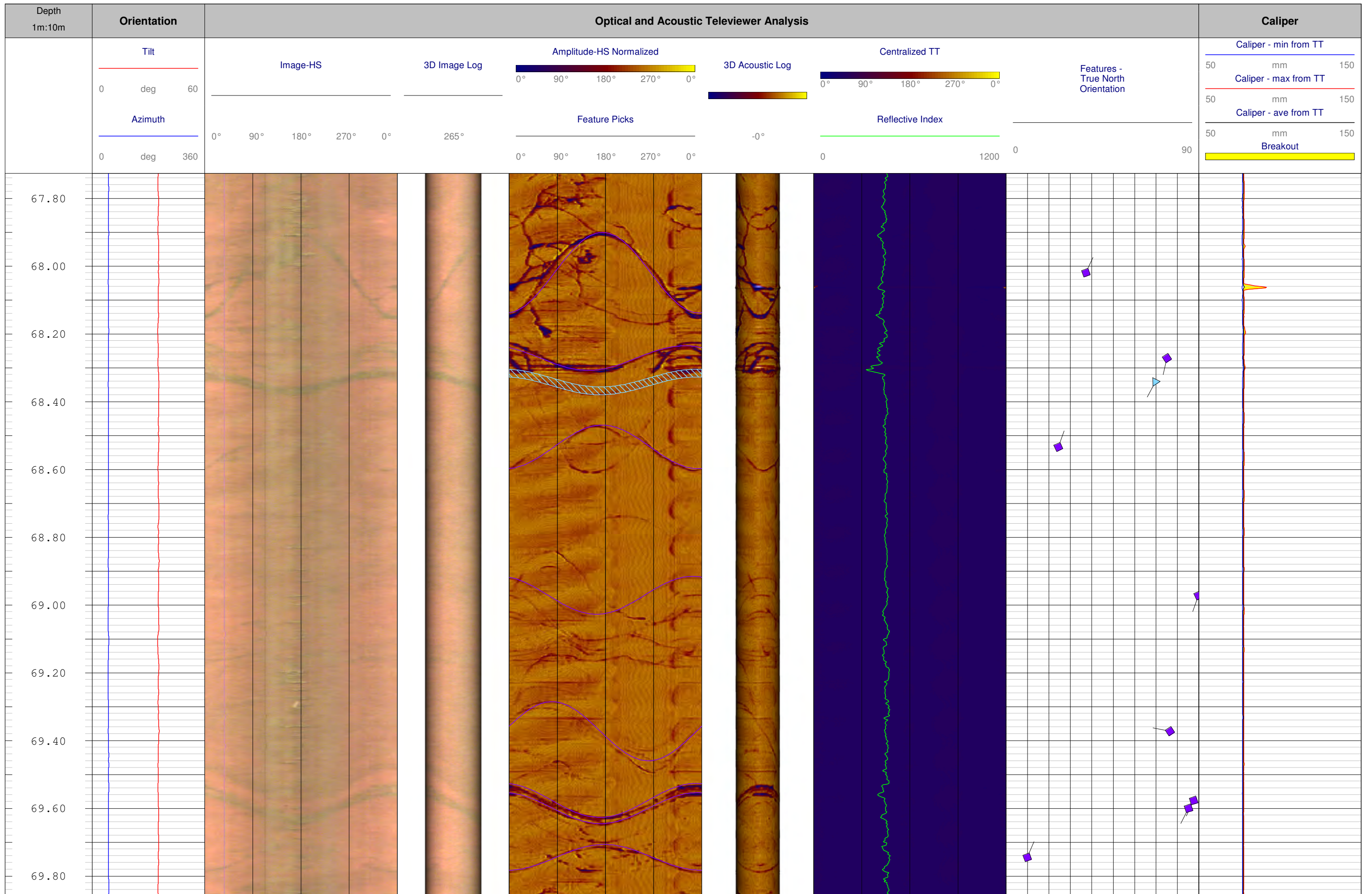


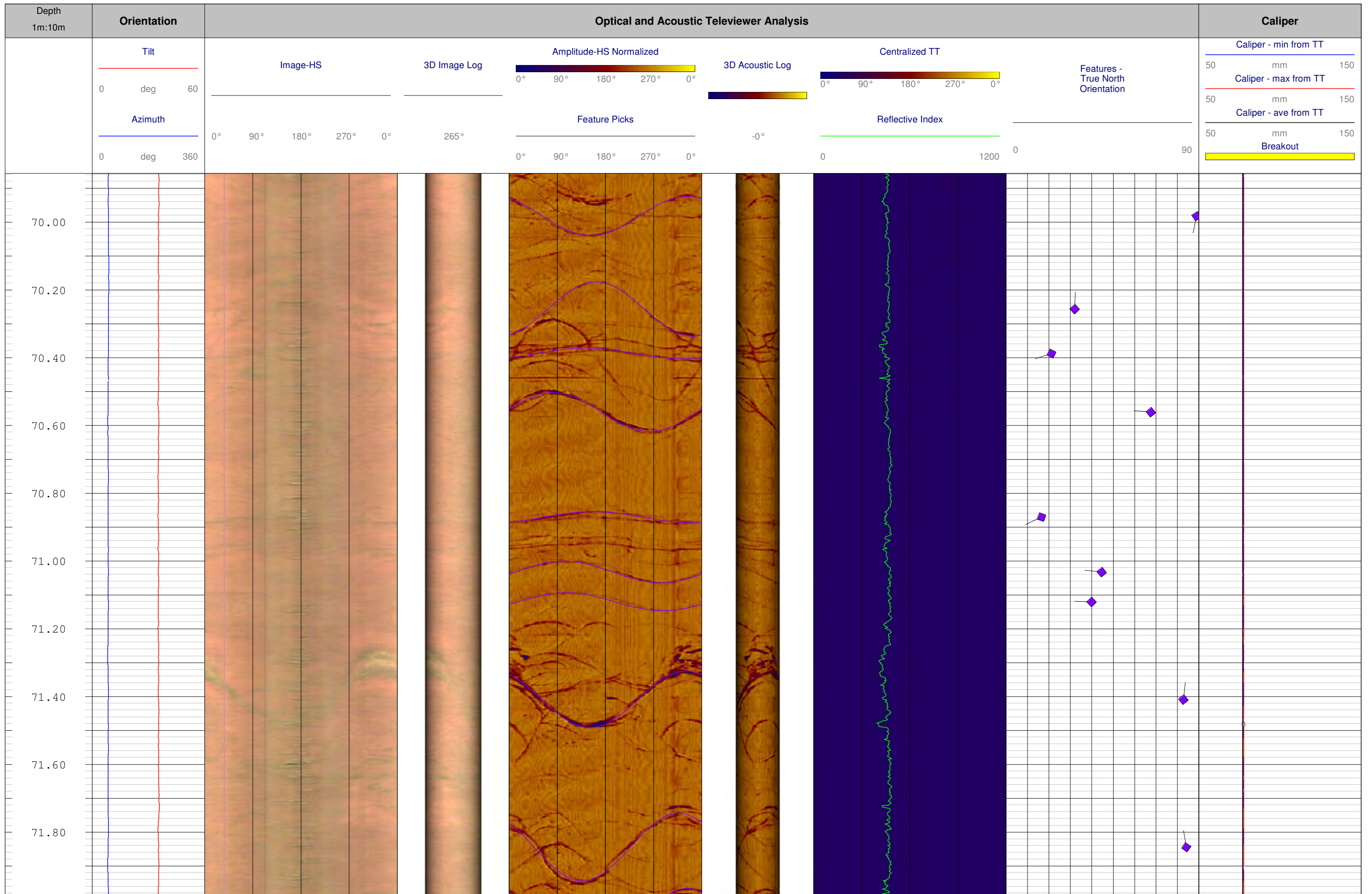


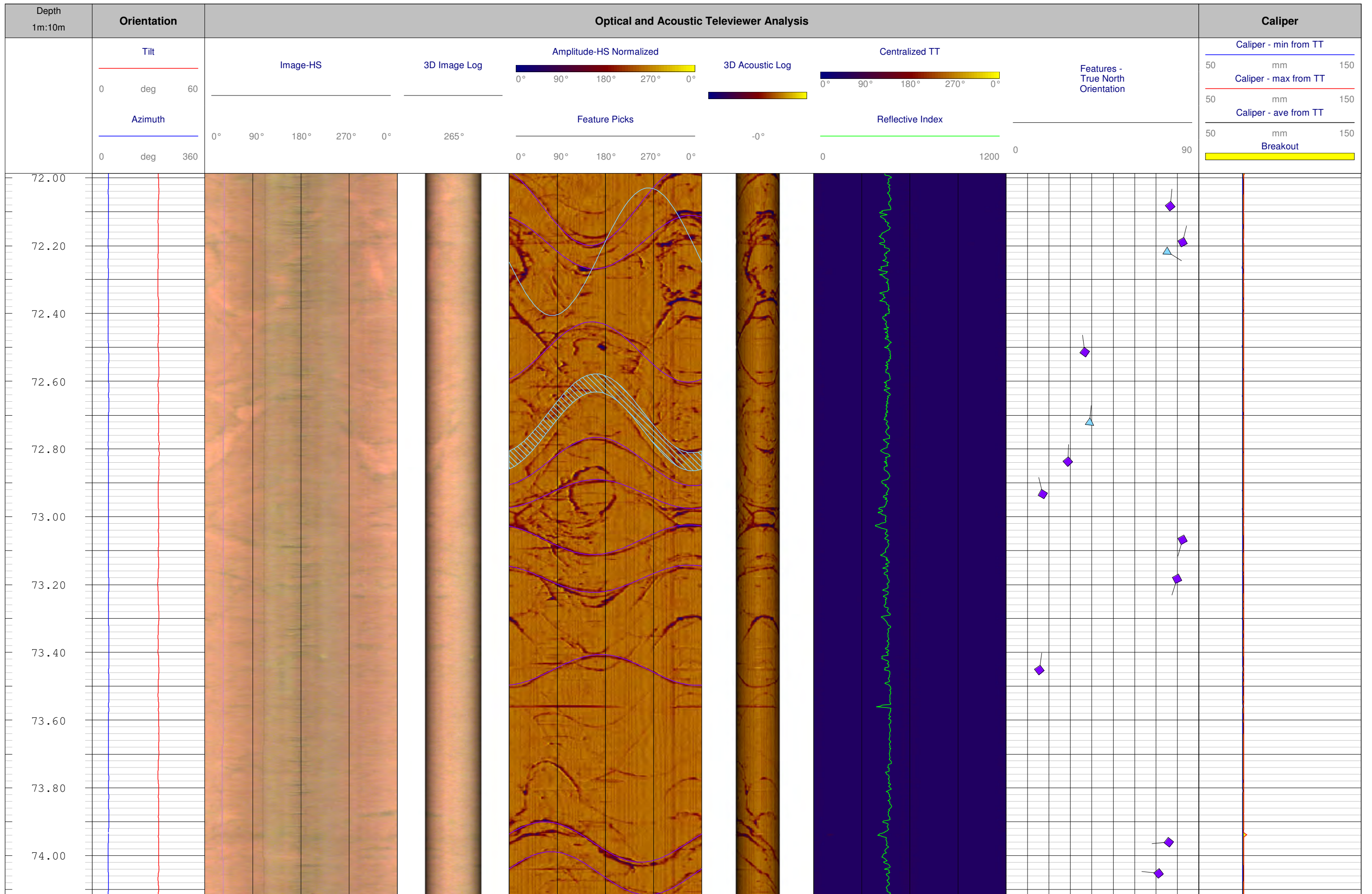


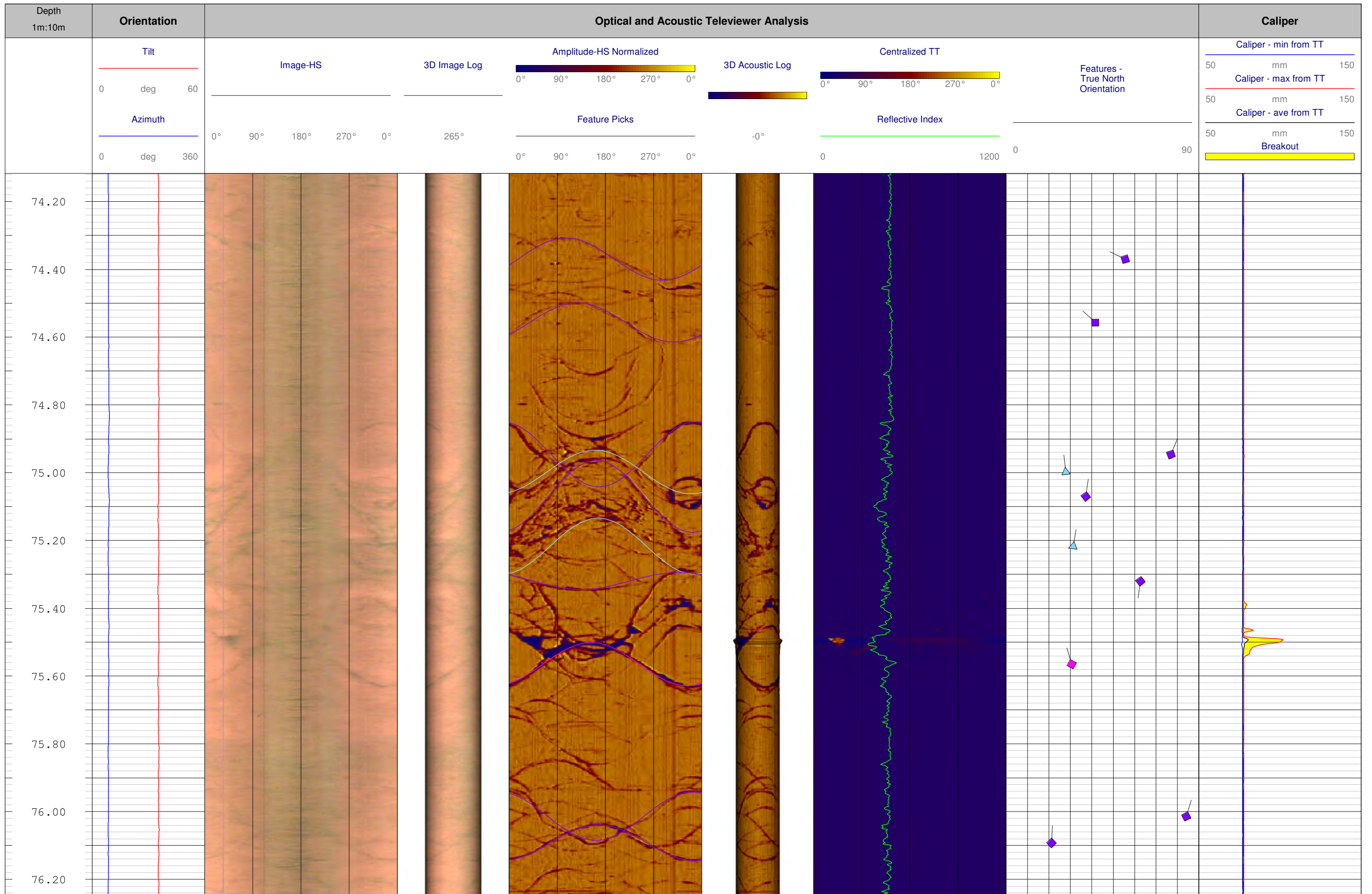


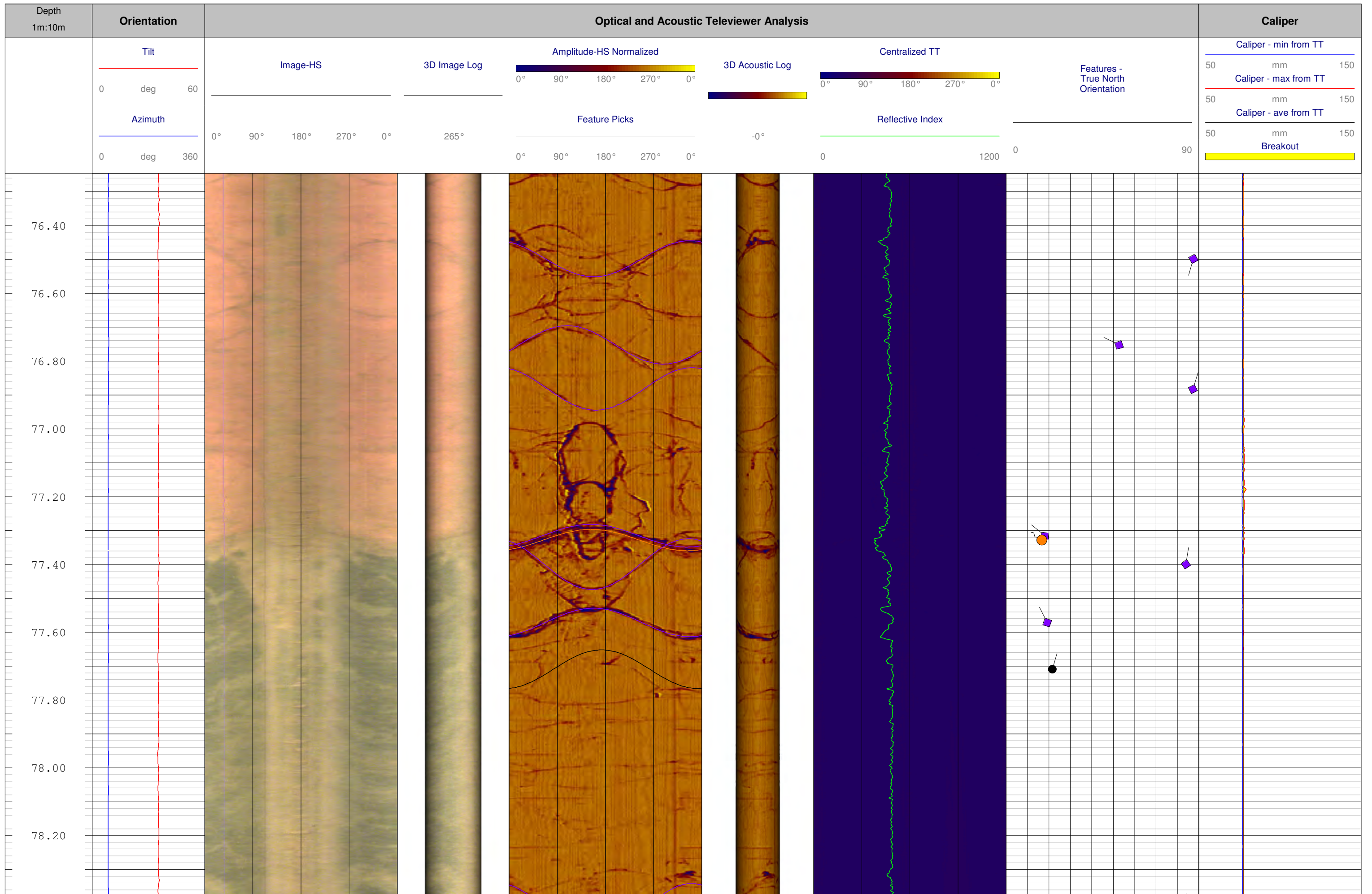


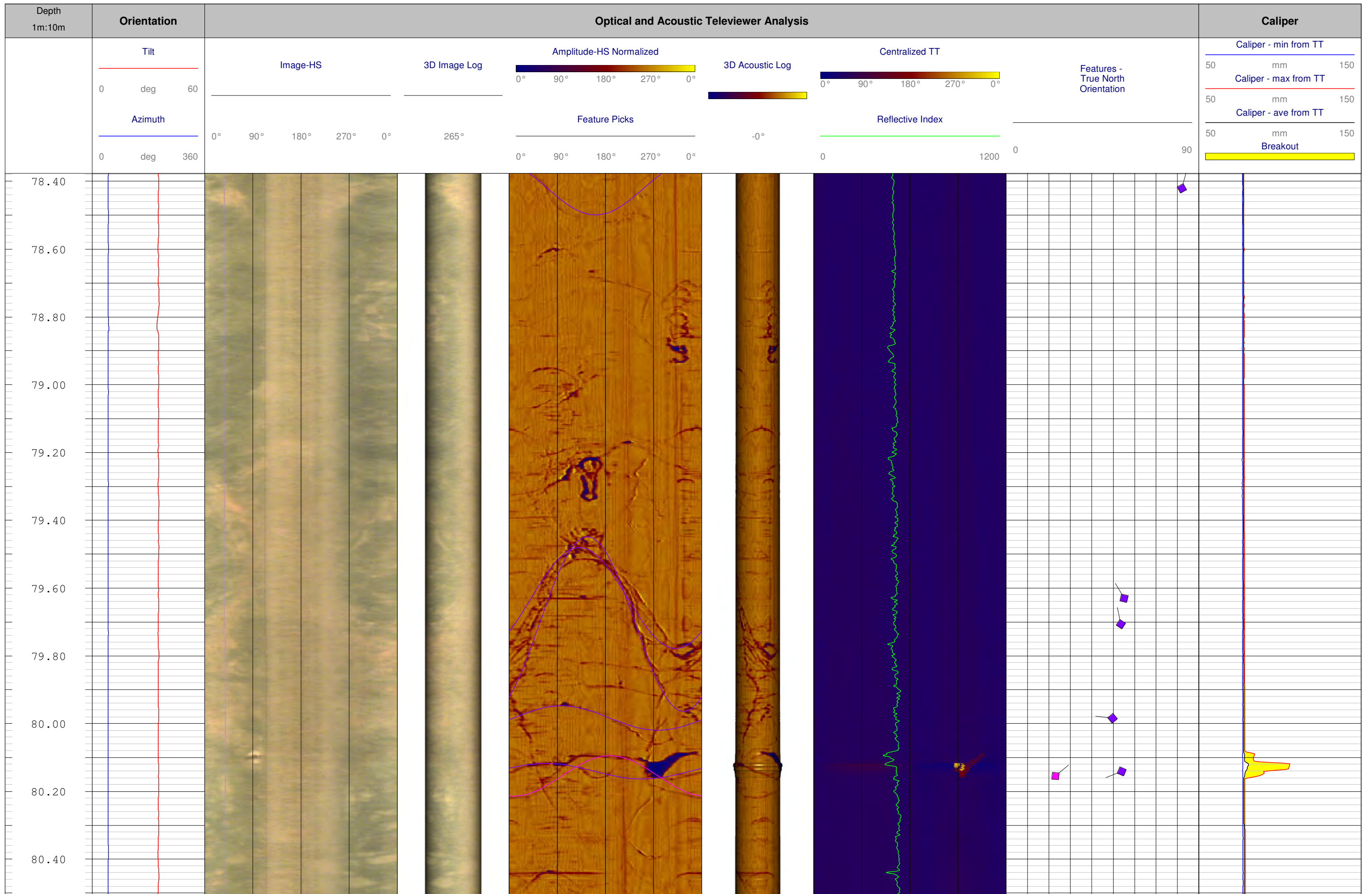


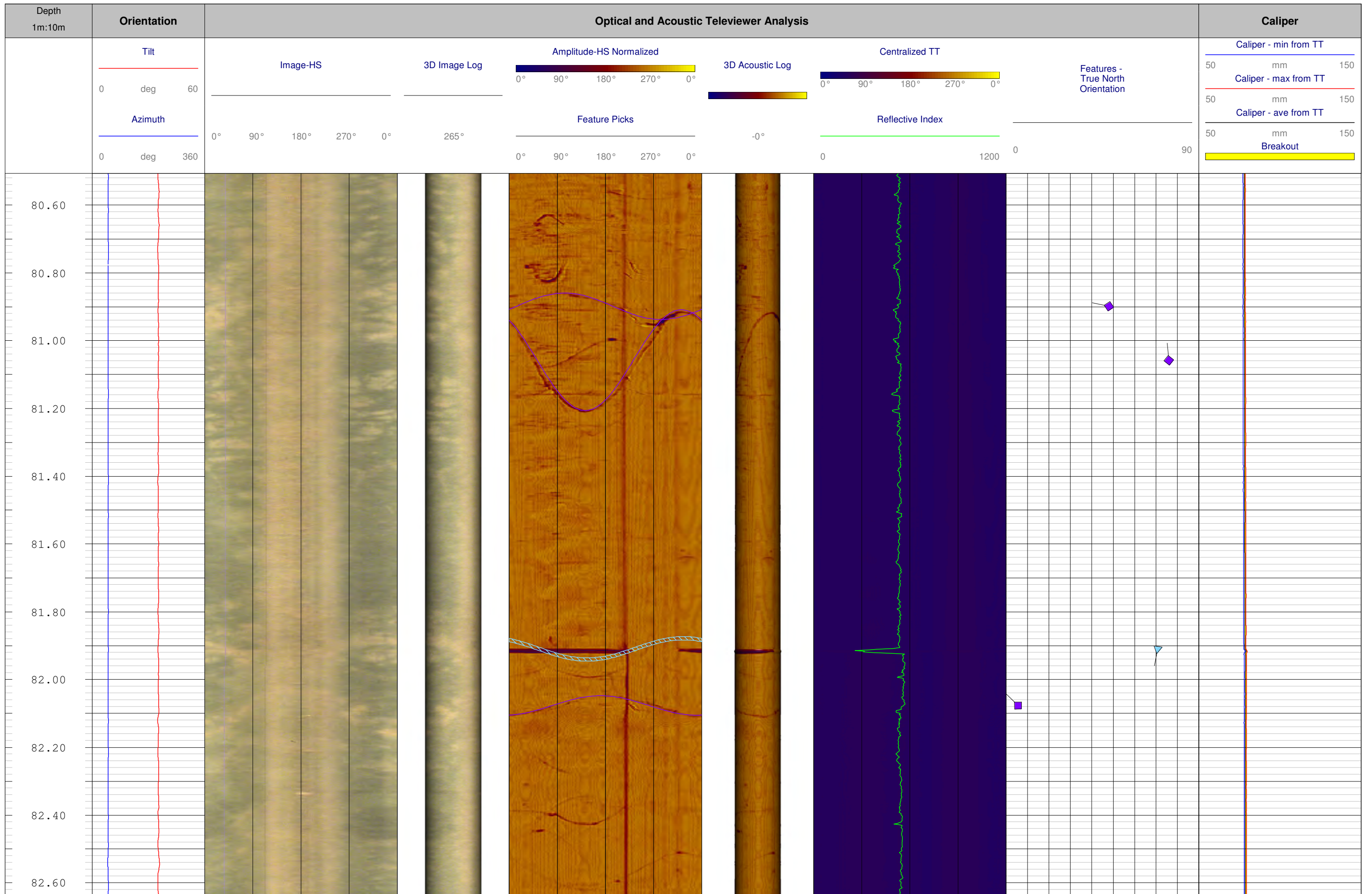


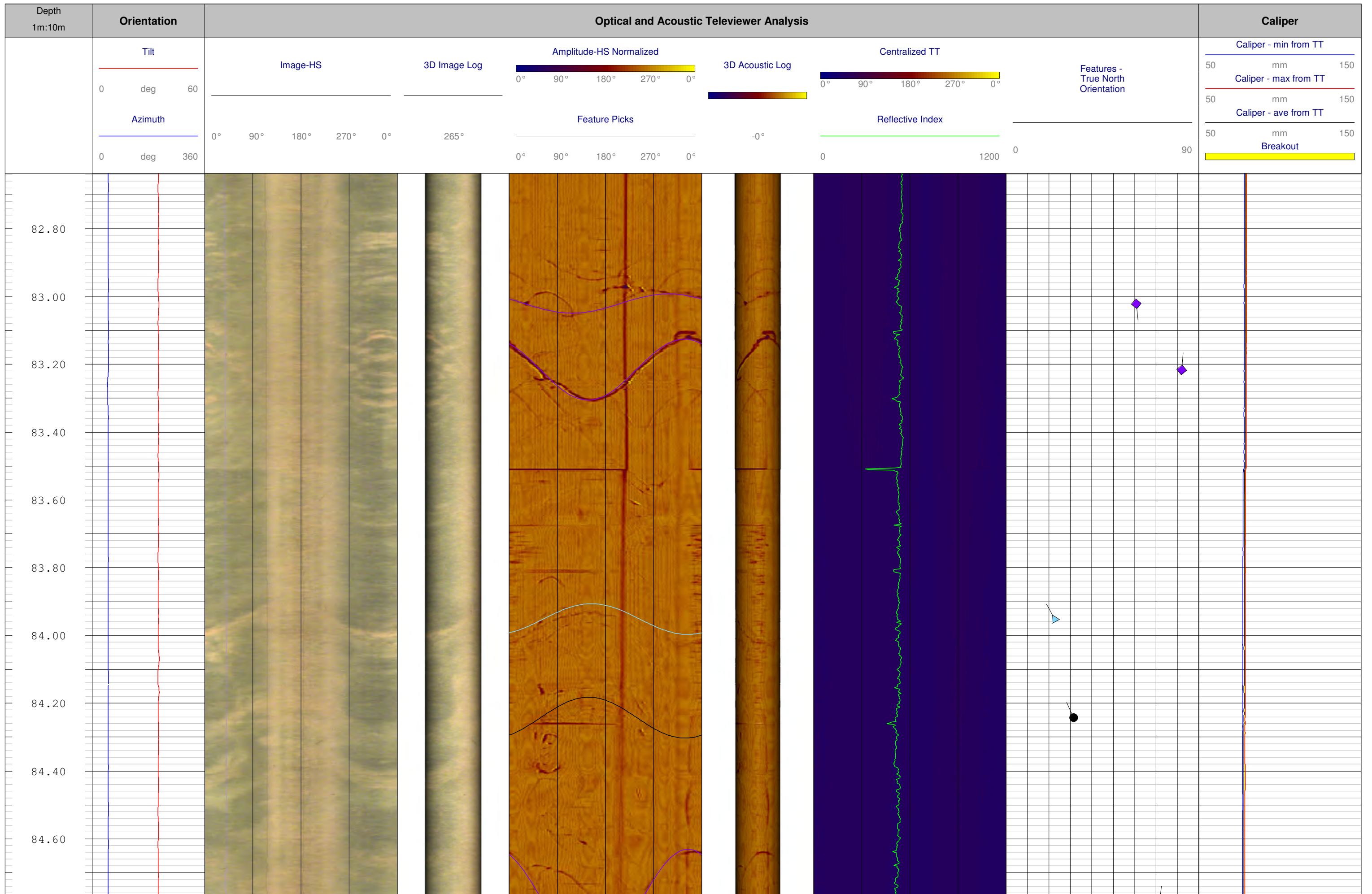


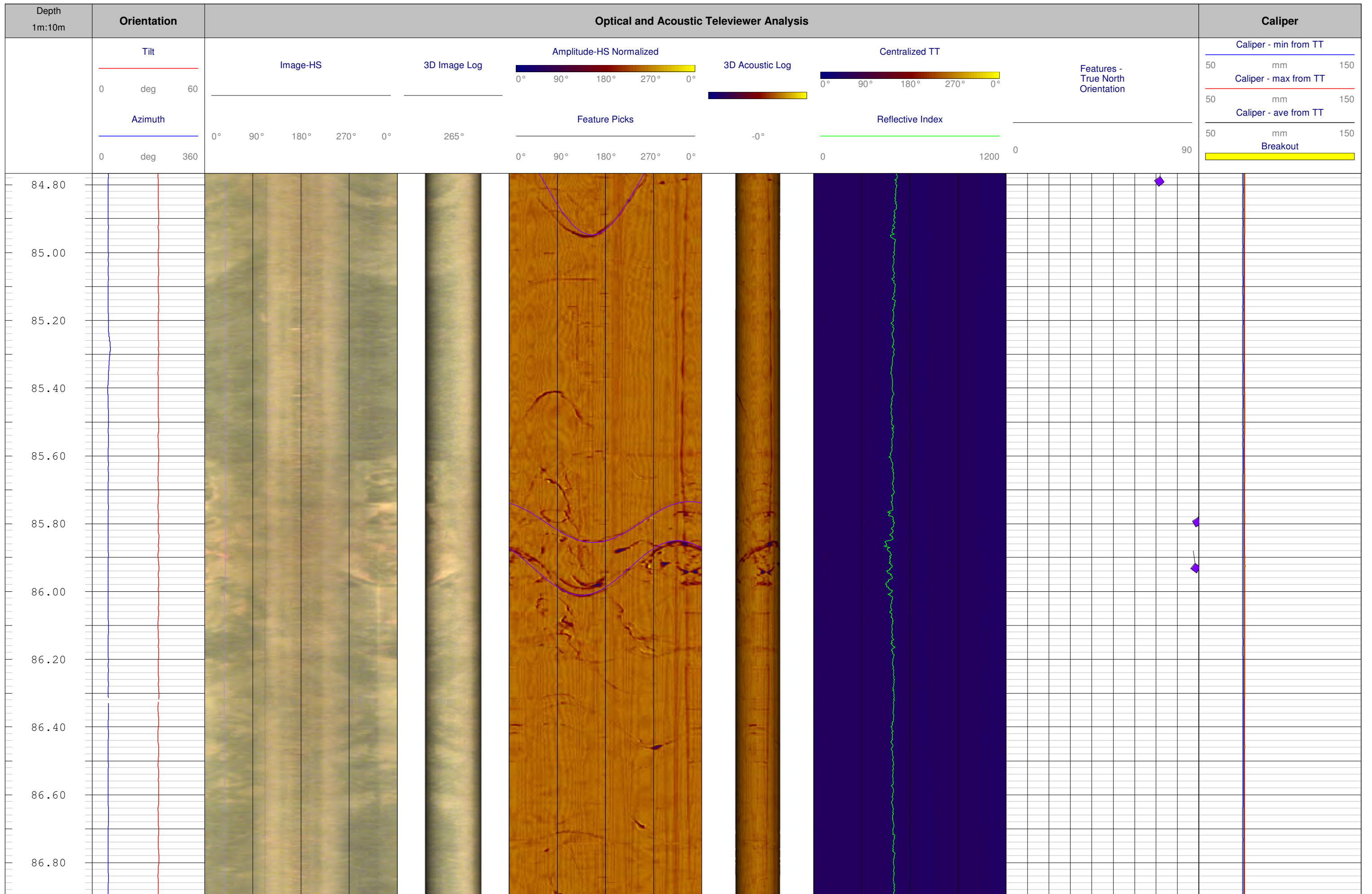


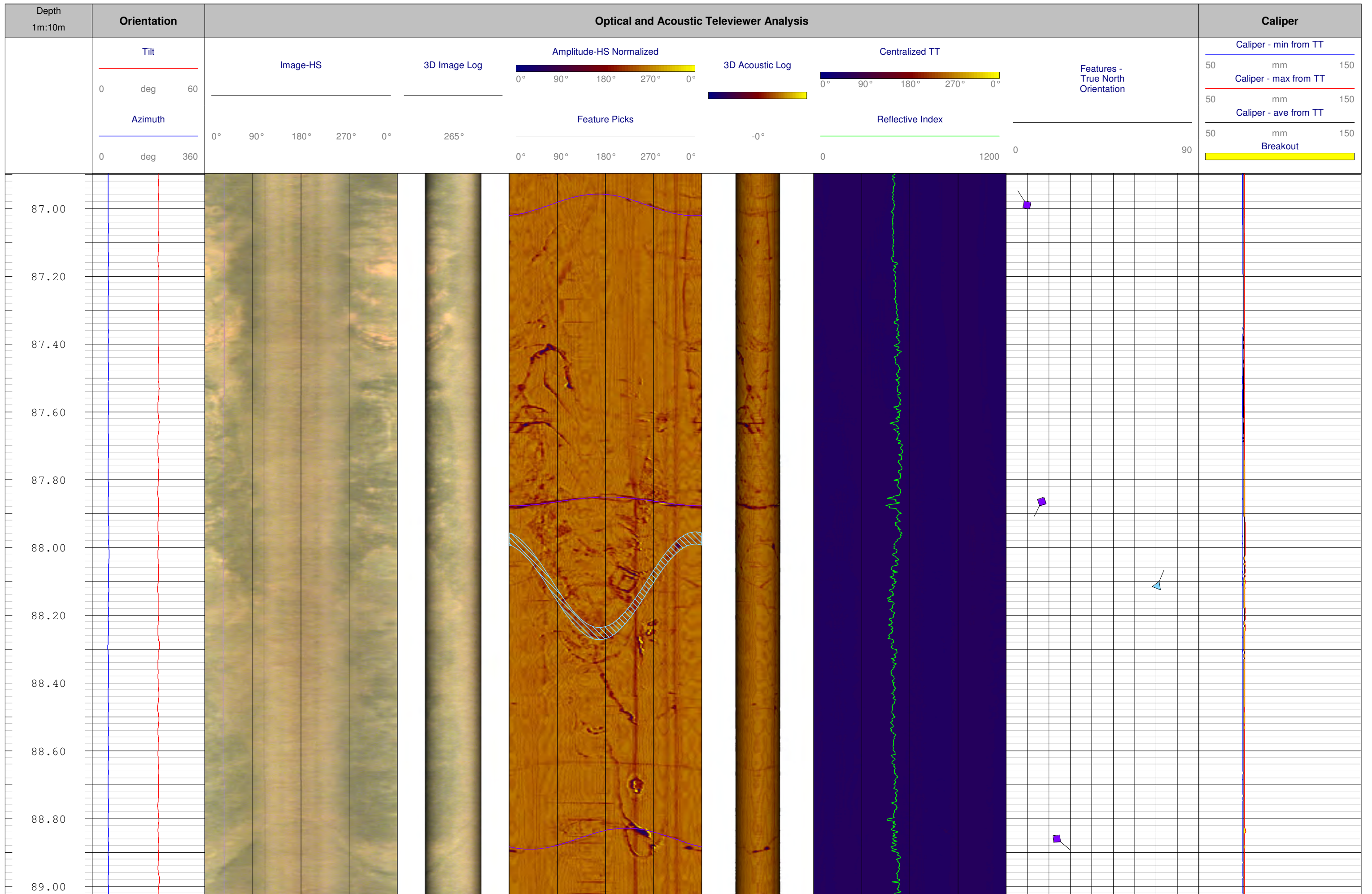


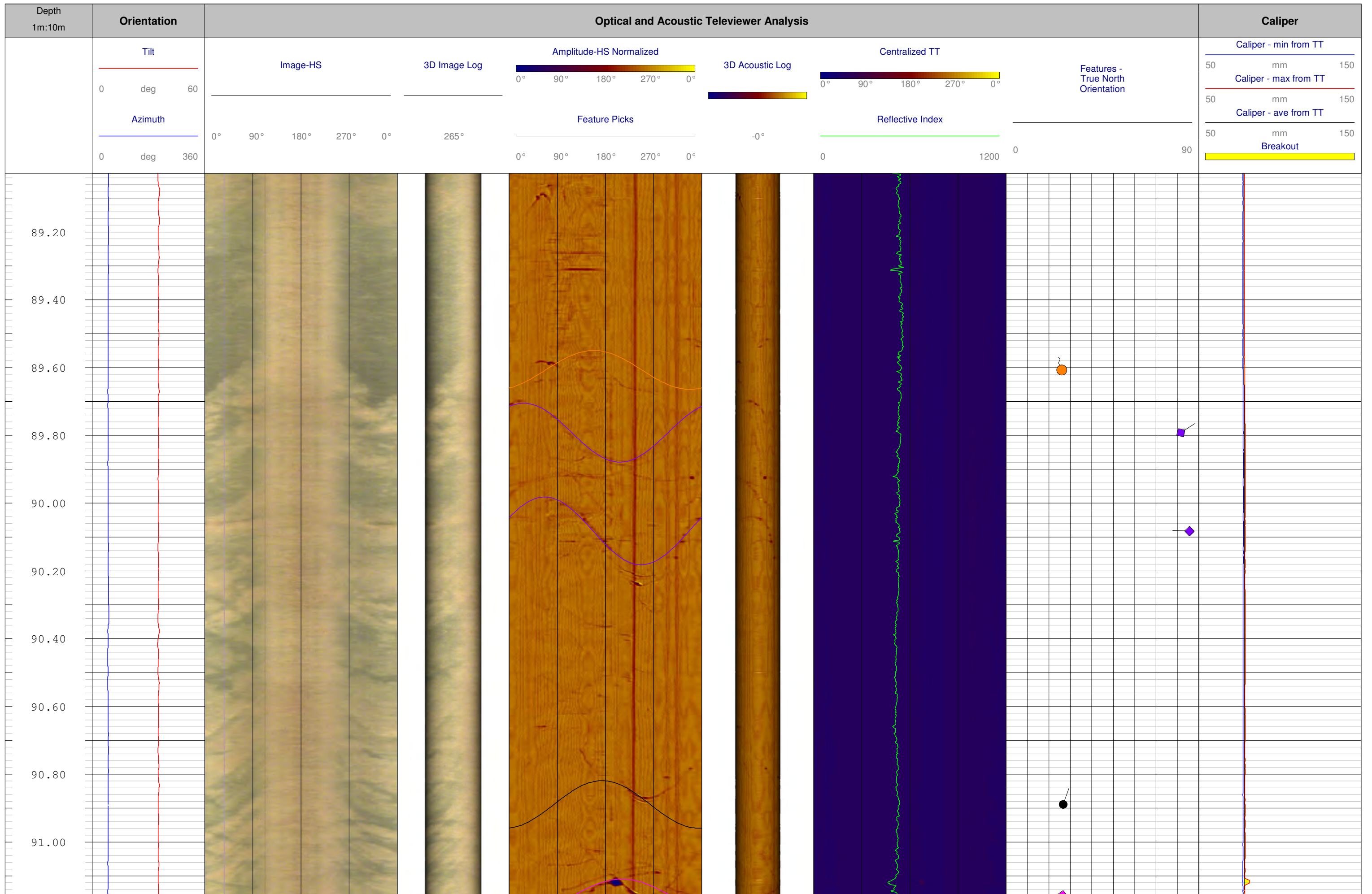


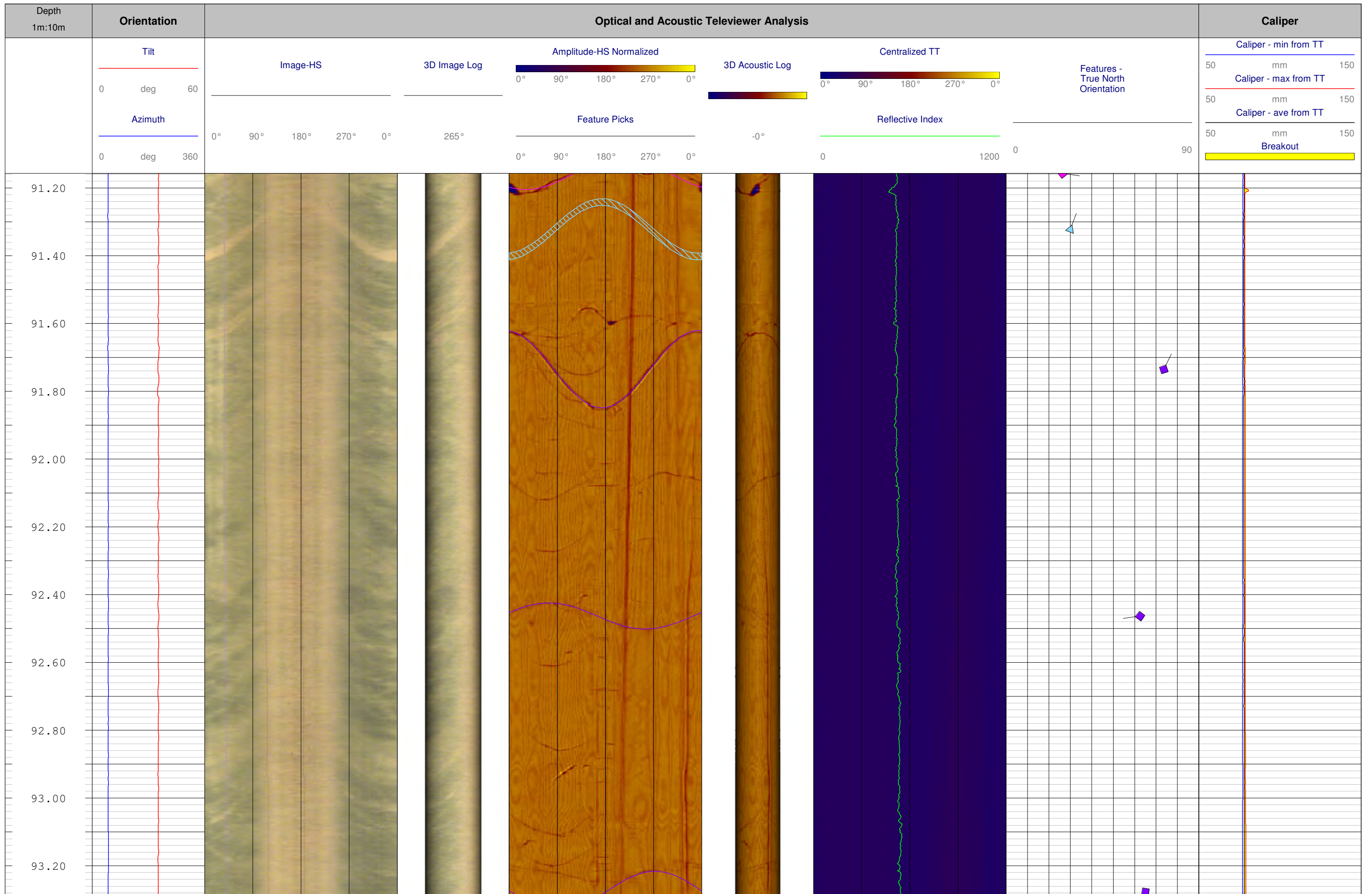


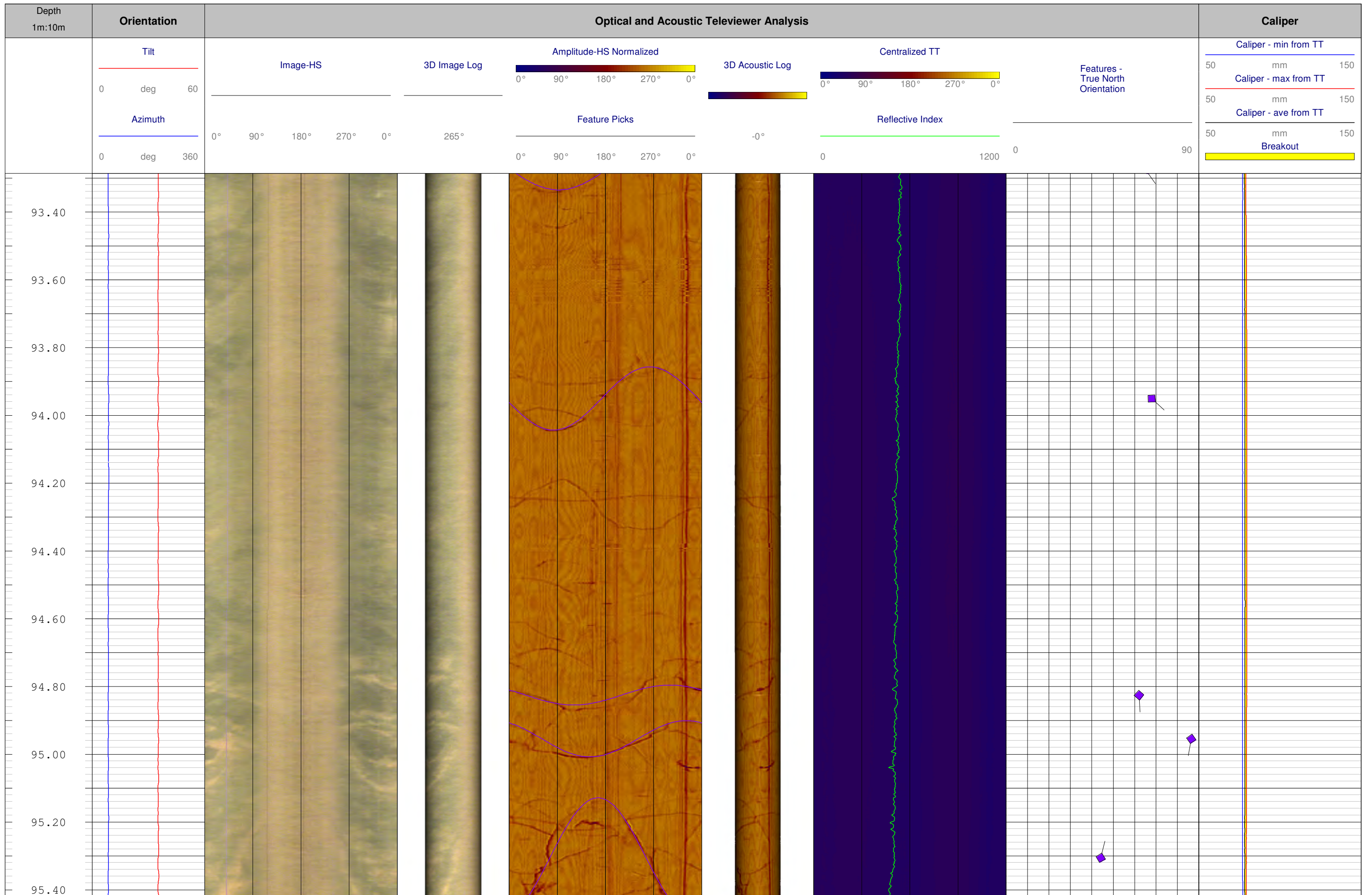


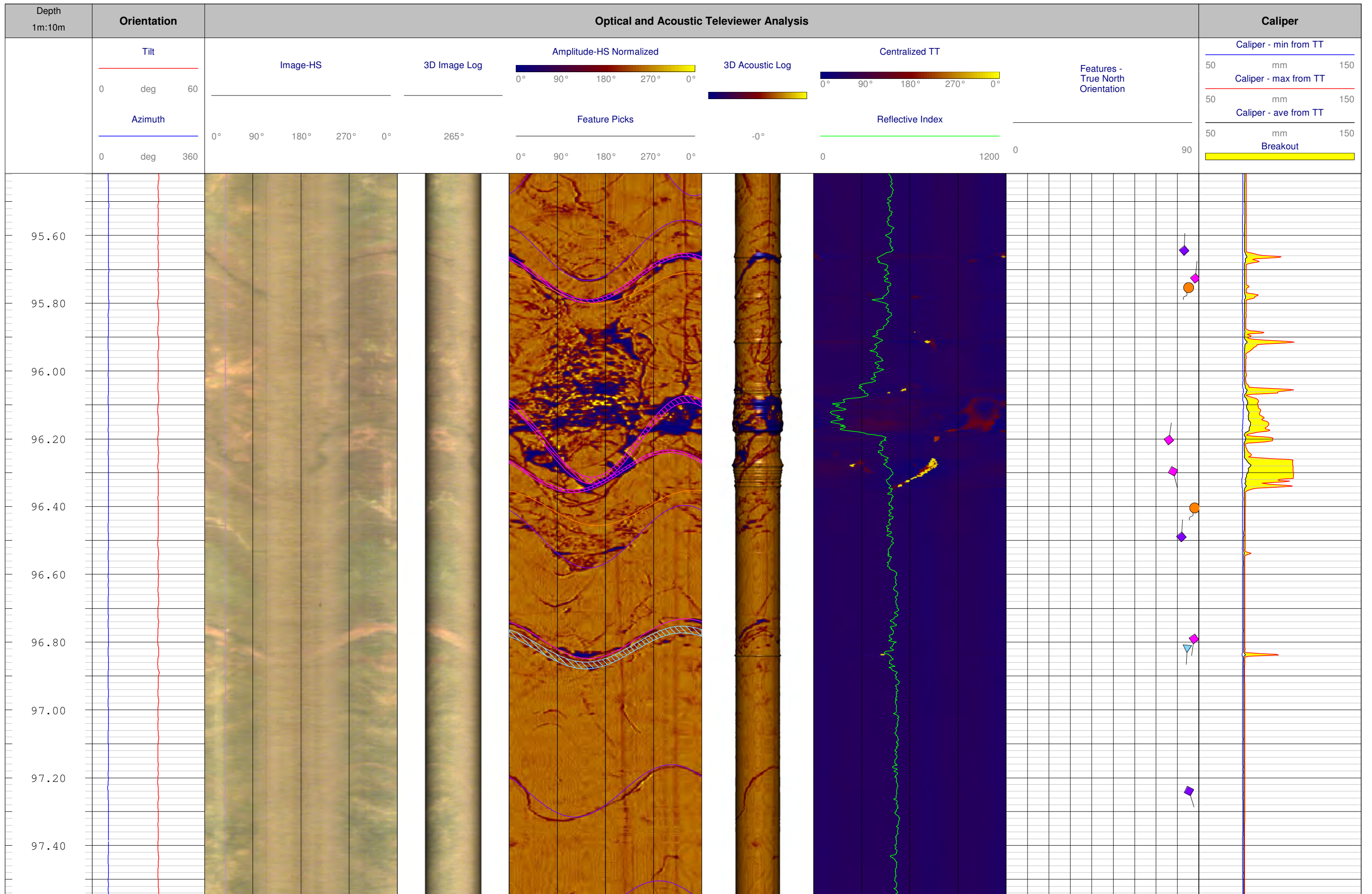


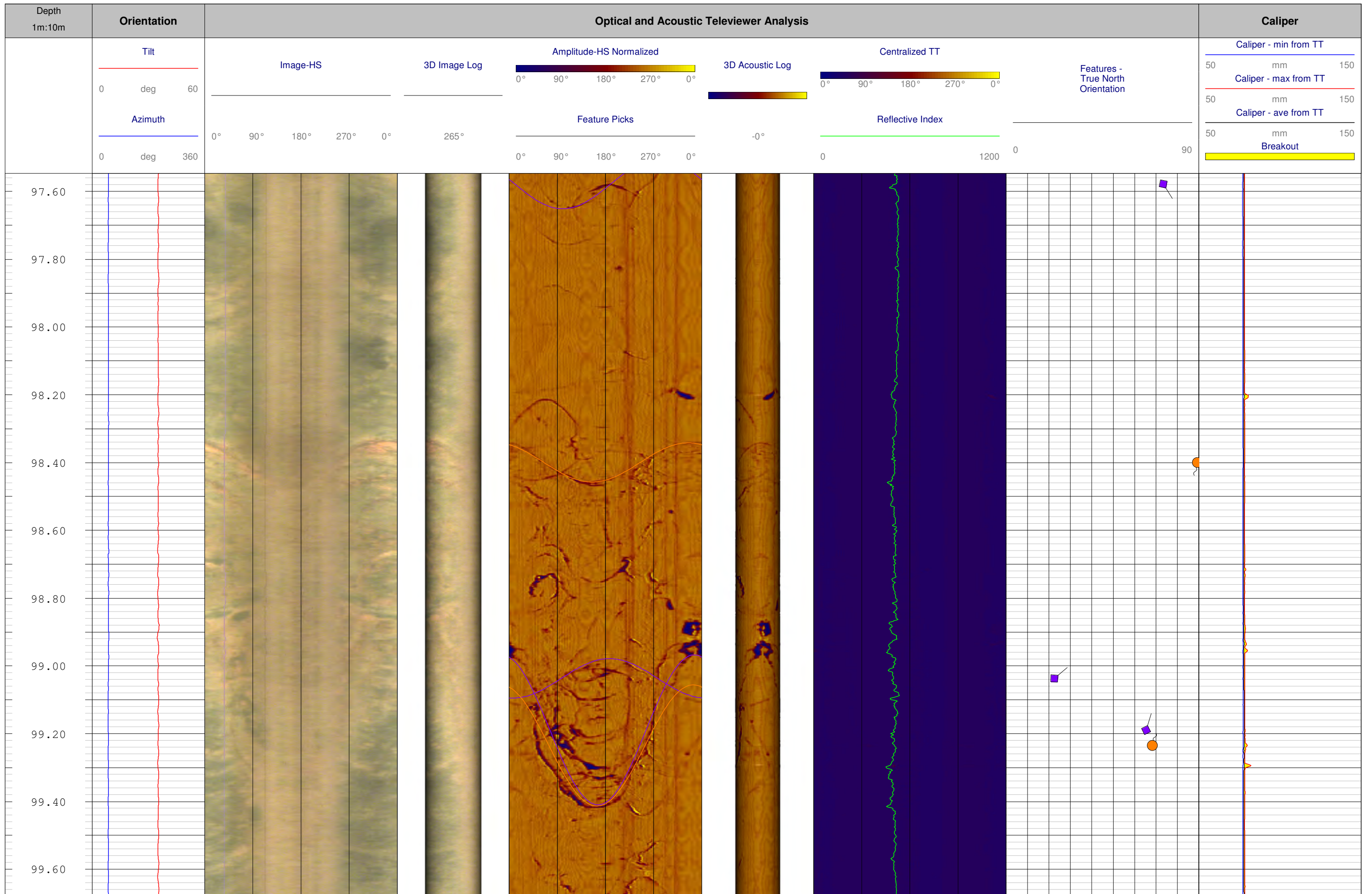


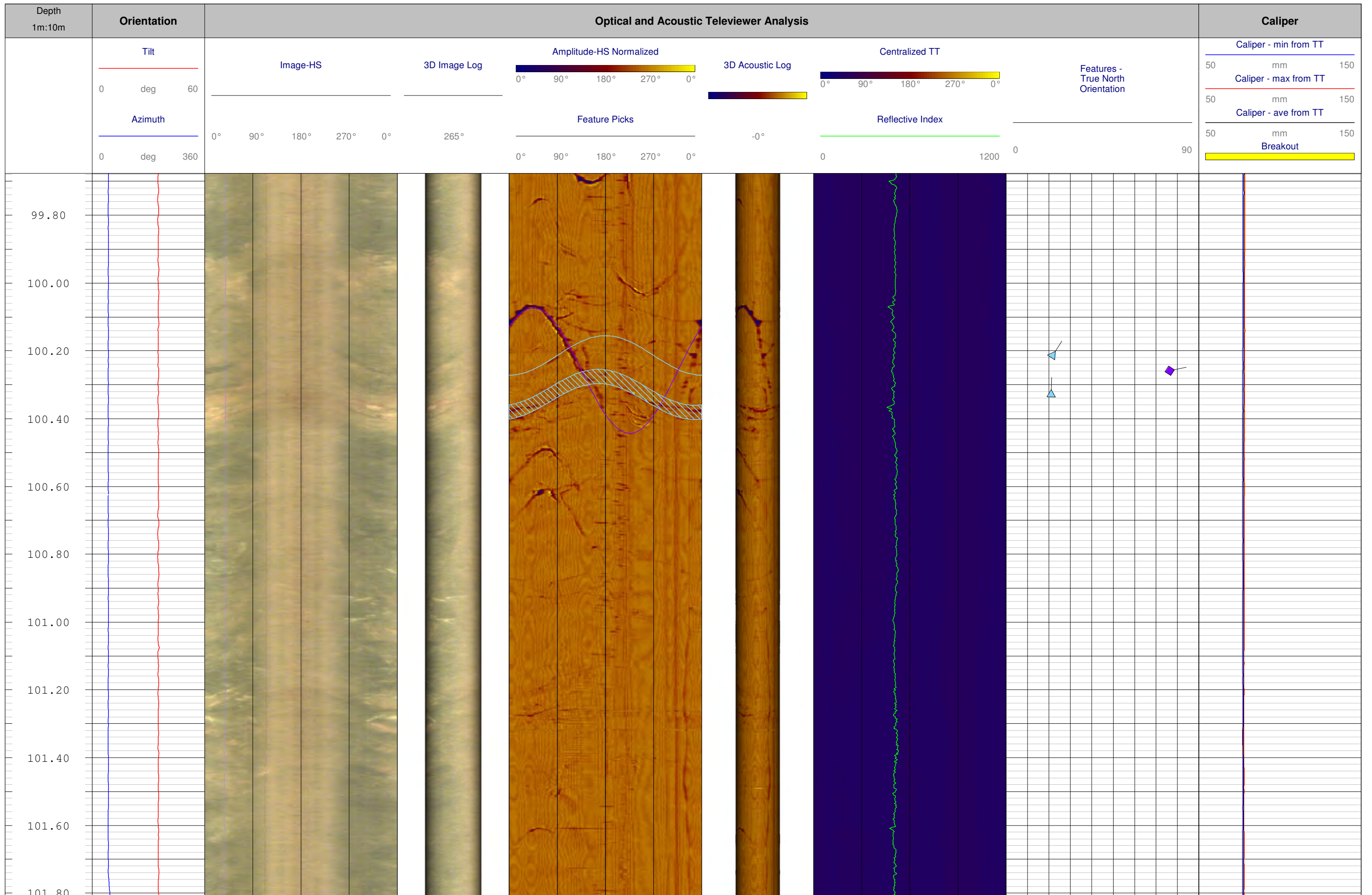


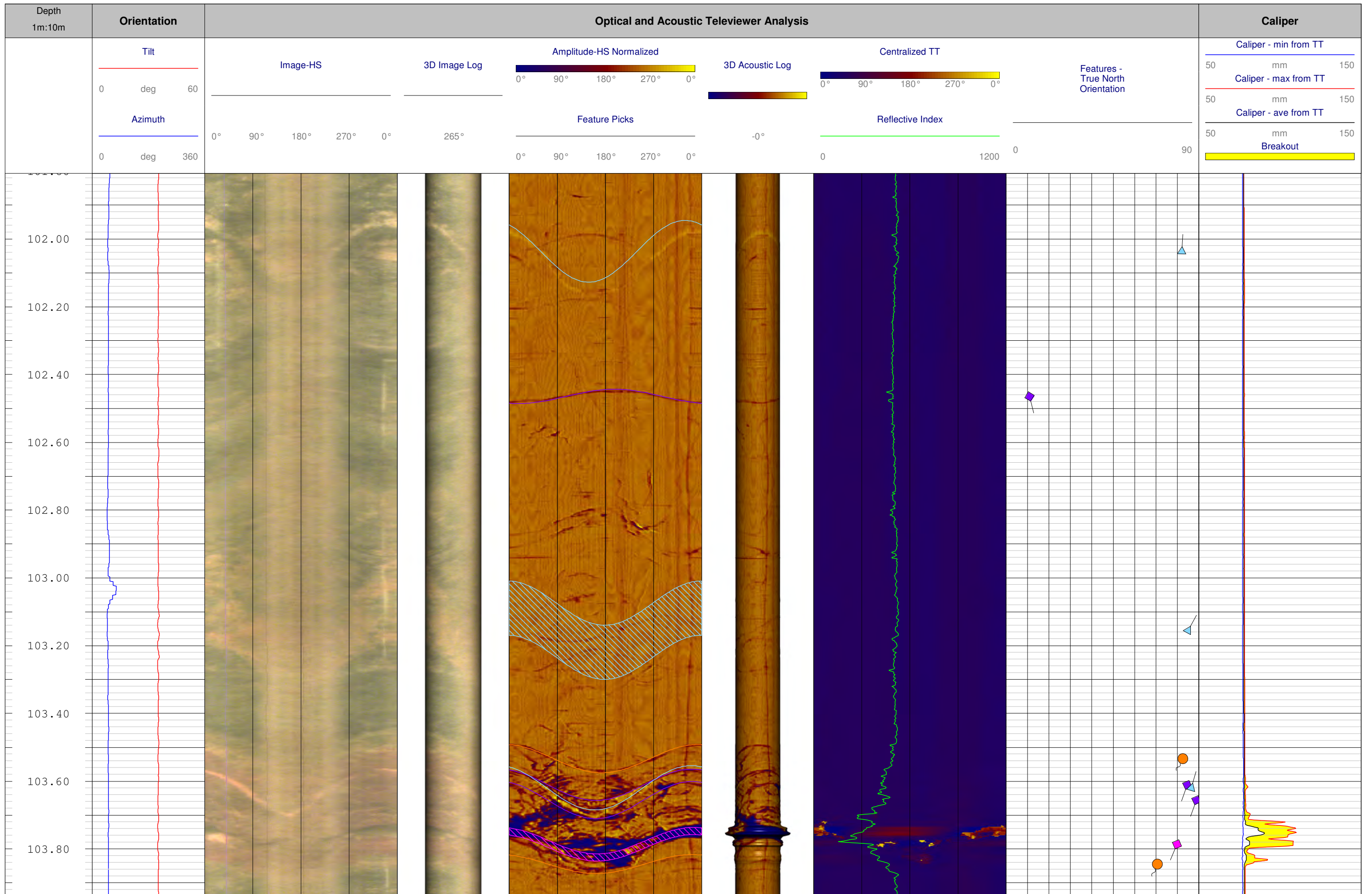


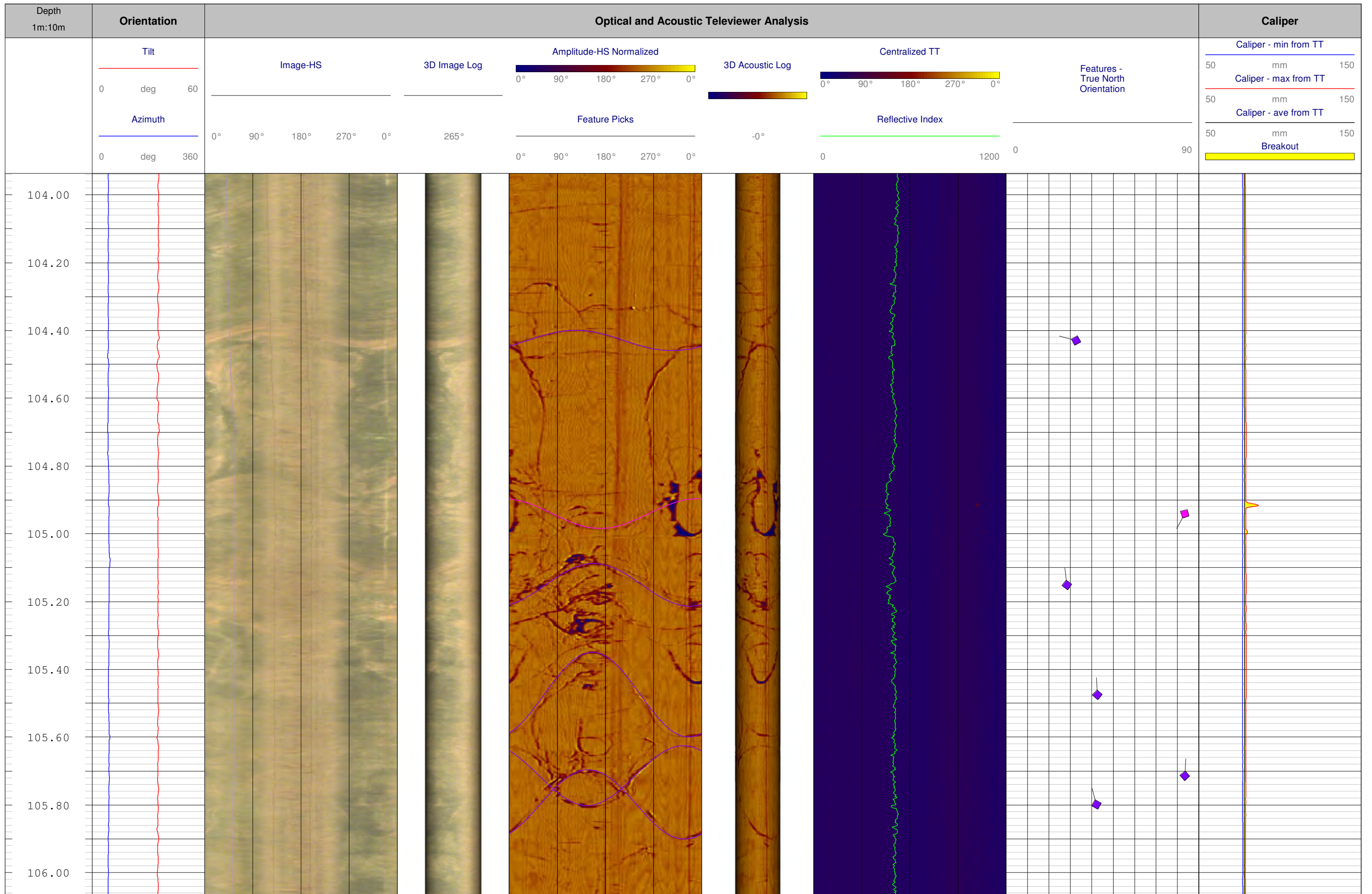


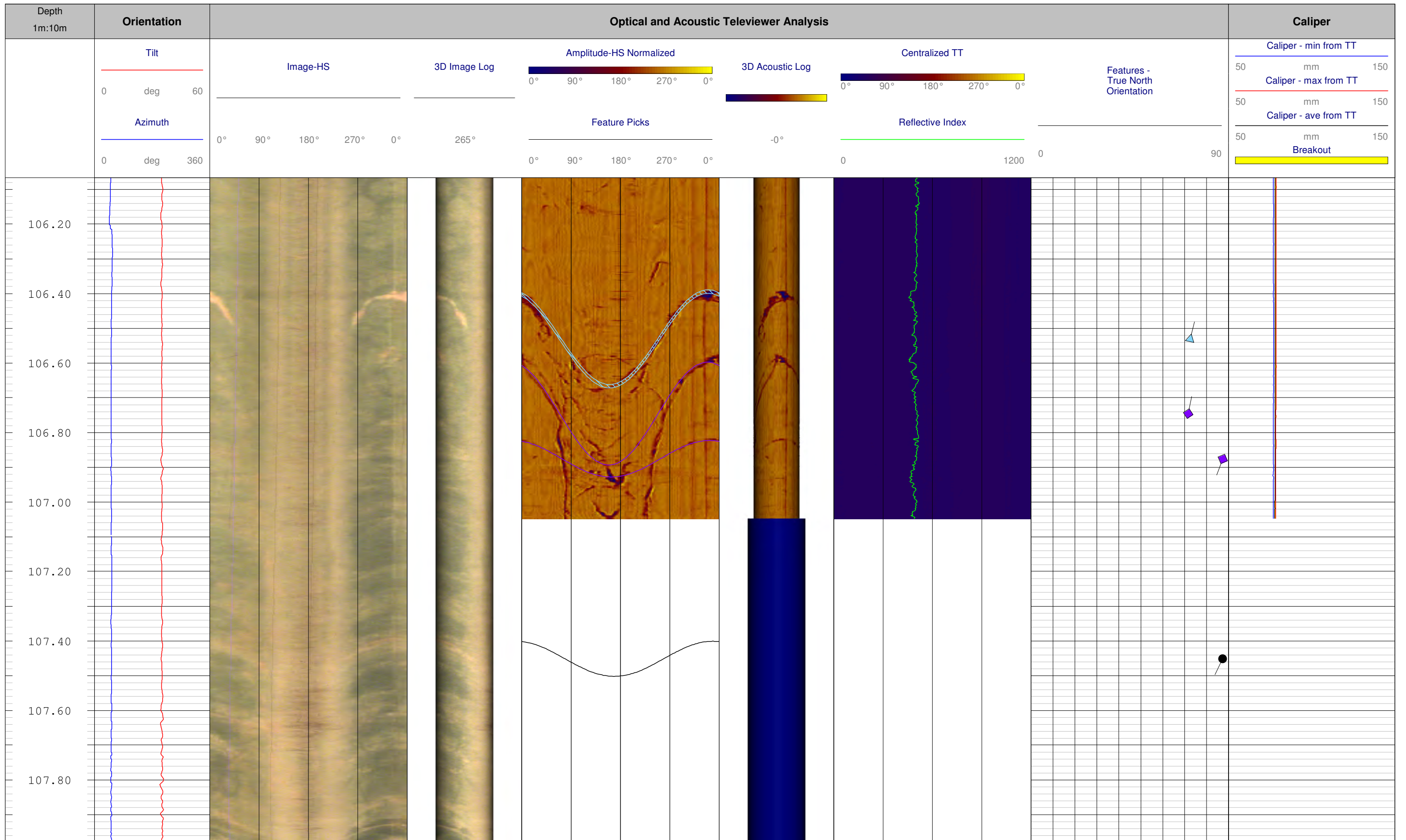










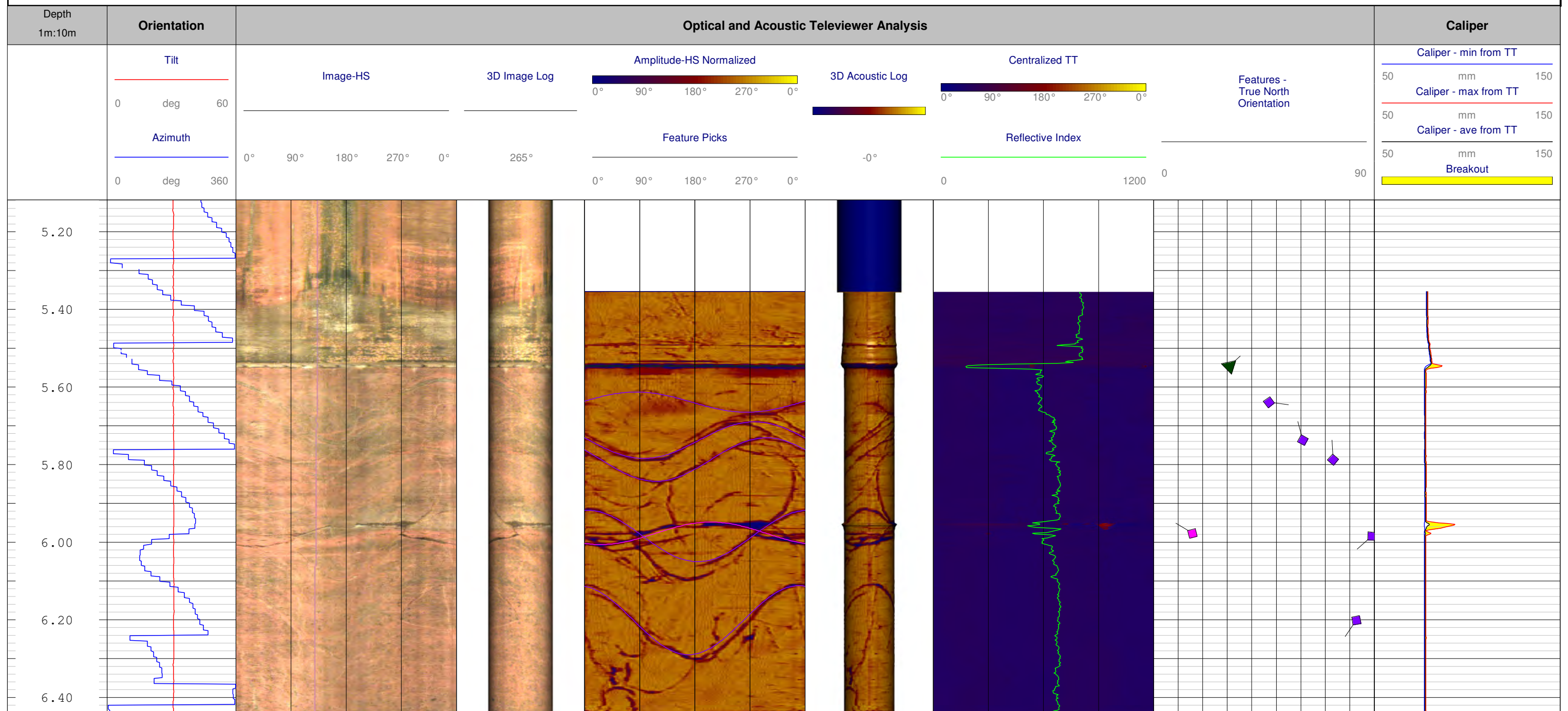


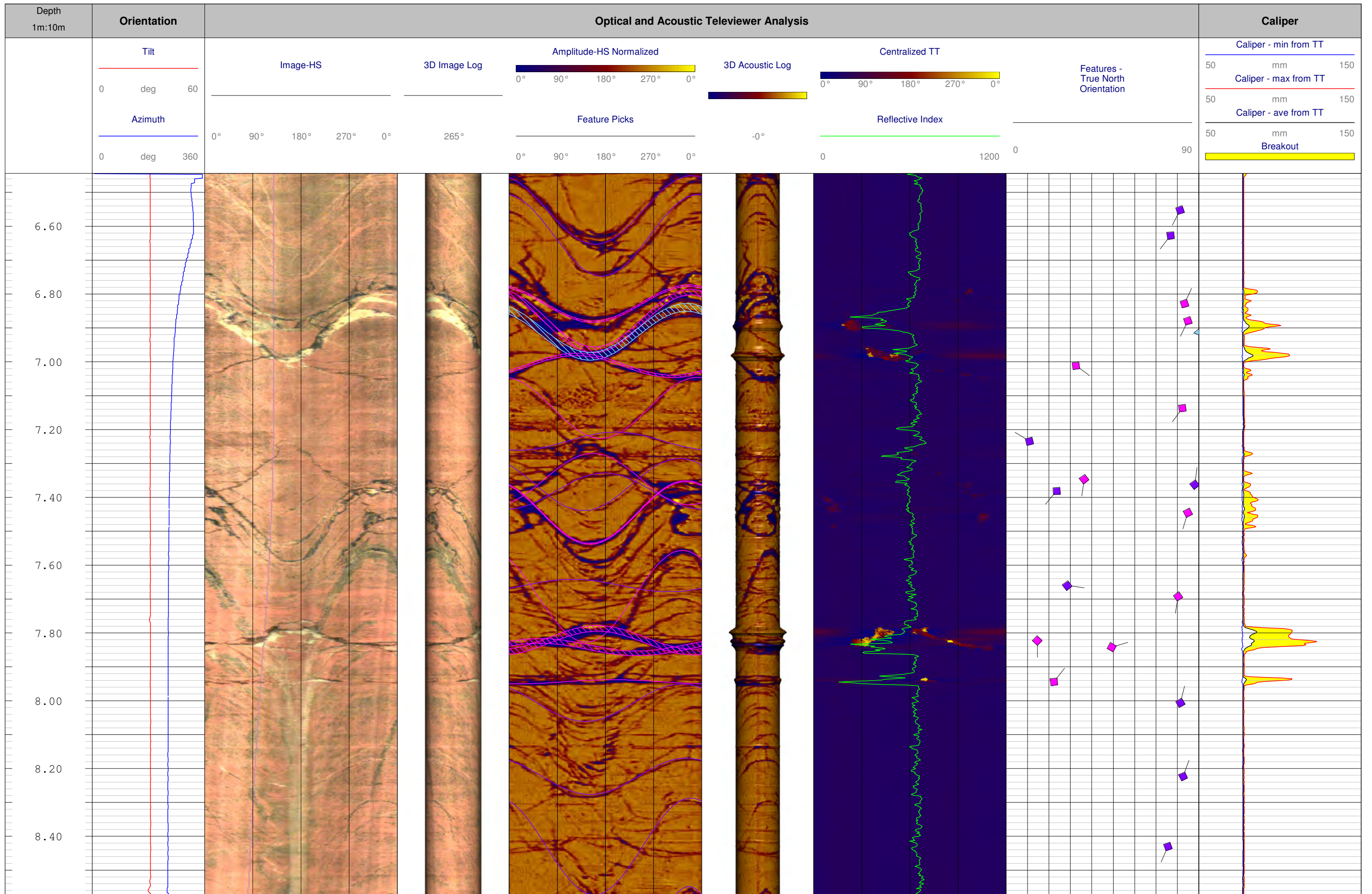
ACOUSTIC and OPTICAL TELEVIEWER PLOT

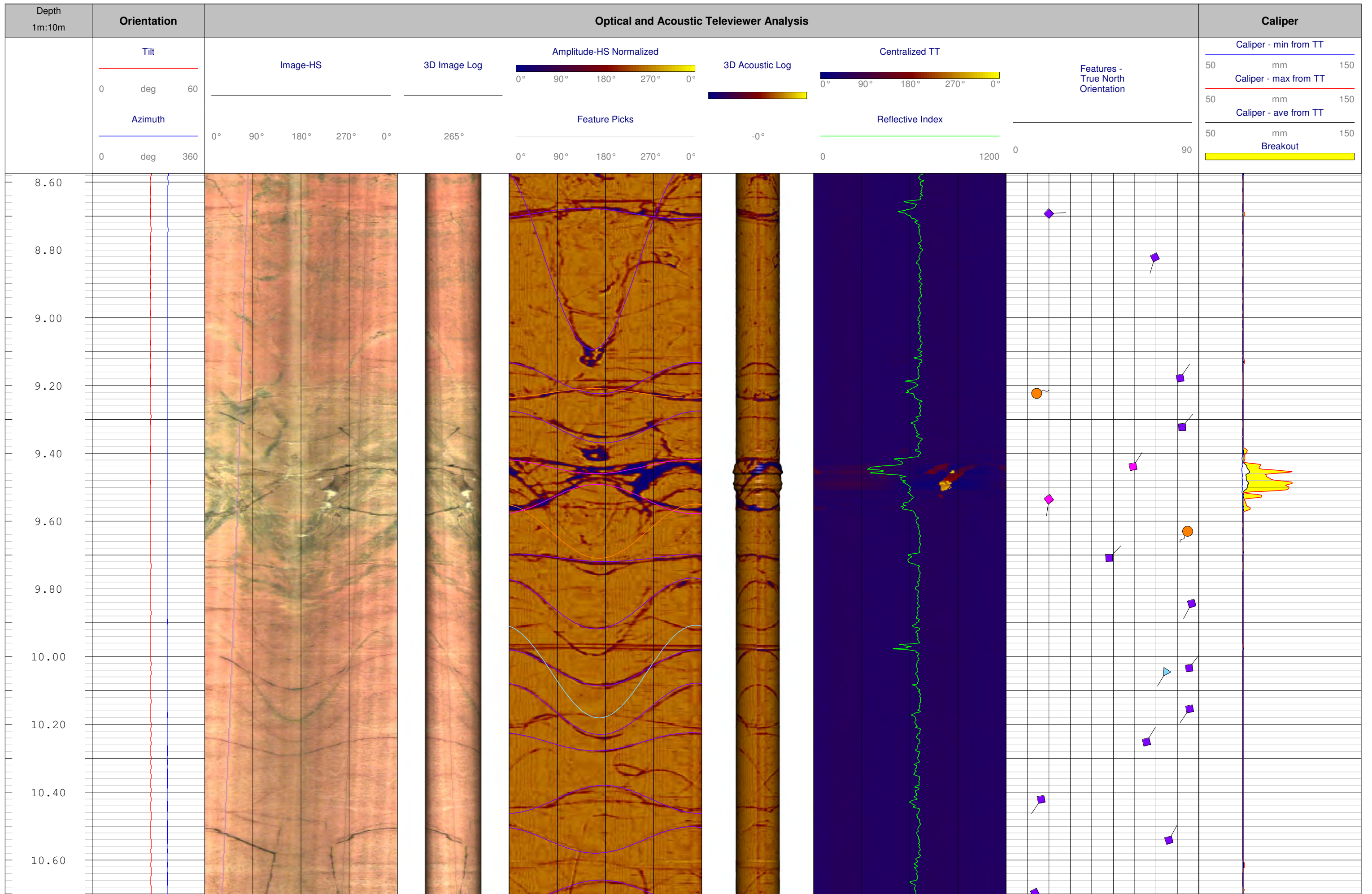
Company:	Canada Fluorspar	Total Depth:	110 m	UTM X (Easting):	N/A	Notes:	DGI Geoscience Inc. 119 Spadina Avenue, Suite 405 Toronto, Ontario Canada, M5V 2L1 416.361.3191
Hole ID:	GS-14-113	Surveyed Depth:	108 m	UTM Y (Northing):	N/A		
Acquisition date(s):	Nov. 05, 2014	Hole Diameter:	NQ	UTM Z (Elevation):	N/A		
Field Personnel:	J. Smith, R. Morrison	Hole Type:	Core				
Legal Location:	Saint Lawrence, NFLD	Casing Depth:	5.5 m				
Survey Day(s):	1	Fluid Type:	Water				

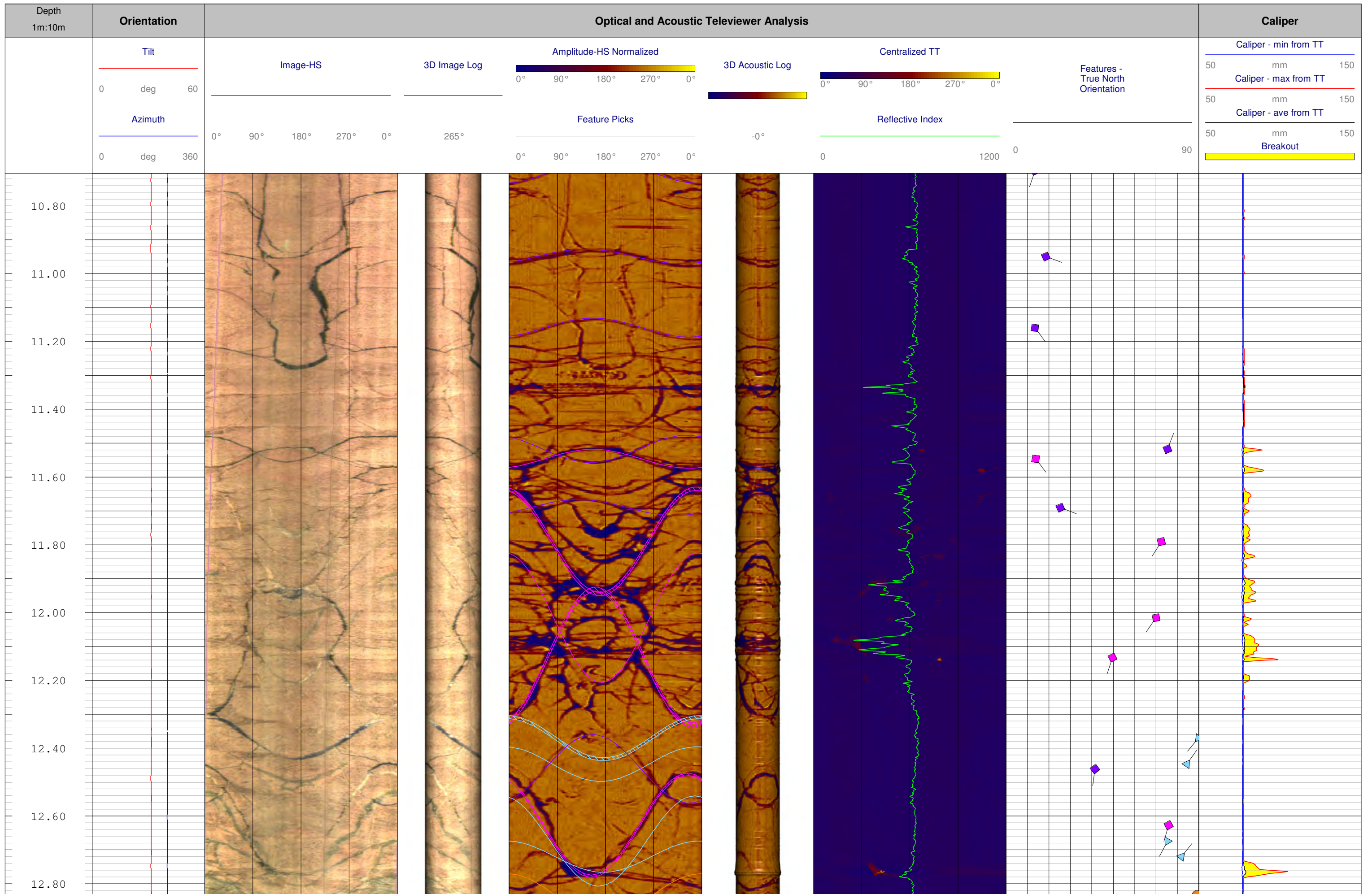
LEGEND - STRUCTURE TYPE

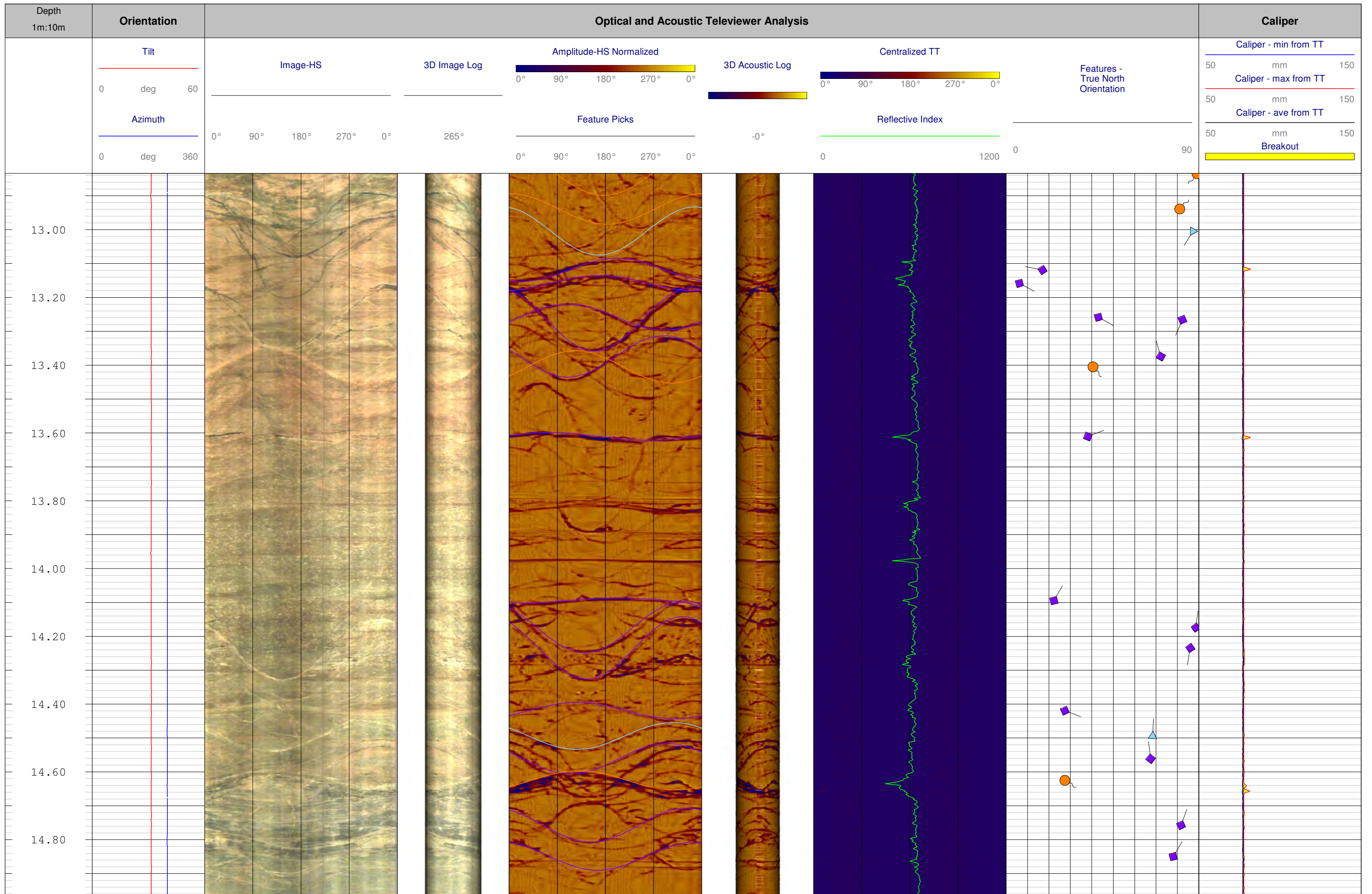
- Btm of Casing
- Major Open Joint/Fracture
- Partially Open Joint/Fracture
- Minor Joint/Fracture
- Bedding/ Banding/ Foliation
- Vein - Group 1
- Lithology Contact

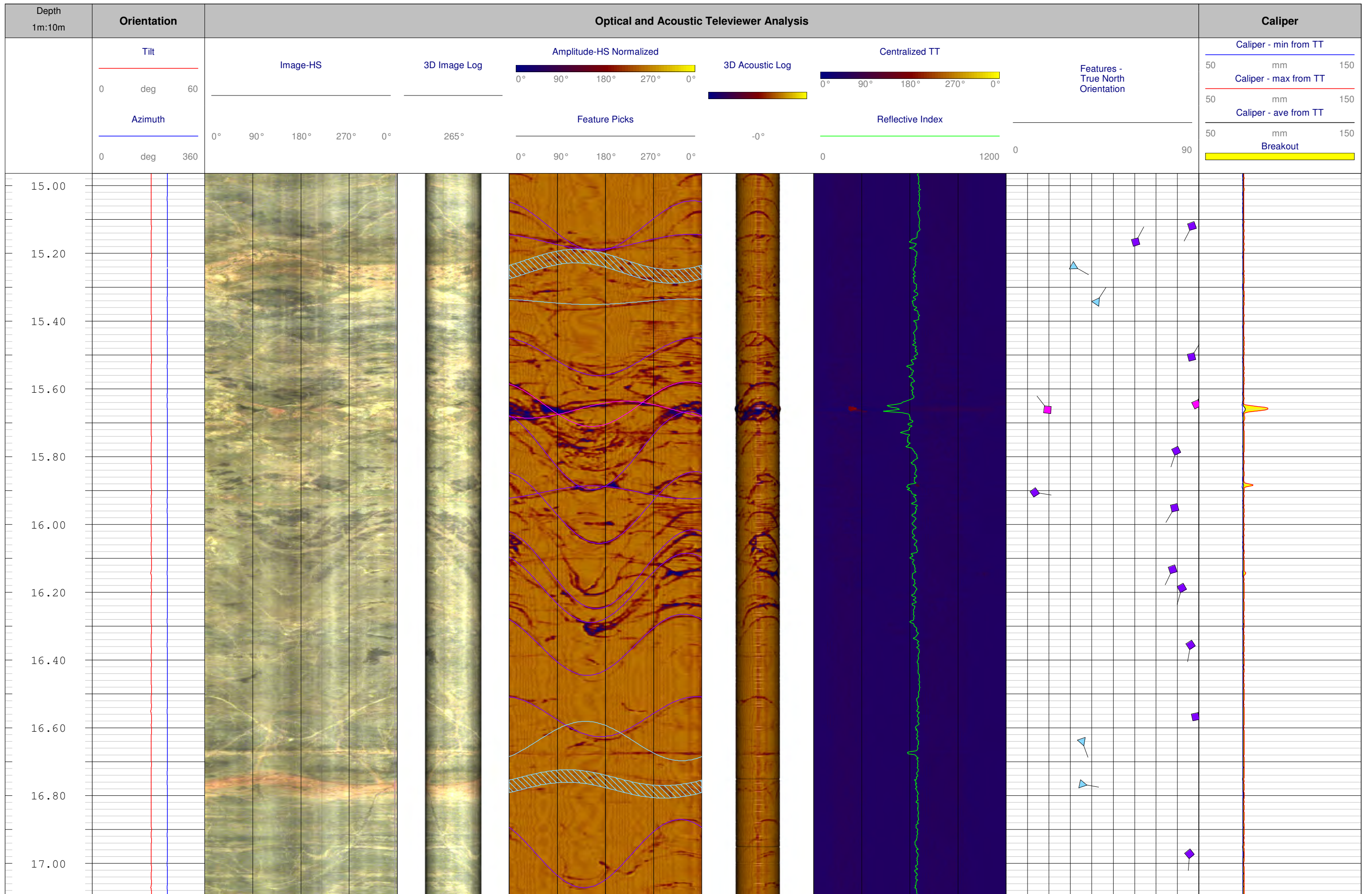


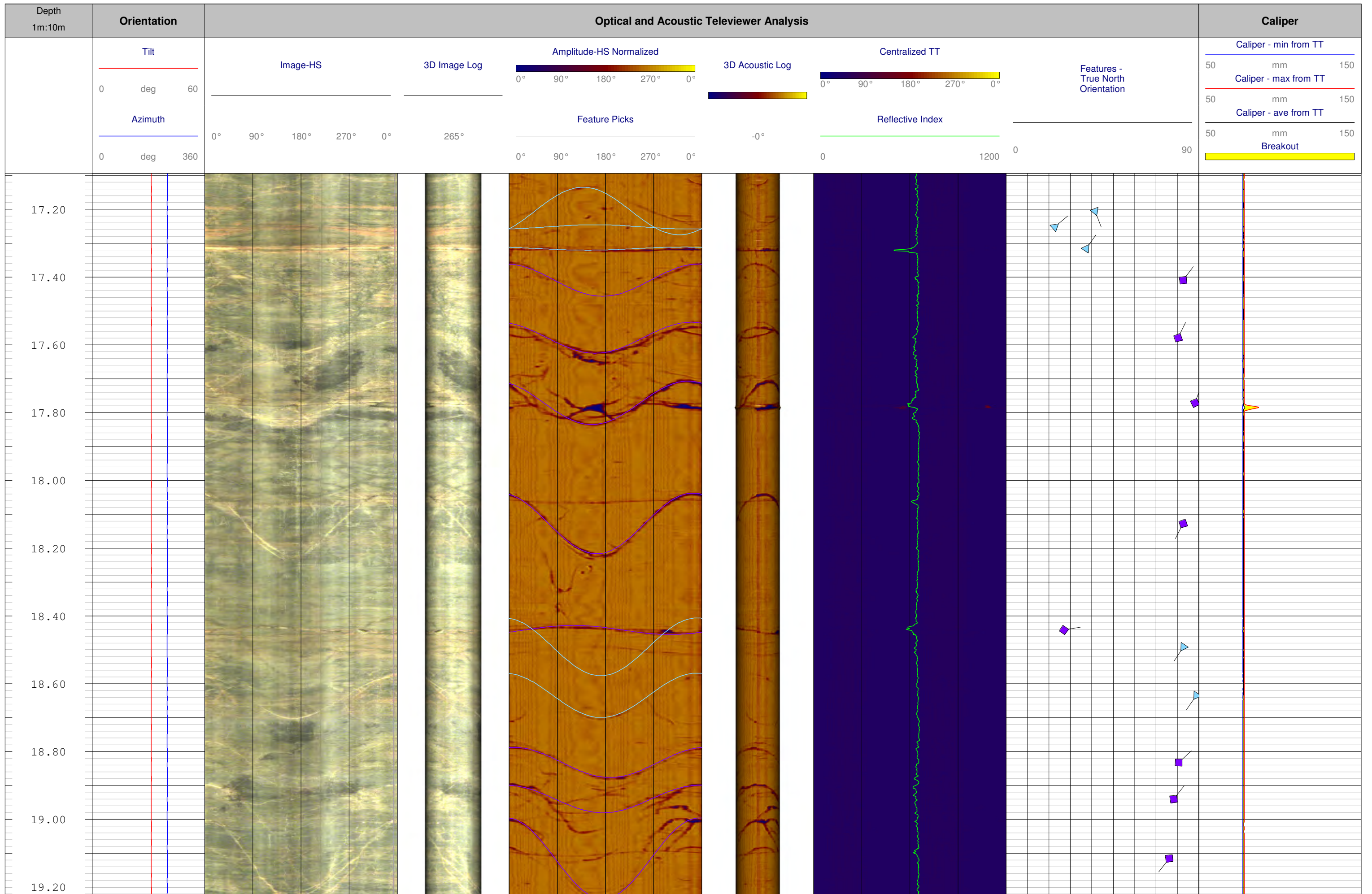


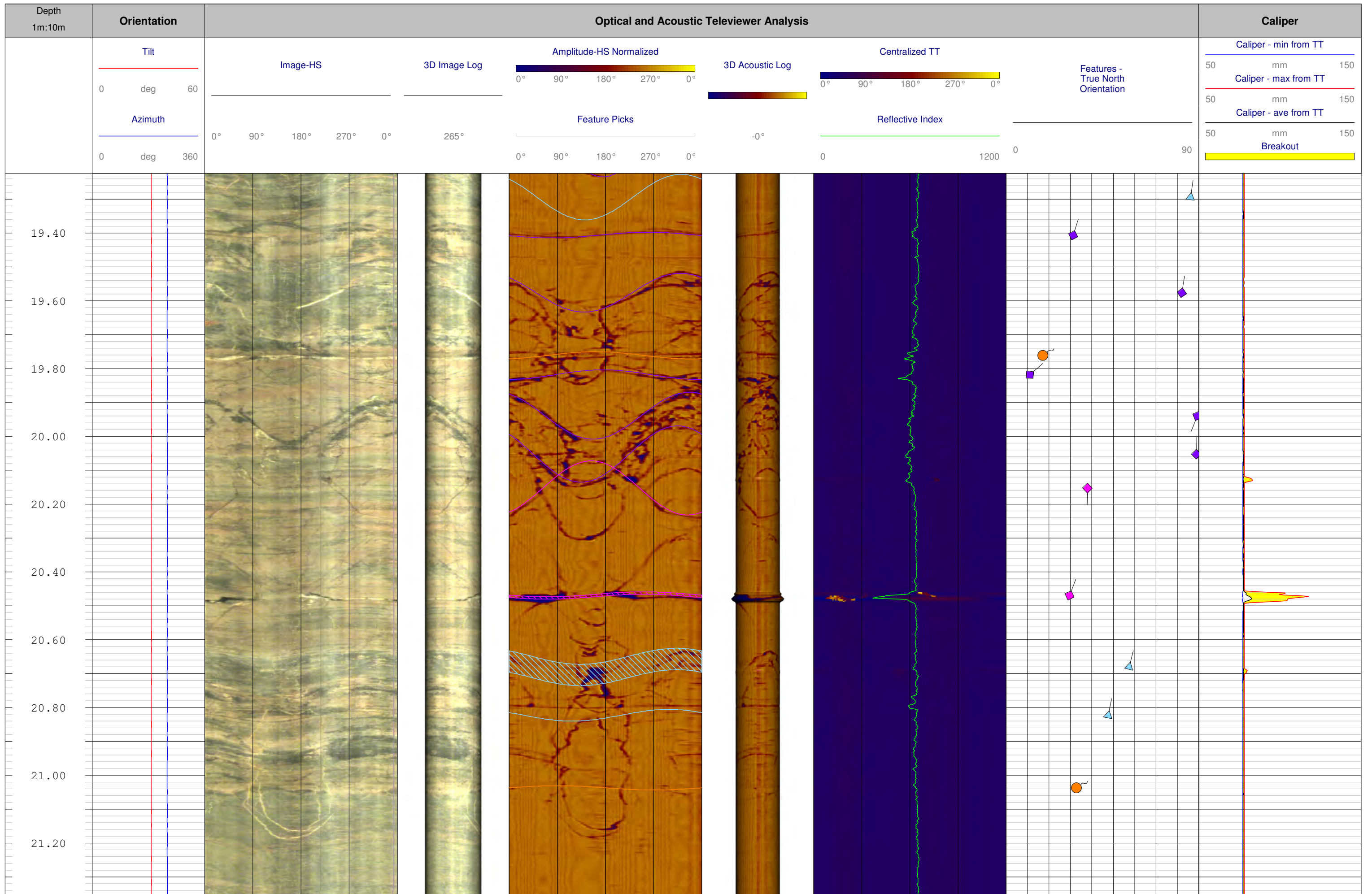


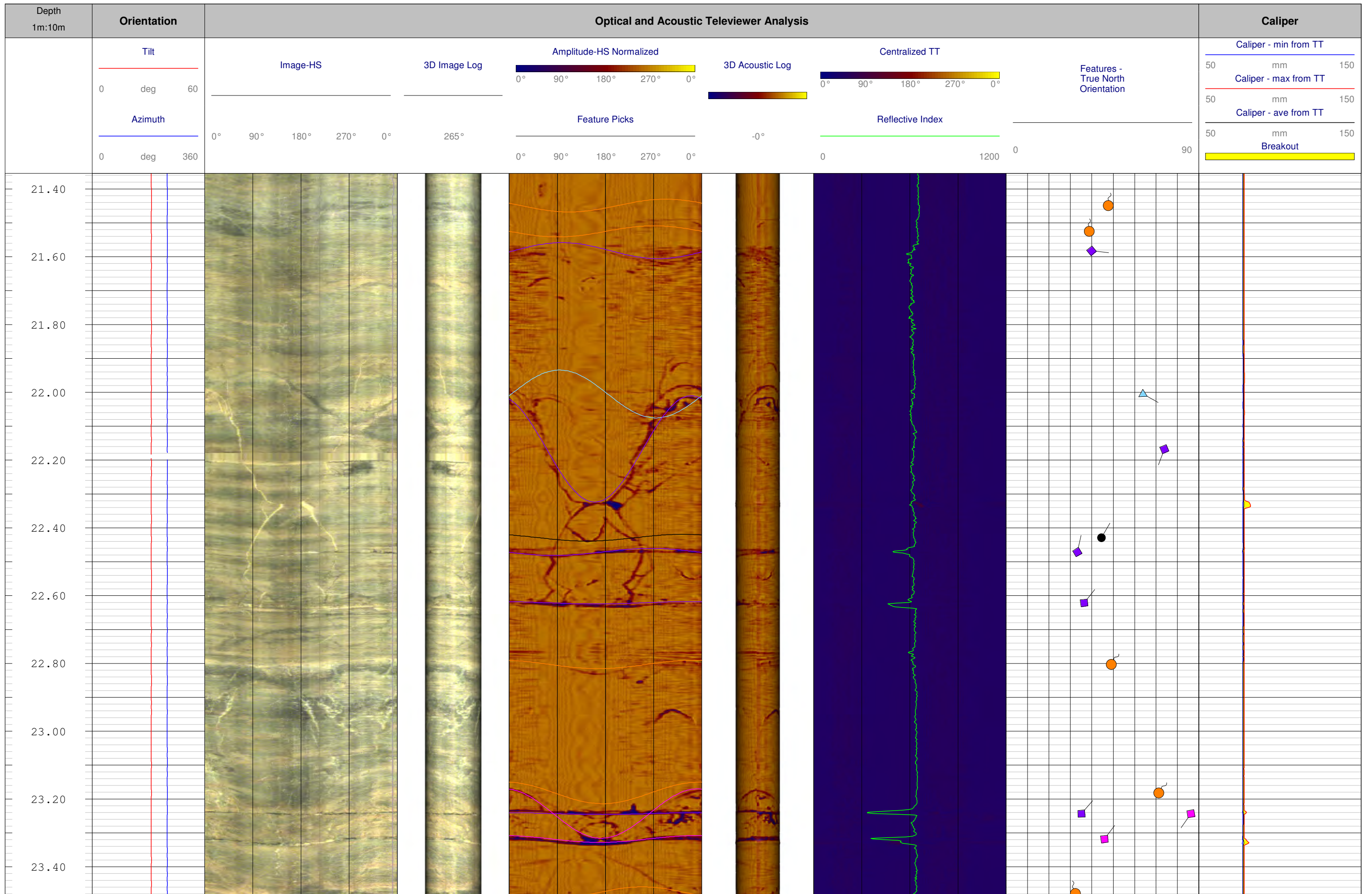


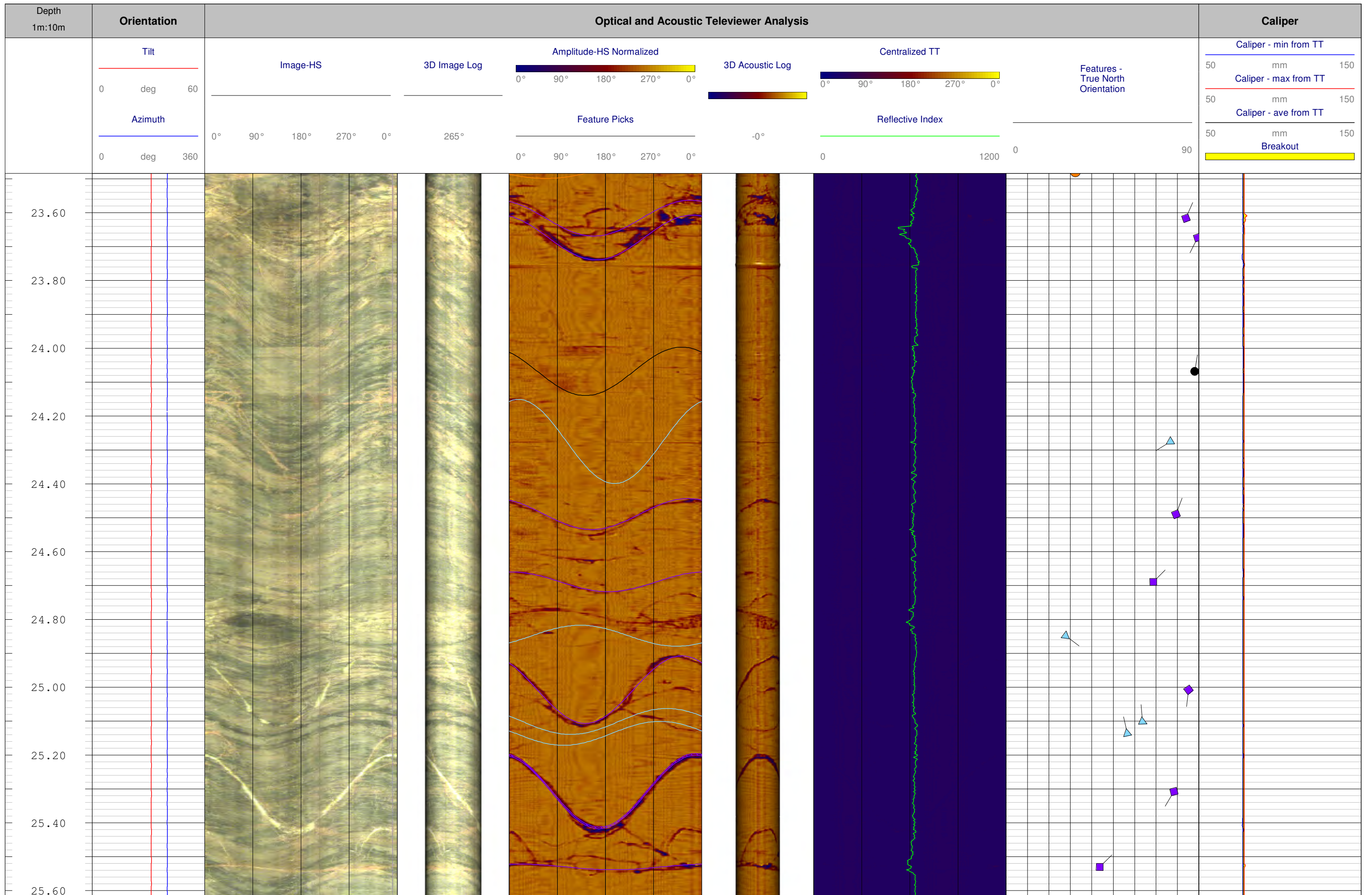


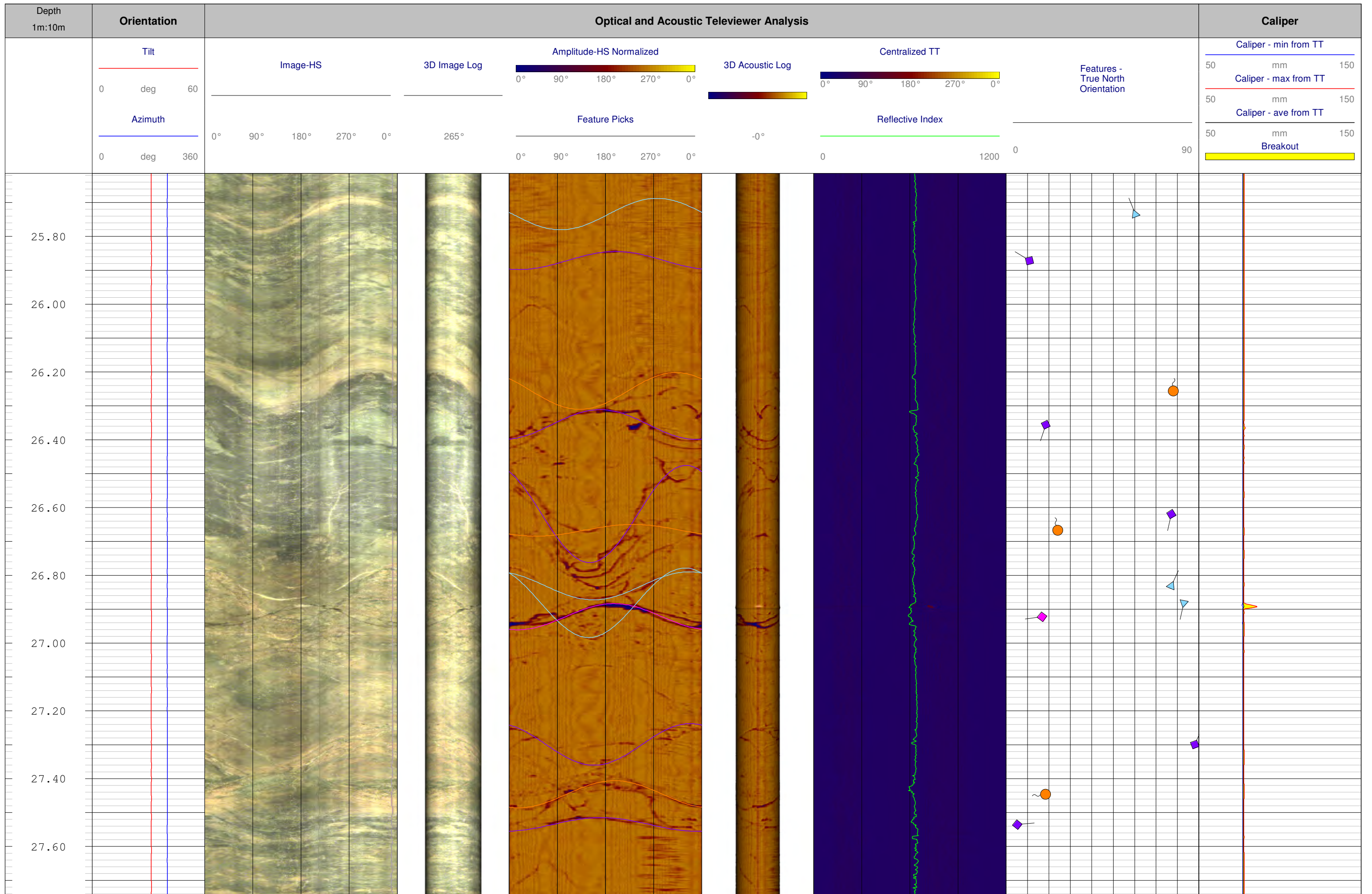


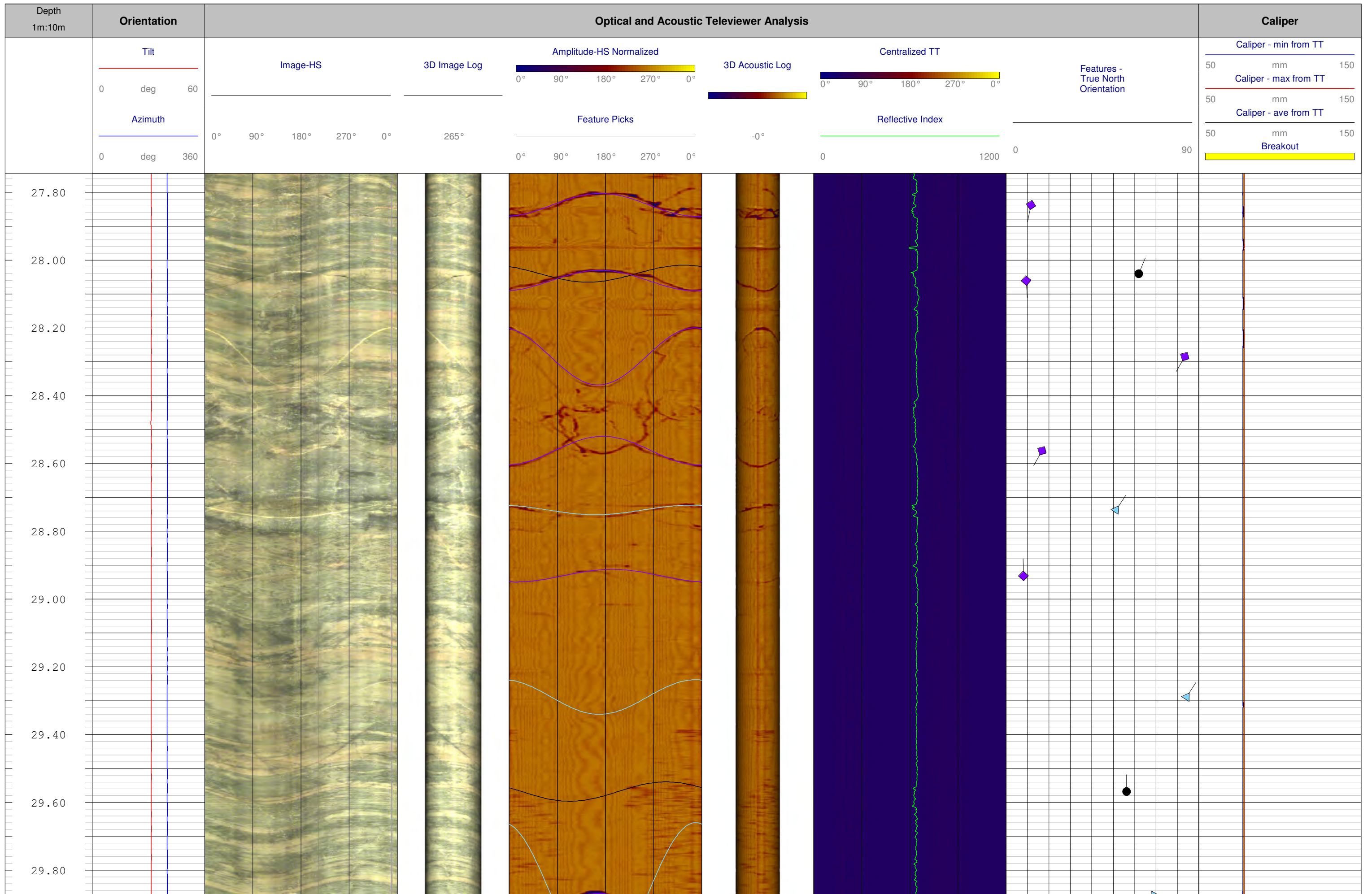


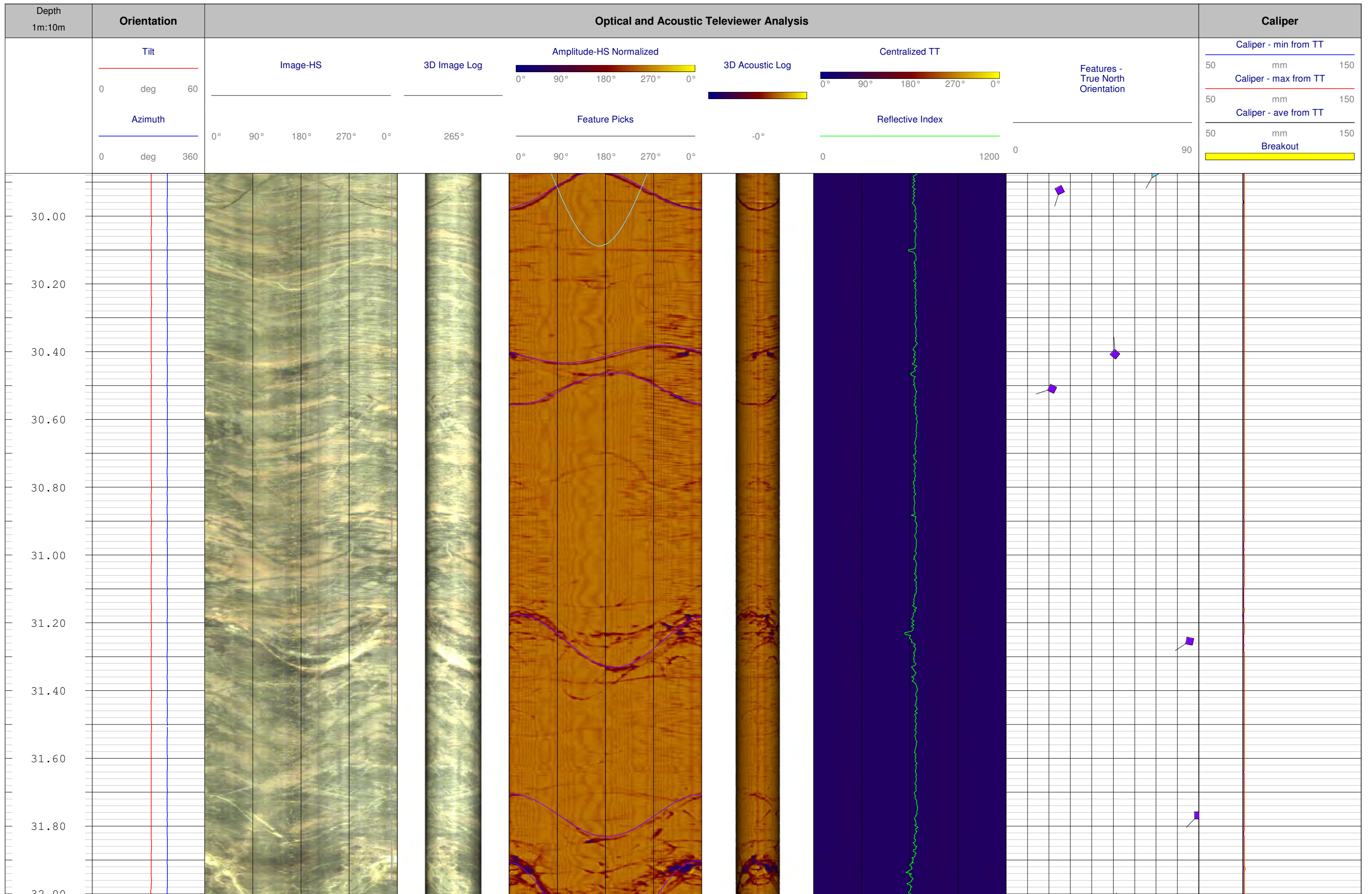


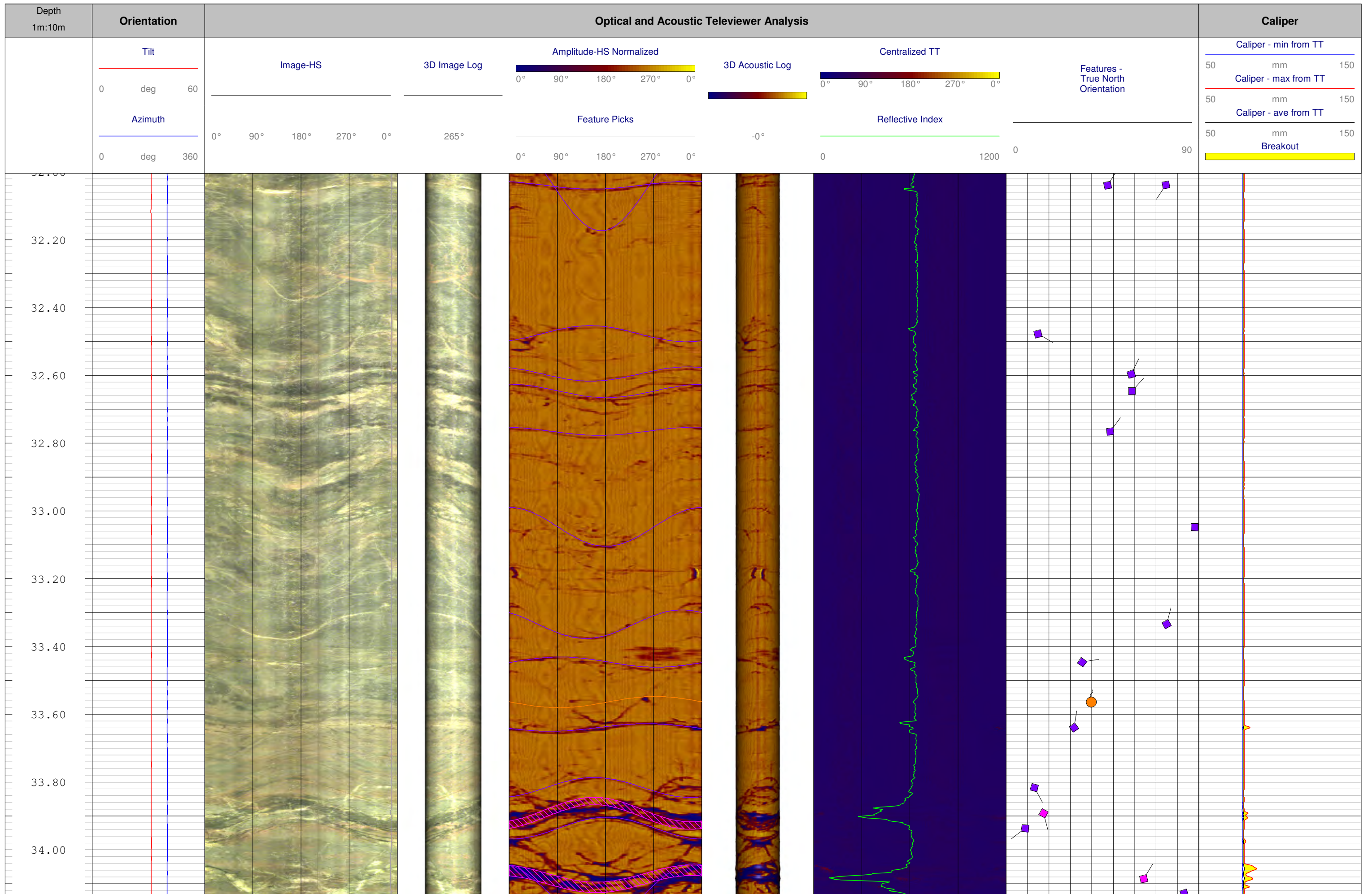


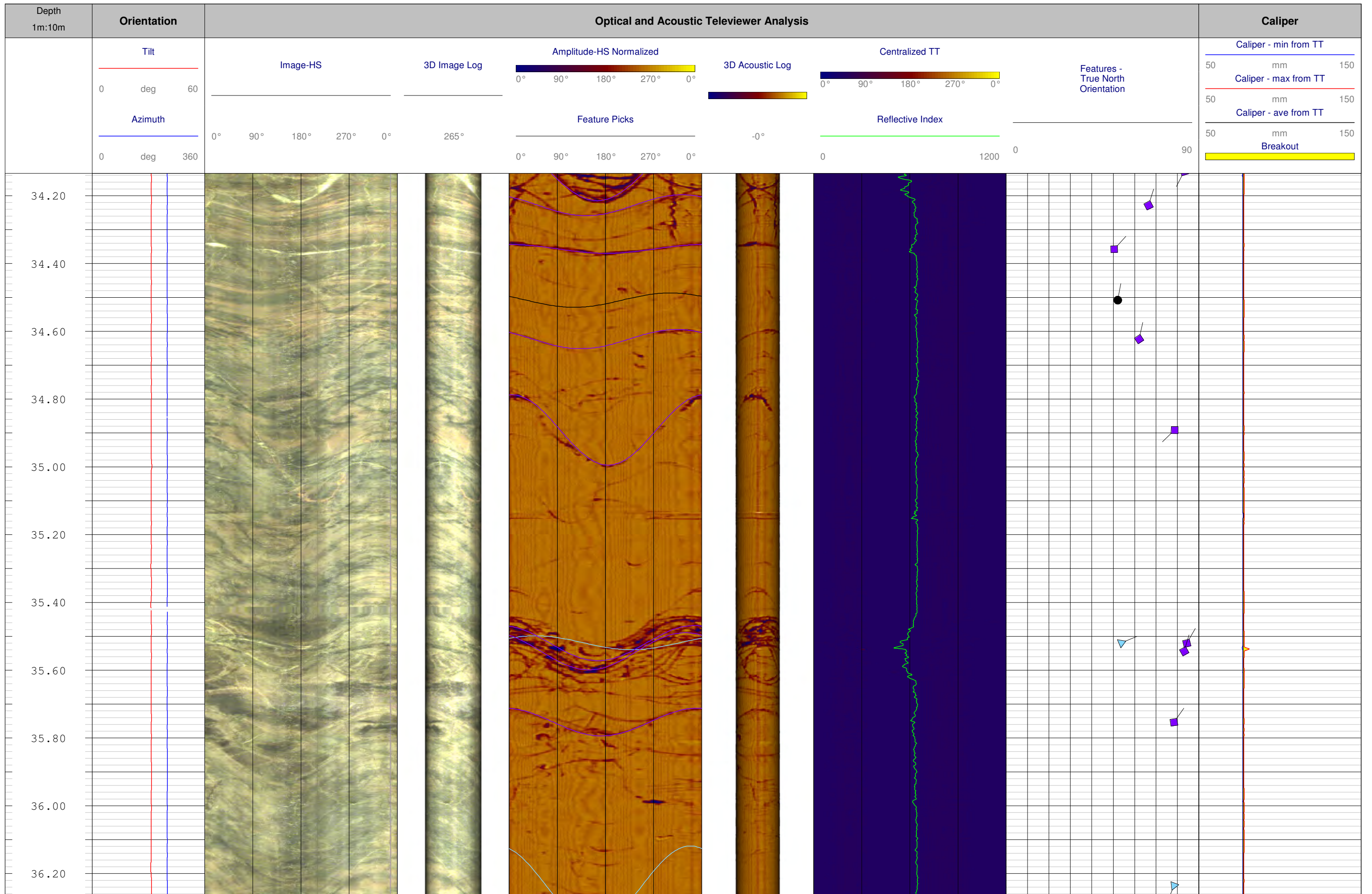


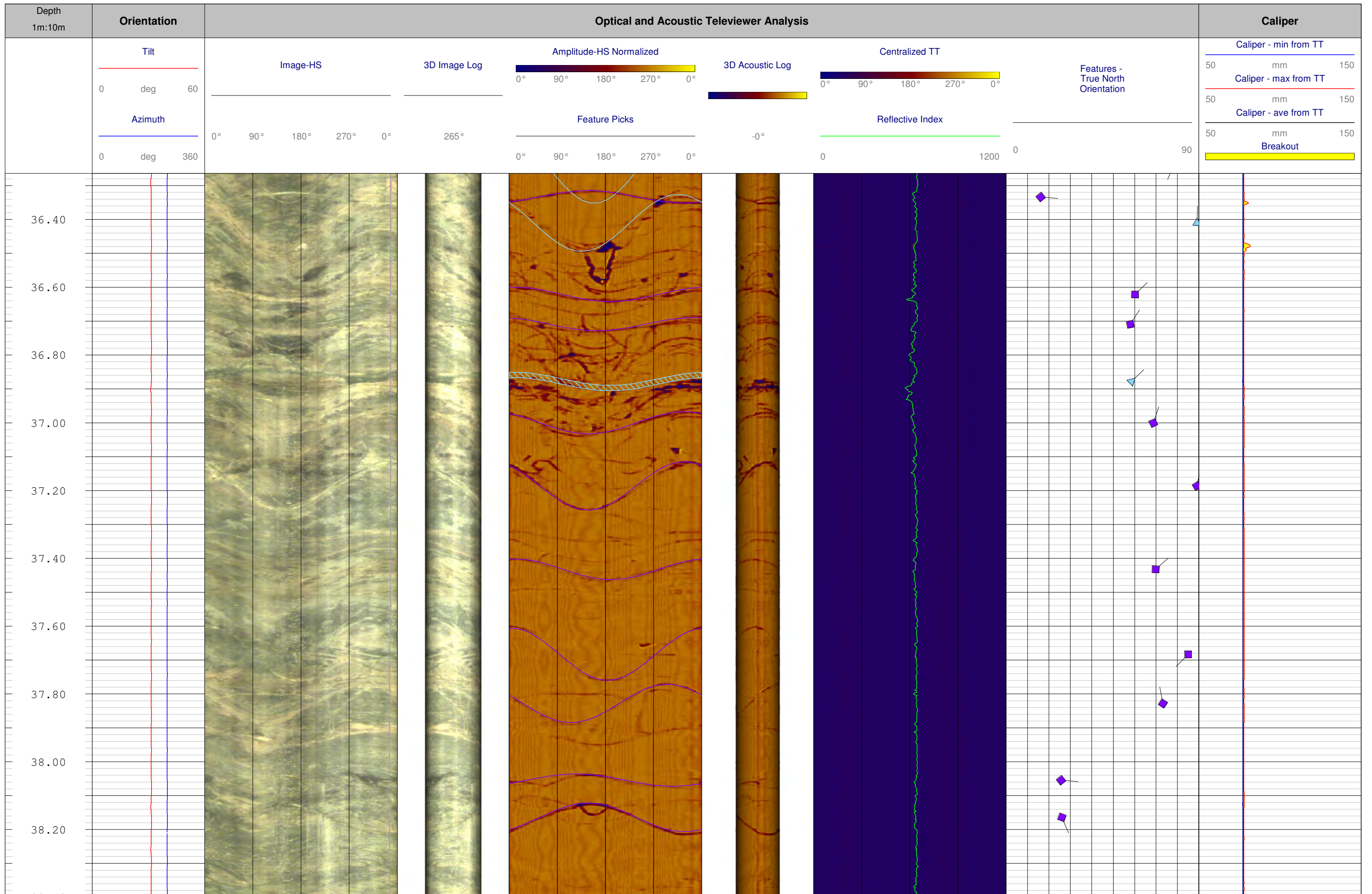


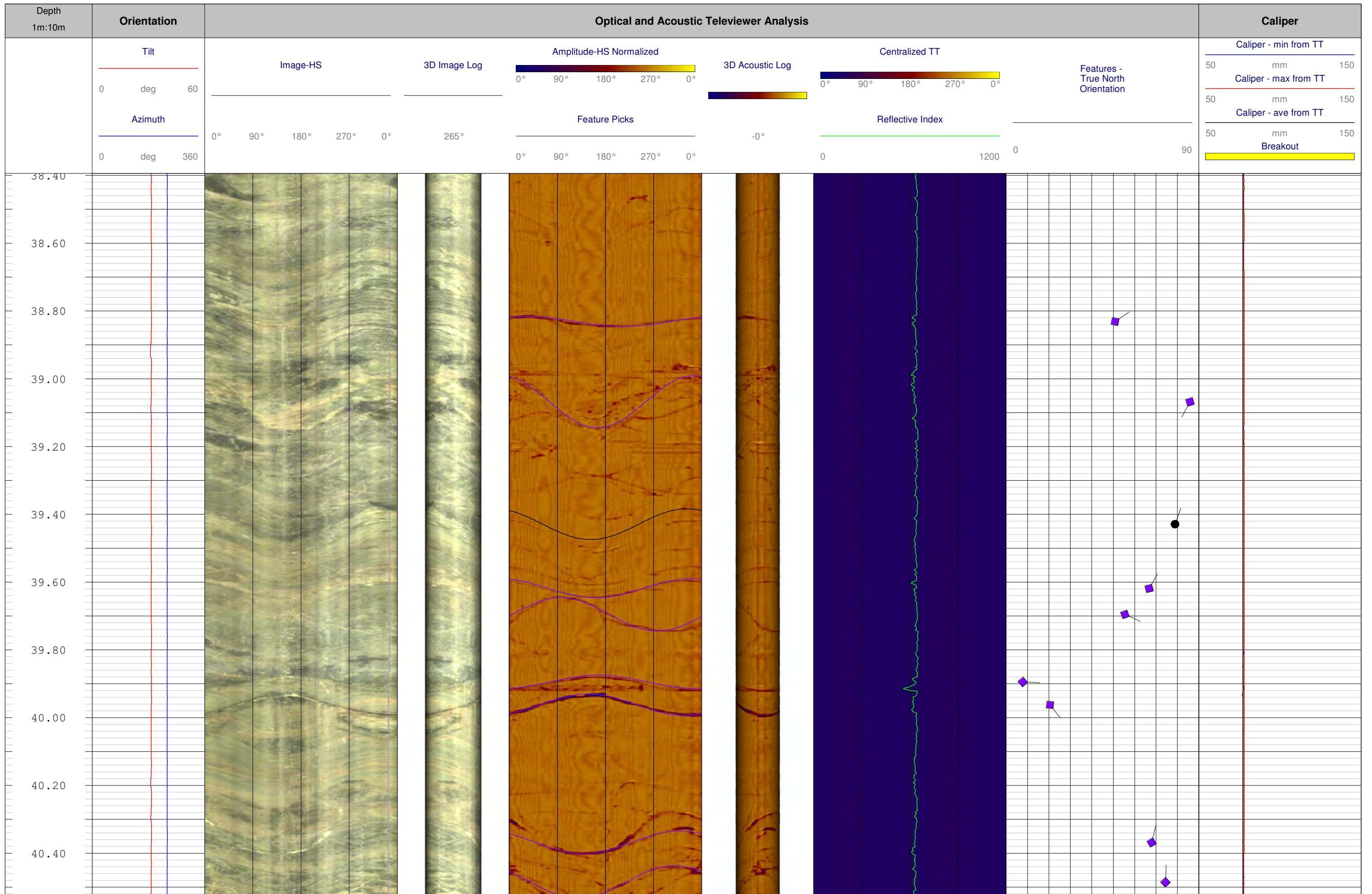


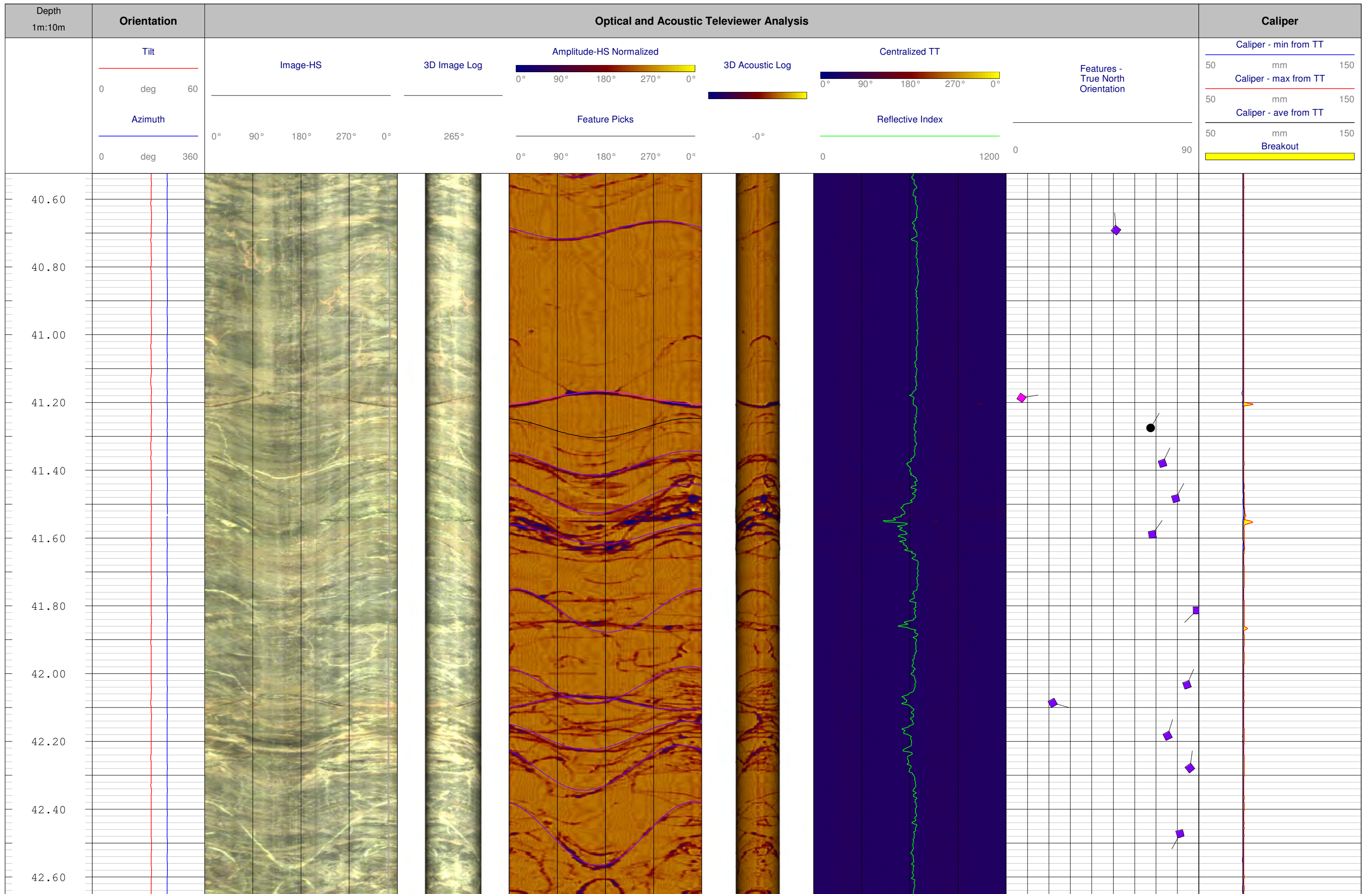


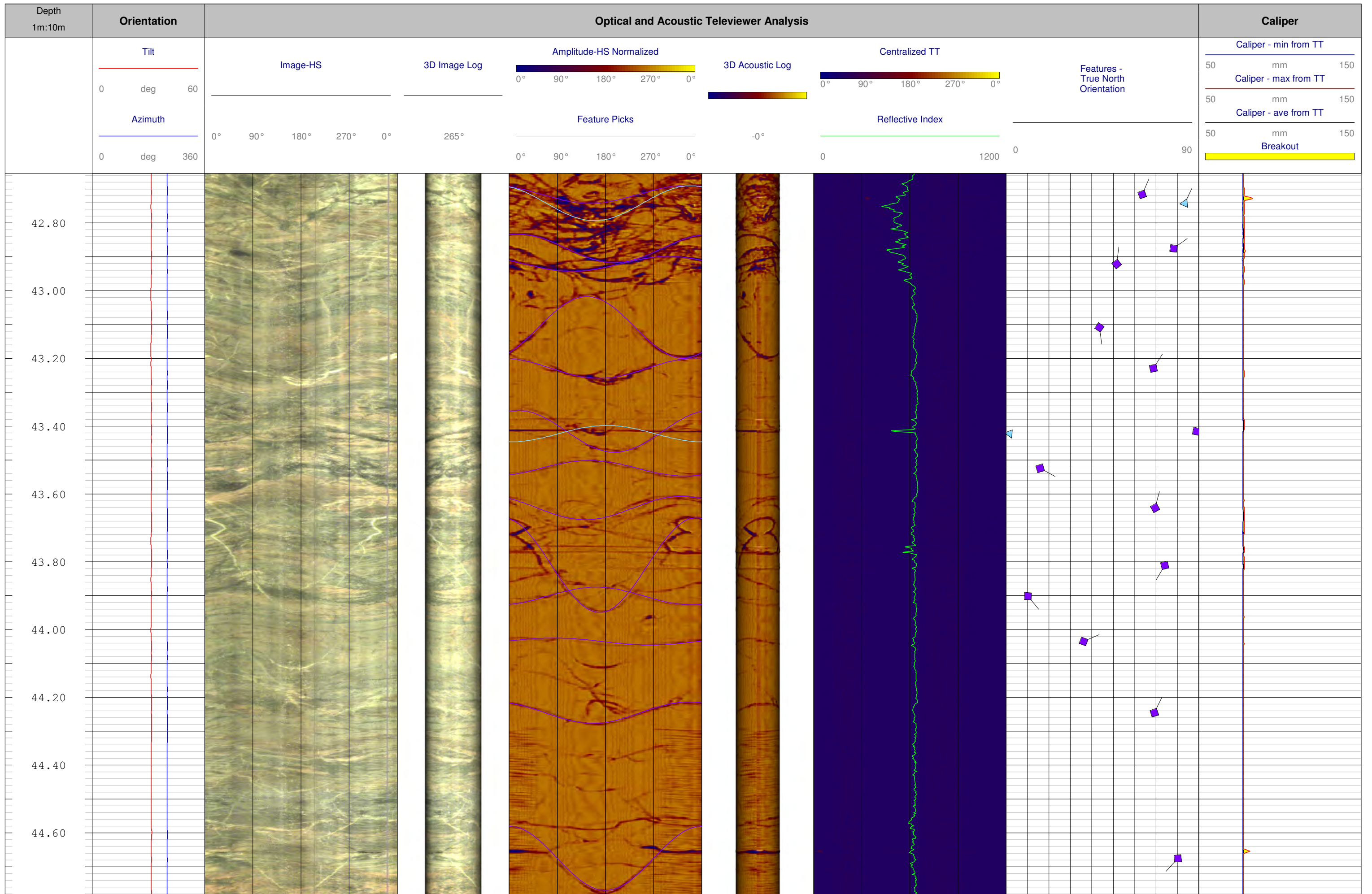


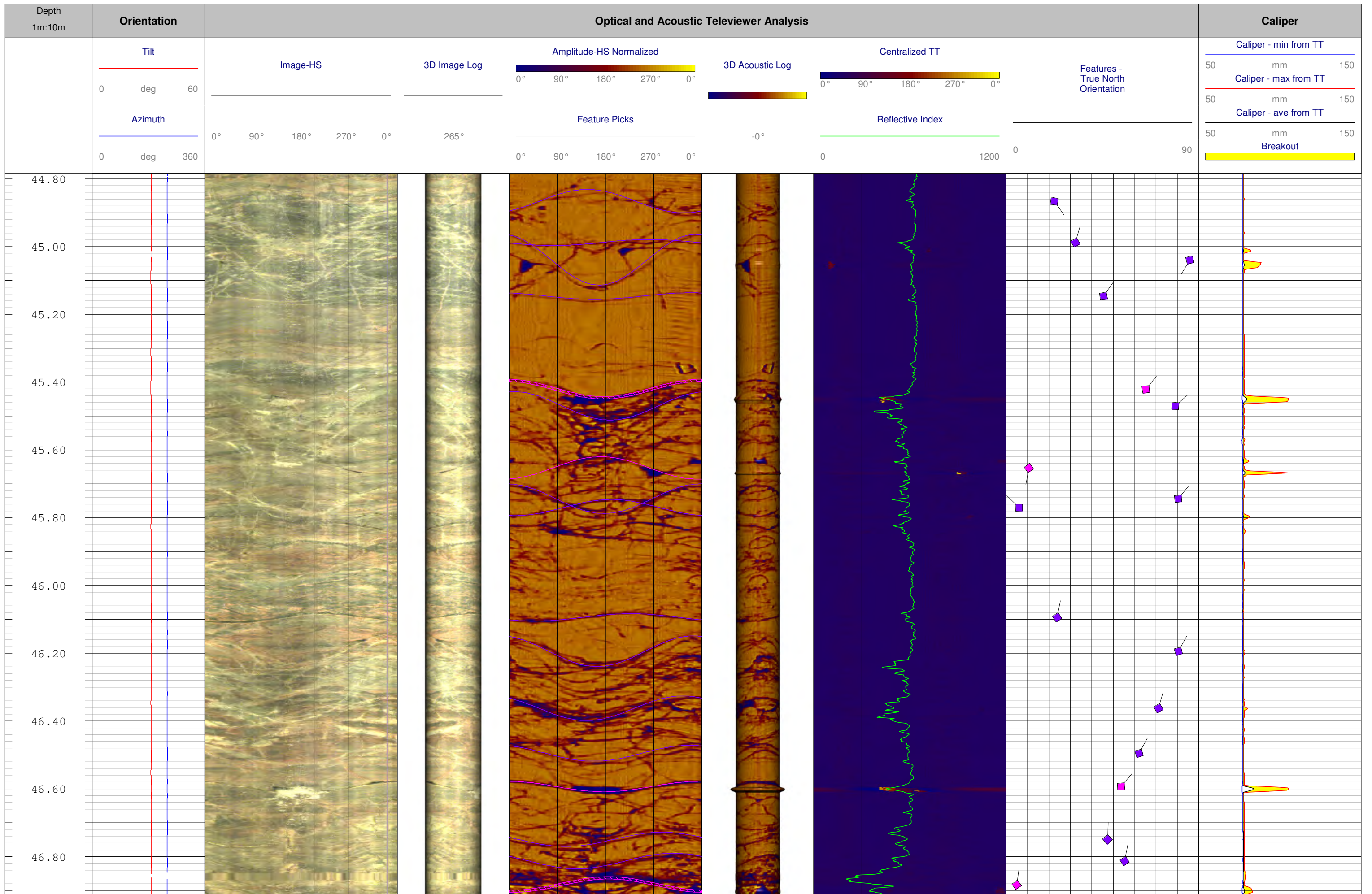


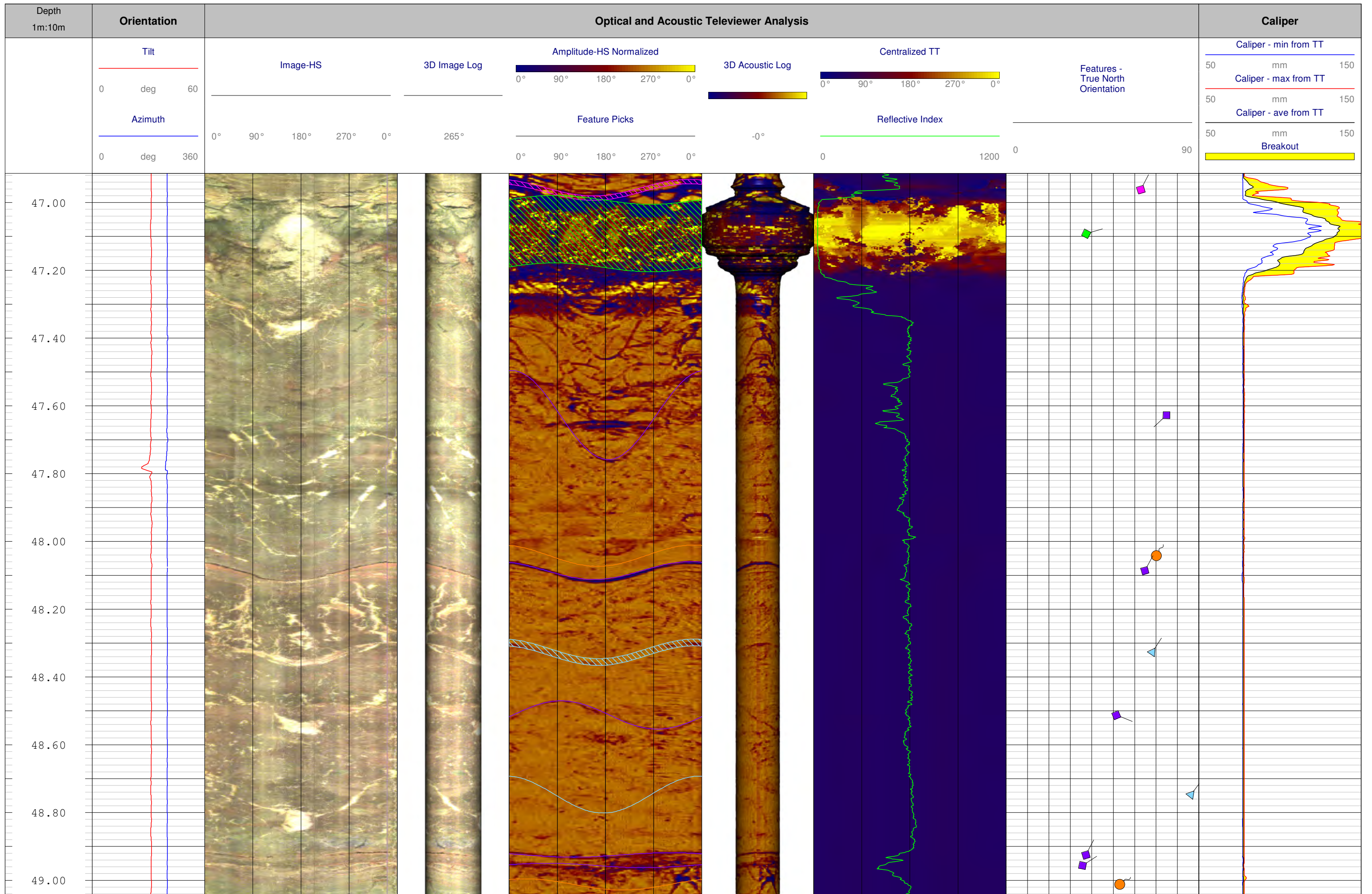


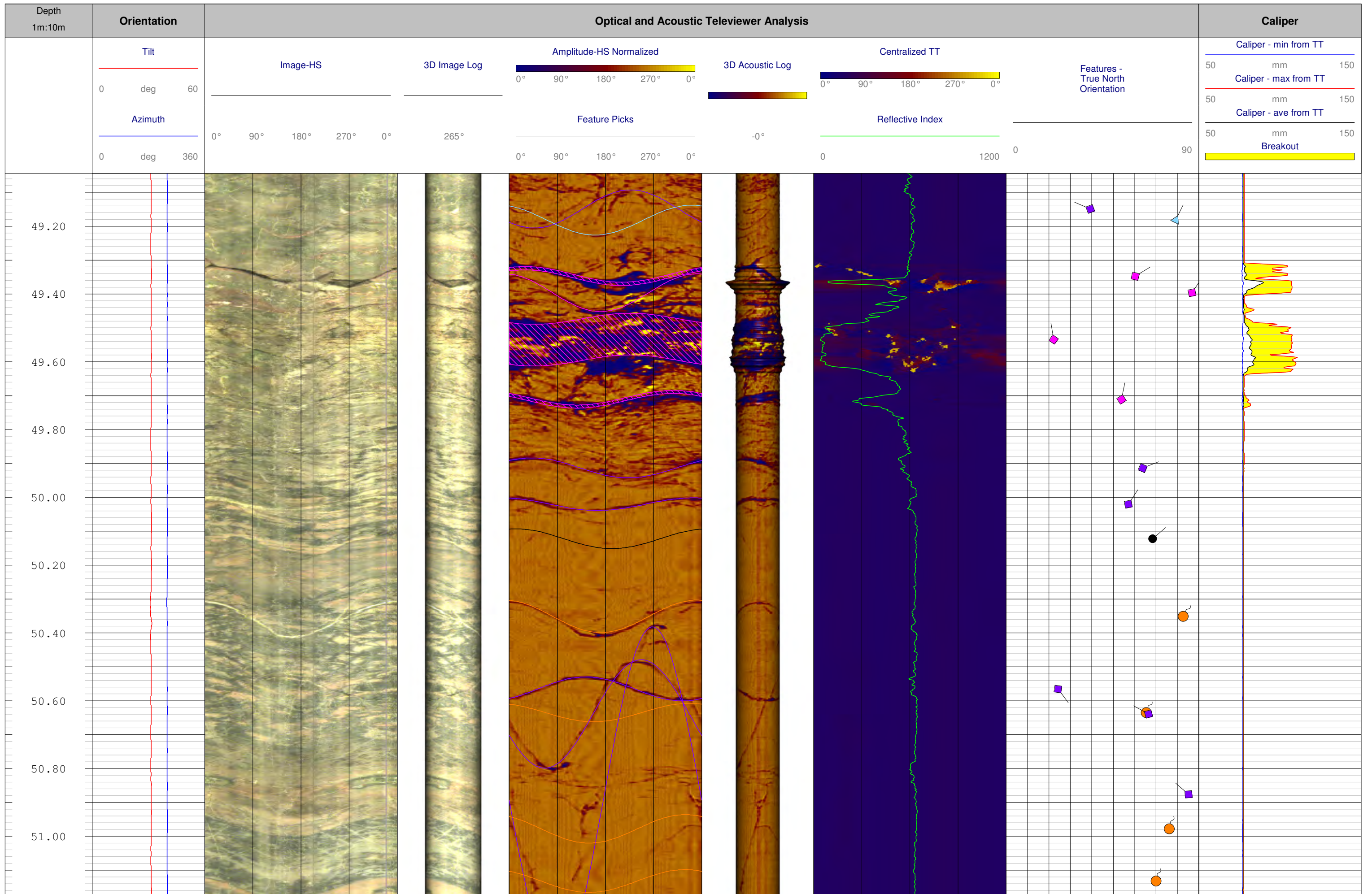


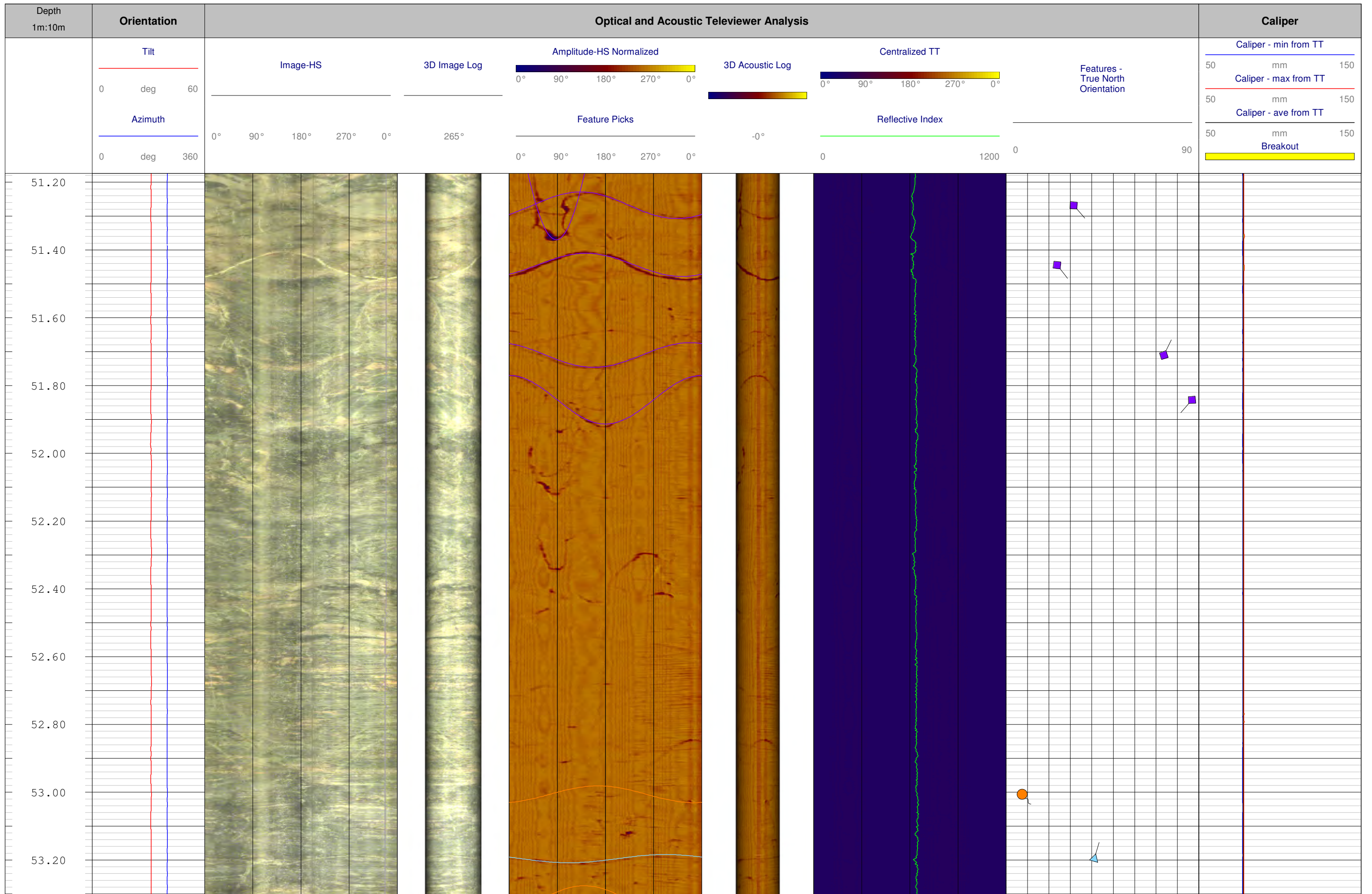


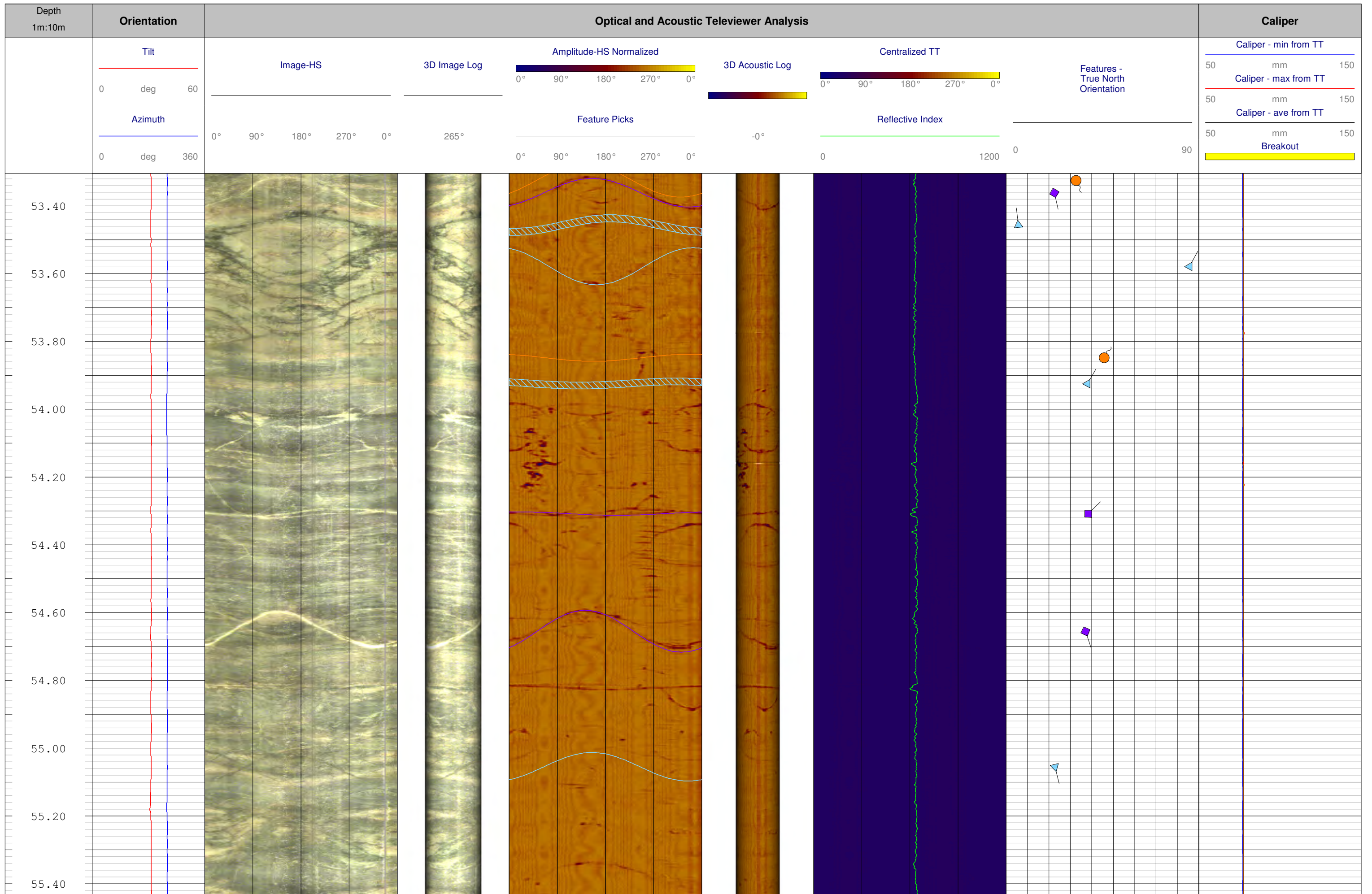


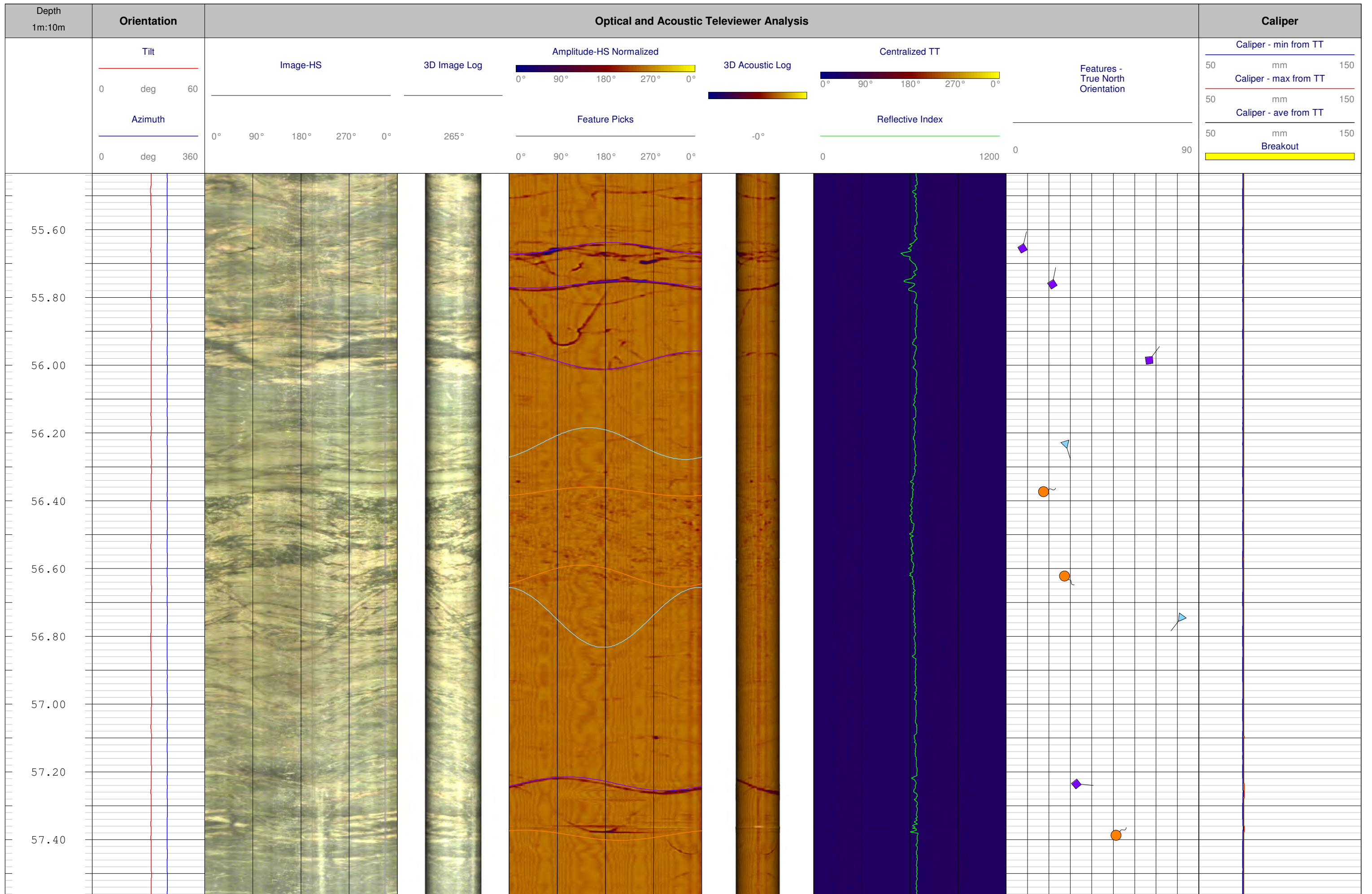


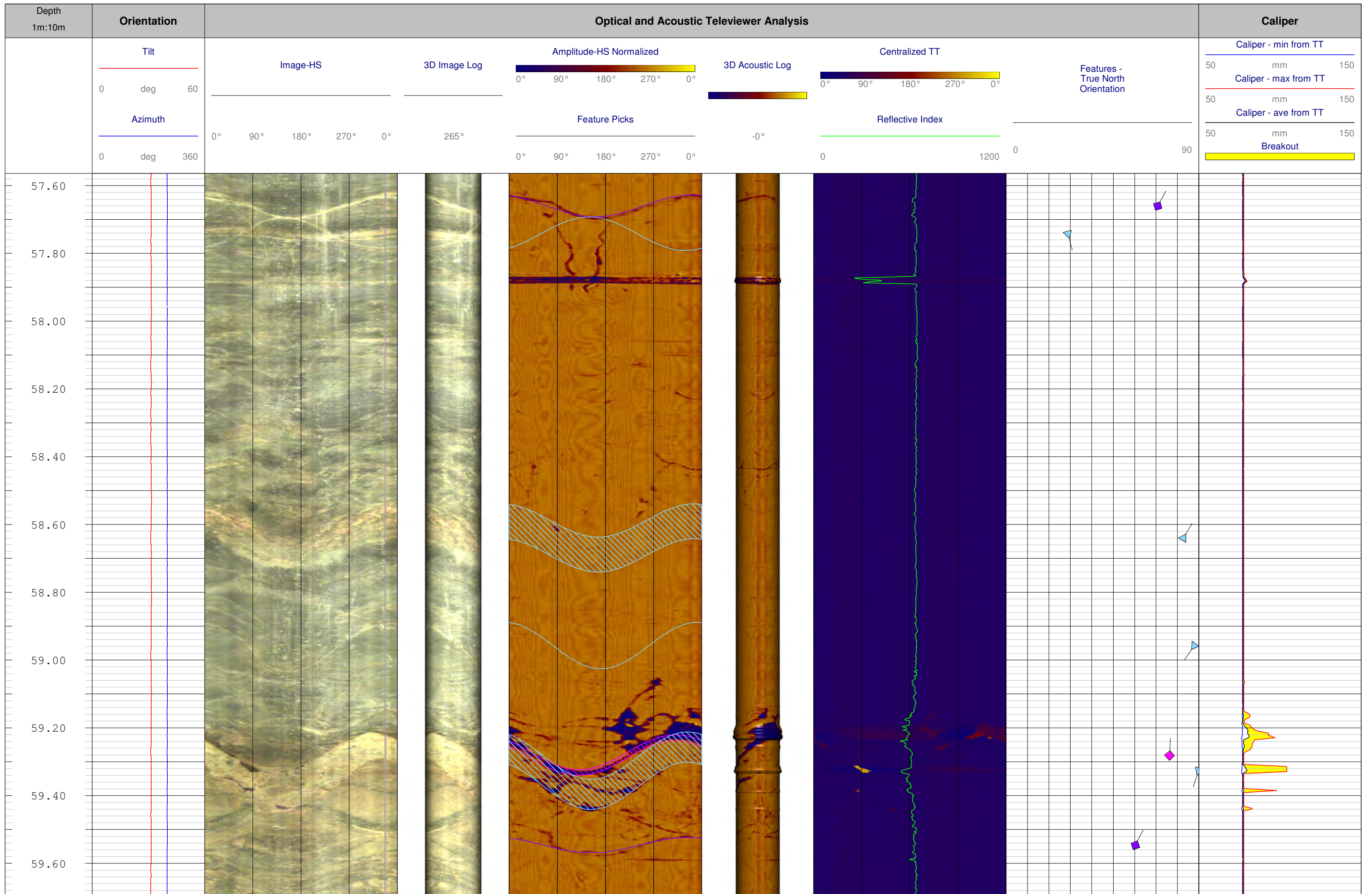


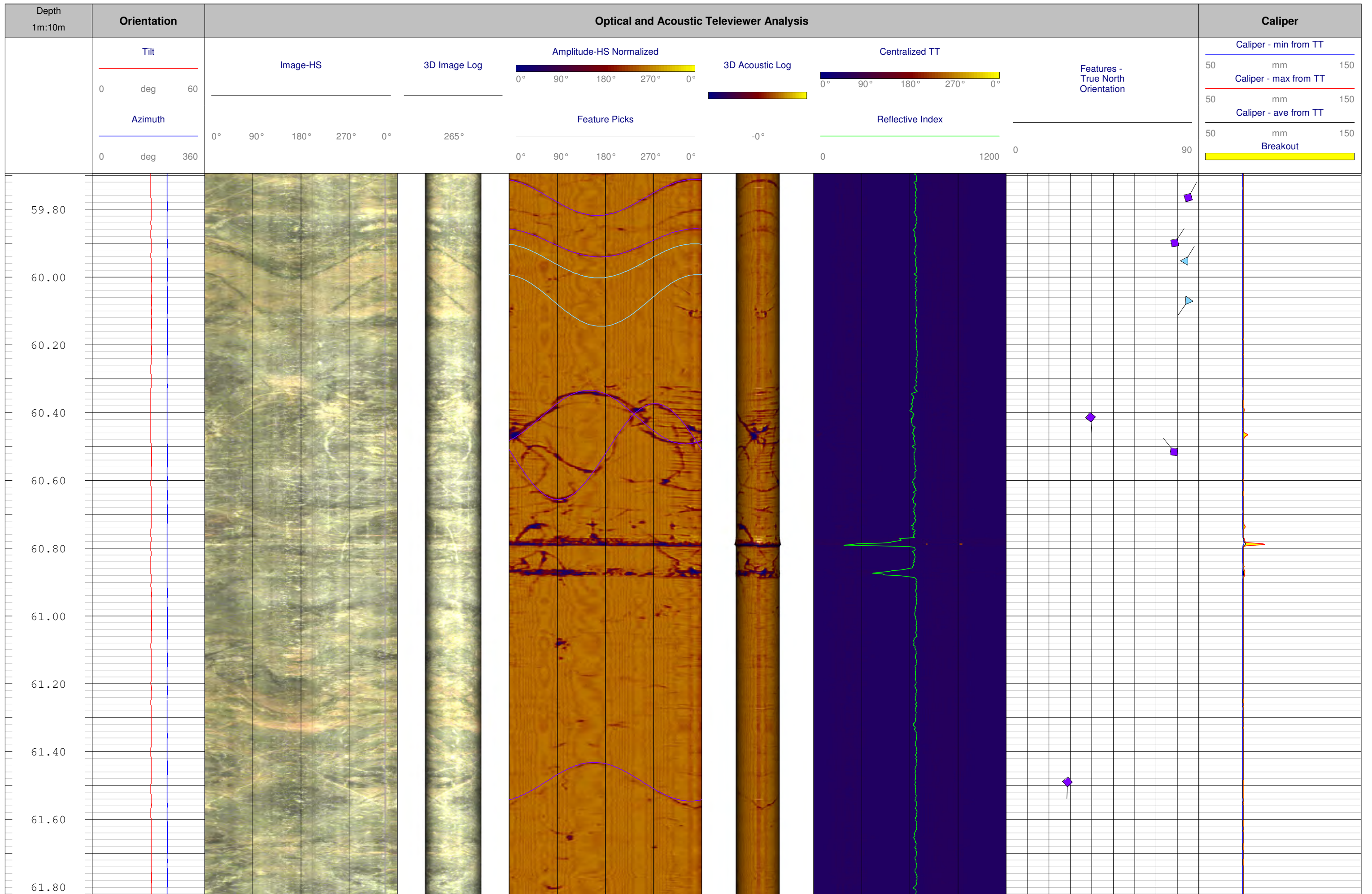


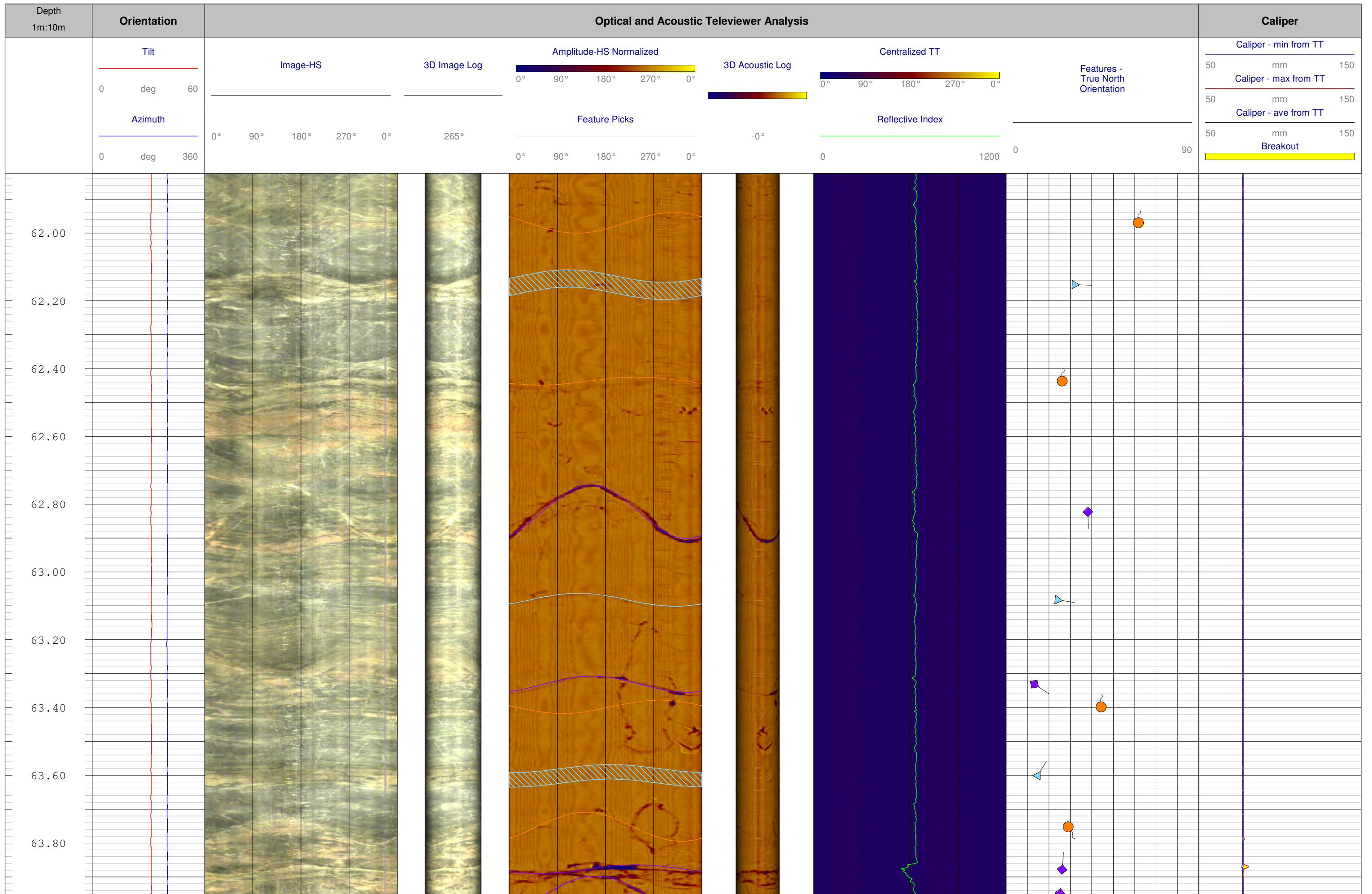


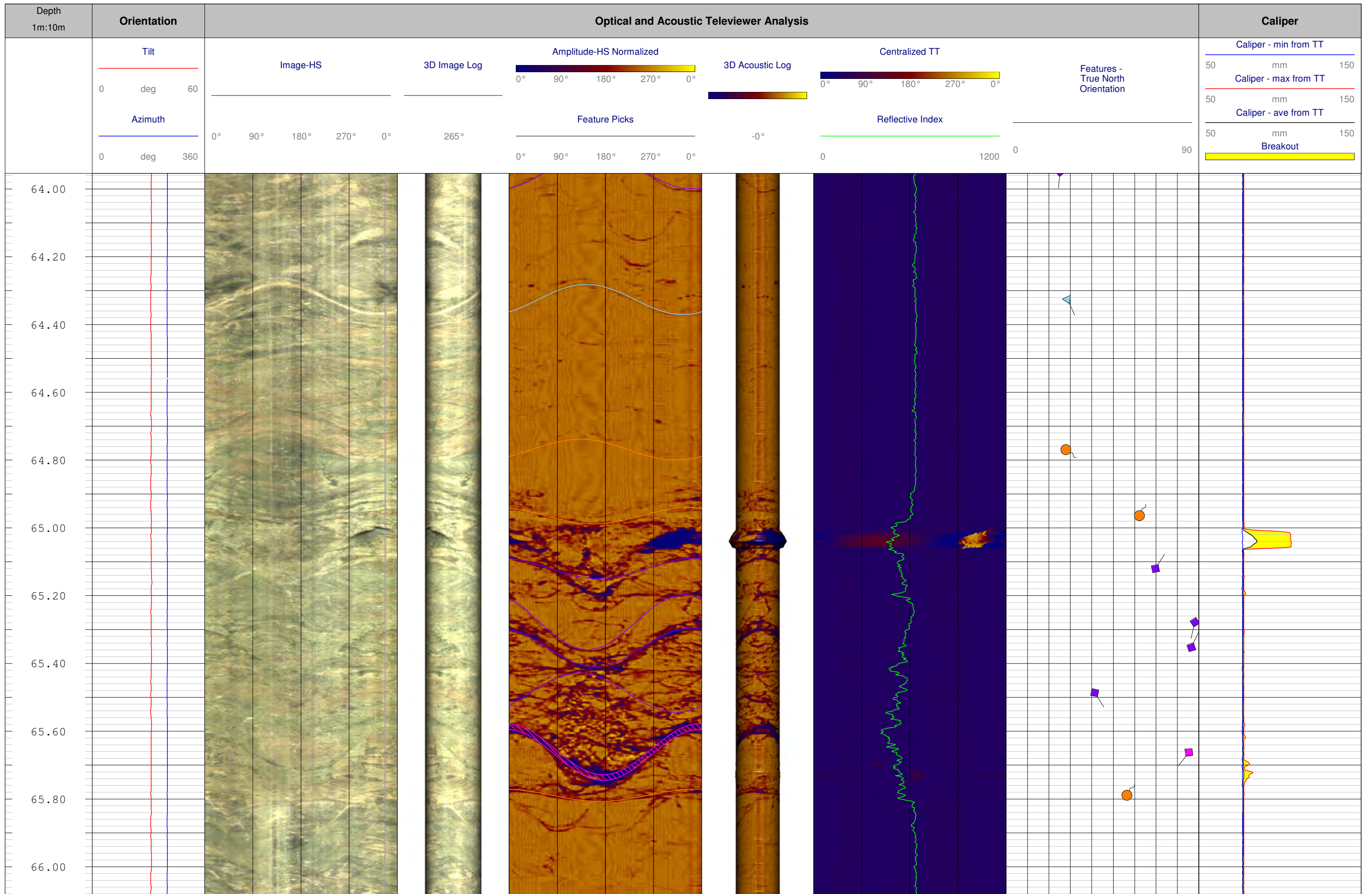


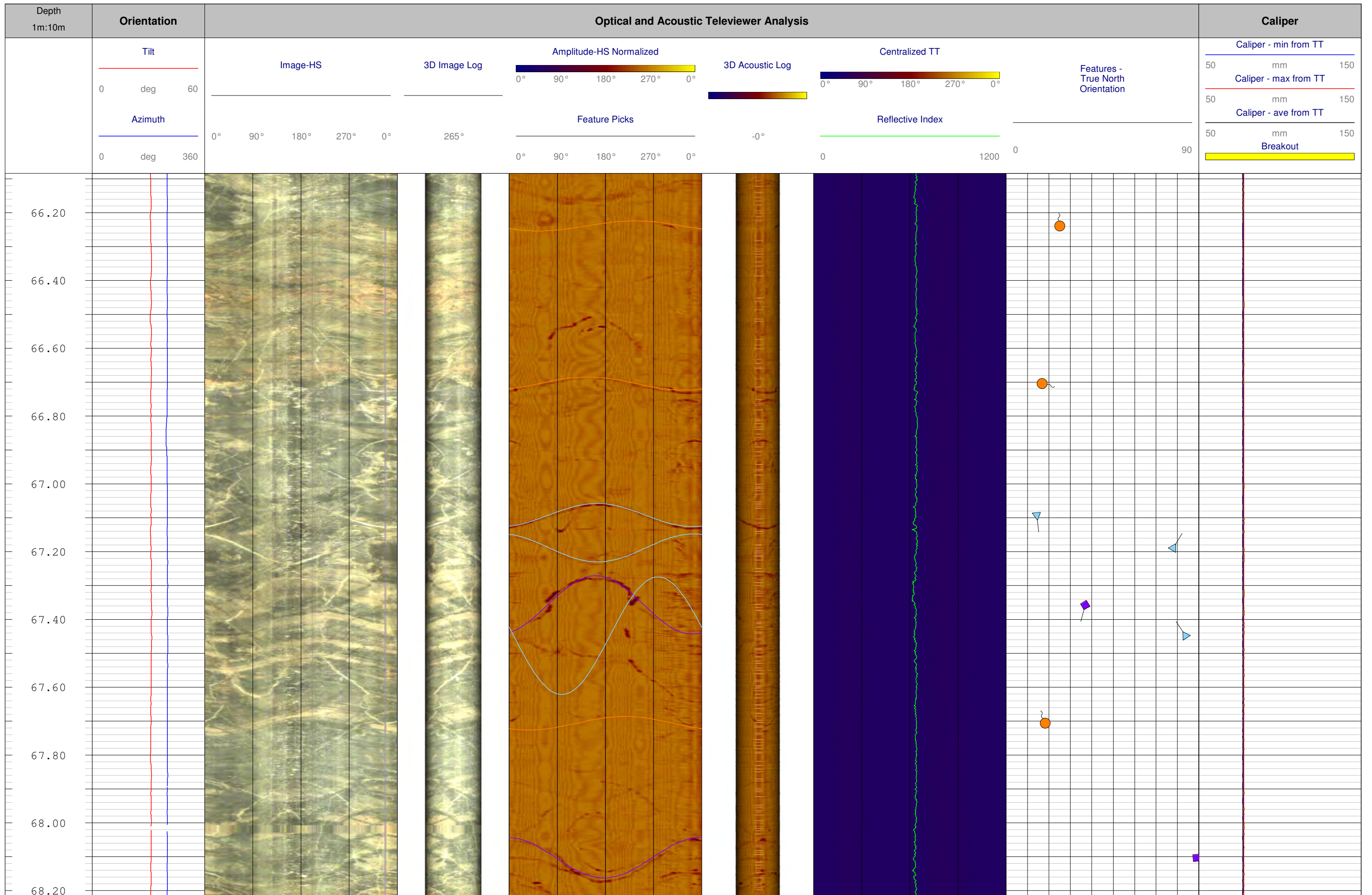


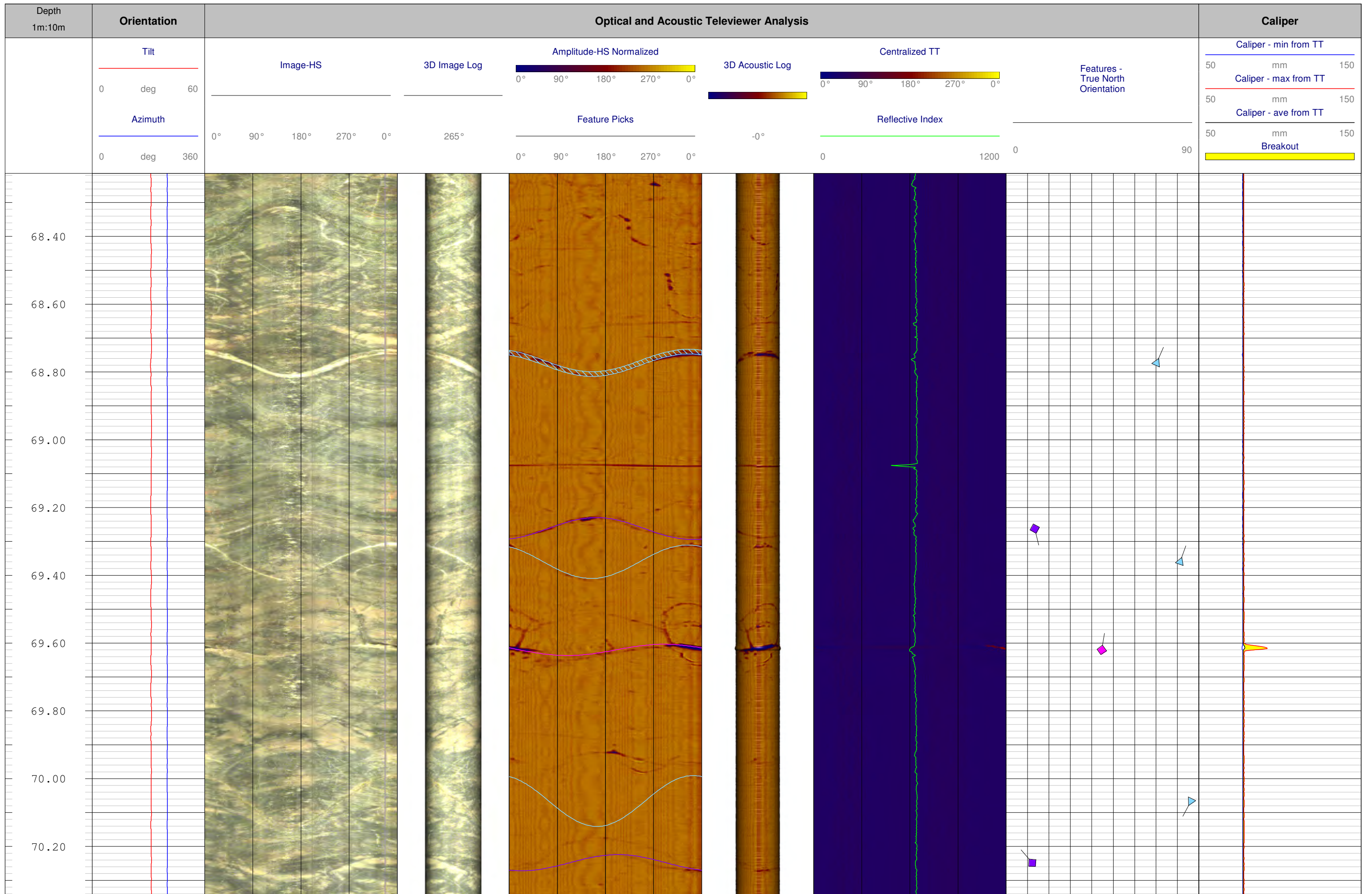


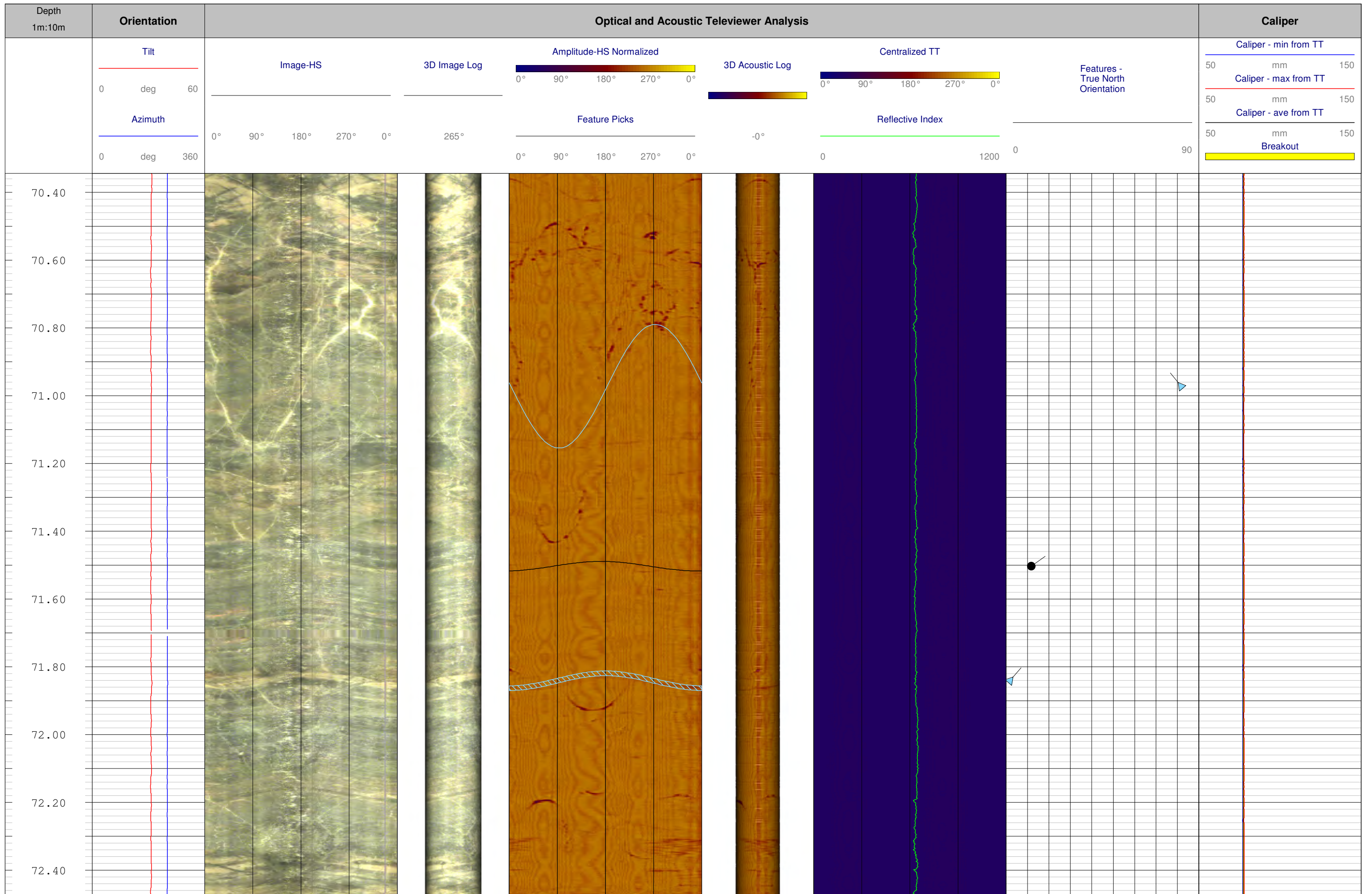


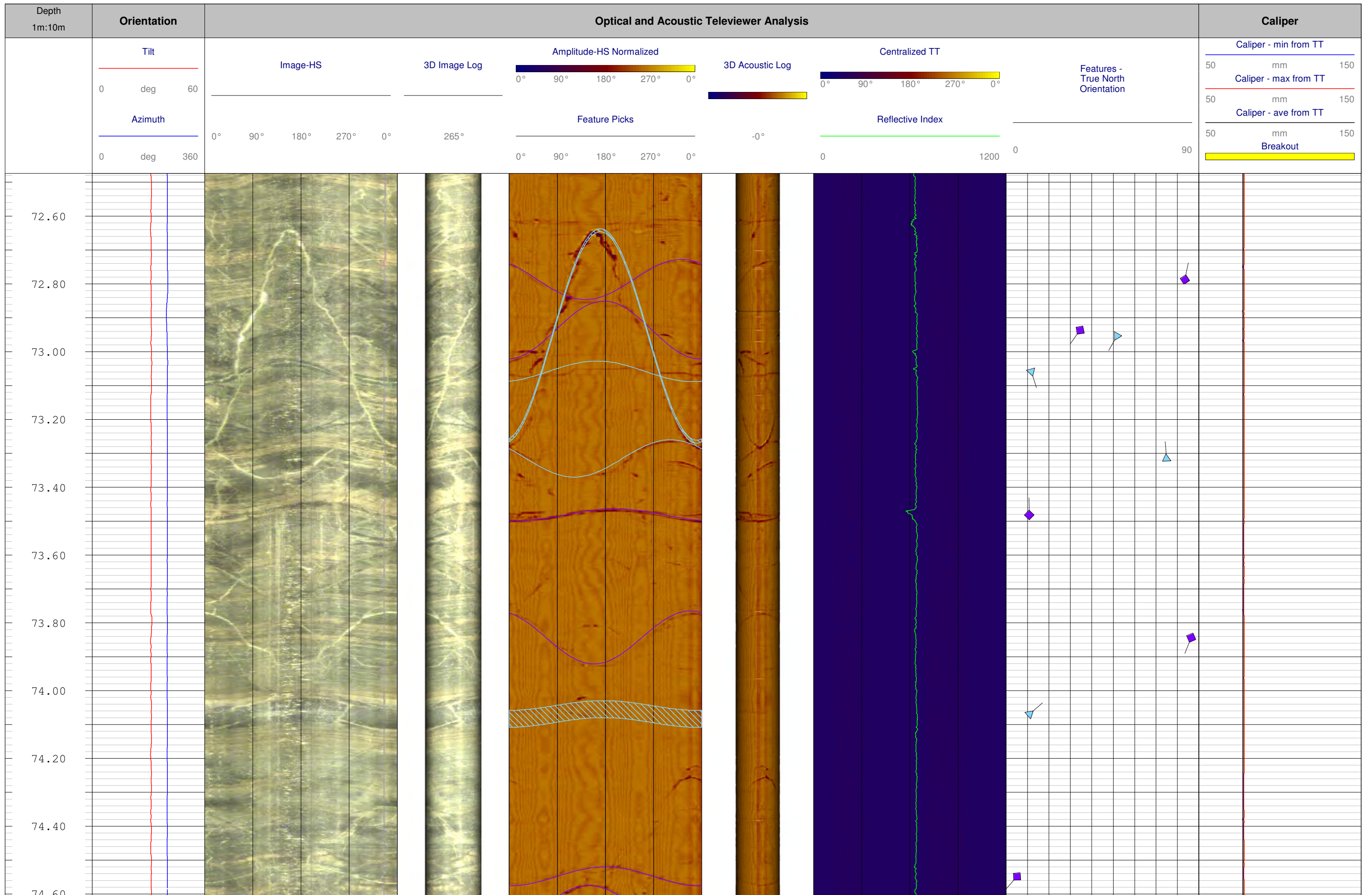


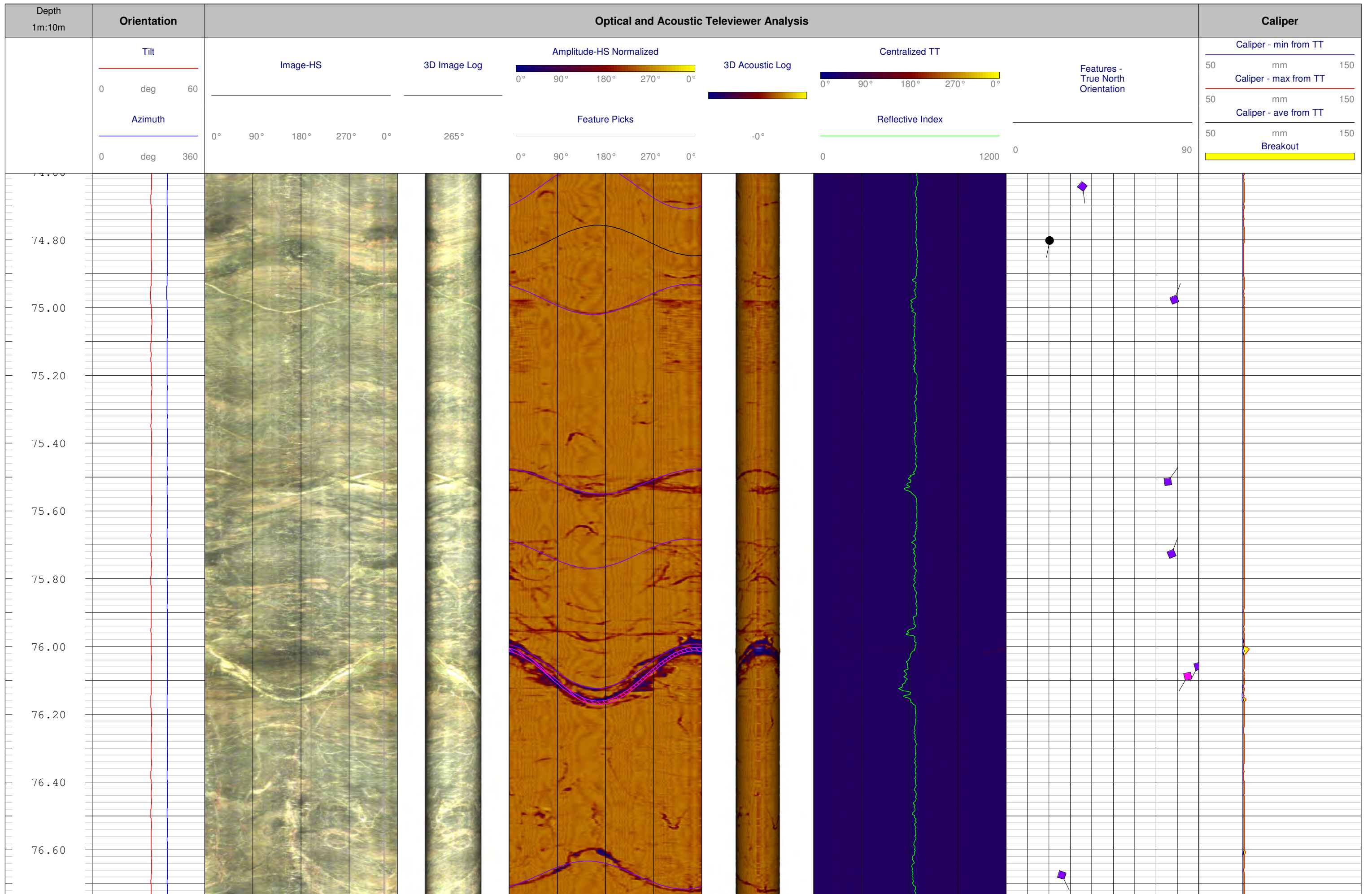


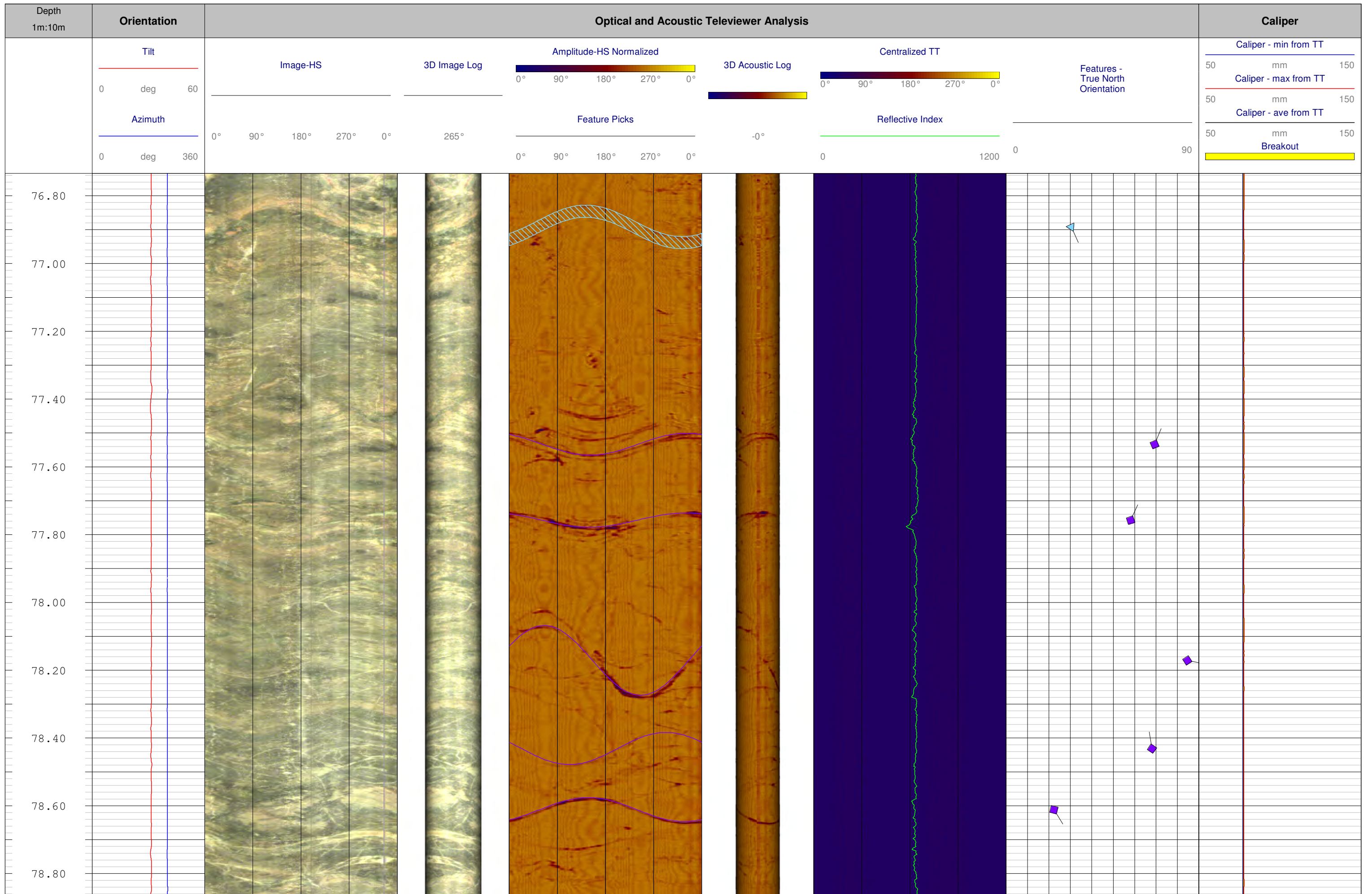


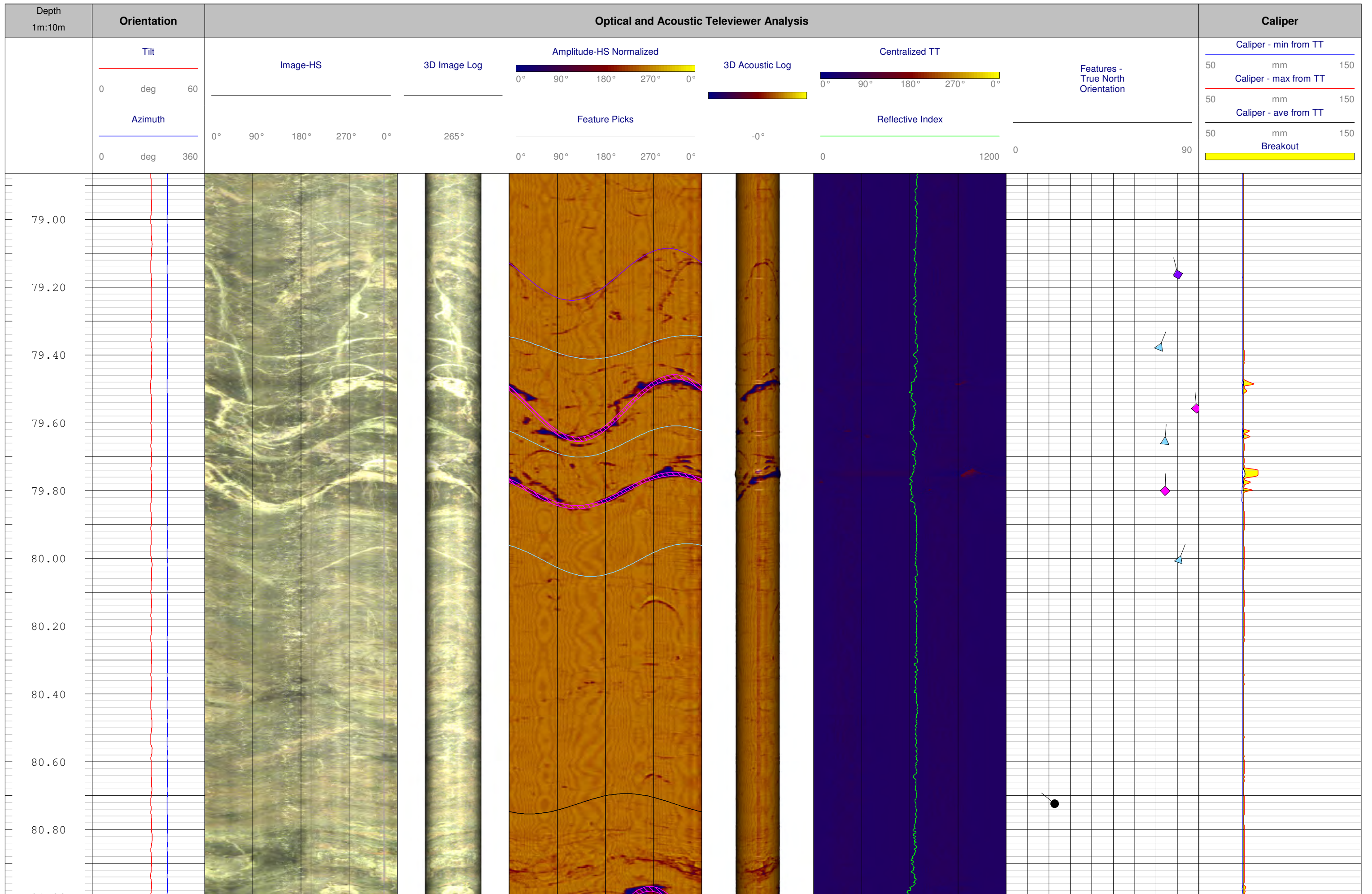


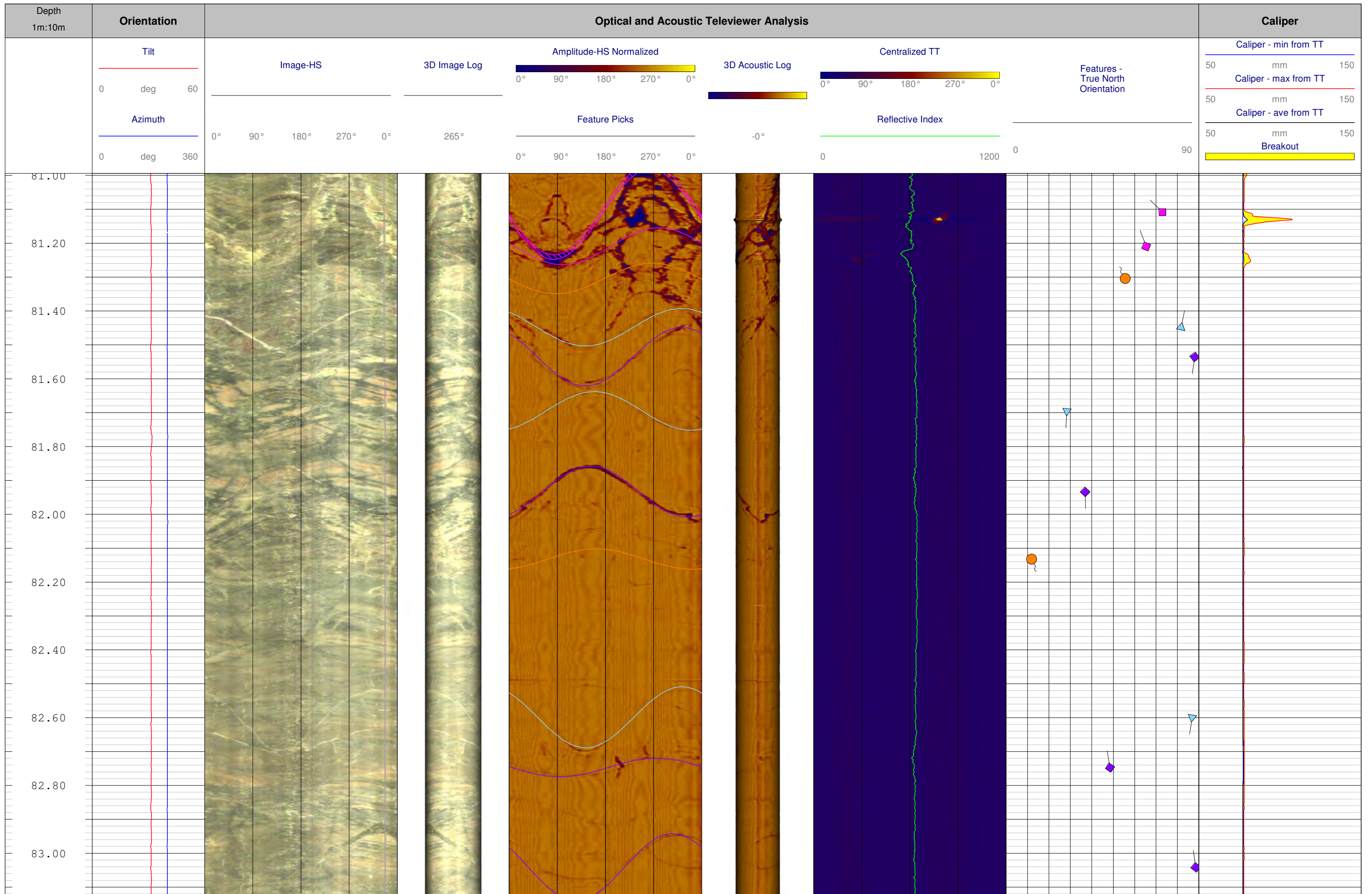


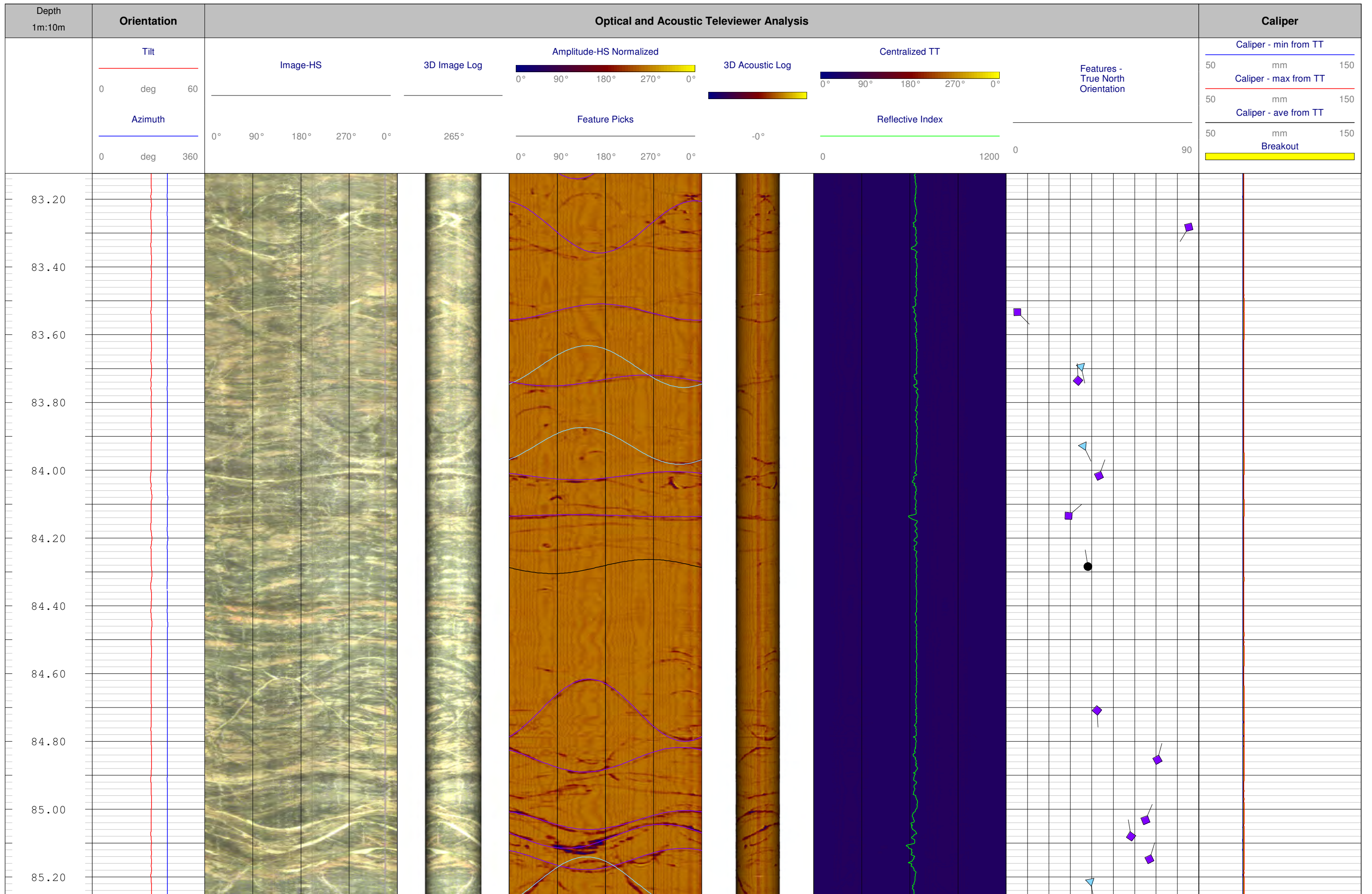


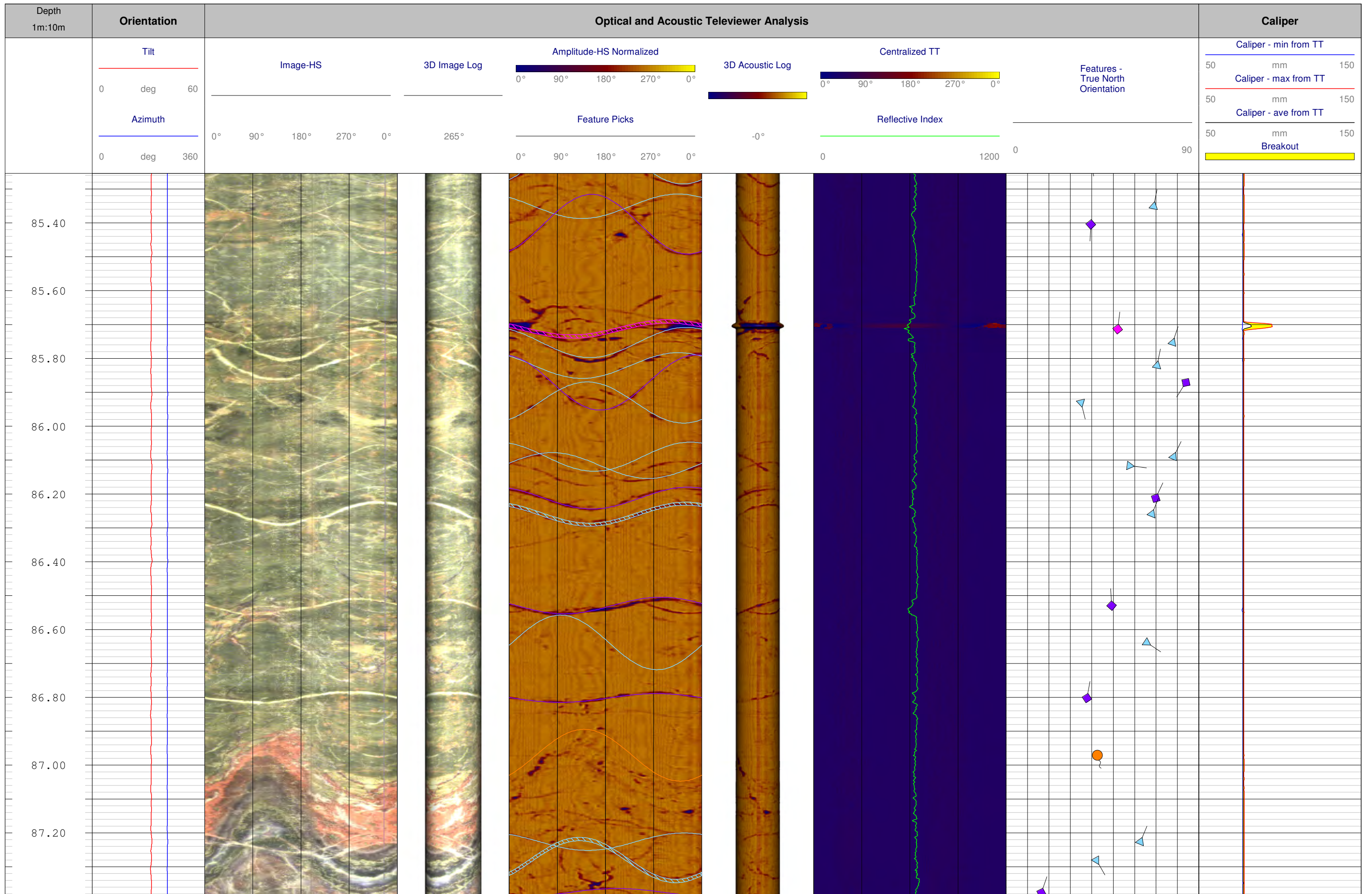


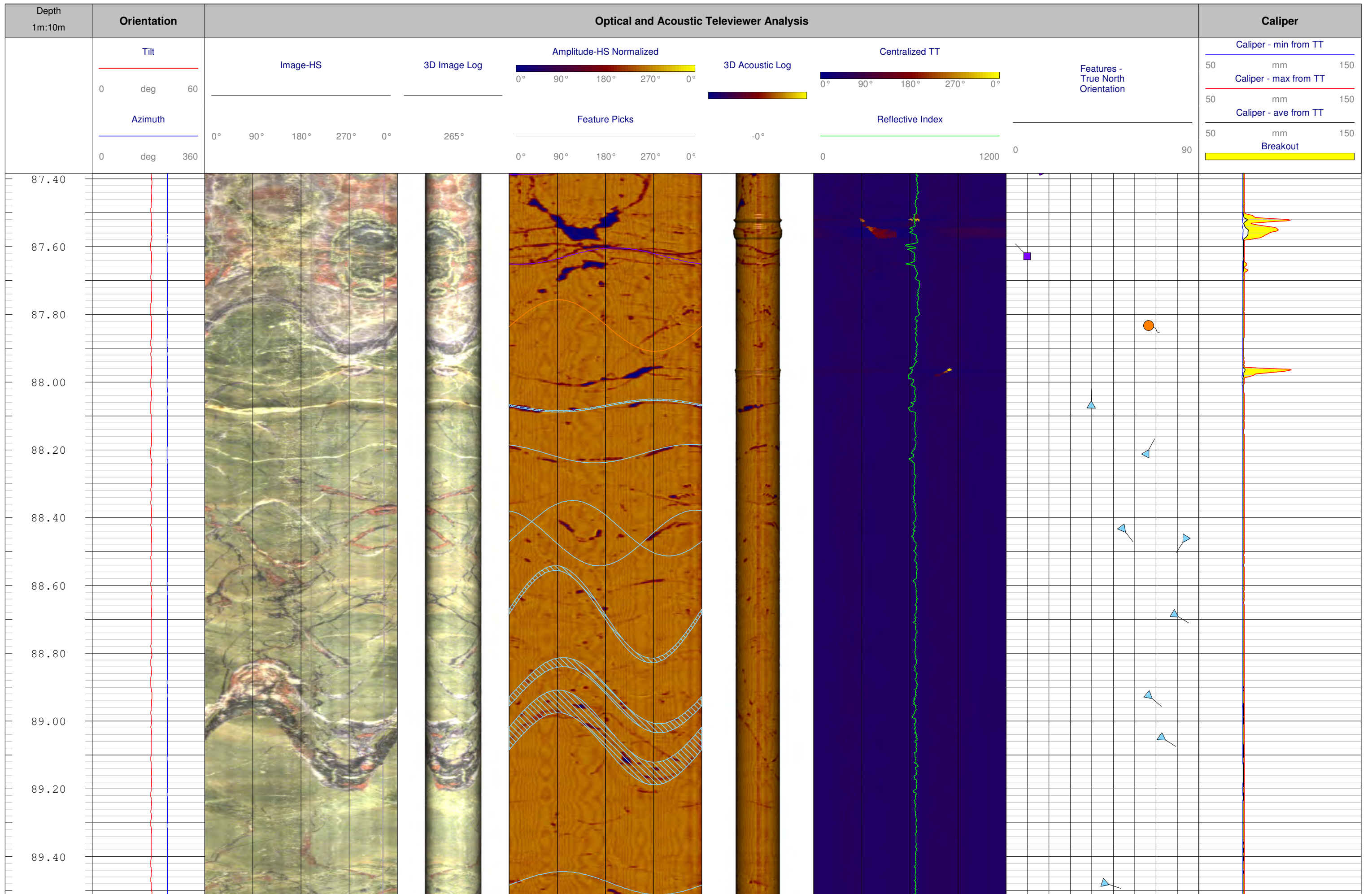


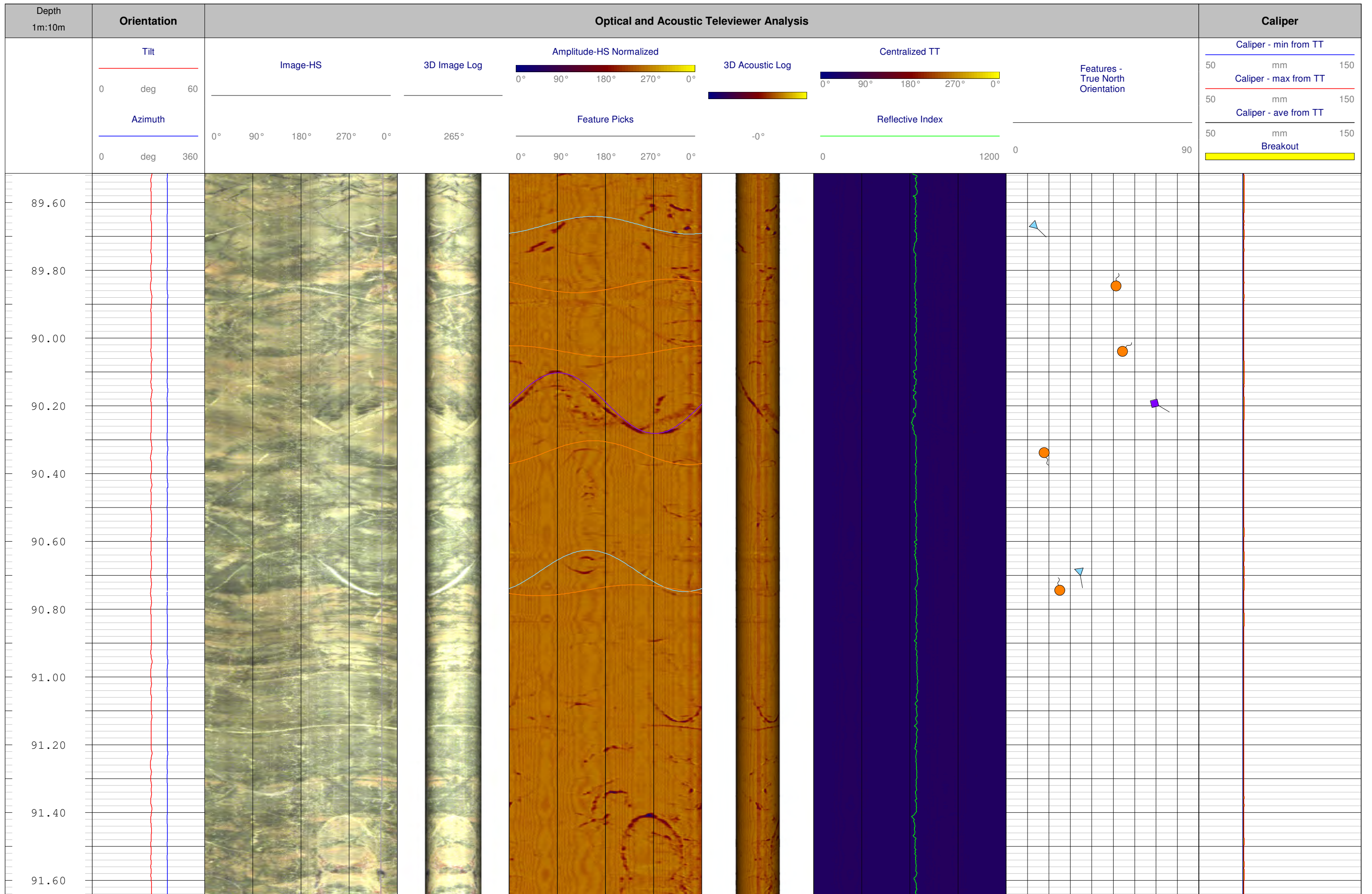


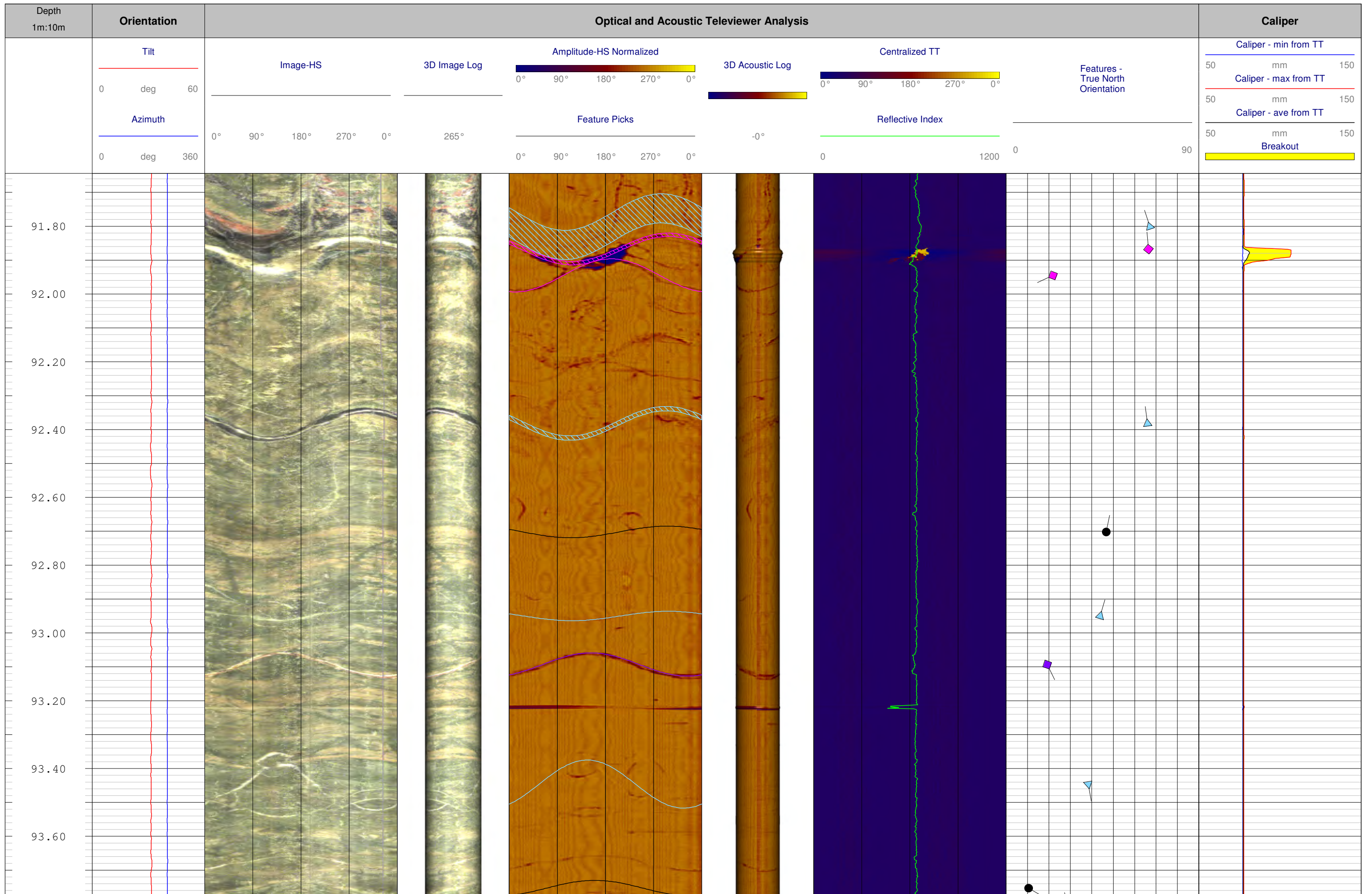


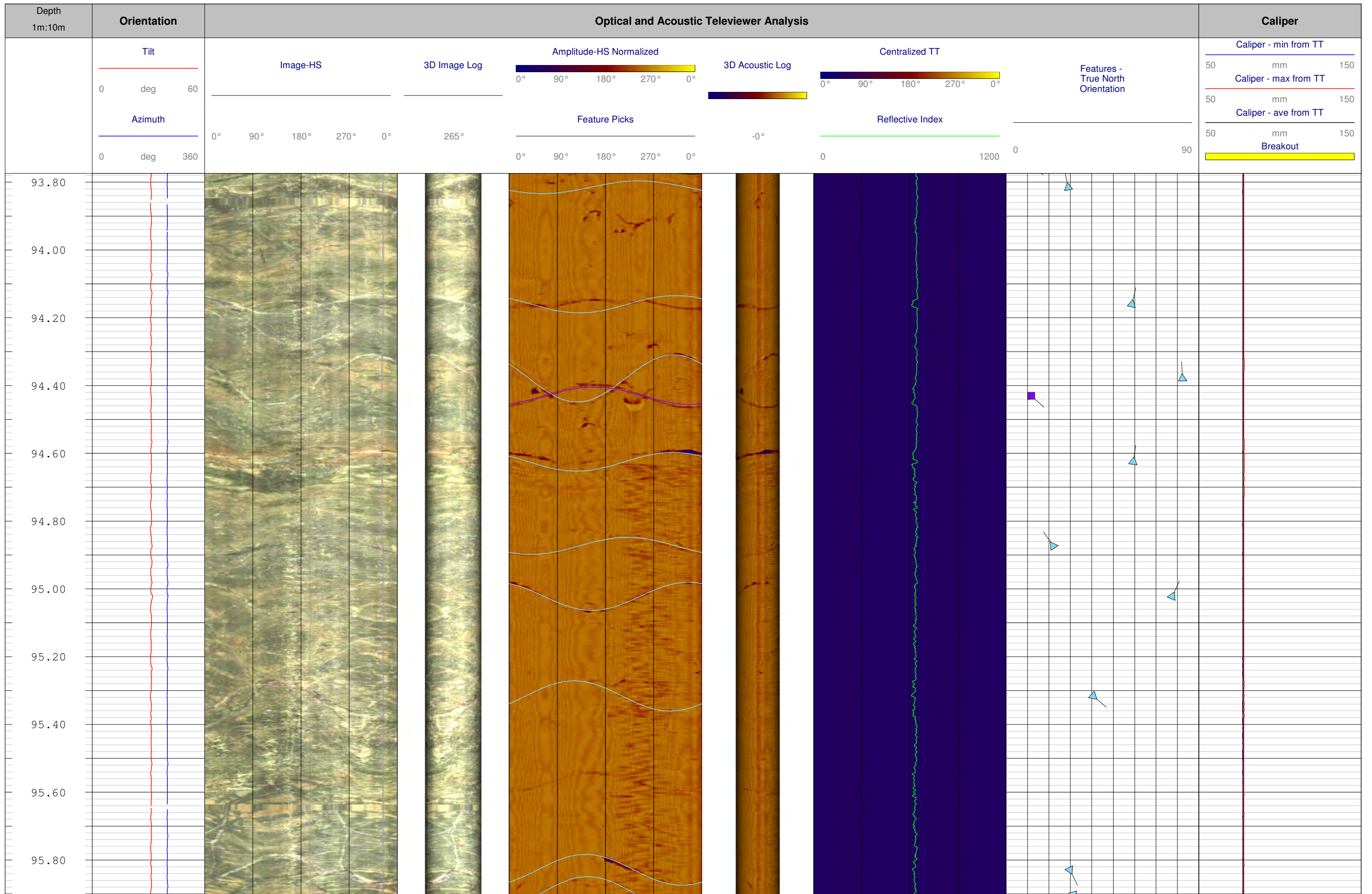


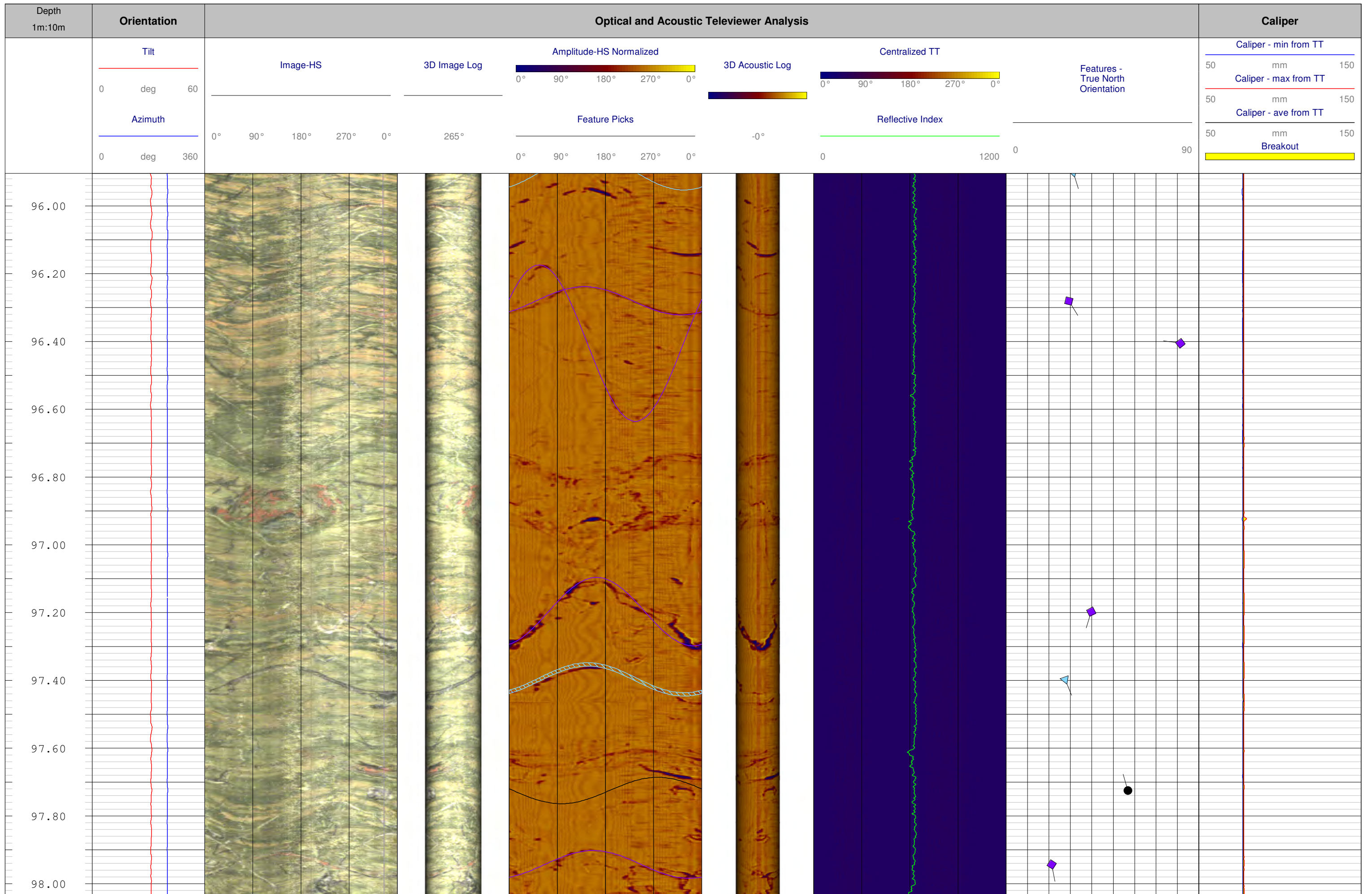


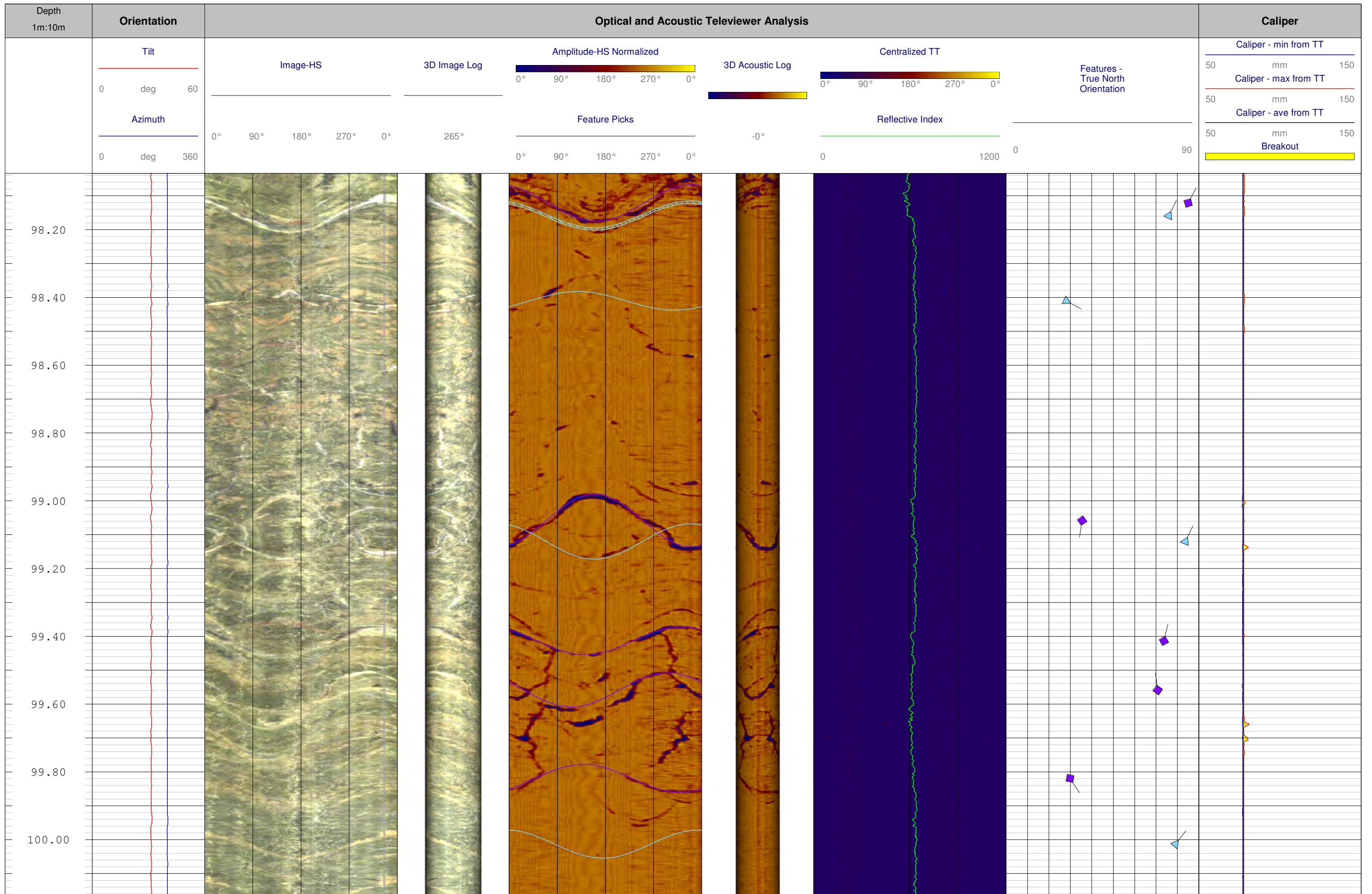


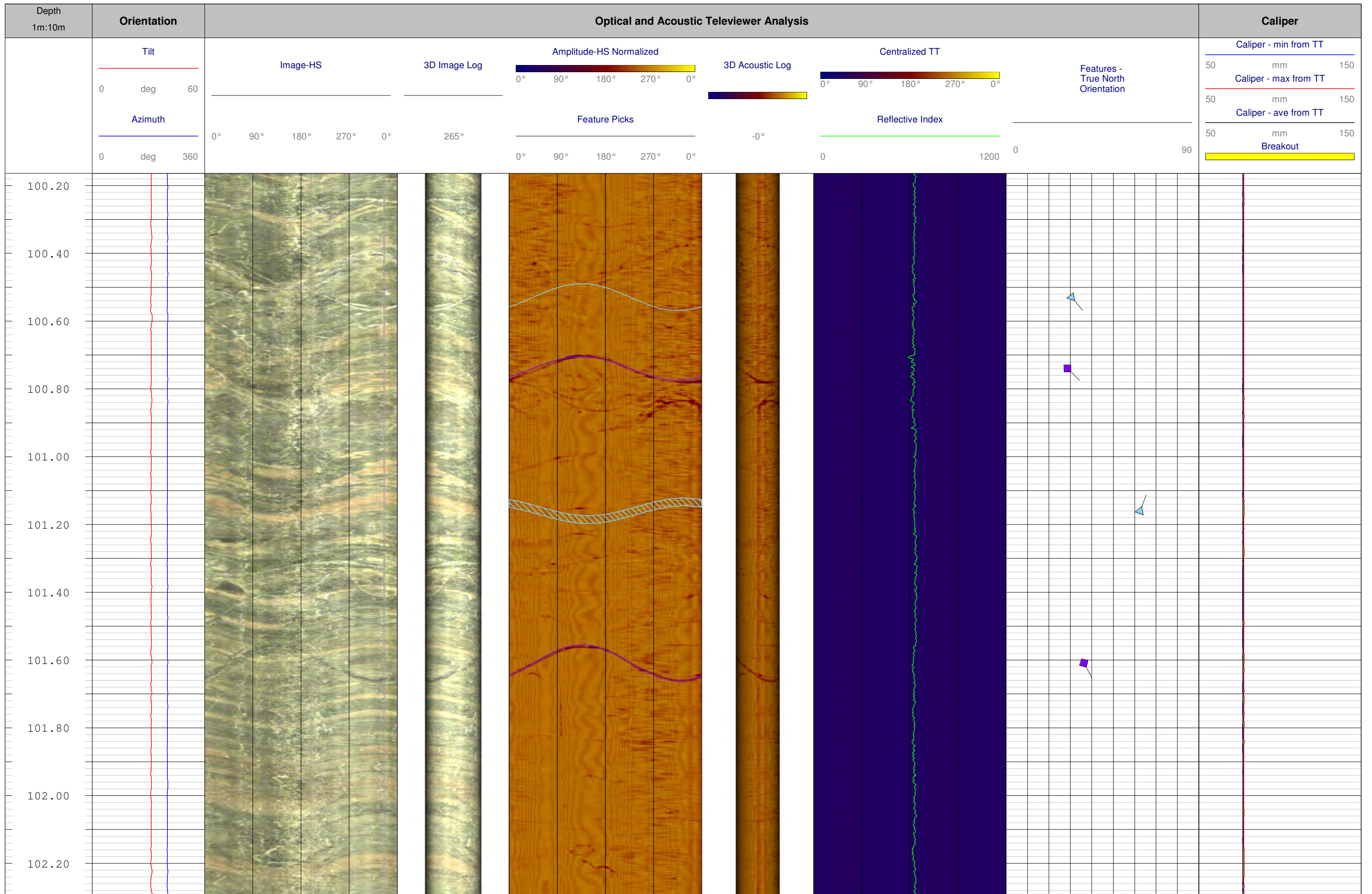


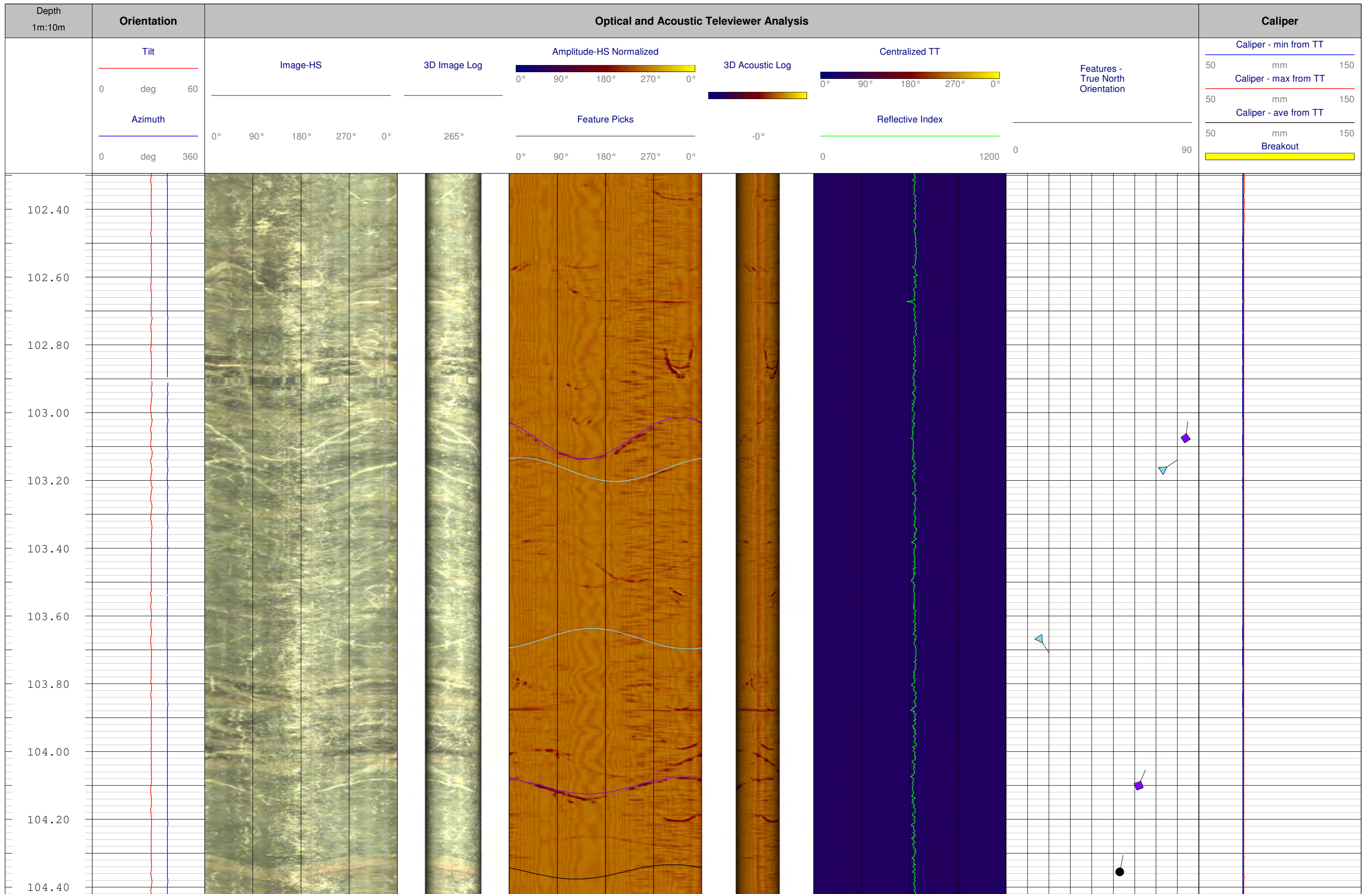


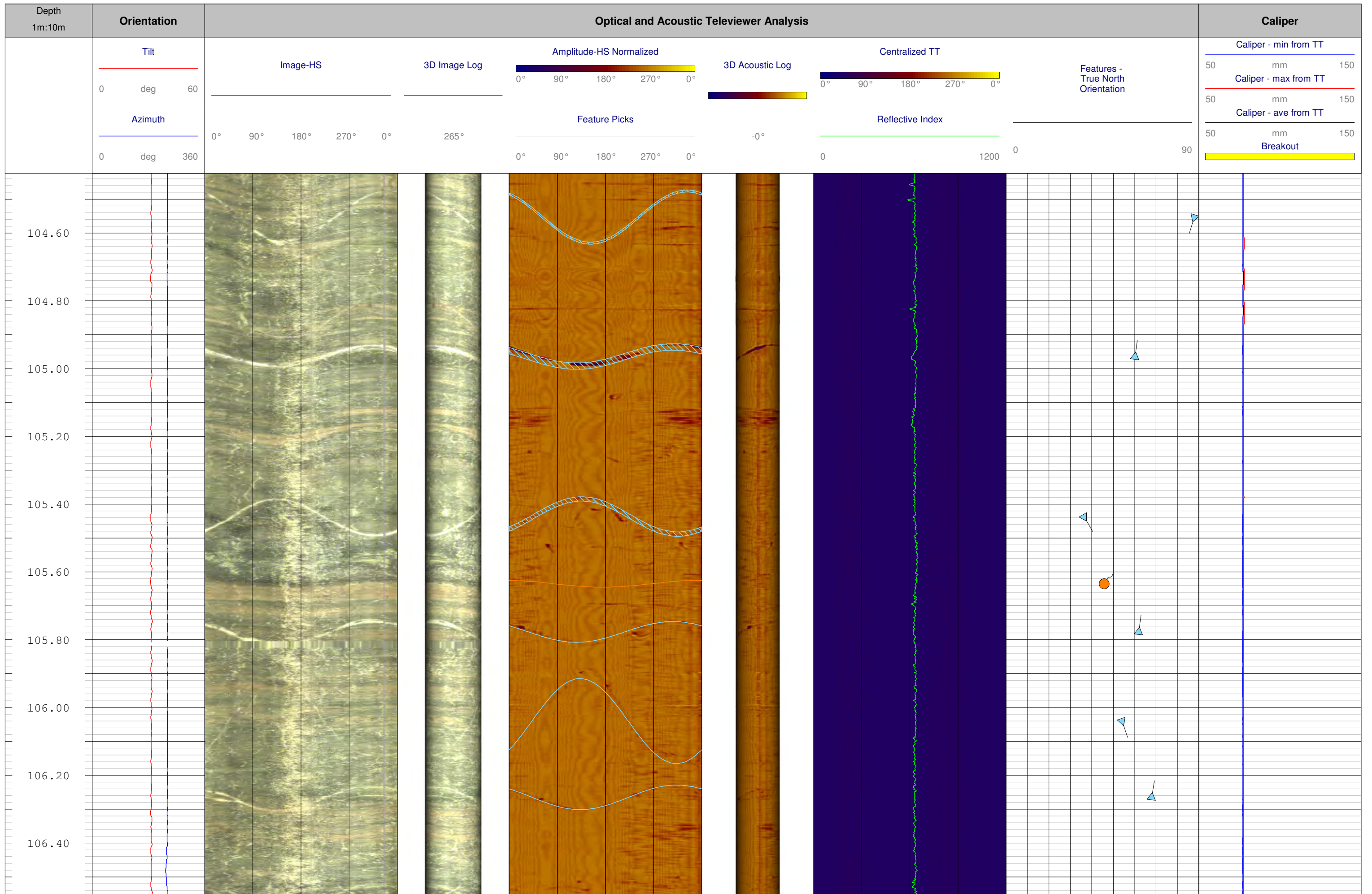


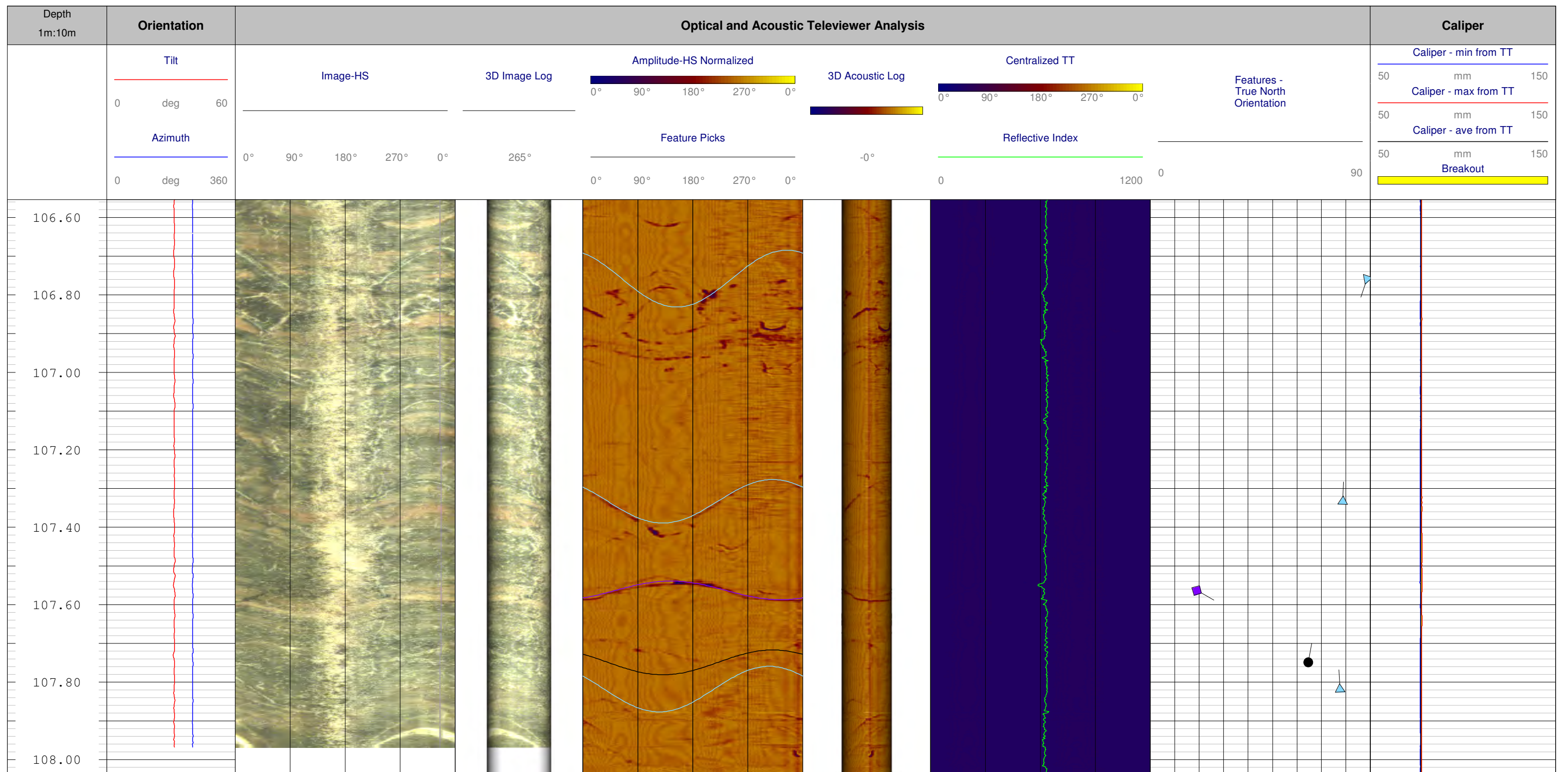












Canada Fluorspar Incorporated Diamond Drill Log Sheet



Drill Hole ID: **GS-14-92**
 Logged By: Alex Chafe
 Start Date: 20-Aug-14
 End Date: 26-Aug-14
 Contractor: Springdale Drilling
 Drill #: 1
 Core Size: NQ
 Final Depth: 400
 Date Surveyed:
 Casing: UNREMOVED 6 m

UTM Coordinates
 Easting: 616377.84
 Northing: 5196081.59
 Elevation: 1123.72
 Grid North Coordinates
 Northing:
 Easting:
 Elevation:
 Location
 Area Section

Units: 616377.84
 5196081.59
 1123.72
 Units: 616377.84
 5196081.59
 1123.72
 AGS Property Line 10+00E

Remarks

Geological and Structural Logging
 Hole Collar Orientation
 Azimuth: 34 UTM
 Dip: -55
 Mag North: 54.3
 Grid North: 0
 Recovery:

Depth (m)	Azimuth	Dip	Remarks
1	19	32.2	-56.2
2	70	33.3	-55.7
3	121	33.6	-56.0
4	172	33.0	-56.1
5	226	35.3	-56.5
6	277	35.0	-56.3
7	334	36.1	-56.3
8	388	36.8	-56.1
9			
10			

Planned Setup
 Northing: 5196086
 Easting: 616381
 Elevation: 1120
 Azimuth: 34
 Dip: -55
 Grid North

Drillhole Header	Lithology				Structural				Core Angle (Degrees)	RQD (%)	Infilling Code	Assays		Tag #	Log Remarks
	From (m)	To (m)	Code	Alteration Code	Structural Code	Jn	Jr	Jf				Width (mm)	CaF ₂ and SS (%)		
GS-14-94	0.00	5.56	OB												Overburden.
GS-14-94	5.56		MS	Chl, K	JT	1	0	3	5560	25					Metasediment. Grey-green metasediment with weak chlorite alteration and m-scale weak K alteration towards top of hole. Meter-scale zones of Jf=4, overall Jf=3 at 20-30°. Green brecciation and reworked CaF ₂ vein, associated with hematite alteration at 30°, surrounded by moderate chlorite alteration. Minor percentage of calcite veinlets throughout approximately parallel to jointing, actual orientations variable.
GS-14-94	10.91	12.70			FZ			4	1790	25					Fracture Zone. Jf increases to 4, where fragments range from 10-50 mm. Chlorite infill.
GS-14-94	17.00	18.27			FZ			4	1270	25					Fracture Zone. Jf increases to 4, where fragments range from 10-30 mm. Chlorite infill.
GS-14-94	18.40	19.10		Chl, Hem	VN				700	30					Green fluorite vein. Reworked green fluorite vein associated with moderate hematization and minor calcite veinlets. Weak shear surrounds vein associated with moderate chloritization. Fluorite vein ~120 mm thick. Detailed photo taken.
GS-14-94	52.23	52.26			CT				30	40					Metasediment-rhyolite contact. At 40°, sharp contact with cm-scale moderate chlorite alteration in metasediment. Rhyolite not altered.
GS-14-94	52.26	72.52	RHY	Chl	JT	2	0	3	20260	25, 5					Pink-orange quartz-feldspar porphyritic rhyolite. Nil to weak chlorite alteration and chlorite infill along moderate-strong fracture and jointed rock. Cm- to dm-scale areas of Jf=4. Cm-scale areas of grey-brown shear and alteration at 60° throughout, trace concentration. Chlorite-filled veinlets throughout oriented at 60°.
GS-14-94	72.52	95.95	MS	Chl	JT	2	0	3	23430	50					Grey-green metasediment with increased chlorite and K alteration from above unit. Chlorite alteration is moderate and K-alteration is moderate and on dm-scale. Areas of K alteration are associated with mm- to cm-scale pyrite blebs. Bedding is at 40°. Alteration and breccia with moderate hematization on m-scale, from 95.95-97.35 m associated with minor green-blue fluorite in euhedral crystals (macro-photos taken). Below 230.50 m, percentage of calcite veins with nil to trace green fluorite, forming a low abundance of weak calcite stockwork within metasediment. Dm-scale weak hematite alteration within. Minor dm-scale moderate brecciation throughout.
GS-14-94	95.95	97.35	GZO		BX, VN				1400						AGS structure lacking significant fluorite. Metasediment breccia associated with fracture and blue fluorite vein. Zone of alteration and brecciation within metasediment. Fracture reaches Jf=4 on dm-scale. Breccia is matrix-supported on cm-scale and weak fragment-supported throughout. Calcite veinlets throughout. At end of alteration zone, 40 mm wide blue fluorite vein with euhedral crystals up to 5 mm. SD between 20 and 50°. Core becomes Jf=2 moving downhole.
GS-14-94	97.35	357.27	MS	Chl	JT	2	0	3	259920	50					Grey-green metasediment similar to the above Metasediment unit.
GS-14-94	104.10	104.45			FLT, Gg				350	35					Faulting and gouge. Faulting associated with hematite alteration and ~20 mm calcite vein with clay to fine sand, hematite-coated gouge. Vein and fault oriented at 35°. Nearly perpendicular to bedding with S0-S0° (photo taken).
GS-14-94	164.30	165.38			BX				1080	30					Moderate-strong brecciation. K-alteration of subangular fragments of fragment-supported breccia. Shear approximately 30°. Interval moderate-strongly jointed with chlorite infill.
GS-14-94	172.72	173.05			VN				10	15					Fluorite-calcite vein. Green-clear fluorite vein with minor calcite, forming weak stockwork surrounding vein. Oriented at 15°, 10 mm thick.
GS-14-94	218.52	221.75			FZ, BX, FLT					30					Fracture and fault zone above matrix-supported breccia with minor green fluorite. Shear and faulting direction between 25-30° with chlorite-calcite infill and fragments of metasediment. Moderate-strong chlorite alteration throughout. Fragments range from 10 mm to 100 mm outside of breccia.
GS-14-94	220.78	221.56			BX					30					Matrix-supported breccia. Very fine-grained chlorite matrix and <1 mm to 5 mm subrounded calcite and metasediment fragments. Galena within <1 mm to 3 mm crystals in stringers ~ 20 mm thick.
GS-14-94	231.95	232.16			VN				210						Green fluorite vein. Green fluorite infills metasediment breccia, 1-3 mm thick. Variable orientations (Photo taken).
GS-14-94	241.05	241.52			BX				470	35					Metasediment Breccia. Predominantly fragment-supported with cm-scale matrix-supported breccia, with moderate chloritization and weakly hematized fragments of metasediment, subrounded to angular. ~10 mm wide vein of green fluorite vein parallel to shear (photo taken). At 35°.
GS-14-94	246.12	252.23			BX				6110						Metasediment breccia. Fragment- and matrix-supported with chlorite matrix, moderate chloritization, and weakly hematite altered fragments. Brecciation on m-scale. Only minor calcite and nil fluorite. Shear orientation unclear. Photo taken.
GS-14-94	253.00	253.10			VN				100	40					Anastomosing thin, 1-3 mm green fluorite vein with minor calcite, around 40°.
GS-14-94	279.24	279.30			VN				5						Calcite vein. Thin, 5 mm calcite vein with euhedral crystals along vuggy vein wall. Crystals ~3 mm.
GS-14-94	286.60	287.24			BX				640						Metasediment breccia. Minor calcite infills fragment-supported weak metasediment breccia.
GS-14-94	305.85	306.84			BX				990						Matrix-supported metasediment breccia with calcite+fluorite infill. Fragments are metasediment, 3-10 mm and subangular. Photo taken.
GS-14-94	310.17	310.70			BX				530						Metasediment breccia. Fragment-supported weak to moderate breccia with vuggy calcite+quartz and minor blue fluorite. Metasediment is weakly K-altered. Photo taken.
GS-14-94	314.43	314.79			VN				360	20					Calcite+chlorite minor purple fluorite vein. Clear and purple fluorite vein with minor calcite, 20 and 150 mm thick at top and bottom of interval. Weak metasediment breccia with calcite infill. Euhedral purple fluorite up to 5 mm covered in <3 mm calcite and quartz. Trace percentage of pyrite.
GS-14-94	318.57	319.19			BX				620	55					Fluorite+calcite breccia and stock work. Fragment-supported metasediment breccia with green-purple fluorite with minor calcite infill. Galena banding, 1-3 mm surrounding fluorite crystals. Vuggy green fluorite. Shear at 55°.

Canada Fluorspar Incorporated Diamond Drill Log Sheet



Drill Hole ID: Tyler Power
Logged By: Tyler Power
Start Date: 23-Sep-11
End Date: 25-Sep-14
Contractor: Springdale Drilling
Drill #: Rig #1
Core Size: NQ
Final Depth: 190.35
Date Surveyed:
Casing: NQ - Left in

UTM Coordinates
Easting
Northing
Elevation
Grid North Coordinates
Northing
Easting
Elevation
Location
Area
Section

Units:
Remarks
Units:
Remarks
AGS Property
Line 19-00E

Hole Collar Orientation
Azimuth: 214 UTM
Dip: -60
Mag North:
Grid North:
Recovery:

Geological and Structural Logging

Table with columns: Depth (m), Azimuth, Dip, Remarks. Rows 1-9.

Table with columns: Depth (m), Azimuth, Dip, Remarks. Rows 1-9.

Planned Setup
Northing
Easting
Elevation
Azimuth
Dip
Grid North

Main geological log table with columns: Drillhole Header, From (m), To (m), Lithology Code, Alteration Code, Structural Code, Sub-code, Width (mm), Core Angle (Degrees), RQD (%), Infilling Code, Assays, Tag #, Log Remarks. Includes detailed descriptions of rock units and alteration zones.

Canada Fluorspar Incorporated Diamond Drill Log Sheet



Drill Hole ID:

Logged By: Tyler Power
 Start Date: 23-Sep-41
 End Date: 25-Sep-14
 Contractor: Springdale Drilling
 Drill #: Rig #1
 Core Size: NQ
 Final Depth: 190.35
 Date Surveyed:
 Casing: NQ - Left in

UTM Coordinates

Easting
 Northing
 Elevation
 Grid North Coordinates
 Northing
 Easting
 Elevation
 Location
 Area
 Section

Units:

0+70S
 19+00E
 1119

Remarks

AGS Property
 Line 19+00E

Geological and Structural Logging

Hole Collar Orientation

Azimuth: 214 UTM
 Dip: -60
 Mag North:
 Grid North:
 Recovery:

Down the hole Surveys

Depth (m)	Azimuth	Dip	Remarks
1	19	225.7	-63.7
2	70	218.2	-59.7
3	121	219	-59.6
4	172	219.4	-59.7
5			
6			
7			
8			
9			
10			

Planned Setup

Northing
 Easting
 Elevation
 Azimuth
 Dip
 Grid North

Drillhole Header	Lithology		Alteration Code	Structural Code	Structural			Width (mm)	Core Angle (Degrees)	RQD (%)	Infilling Code	Assays		Tag #	Log Remarks
	From (m)	To (m)			Jn	Jr	Jf					CaF ₂ and ISE (%)	ISE (%)		
GS-14-113	153.00	154.00						1.00						92945	BX/MS unit; 2%-5% CaF ₂ ; P>RYC-GWB; hematized within; mg BX within in filled by cement/CaCO ₃ + Qtz; minor Py/sulphides within;
GS-14-113	154.00	154.57						0.57						92946	BX/MS unit; 3%-5% CaF ₂ ; P>RYC-GWB; infill/fracture filling mineralization; altered (Cl + K); trace sphalerite;
GS-14-113	154.57	155.00						0.43						92947	BX/MS unit; 10%-18% CaF ₂ ; RYC-GWB-P; chocolate brown CaF ₂ within; fracture filling and infill; CaCO ₃ + sulphides in unit; vuggy; mg rotated angular MS clasts suspended in CaF ₂ -rich matrix; majority of structure/vein is running // TCA; BX/MS/VN unit; 20%-23% CaF ₂ ; GWB>RYC-P; sulphide bearing; Py, Gn, and sphalerite; vuggy; Cl altered; vein is // TCA; continued from above;
GS-14-113	155.00	156.00						1.00						92948	
GS-14-113	156.00	157.00						1.00						92949	BX/MS unit; 5%-10% CaF ₂ ; RYC-GWB>P; infill and fracture filling CaF ₂ ; chocolate brown CaF ₂ within;
GS-14-113	157.00	158.00						1.00						92950	MS/BX unit; 10%-20% CaF ₂ ; RYC-GWB-P; CaCO ₃ within; chocolate brown in areas; fracture filling mineralization; MS/BX unit; 4%-8% CaF ₂ ; RYC-GWB>P; hematized throughout; fracture fill CaF ₂ mineralization; minor sericite alteration within;
GS-14-113	158.00	159.00						1.00						138551	
GS-14-113	159.00	160.00						1.00						138552	MS/BX unit; 5% CaF ₂ ; P>GWB>RYC; fracture filling CaF ₂ mineralization; weakly hematized; CaCO ₃ within;
GS-14-113	160.00	161.00						1.00						138553	MS/BX unit; 2%-3% CaF ₂ ; RYC-GWB>P; CaCO ₃ + CaF ₂ + Qtz BX @ upper limit;
GS-14-113	161.00	161.58						0.58						138554	MS/BX unit; 2%-3% CaF ₂ ; RYC-GWB>P; continued from above;
GS-14-113	161.58	162.00						0.42						138555	MS unit; 1%-2% CaF ₂ ;
GS-14-113	162.00	163.00						1.00						138556	MS unit; 3%-5% CaF ₂ ; RYC-GWB>P;
GS-14-113	163.00	164.00						1.00						138557	MS unit; 5%-10% CaF ₂ ; P>RYC-GWB; stockwork and fracture filling mineralization;
GS-14-113	164.00	165.00						1.00						138558	MS/BX unit; 5%-10% CaF ₂ ; P>RYC-GWB; stockwork and fracture filling mineralization;
GS-14-113	165.00	166.00						1.00						138559	MS/BX unit; 10%-15% CaF ₂ ; P>RYC-GWB; infill and fracture filling mineralization;
GS-14-113	166.00	166.47						0.47						138560	MS unit; <2% CaF ₂ ;
GS-14-113	166.47	167.52						1.05						138561	BX unit; 3%-5% CaF ₂ ; P>RYC-GWB; hematized; fracture filling mineralization;
GS-14-113	167.52	168.20						0.68						138562	MS/BX unit; 15% CaF ₂ ; P>RYC-GWB; fracture filling CaCO ₃ + CaF ₂ ; sphalerite + Py within;
GS-14-113	168.20	168.60						0.40						138563	MS/BX unit; 5%-10% CaF ₂ ; P>RYC-GWB; sphalerite within;
GS-14-113	168.60	169.00						0.40						138564	MS unit; 3%-5% CaF ₂ ; P>RYC-GWB; fracture filling mineralization;
GS-14-113								0.00						138565	STANDARD
GS-14-113	169.00	170.00						1.00						138566	MS/BX unit; 2%-3% CaF ₂ ; P, Cl + K + Hm alteration within;
GS-14-113	170.00	171.00						1.00						138567	MS unit; 5%-8% CaF ₂ ; P>RYC-GWB; one vein @ 25° TCA; fracture filling CaF ₂ ;
GS-14-113								0.00						138568	BLANK
GS-14-113	171.00	172.00						1.00						138569	MS unit; 5%-10% CaF ₂ ; P>RYC-GWB; fracture filling mineralization; BX'd in places;
GS-14-113	172.00	173.00						1.00						138570	MS unit; 20%-25% CaF ₂ ; P>RYC-GWB; fracture filling and chaotic veining throughout; chocolate brown CaF ₂ within; CaCO ₃ within as well;
GS-14-113	173.00	173.40						0.40						138571	BX/MS unit; 25%-30% CaF ₂ ; RYC-GWB>P; mg sub-angular rotated clasts of MS in CaF ₂ + CaCO ₃ -rich matrix;
GS-14-113	173.40	174.40						1.00						138572	VN unit; 75%-90% CaF ₂ ; GWB>RYC-P; MS clasts/fragments within; sulphide bearing; CaCO ₃ within; visible zoning within; chocolate CaF ₂ within; Py + sphalerite as well;
GS-14-113	174.40	174.88						0.48						138573	VN unit; 95% CaF ₂ ; RYC-GWB>P; visible zoning; sulphide bearing;
GS-14-113	174.88	175.23						0.35						138574	VN/BX unit; 70%-80% CaF ₂ ; P>GWB>RYC; MS fragments within; Cl altered; CaCO ₃ within;
GS-14-113	175.23	176.21						0.98						138575	MS/BX unit; 20%-25% CaF ₂ ; cg rotated angular MS fragments; chocolate brown CaF ₂ within; 20%-25% CaF ₂ ; fg BX as well; CaCO ₃ within;
GS-14-113								0.00						138576	DUPLICATE OF 138575
GS-14-113	176.21	177.21						1.00						138577	MS/BX unit; 2%-5% CaF ₂ ; RYC-GWB>P; chocolate brown CaF ₂ within; cl altered;
GS-14-113	177.21	178.25						1.04						138578	MS/BX unit; 4%-8% CaF ₂ ; RYC-GWB>P; fracture fill mineralization; CaCO ₃ within;
GS-14-113	178.25	179.25						1.00						138579	MS/BX unit; 10%-12% CaF ₂ ; P>RYC-GWB;
GS-14-113	179.25	179.62						0.37						138580	MS/BX unit; 5% CaF ₂ ; P>RYC-GWB;
GS-14-113	179.62	180.62						1.00						138581	MS unit; 1m wallrock sample; 3%-4% CaF ₂ ;