Acquiring VLF-EM data with the hand-held Geonics EM-16 receiver

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- Basic principles EM method
- EM-16 use/demo & survey set-up
- Data presentation, Fraser Filter
- Basic interpretation

Electromagnetics (EM)

Theory

- Passing a current (AC) through a wire induces a primary magnetic field in the vicinity of the wire.
- The primary magnetic field induces currents in bedrock conductors (if present).
- The currents in the conductor induce a secondary magnetic field.
- The secondary field is measured by a receiver

Electromagnetics (EM)

Uses

To detect buried metal in urban settings.

- To map conductive geological strata, fault zones.
- To delineate mineralized horizons (if conductive)

There are several types of EM surveys.

VLF-EM (Very Low Frequency)

The primary signal field induces a secondary field in a conductor in the bedrock.

A conductor can be

Metallic body, Graphitic horizons, Faults, Contacts between different bedrock units.

Conductor = Continuous body



Submarine communications systems use VLF transmitter stations at

Cutler, Maine Annapolis, Maryland Seattle, Washington Rugby, England Bordeaux, France (and others around the globe)



Uses:

 Primarily used for locating/mapping near vertical mineralized beds or structures.

Depth of penetration approx. 50 m



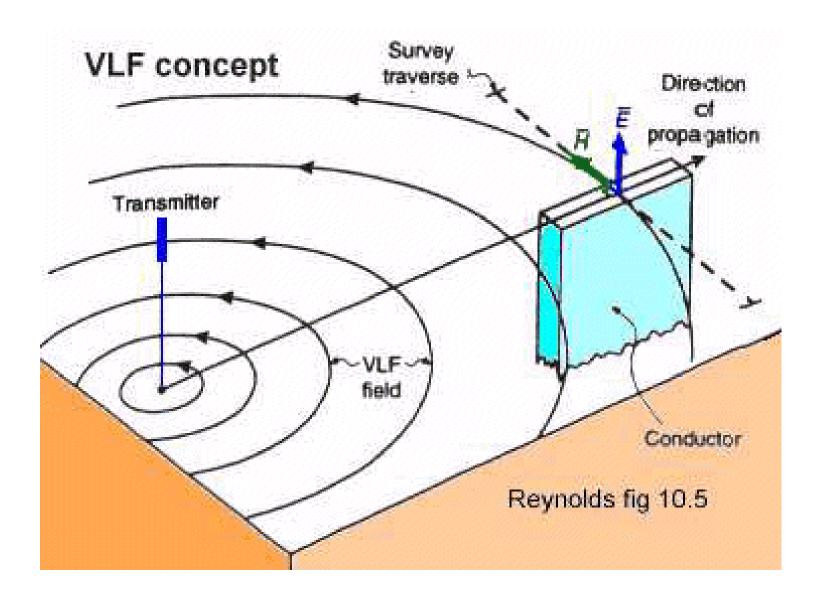
Advantages:

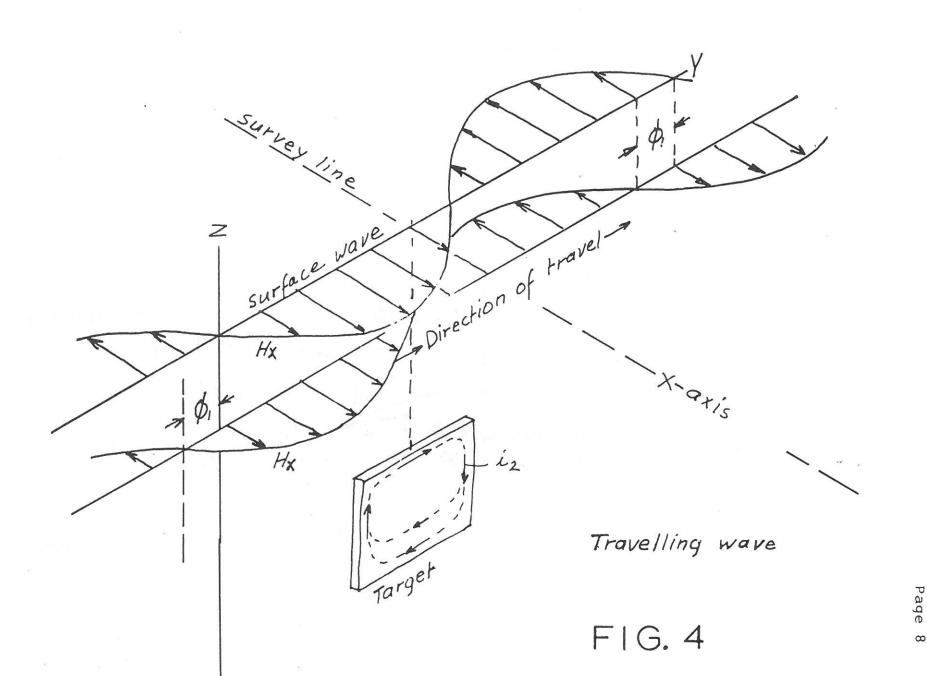
- Measurements are easily acquired;
- Relatively cheap and good for reconnaissance;
- Uses an existing transmitter source;
- Does not require ground contact;
- Can provide relatively deep measurements.

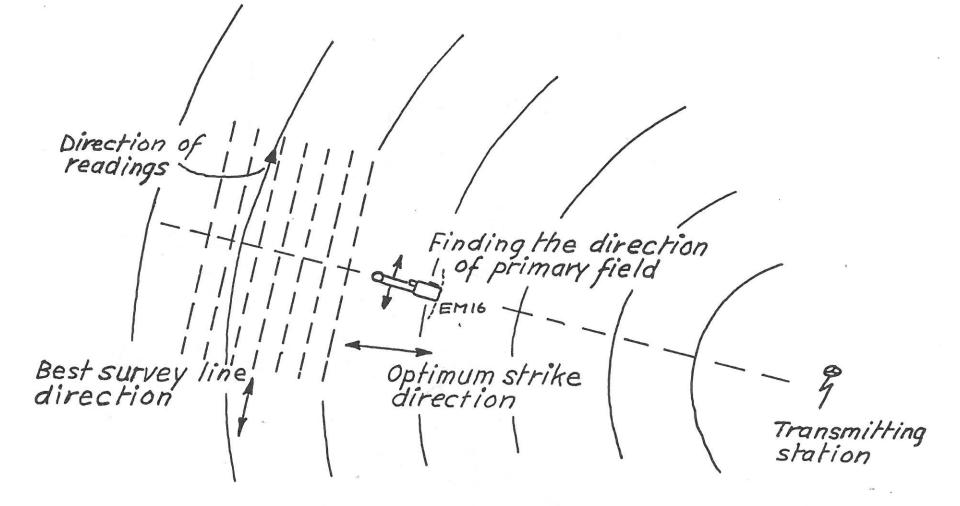


Ineffective if

- Rock layers are horizontal
- Soil is electrically conductive
- Body not aligned approx. towards transmitter
- Metal pipes, cables, power lines etc nearby
- Loss of signal from the VLF transmitter!!

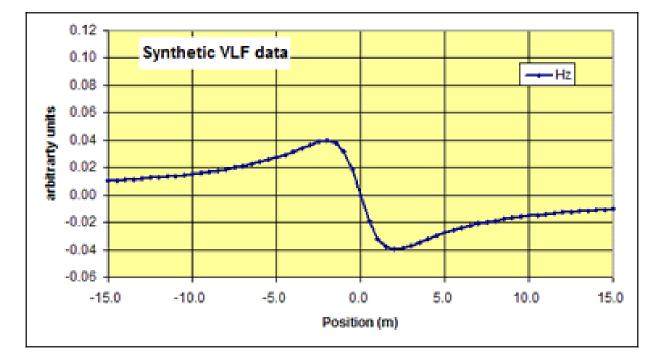


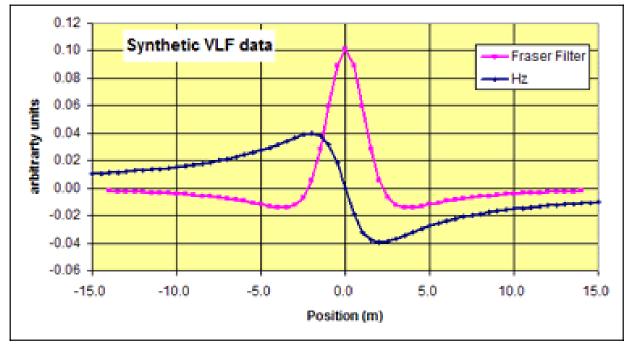


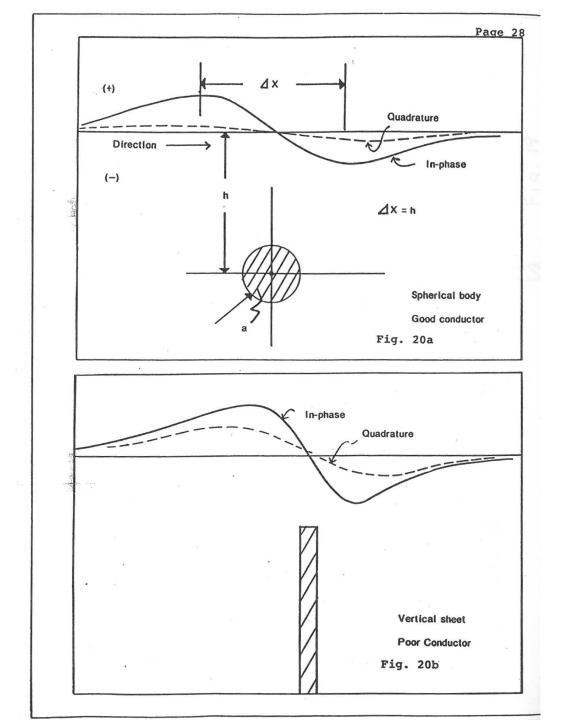


Planning of survey

FIG. 3







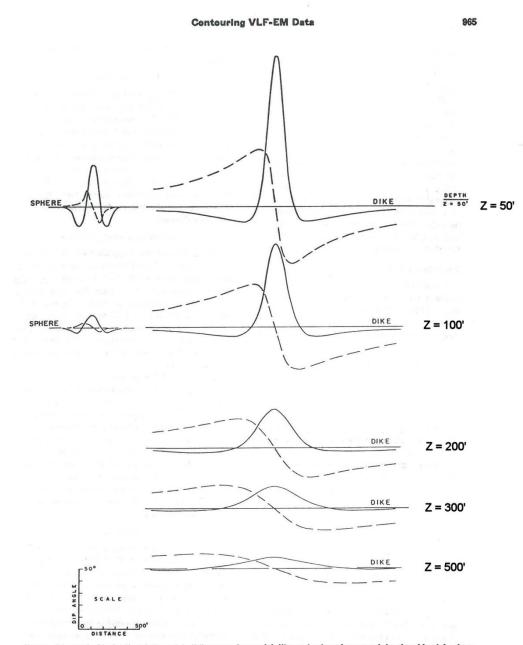
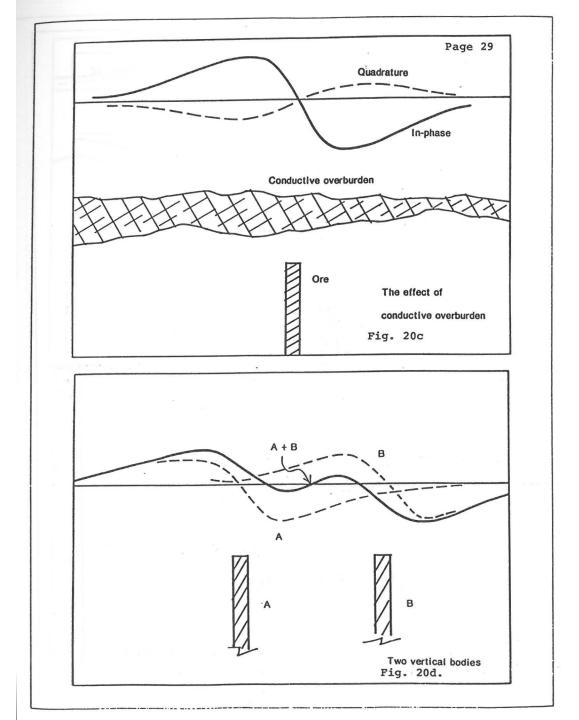
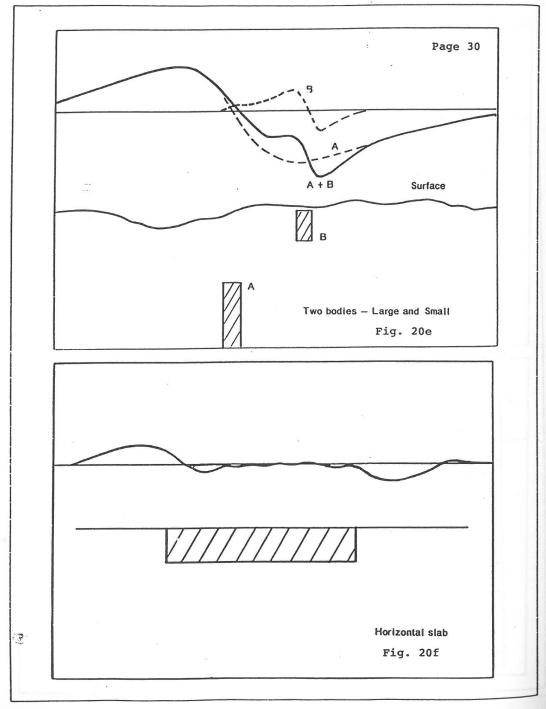


Fig. 6. Dip-angle (dashed) and filtered (solid) curves for model dike and sphere for several depths of burial, where z is depth to top of dike and to center of sphere.

(Fraser, 1969)

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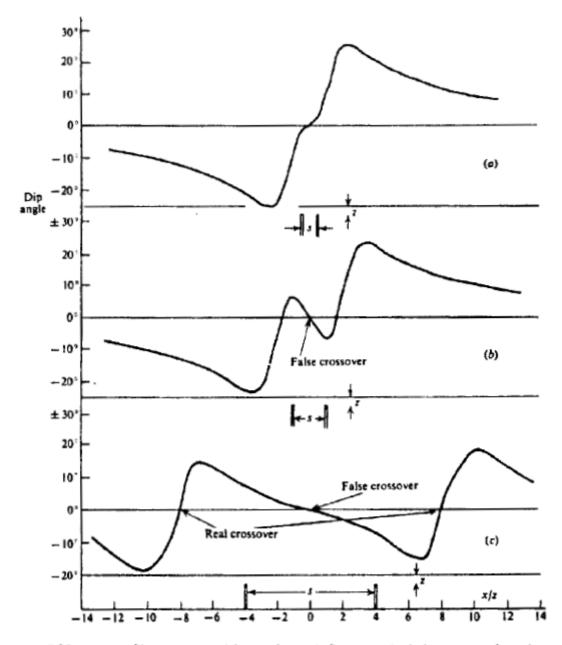


Figure 7.39. VLF profiles over two identical semiinfinite vertical sheets as a function of distance between the sheets. (a) s = 2z. (b) s = 4z. (c) s = 16z. (Telford et al., 1990)

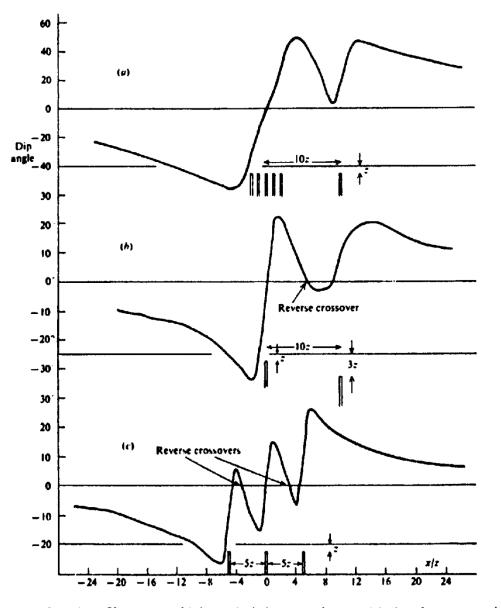
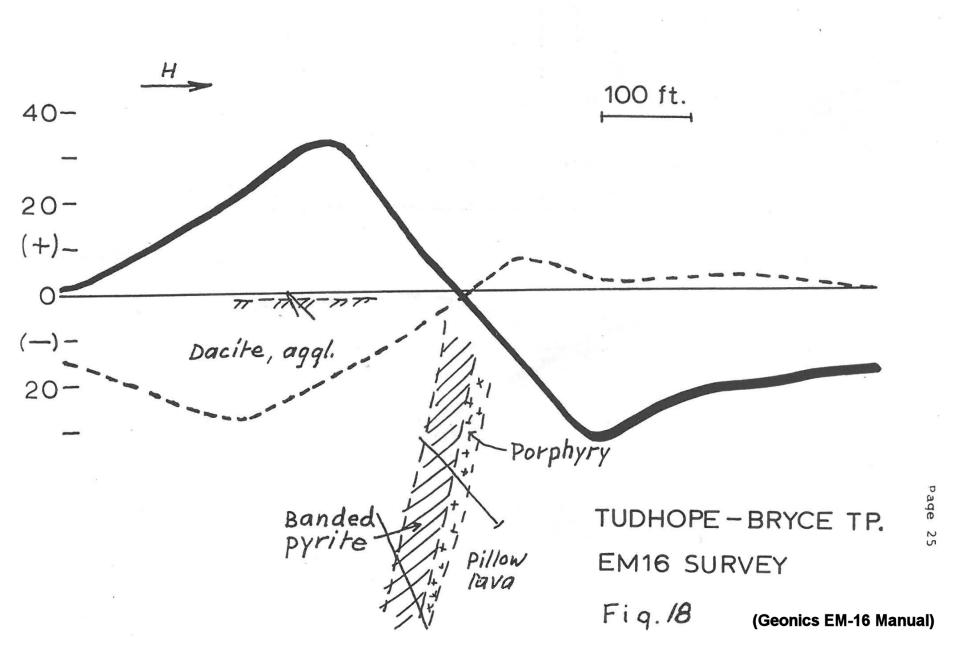
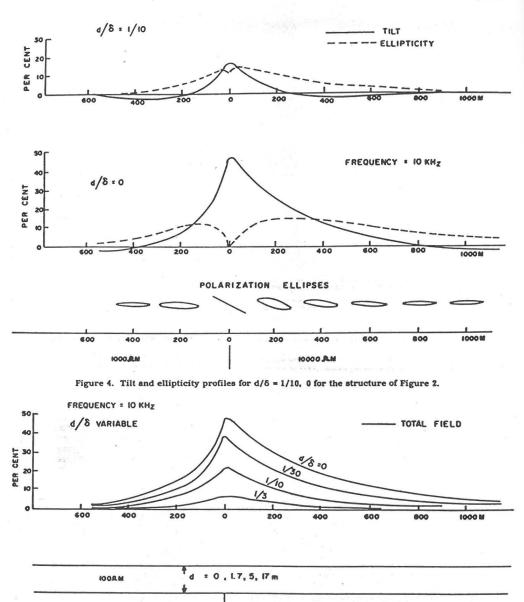


Figure 7.40. VLF profiles over multiple vertical-sheet conductors. (a) Five sheets spaced z apart plus one sheet distant 10z from the midpoint of the five sheets, all at depth z. (b) Two sheets at depths of z and 3z, spaced 10z apart. (c) Three sheets at depth z and spaced 5z apart.

(Telford et al., 1991)





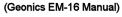


Figure 5. Total field, $|H_z/H_x|$, profiles over the structure of Figure 2 with d/6 = 0, 1/30, 1/10, 1/3.

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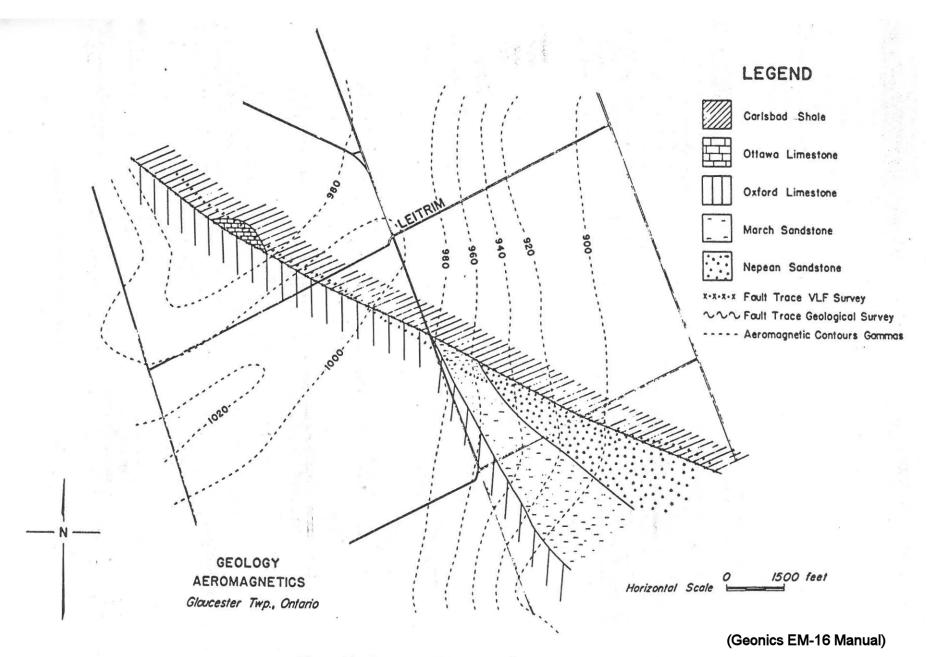


Figure 10. Geology and aeromagnetic contours, Leitrim area.

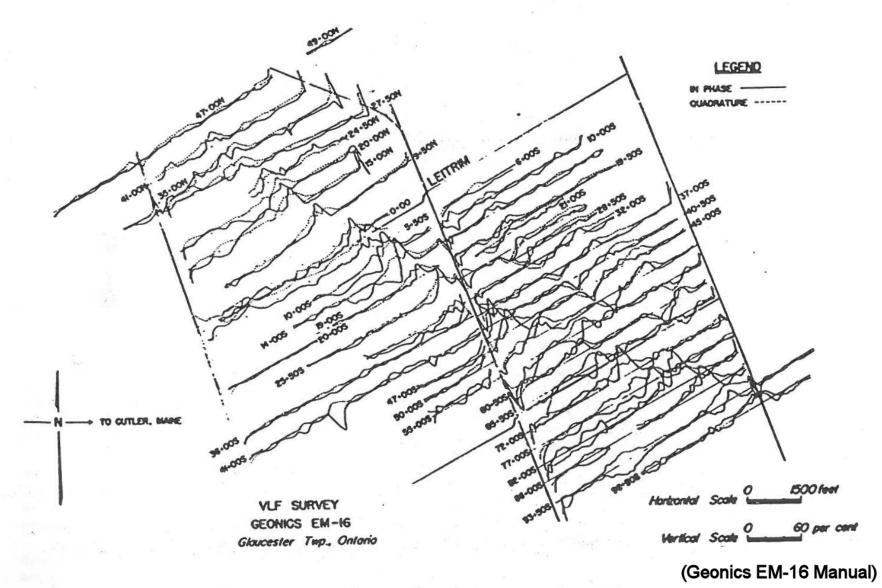


Figure 11. VLF in-phase and quadrature profiles, Leitrim area.

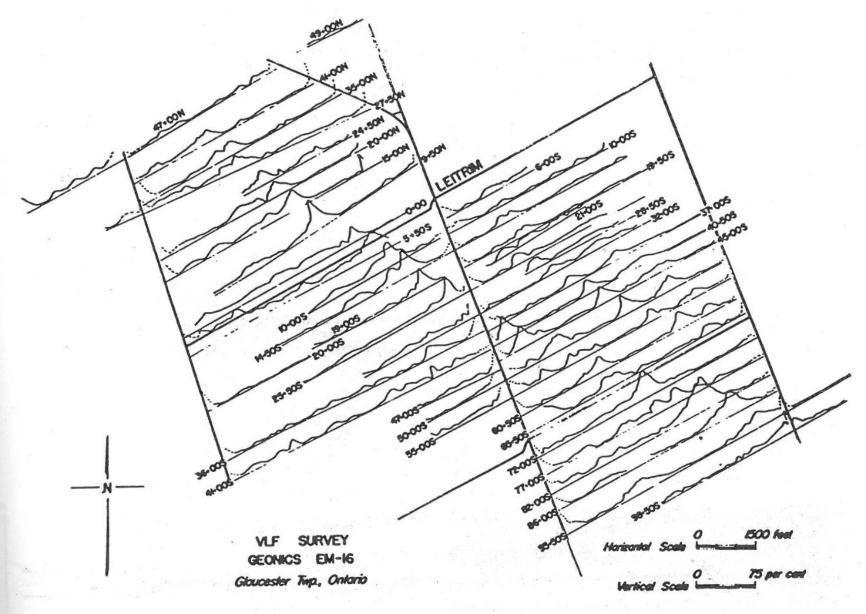


Figure 12. VLF total field profiles, Leitrim area.

(Geonics EM-16 Manual)

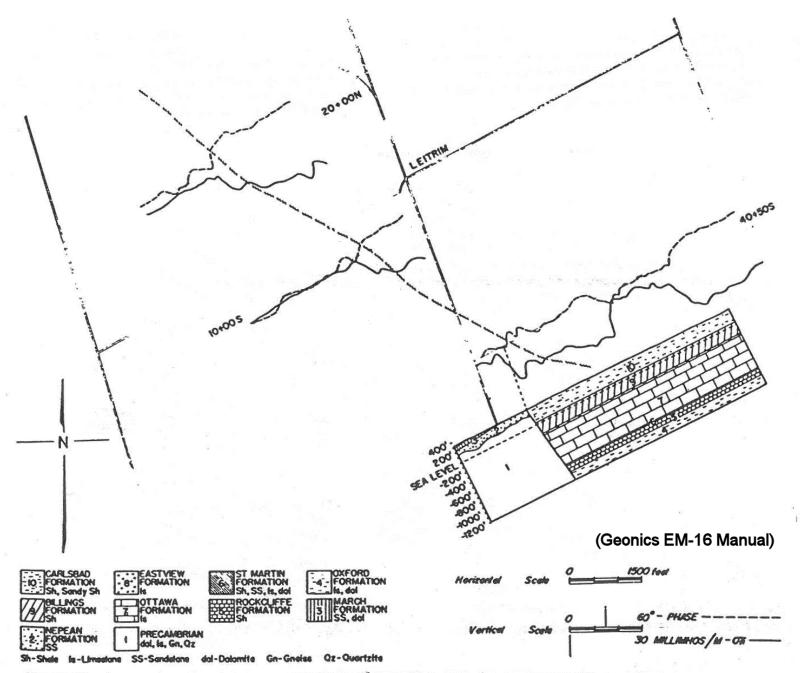
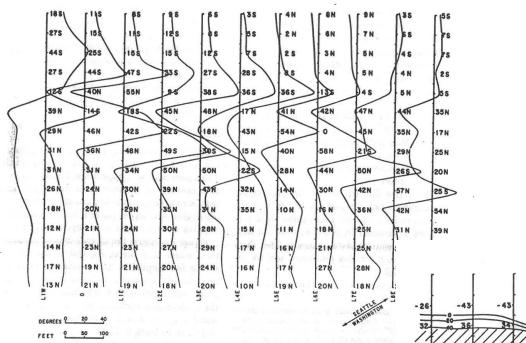


Figure 13. Apparent conductivity (σ_a) and phase (ϕ) profiles on lines 20+00N, 10+00S, and 40+50S. Leitrim area.



Fraser

FIG. 1. Dip-angle data in the vicinity of the Temagami mine. The arrow defines the VLF-EM primar from the transmitter at Seattle, Washington.

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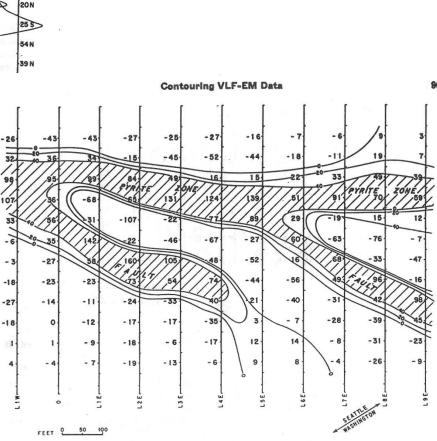
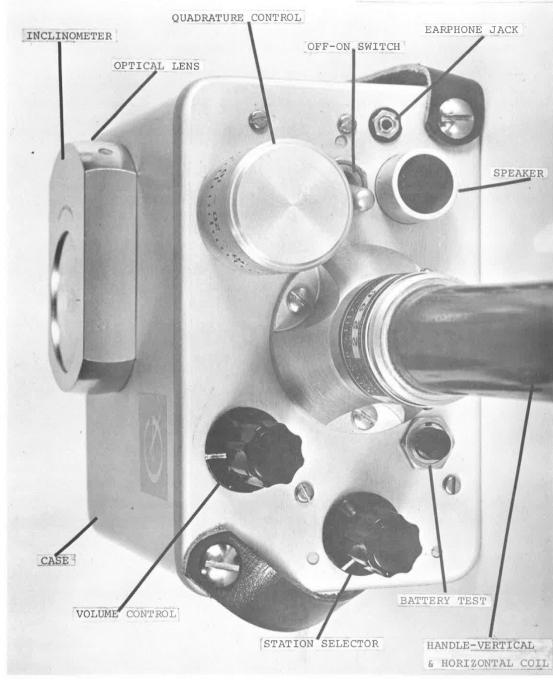


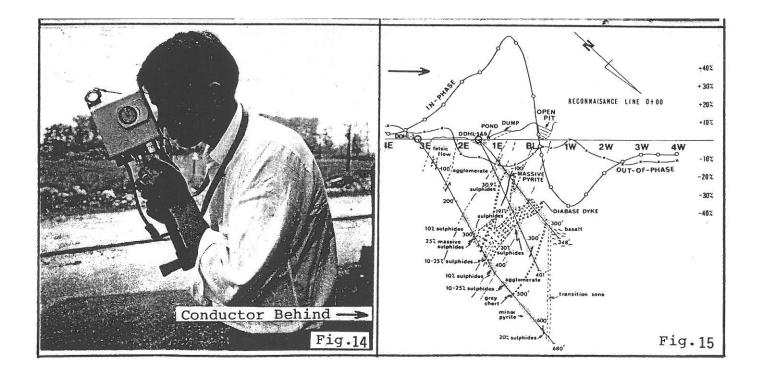
FIG. 2. Filtered data computed from the map of Figure 1.

EM-16 Receiver

FIG. I EM I6

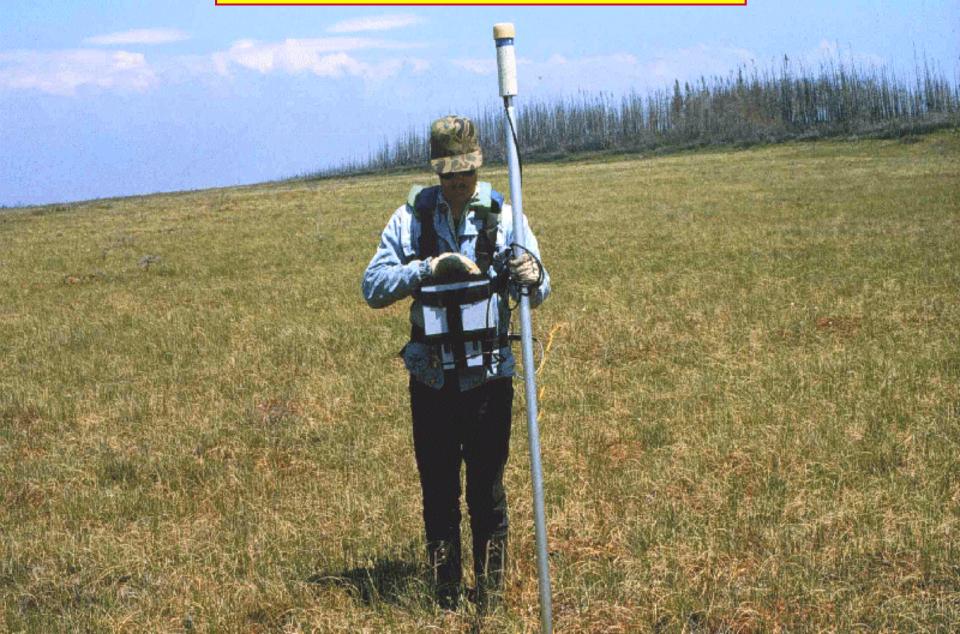


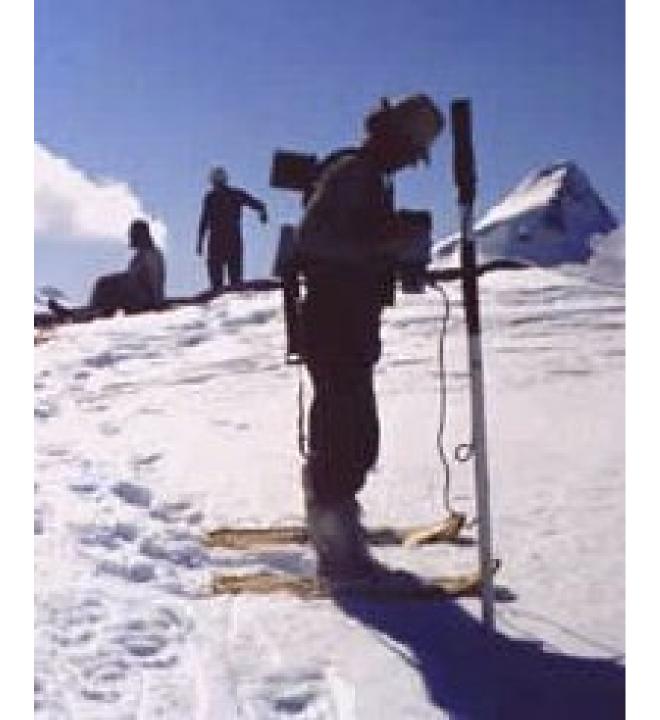






Omni Plus Magnetometer / VLF-EM

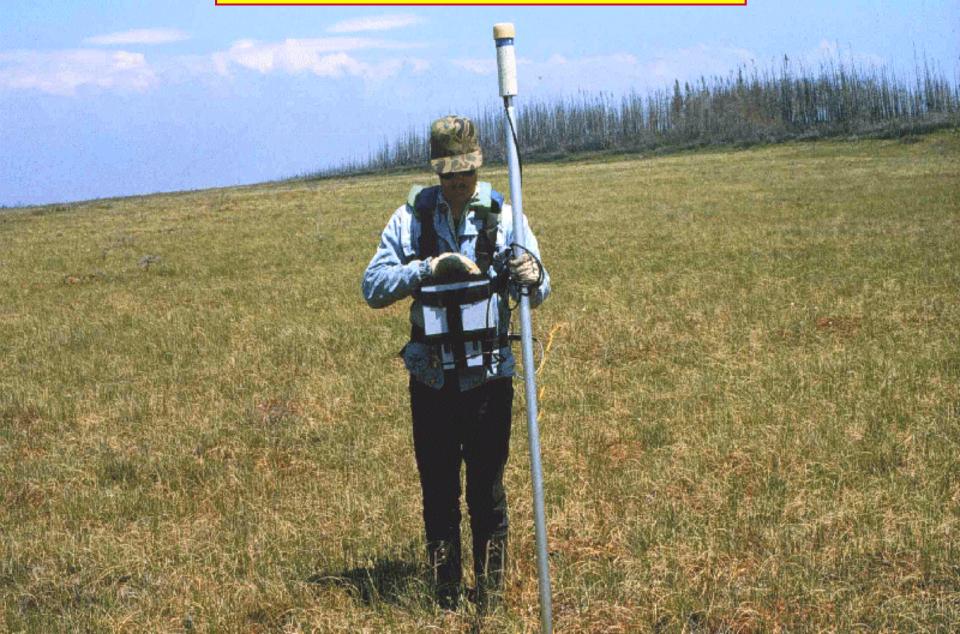




VLF-EM Data Recording and Plotting

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| | 70.0 48 76 549428 60.0 0 76 54878.1 80.0 -17 71 54653.4 1.70.0 10 43 609771 5161 3 |
| | (200 -2) -4 5395711 Fa Mart 90.0 120.0 -15 6 54238.6 Larch her 120.0 +5.5 -3 59693.1 140.0 +5.5 -3 59693.1 |
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| | 220.0 -2.0 -8.0 33595.4 220.0 -6.0 -30 594994.0 240.0 -1.5 +20 55750.1 260.9 -0.5 +20 55239.1 Eenlot 260.9 -0.5 +20 55239.1 Eenlot |
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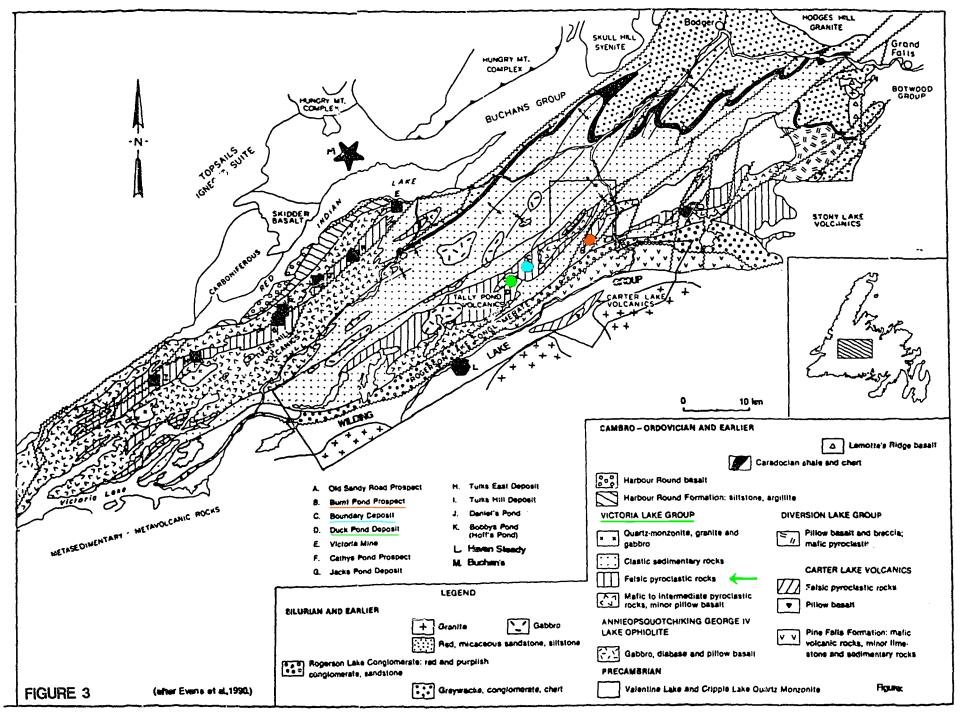
Omni Plus Magnetometer / VLF-EM



| OMNI-PLUS Tie-line MAG/VLF R22N Ser #428061 | |
|----------------------------------------------------------|-------------------------------------------------------------------------------------------------------------|
| VLF TOTAL FIELD DATA uncorrected | |
| Date 18 JUL 89 | |
| Operator: 3001 | |
| Records: 712 | |
| Bat: 17.6 Volt Lithium: 3.48 Volt | |
| Last time update: 7/16 5:15:00 | |
| Start of print: 7/18 18:44:17 | |
| | |
| | |
| Line 000 E Date 18 JUL 89 24.0 #1 | |
| POSITION I/P QUAD T.FLD TILT TIME CULT S DIR 4-FRA 5-FRA | |
| #1 −71.5 −0.1 2461. −8.0 7:23:34 99 0.0 | |
| #2 7.3 -24.2 19.23 4.4 7:24:37 69 17.8 | |
| #3 7.3 -22.3 19.42 4.4 7:24:56 69 6.4 | 1875S 42.6 -25.5 26.90 24.2 8:09:41 49 15.1 -8.7 -6.5 |
| #4 6.1 -22.1 19.24 3.7 7:25:13 59 -8.8 | 200 S 37.0 -25.9 26.09 21.5 8:10:02 49 23.3 -10.5 -9.6 |
| | 21255 31.3 -26.6 25.73 18.5 8:10:20 59 17.6 -11.2 -10.9 |
| Line 1200 E Date 18 JUL 89 24.0 #5 | 225 S 25.3 -27.1 25.49 15.2 8:10:38 49 15.7 -12.0 -11.6 |
| POSITION I/P QUAD T.FLD TILT TIME CULT S DIR 4-FRA 5-FRA | 23755 20.5 -27.1 25.27 12.4 8:11:02CROP 59 18.2 -12.4 -12.2 |
| 2100 N -28.7 -7.0 42.55 -16.1 9:54:32 65 16.4 | 250 S 18.3 -25.6 25.84 11.0 8:11:31 69 17.9 -10.3 -11.4 |
| 20875N -20.0 -3.4 44.64 -11.3 9:55:21 44 13.2 | 26255 16.9 -24.2 25.37 10.1 8:11:51 59 15.9 -6.5 -8.4 |
| 2075 N -8.7 -0.2 45.41 -4.9 9:55:40 69 18.5 | 275 S 15.3 -22.4 25.40 9.1 8:12:07 49 13.5 -4.2 -5.4 |
| 20625N -1.8 2.7 40.81 -1.0 9:56:00 59 11.6 21.5 | 28755 14.3 -21.1 25.27 8.5 8:12:26 59 16.5 -3.5 -3.9 |
| 2050 N -3.6 1.2 39.10 -2.1 9:56:24 49 16.6 13.1 17.3 | 300 S 11.7 -20.6 25.25 7.0 8:12:48CREC 59 19.2 -3.7 -3.6 |
| 20375N -11.3 -4.0 38.47 -6.4 9:56:53 58 13.3 -2.6 5.2 | |
| 2025 N -14.3 -7.2 41.04 -8.1 9:57:11 58 15.7 -11.4 -7.0 | Line 1100 E Date 18 JUL 89 24.0 #146 |
| 20125N -7.0 -4.4 44.27 -4.0 9:57:47 49 4.9 -3.6 -7.5 | POSITION I/P QUAD T.FLD TILT TIME CULT S DIR 4-FRA 5-FRA |
| 2000 N 3.9 1.1 43.39 2.2 9:58:05 59 10.6 12.7 4.5 | 23755 16.0 -18.1 27.08 9.4 8:46:29 56 14.8 |
| 19875N 7.9 4.3 38.91 4.5 9:58:25 59 10.4 18.8 15.7 | 225 S 19.1 -18.6 27.12 11.2 8:47:14 56 16.4 0.6 |
| 1975 N 5.0 2.0 37.26 2.8 9:58:40 49 11.3 9.1 13.9 | 21255 23.6 -18.8 27.33 13.7 8:47:37 55 12.3 -3.7 -1.6 |
| 19625N 3.2 0.8 36.54 1.8 9:59:01 49 7.0 -2.1 3.5 | 200 S 28.0 -18.2 27.30 16.1 8:47:55 44 16.5 -9.2 -6.5 |
| 1050 27 0.1 0.0 0.6 1.0 0.50.16 40 0.1 4.0 0.0 | 18755 32.4 -18.0 28.35 18.4 8:48:14 54 13.0 -9.6 -9.4 |
| | 175 S 38.7 -17.4 28.72 21.6 8:48:32 42 12.2 -10.2 -9.9 |
| | 16255 40.3 -18.6 29.53 22.5 8:48:53 55 13.8 -9.6 -9.9 |
| | 150 S 46.5 -17.0 30.88 25.4 8:49:11 64 16.0 -7.9 -8.8 |
| | 13755 54.1 -15.7 32.92 28.8 8:49:31 64 16.0 -10.1 -9.0 |
| | 125 S 61.2 -13.2 34.79 31.7 8:49:46 52 20.2 -12.6 -11.4 |
| | 11255 67.3 -12.5 40.63 34.2 8:50:09 54 10.9 -11.7 -12.2 |
| | 100 S 70.3 -10.7 46.56 35.3 8:50:24 52 9.6 -9.0 -10.4 |
| | 08755 57.0 -10.3 60.00 29.9 8:50:42 63 13.9 0.7 -4.2 |
| | 075 S 18.6 -10.8 71.55 10.6 8:51:02 55 17.0 29.0 14.8 |
| | 06255 -5.7 -0.8 59.82 -3.3 8:51:22 59 11.0 57.9 43.4 |
| | 050 S -9.9 1.8 55.35 -5.6 8:51:39 49 13.9 49.4 53.6 |
| | 03755 -14.4 6.6 52.23 -8.2 8:51:56 59 5.2 21.1 35.2 025 5 -21.8 3.9 49.66 -12.3 8:52:14 49 7.9 11.6 16.3 |
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| 4 | 9900.0 | 9712.5 | 400.7 | -8.6 | -7.3 | | 13.5 | 9706.3 | 549397.55 | 5394756.24 | |
| 5 | 9900.0 | 9725.0 | 372.4 | -11.7 | -10.4 | =(D3+D4)-(D5 | -6.1 | 9718.8 | 549408.64 | 5394750.47 | |
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| 7 | 9900.0 | 9750.0 | 358.2 | 0.1 | -5.6 | -10.4 | -3.6 | 9743.8 | 549430.81 | 5394738.92 | |
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| 9 | 9900.0 | 9775.0 | 500.2 | -1.8 | -9.0 | -3.4 | -5.7 | 9768.8 | 549452.99 | 5394727.38 | |
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| 12 | 9900.0 | 9812.5 | 375.7 | 1.3 | -10.9 | -3.1 | -4.0 | 9806.3 | 549486.25 | 5394710.06 | |
| 13 | 9900.0 | 9825.0 | 371.3 | 2.8 | -11.2 | -4.9 | -4.7 | 9818.8 | 549497.34 | 5394704.29 | |
| 14 | 9900.0 | 9837.5 | 364.2 | 4.2 | -12.0 | -4.5 | -4.8 | 9831.3 | 549508.42 | 5394698.52 | |
| 15 | 9900.0 | 9850.0 | 363.0 | 4.4 | -12.5 | -5.0 | -7.7 | 9843.8 | 549519.51 | 5394692.75 | |
| 16 | 9900.0 | 9862.5 | 341.3 | 7.6 | -12.3 | -10.3 | -11.7 | 9856.3 | 549530.60 | 5394686.98 | |
| 17 | 9900.0 | 9875.0 | 332.2 | 11.3 | -11.6 | -13.1 | -10.7 | 9868.8 | 549541.69 | 5394681.20 | |
| 18 | 9900.0 | 9887.5 | 318.8 | 13.8 | -11.0 | -8.3 | -5.7 | 9881.3 | 549552.77 | 5394675.43 | |
| 19 | 9900.0 | 9900.0 | 282.9 | 13.4 | -12.4 | -3.1 | -3.2 | 9893.8 | 549563.86 | 5394669.66 | |
| 20 | 9900.0 | 9912.5 | 333.8 | 14.8 | -13.3 | -3.2 | -4.8 | 9906.3 | 549574.95 | 5394663.89 | |
| 21 | 9900.0 | 9925.0 | 719.9 | 15.6 | -15.5 | -6.3 | -8.3 | 9918.8 | 549586.04 | 5394658.12 | |
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| 23 | 9900.0 | 9950.0 | 702.7 | 21.8 | -15.3 | -16.0 | -16.9 | 9943.8 | 549608.21 | 5394646.57 | |
| 24 | 9900.0 | 9962.5 | 1031.1 | 28.7 | -12.5 | -17.8 | -15.0 | 9956.3 | 549619.30 | 5394640.80 | |
| 25 | 9900.0 | 9975.0 | 558.5 | 29.8 | -14.2 | -12.2 | -10.2 | 9968.8 | 549630.39 | 5394635.03 | |
| 26 | 9900.0 | 9987.5 | 454.2 | 32.9 | -13.8 | -8.2 | -7.3 | 9981.3 | 549641.47 | 5394629.26 | |



SCANNED IMAGE

012A/09/0606 MAP 012A/09/0606/1-16

CONFIDENTIAL

Fourth Year Assessment Report

Burnt Pond Property (6777)

NTS 12A/9

Licence 3881, 3107, 3108

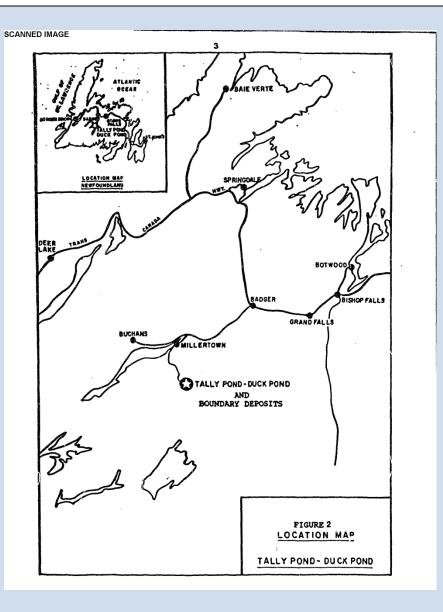
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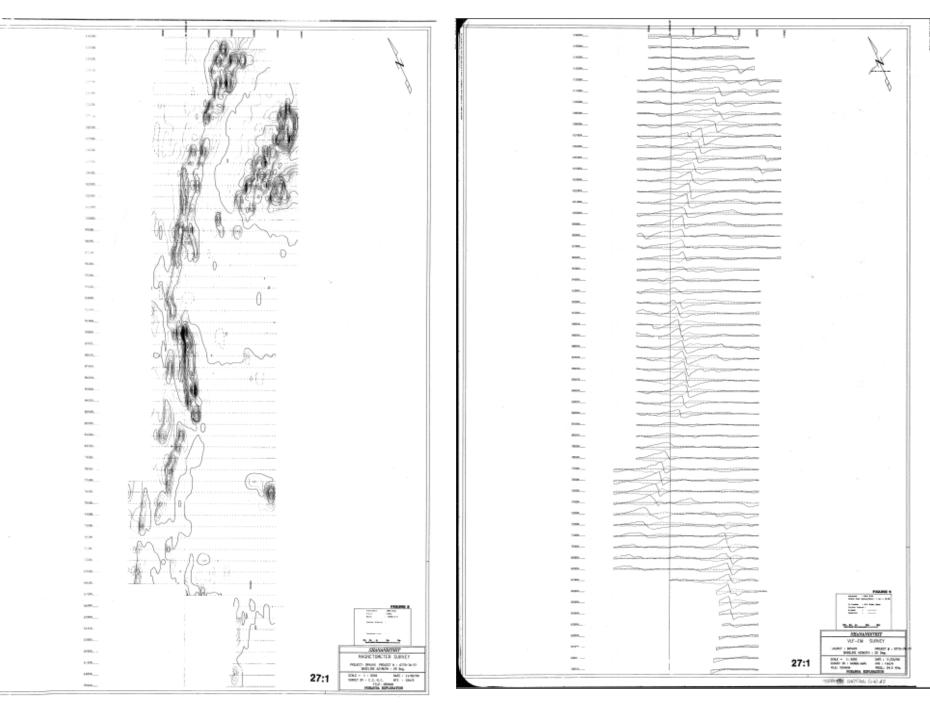
Chris Collins, P.Geo.

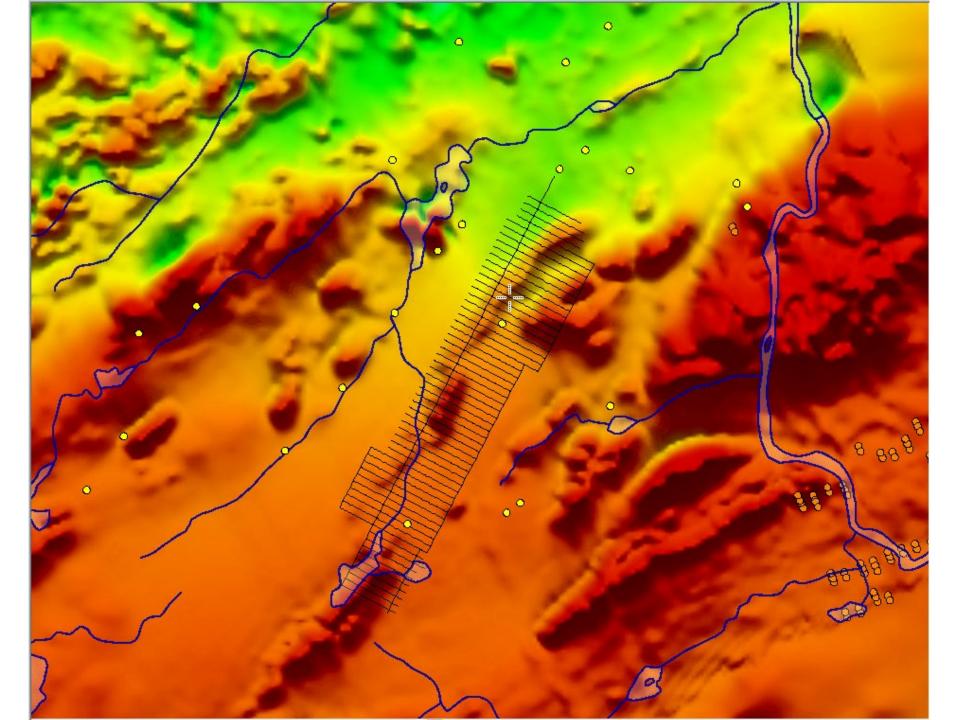
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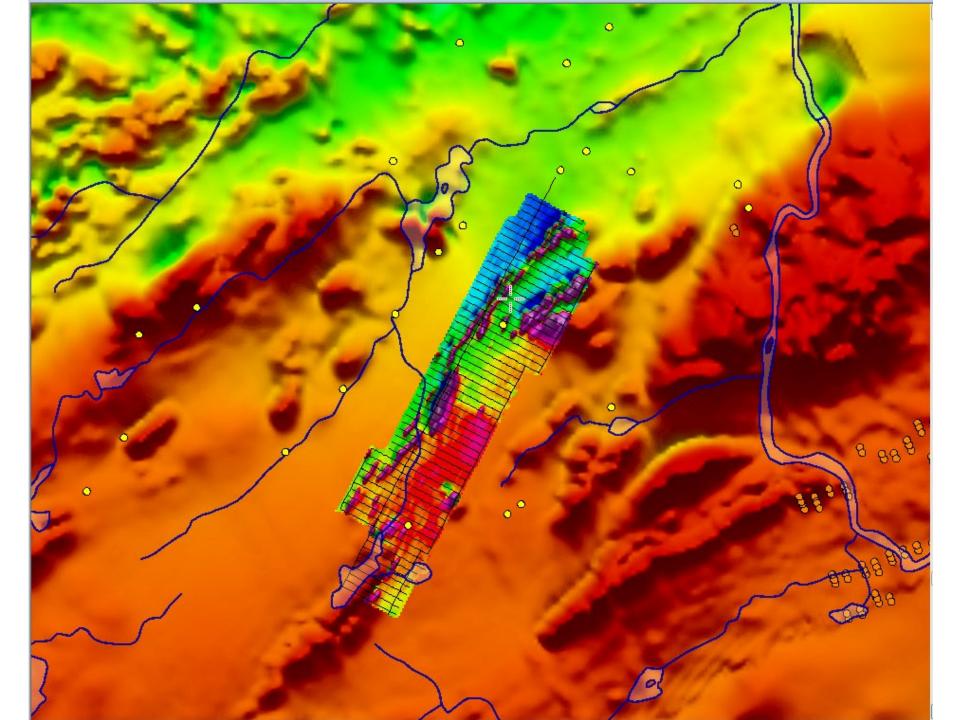
Noranda Exploration Company, Limited (No Personal Liability)

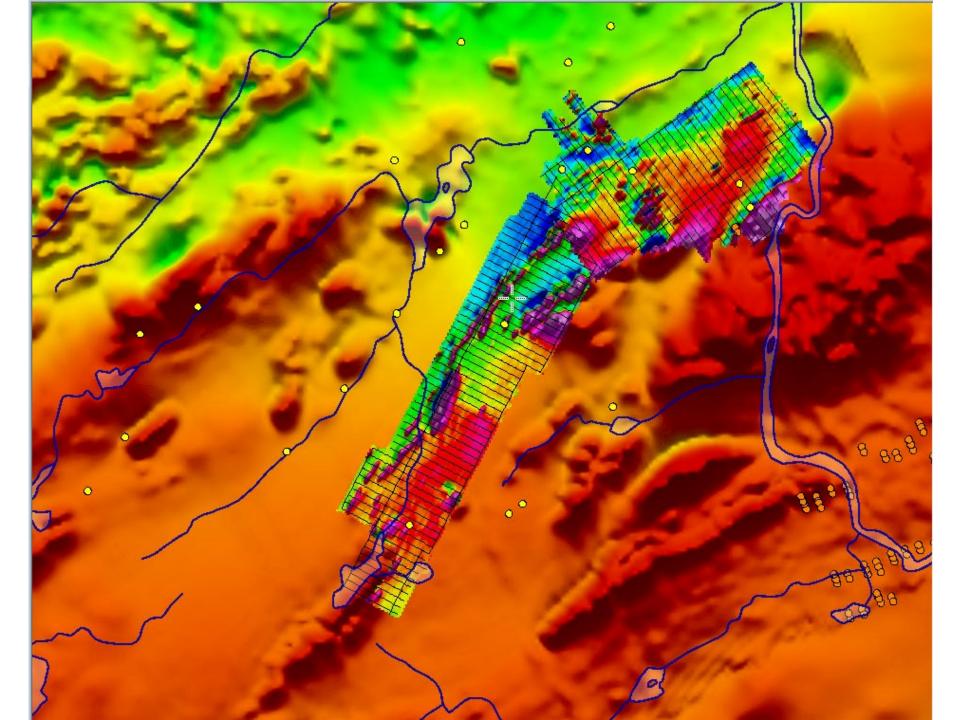
September, 1991

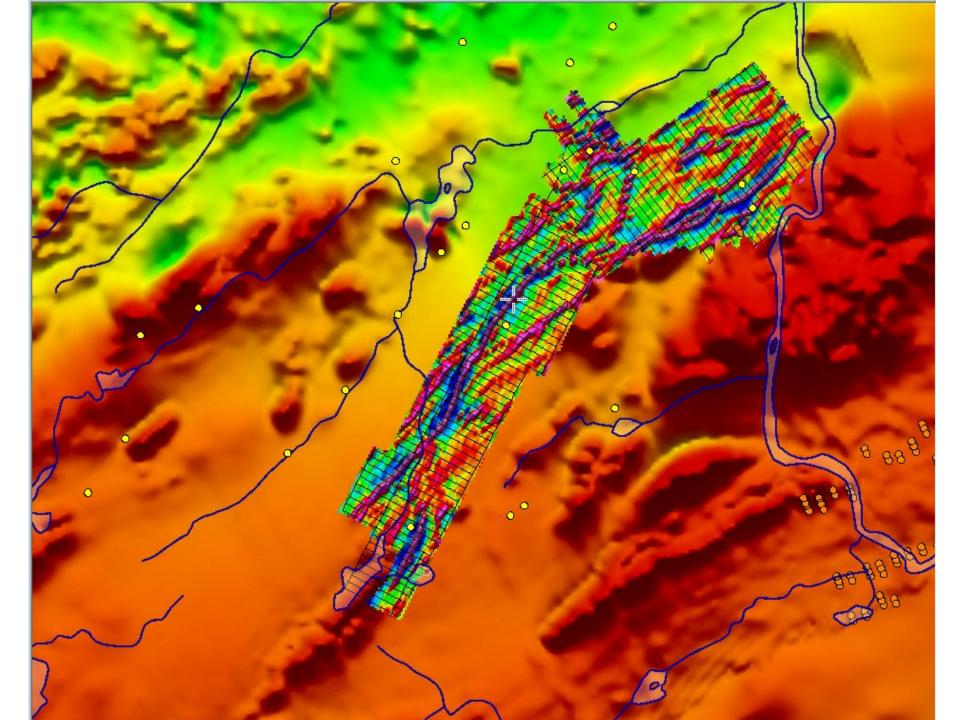


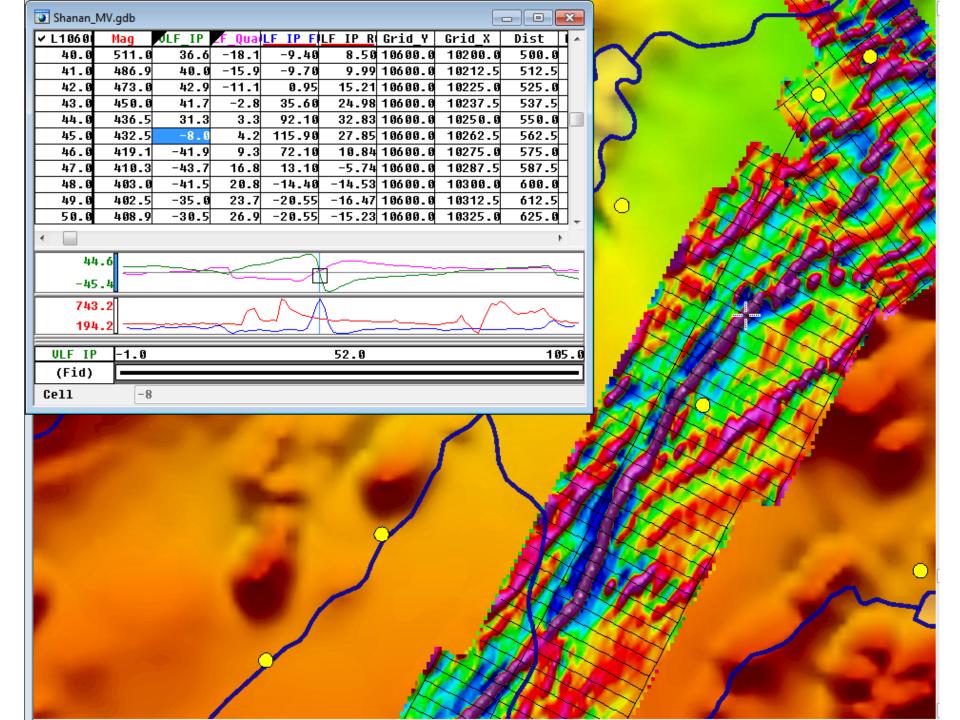


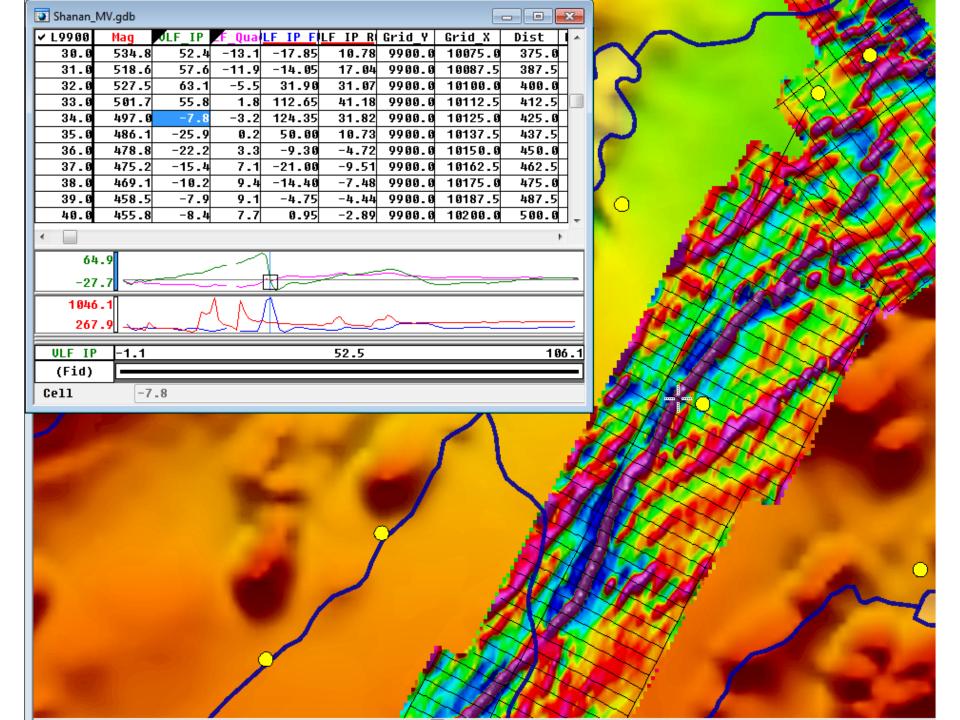


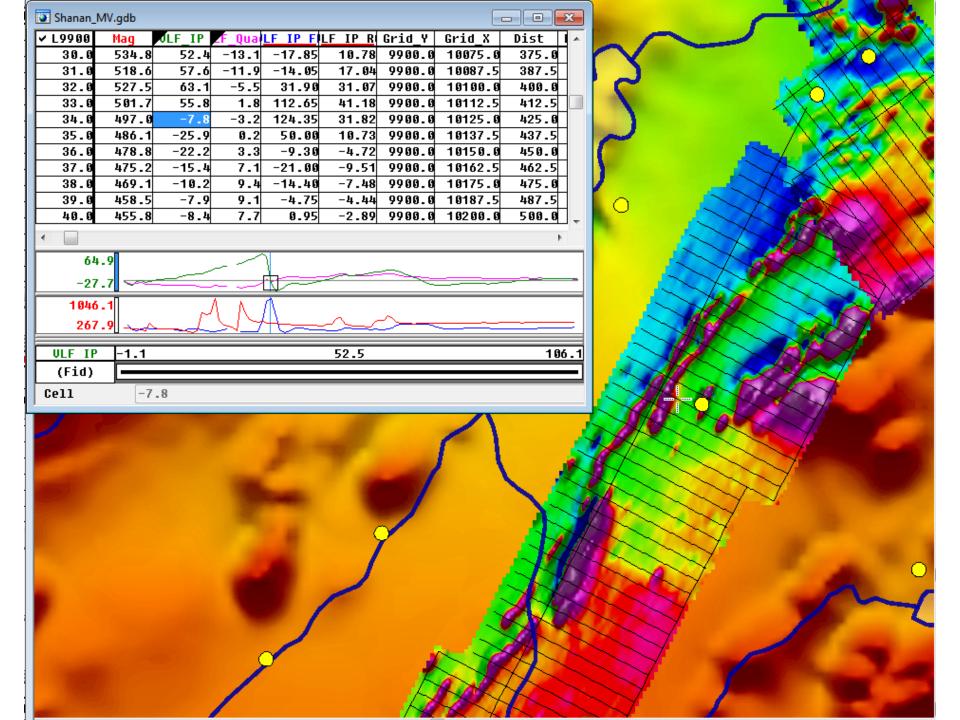


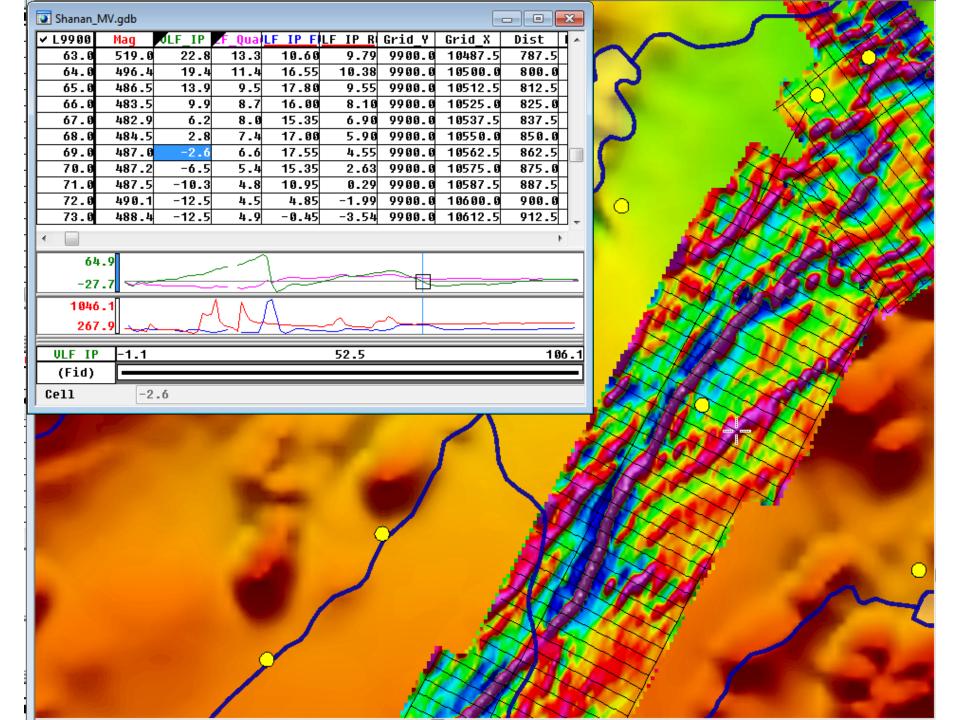


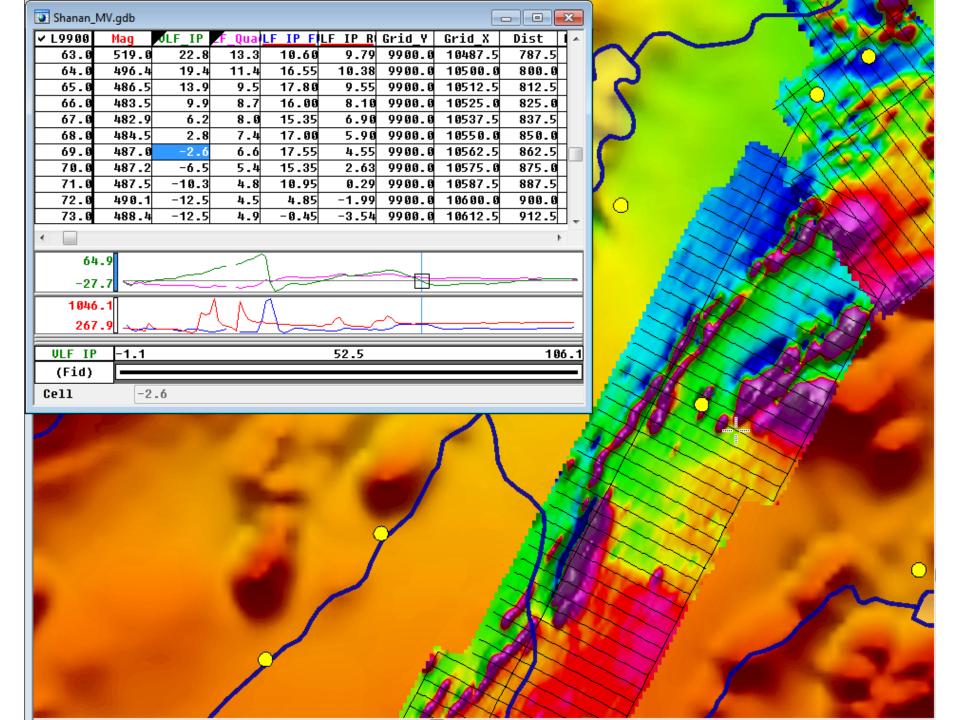


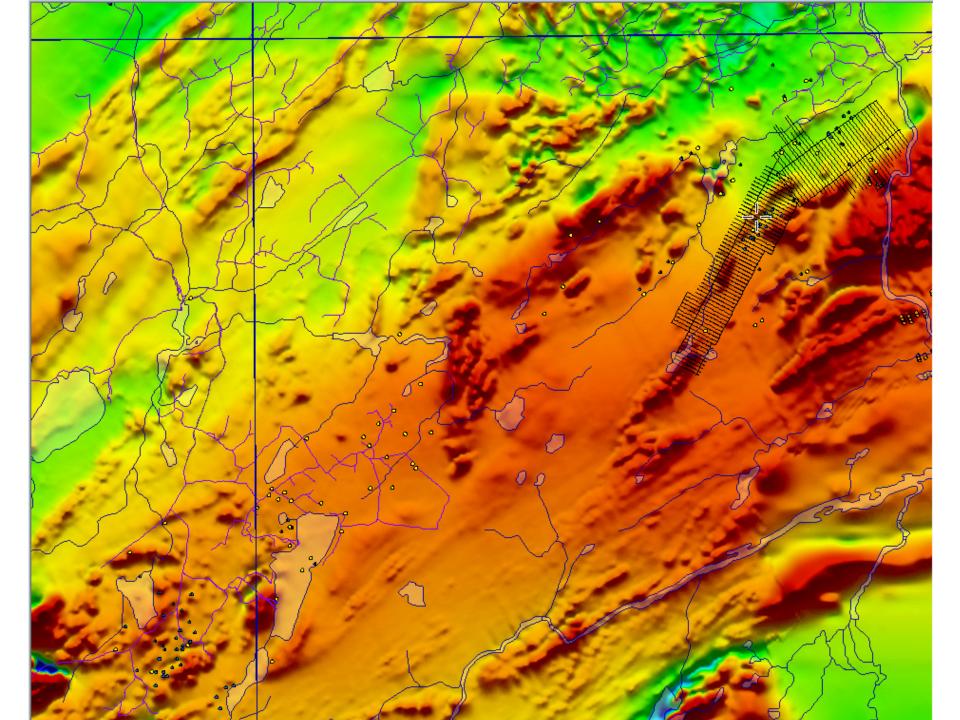


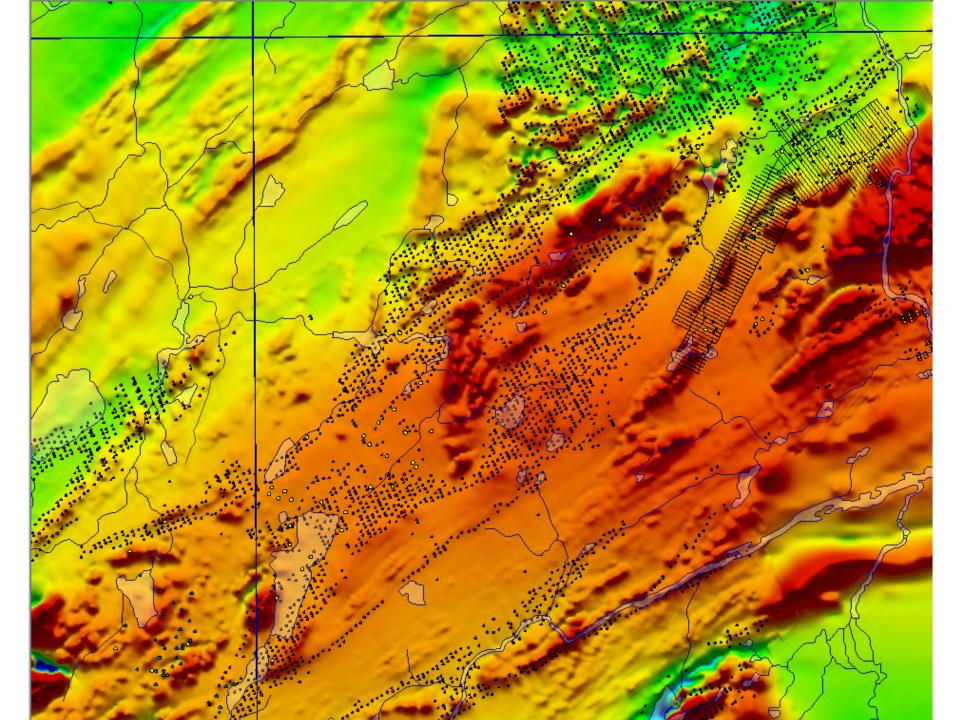


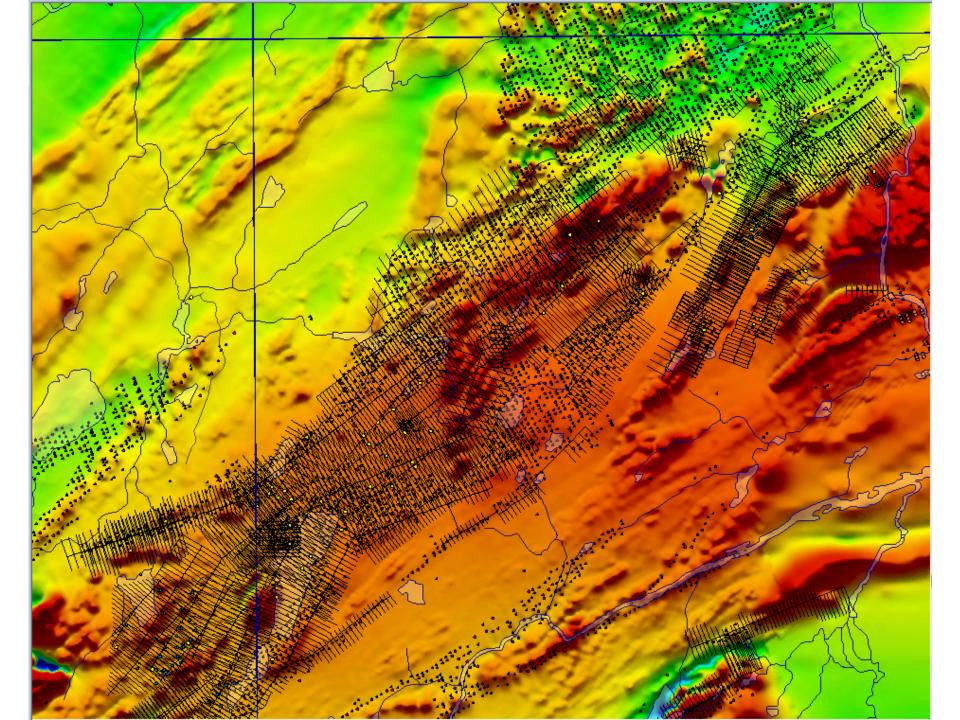












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| 1 | A | B Grid X | C Mag In | D n-Phase | - | F Fraser Filter F | G EF intern G | H Srid X+1/2 | Fasting | J | K | L | М | N | 0 | Р | Q | R | S | Т | U | v w | / X | Y | Z | AA | AB | AC | AD |
| 1 2 L | | 9900 | Mag In | i nase | Quad F | Fraser Filter F | merp G | | casting | Northing | | | | | | | | | | | | | | | | | | | |
| 3 | 9900.0 | 9700.0 | 397.0 | -2.2 | -3.0 | | | | 549386.46 | 5394762.01 | | | | | | | | | | | | 0.00 | , | | | | | | |
| 4 | 9900.0 | 9712.5 | 400.7 | -8.6 | -7.3 | | 13.5 | 9706.3 | | 5394756.24 | | | | | | | | | | Sha | nan Line 9 | 1900 - VLF | - | | | | | | |
| 5 | 9900.0 | 9725.0 | 372.4 | -11.7 | -10.4 | 4.6 | -6.1 | 9718.8 | | 5394750.47 | | 180 | | | | | | | | | | | | | | | | | |
| 6 7 | 9900.0 9900.0 | 9737.5 9750.0 | 364.4 358.2 | -3.7 0.1 | -7.5 -5.6 | -16.7 -10.4 | -13.6 -3.6 | 9731.3 9743.8 | | 5394744.69 5394738.92 | | | | | | | | | | | | | | | | | | | |
| 8 | 9900.0 9900.0 | 9750.0 9762.5 | 358.2 328.1 | -5.1 | -5.6 | -10.4 3.3 | -3.6 | 9743.8 9756.3 | | 5394738.92 5394733.15 | | 160 | | | | | | | | | | | | | | | | | |
| 9 | 9900.0 | 9775.0 | 500.2 | -1.8 | -9.2 | -3.4 | -5.7 | 9768.8 | | 5394727.38 | | | | | | | 1 | 1 | | | | | | D | | | | | |
| 10 | 9900.0 | 9787.5 | 392.6 | 0.2 | -9.1 | -7.9 | -5.8 | 9781.3 | | 5394721.61 | | 140 | | | | | | 1 | | | | | In | n-Phase | | | | | |
| 11 | 9900.0 | 9800.0 | 379.9 | 0.8 | -10.4 | -3.7 | -3.4 | 9793.8 | | 5394715.84 | | | | | | | | 1 | | | | | — Qu | uad | | | | | |
| 12 | 9900.0 | 9812.5 | 375.7 | 1.3 | -10.9 | -3.1 | -4.0 | 9806.3 | | 5394710.06 | | 120 | | | | | | 11 | | | | | | | | | | | |
| 13 | 9900.0 | 9825.0 | 371.3 | 2.8 | -11.2 | -4.9 | -4.7 | 9818.8 | | 5394704.29 | | | | | | | | 11 | | | | | Fr | raser Filt | er | | | | |
| 14 15 | 9900.0 9900.0 | 9837.5 9850.0 | 364.2 363.0 | 4.2 4.4 | -12.0 -12.5 | -4.5 -5.0 | -4.8 | 9831.3 9843.8 | | 5394698.52 5394692.75 | | 100 | | | | | Ļ | 4 | | | | | | | | | | | |
| 15 16 | 9900.0 9900.0 | 9850.0 9862.5 | 363.0 | 4.4 7.6 | -12.5 | -5.0 | -7.7 | 9843.8 9856.3 | | | | | | | | | I | | | | | | | | | | | | |
| 17 | 9900.0 | 9802.3 | 332.2 | 11.3 | -12.3 | -10.3 | -10.7 | 9868.8 | | 5394681.20 | | 80 | | | | | <u> </u> | 4 | | | | | | | | | | | |
| 18 | 9900.0 | 9887.5 | 318.8 | 13.8 | -11.0 | -8.3 | -5.7 | 9881.3 | 549552.77 | | | | | | | | | | | | | | | | | | | | |
| 19 | 9900.0 | 9900.0 | 282.9 | 13.4 | -12.4 | -3.1 | -3.2 | 9893.8 | | 5394669.66 | | 60 | | | | | A | | | | | | | | | | | | |
| 20 | 9900.0 | 9912.5 | 333.8 | 14.8 | -13.3 | -3.2 | -4.8 | 9906.3 | | 5394663.89 | | | | | | | /N | | | | | | | | | | | | |
| 21 | 9900.0 | 9925.0 | 719.9 | 15.6 | -15.5 | -6.3 | -8.3 | 9918.8 | | 5394658.12 | | 40 | | | | | | \square | | | | | | | | | | | |
| 22 | 9900.0 9900.0 | 9937.5 9950.0 | 687.2 702.7 | 18.9 21.8 | -15.4 -15.3 | -10.3 -16.0 | -13.2 -16.9 | 9931.3 9943.8 | 549597.12 549608.21 | 5394652.35 5394646 57 | | | | | | 1 | † | | | | | | | | | | | | |
| 23 | 9900.0 9900.0 | 9950.0 9962.5 | 1031.1 | 21.8 | -15.3 | -16.0 | -16.9 | 9943.8 9956.3 | | 5394646.57 5394640.80 | | 20 | | | | | | | | | | | | | | | | | |
| 24 | 9900.0 | 9962.5 9975.0 | 558.5 | 28.7 | -12.5 | -17.8 | -10.2 | 9956.3 | | 5394640.80 5394635.03 | | 20 | | | ~ | / | | | | ~ | | \sim | | | | | | | |
| 26 | 9900.0 | 9987.5 | 454.2 | 32.9 | -13.8 | -8.2 | -7.3 | 9981.3 | | 5394629.26 | | 0 | | | | | | V | \sim | 1~ | / | 14 | | ~ | | | | | |
| 27 | | 10000.0 | 428.2 | 33.8 | -14.7 | | -6.0 | 9993.8 | 549652.56 | 5394623.49 | | 9600 | | ASC | \sim | 20 | 000 V | 1 | 6200 | $\langle N \rangle$ | 10400 | Ner | 10 | 108 | 100 | 11000 |) | 1120 | 0 |
| 28 | | 10012.5 | 401.5 | | | | | 10006.3 | | 5394617.71 | | -20 | ` | V | | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ | 1 | 1V | | \sim | | | | 100 | - | 1000 | | | |
| 29 | | 10025.0 | 337.9 | 36.9 | -17.4 | | | 10018.8 | | 5394611.94 | | 23 | | | | | | V | | | | | | | | | | | |
| 30 31 | | 10037.5 10050.0 | 970.1 695.7 | 40.0 44.4 | -19.5 -15.9 | -16.6 | -14.4 -16.9 | 10031.3 10043.8 | 549685.83 549696 91 | 5394606.17 5394600.40 | | -40 | | | | | | | | | | | | | | | | | |
| 31 | | 10050.0 | 573.1 | 44.4 | -13.9 | -16.6 | -16.9 | 10043.8 | | 5394600.40 5394594.63 | | 40 | | | | | | | | | | | | | | | | | |
| 33 | | 10075.0 | 534.8 | 52.4 | -13.1 | -17.1 | -17.9 | 10050.3 | | 5394588.86 | | | | | | | | | | | | | | | | | | | |
| 34 | | 10087.5 | 518.6 | 57.6 | -11.9 | -19.2 | -14.1 | 10081.3 | | 5394583.08 | | | | | | | | | | | | | | | | | | | |
| 35 | 9900.0 | 10100.0 | 527.5 | 63.1 | -5.5 | -8.9 | 31.9 | 10093.8 | 549741.26 | 5394577.31 | | | | | | | | | | | | | | | | | | | |
| 36 | | 10112.5 | 501.7 | 55.8 | 1.8 | 72.7 | 112.7 | 10106.3 | | 5394571.54 | | | | | | | | | | | | | | | | | | | |
| 37 | | 10125.0 | 497.0 | -7.8 | -3.2 | 152.6 | 124.4 | 10118.8 | | 5394565.77 | | | | | | | | | | | | | | | | | | | |
| 38 39 | | 10137.5 10150.0 | 486.1 478.8 | -25.9 -22.2 | 0.2 | 96.1 3.9 | 50.0 -9.3 | 10131.3 10143.8 | | 5394560.00 5394554.22 | | | | | | | | | | | | | | | | | | | |
| 40 | | 10150.0 | 478.8 | -22.2 | 3.3 | -22.5 | -9.3 | 10143.8 10156.3 | | 5394554.22 5394548.45 | | | | | | | | | | | | | | | | | | | |
| 41 | | 10102.3 | 473.2 | -13.4 | 9.4 | -22.5 | -21.0 | 10156.5 | | 5394542.68 | | | | | | | | | | | | | | | | | | | |
| 42 | | 10187.5 | 458.5 | -7.9 | 9.1 | -9.3 | -4.8 | 10181.3 | 549818.88 | | | | | | | | | | | | | | | | | | | | |
| 43 | 9900.0 | 10200.0 | 455.8 | -8.4 | 7.7 | -0.2 | 1.0 | 10193.8 | 549829.96 | 5394531.14 | | | | | | | | | | | | | | | | | | | |
| 44 | | 10212.5 | 452.1 | -9.5 | 6.2 | 2.1 | 0.1 | 10206.3 | | 5394525.37 | | | | | | | | | | | | | | | | | | | |
| 45 | | 10225.0 | 448.7 | -8.9 | 5.6 | -1.9 | -4.0 | 10218.8 | | 5394519.59 | | | | | | | | | | | | | | | | | | | |
| 46 47 | | 10237.5 10250.0 | 450.2 446.1 | -7.1 -5.2 | 6.4 6.3 | -6.1 -7.9 | -7.0 | 10231.3 10243.8 | | 5394513.82 5394508.05 | | | | | | | | | | | | | | | | | | | |
| 47 | | 10250.0 | 446.1 435.7 | -5.2 -2.9 | 6.3 7.8 | -7.9 -8.2 | -8.1 -8.0 | 10243.8 10256.3 | | 5394508.05 5394502.28 | | | | | | | | | | | | | | | | | | | |
| 49 | | 10282.3 | 433.7 | -2.9 | 8.4 | -0.2 | -8.3 | 10258.8 | | 5394502.28 | | | | | | | | | | | | | | | | | | | |
| 50 | | 10275.5 | 482.7 | 0.8 | 9.3 | -8.9 | -10.4 | 10281.3 | | 5394490.73 | | | | | | | | | | | | | | | | | | | |
| 51 | | 10300.0 | 476.6 | 4.0 | 10.7 | -11.9 | -12.8 | 10293.8 | | | | | | | | | | | | | | | | | | | | | |
| 52 | | 10312.5 | 585.9 | 7.5 | 12.6 | -13.7 | -12.9 | 10306.3 | | 5394479.19 | | | | | | | | | | | | | | | | | | | |
| 53 | | 10325.0 | 623.3 | 11.0 | 14.9 | -12.1 | -8.4 | 10318.8 | | 5394473.42 | | | | | | | | | | | | | | | | | | | |
| 54 | 9900.0 | 10337.5 | 465.2 | 12.6 | 14.2 | -4.7 | -1.5 | 10331.3 | 549951.93 | | | | | | | | | | | | | | | | | | | | |
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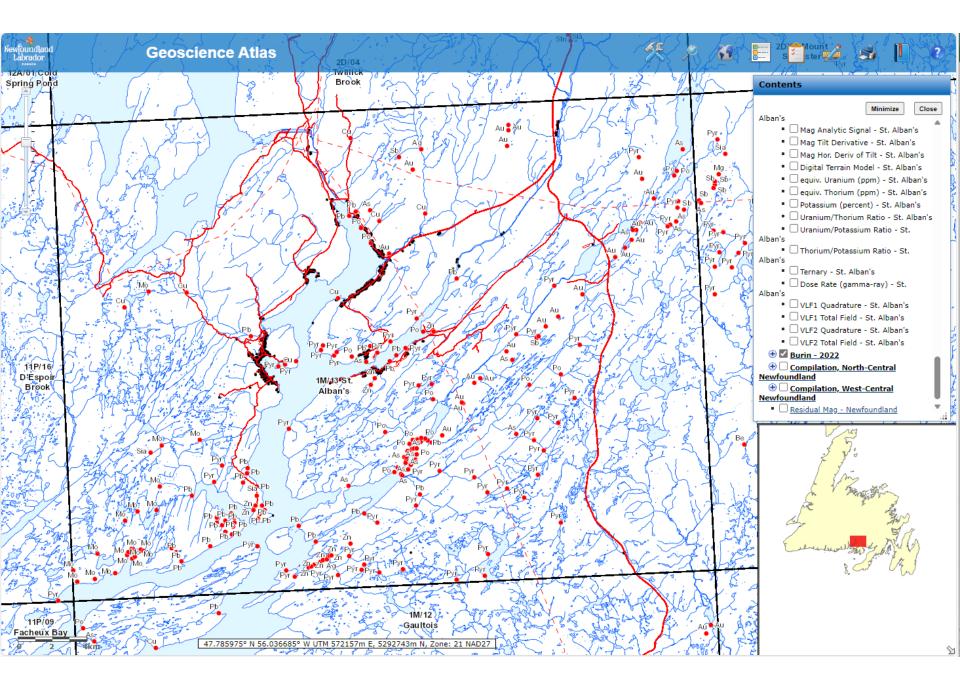
| F. | 5 •∂ |) | | | | | Cha | art Tools | | | | | | Shanan | MV_L99.xlsx - | - Excel | | _ | | | | | | | | | | 团 | - 0 | × |
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| | А | В | с | D | E | | | | | J | к | L | м | N | 0 | Р | Q | R | S | т | U | v | w | х | Y | Z | AA | AB | AC A | D |
| 1 | Line | Grid X 9900 | Mag | In-Phase | Quad F | Fraser Filter F | F_interp G | Grid_X+1/2 | Easting | Northing | | | | | | | | | | | | | | | | | | | | |
| 3 | 9900.0 | | 397.0 | -2.2 | -3.0 | | | | 549386.46 | 5394762.01 | c |) —— | | | | | | | | | 0 | | | | | | | | | , |
| 4 | 9900.0 | 9712.5 | 400.7 | -8.6 | -7.3 | | 13.5 | 9706.3 | | 5394756.24 | | | | | | | | | | Sha | inan Lir | ne 9900 | - VLF | | | | | | | |
| 5 | 9900.0 | 9725.0 | 372.4 | | -10.4 | 4.6 | -6.1 | 9718.8 | | 5394750.47 | | 180 | | | | | | | | | | | | | | | | | | |
| 6 7 | 9900.0 9900.0 | 9737.5 9750.0 | 364.4 358.2 | -3.7 0.1 | -7.5 -5.6 | -16.7 -10.4 | -13.6 -3.6 | 9731.3 9743.8 | | 5394744.69 5394738.92 | | | | | | | | | | | | | | | | | | | | _ |
| 8 | 9900.0 | 9762.5 | 328.1 | -5.1 | -9.2 | 3.3 | -0.1 | 9756.3 | | 5394733.15 | | 160 | | | | | | | | | | | | | | | | | | |
| 9 | 9900.0 | 9775.0 | 500.2 | -1.8 | -9.0 | -3.4 | -5.7 | 9768.8 | | 5394727.38 | | | | | | | | 1 | | | | | | — In-Pha | | | | | | |
| 10 | 9900.0 | 9787.5 | 392.6 | 0.2 | -9.1 | -7.9 | -5.8 | 9781.3 | | 5394721.61 | | 140 | | | | | | 1 | | | | | | - m-Phas | be | | | | | |
| 11 | 9900.0 9900.0 | 9800.0 9812.5 | 379.9 | 0.8 | -10.4 | -3.7 | -3.4 | 9793.8 | | 5394715.84 | | | | | | | | 1 | | | | | | — Quad | | | | | | |
| 12 13 | 9900.0 | 9812.5 | 375.7 371.3 | 1.3 2.8 | -10.9 -11.2 | -3.1 -4.9 | -4.0 -4.7 | 9806.3 9818.8 | | 5394710.06 5394704.29 | | 120 | | | | | | 11 | | | | | | | Filter | | | | | |
| 14 | 9900.0 | 9837.5 | 364.2 | 4.2 | -12.0 | -4.5 | -4.8 | 9831.3 | | 5394698.52 | | | | | | | | 11 | | | | | | 114301 | | | | | | |
| 15 | 9900.0 | 9850.0 | 363.0 | 4.4 | -12.5 | -5.0 | -7.7 | 9843.8 | | 5394692.75 | | 100 | | | | | | | | | | | | | | | | | | |
| 16 17 | 9900.0 9900.0 | 9862.5 9875.0 | 341.3 | 7.6 | -12.3 | -10.3 | -11.7 | 9856.3 9868.8 | | 5394686.98 | | 80 | | | | | | | | | | | | | | | | | | |
| 17 | 9900.0 | 9875.0 | 332.2 318.8 | 11.3 13.8 | -11.6 -11.0 | -13.1 -8.3 | -10.7 -5.7 | 9881.3 | | 5394681.20 5394675.43 | | | | | | | | | | | | | | | | | | | | _ |
| 19 | 9900.0 | 9900.0 | 282.9 | 13.4 | -12.4 | -3.1 | -3.2 | 9893.8 | | 5394669.66 | | 60 | | | | | | | | | | | | | | | | | | |
| 20 | 9900.0 | 9912.5 | 333.8 | 14.8 | -13.3 | -3.2 | -4.8 | 9906.3 | | 5394663.89 | | 00 | | | | | | ¥ | | | | | | | | | | | | |
| 21 | 9900.0 9900.0 | 9925.0 9937.5 | 719.9 687.2 | 15.6 18.9 | -15.5 -15.4 | -6.3 -10.3 | -8.3 -13.2 | 9918.8 9931.3 | | 5394658.12 5394652.35 | | 40 | | | | | | | | | | | | | | | | | | _ |
| 22 23 | 9900.0 | 9937.5 | 702.7 | 21.8 | -15.4 | -10.3 | -13.2 | 9931.3 9943.8 | | 5394652.35 | | | | | | ~ | 88 | | | | | | | | | | | | | |
| 24 | 9900.0 | 9962.5 | 1031.1 | 28.7 | -12.5 | -17.8 | -15.0 | 9956.3 | | 5394640.80 | | 20 | | | | | | | | | * | | ~ | | | | | | | |
| 25 | 9900.0 | 9975.0 | 558.5 | 29.8 | -14.2 | -12.2 | -10.2 | 9968.8 | | 5394635.03 | | | | | × | | | | ~ | \sim | | \sim | | | | | | | | |
| 26 | 9900.0 | 9987.5 10000.0 | 454.2 428.2 | 32.9 33.8 | -13.8 -14.7 | -8.2 | -7.3 -6.0 | 9981.3 9993.8 | | 5394629.26 | | 0 | 8 | A Ar | | <u> </u> | | NK- | \wedge | | | | | | 88 | | | | | _ |
| 27 28 | 9900.0 9900.0 | 10000.0 | 428.2 | 33.8 | -14.7 | | -6.0 | 10006.3 | | 5394623.49 5394617.71 | | 960 | 00 | V~× | 200 | 20 | 000 | 111 | 10200 | \sim | 10400 | | 10600 | | 10800 | | 11000 |) | 11200 | |
| 29 | 9900.0 | 10025.0 | 337.9 | 36.9 | -17.4 | | | 10018.8 | | 5394611.94 | | -20 | | | | ~ | ~~ | V | | | | | | | | | | | | |
| 30 | 9900.0 | 10037.5 | 970.1 | 40.0 | -19.5 | | -14.4 | 10031.3 | | 5394606.17 | | | | | | | | | | | | | | | | | | | | |
| 31 32 | 9900.0 9900.0 | 10050.0 10062.5 | 695.7 573.1 | 44.4 49.1 | -15.9 -13.7 | -16.6 -17.1 | -16.9 -16.8 | 10043.8 10056.3 | | 5394600.40 5394594.63 | | -40 | | | | | | | | | | | | | | | | | | |
| 33 | 9900.0 | 10002.5 | 534.8 | 52.4 | -13.1 | -17.1 | -10.8 | 10050.3 | | 5394588.86 | | | | | | | | | | | | | | | | | | | | |
| 34 | 9900.0 | 10087.5 | 518.6 | 57.6 | -11.9 | -19.2 | -14.1 | 10081.3 | | 5394583.08 | Ċ |) | | | | | | | | | 0 | | | | | | | | ċ | · · · · · |
| 35 | 9900.0 | 10100.0 | 527.5 | | -5.5 | -8.9 | 31.9 | 10093.8 | | 5394577.31 | | | | | | | | | | | | | | | | | | | | |
| 36 37 | 9900.0 9900.0 | 10112.5 10125.0 | 501.7 497.0 | 55.8 -7.8 | 1.8 -3.2 | 72.7 152.6 | 112.7 124.4 | 10106.3 10118.8 | | 5394571.54 5394565.77 | | | | | | | | | | | | | | | | | | | | |
| 38 | 9900.0 | 10125.0 | 497.0 | -25.9 | -3.2 | 96.1 | 50.0 | 10118.8 | | 5394560.00 | | | | | | | | | | | | | | | | | | | | |
| 39 | 9900.0 | 10150.0 | 478.8 | -22.2 | 3.3 | 3.9 | -9.3 | 10143.8 | | 5394554.22 | | | | | | | | | | | | | | | | | | | | |
| 40 | 9900.0 | 10162.5 | 475.2 | -15.4 | 7.1 | -22.5 | -21.0 | 10156.3 | | 5394548.45 | | | | | | | | | | | | | | | | | | | | |
| 41 42 | 9900.0 9900.0 | 10175.0 10187.5 | 469.1 458.5 | -10.2 -7.9 | 9.4 9.1 | -19.5 -9.3 | -14.4 -4.8 | 10168.8 10181.3 | | 5394542.68 5394536.91 | | | | | | | | | | | | | | | | | | | | |
| 42 43 | 9900.0 | 10187.5 | 458.5 | -7.9 | 7.7 | -9.3 | -4.8 | 10181.3 | | 5394536.91 | | | | | | | | | | | | | | | | | | | | |
| 44 | 9900.0 | 10212.5 | 452.1 | -9.5 | 6.2 | 2.1 | 0.1 | 10206.3 | 549841.05 | 5394525.37 | | | | | | | | | | | | | | | | | | | | |
| 45 | 9900.0 | 10225.0 | 448.7 | -8.9 | 5.6 | -1.9 | -4.0 | 10218.8 | | 5394519.59 | | | | | | | | | | | | | | | | | | | | |
| 46 47 | 9900.0 9900.0 | 10237.5 10250.0 | 450.2 446.1 | -7.1 -5.2 | 6.4 6.3 | -6.1 -7.9 | -7.0 -8.1 | 10231.3 10243.8 | | 5394513.82 5394508.05 | | | | | | | | | | | | | | | | | | | | |
| 47 | 9900.0 | 10250.0 | 440.1 | -3.2 | 7.8 | -7.9 | -8.1 | 10245.8 | | 5394502.28 | | | | | | | | | | | | | | | | | | | | |
| 49 | 9900.0 | 10275.0 | 427.4 | -1.2 | 8.4 | -7.7 | -8.3 | 10268.8 | | 5394496.51 | | | | | | | | | | | | | | | | | | | | |
| 50 | 9900.0 | 10287.5 | 482.7 | 0.8 | 9.3 | -8.9 | -10.4 | 10281.3 | | 5394490.73 | | | | | | | | | | | | | | | | | | | | |
| 51 52 | 9900.0 9900.0 | 10300.0 10312.5 | 476.6 585.9 | 4.0 7.5 | 10.7 12.6 | -11.9 -13.7 | -12.8 -12.9 | 10293.8 10306.3 | | 5394484.96 5394479.19 | | | | | | | | | | | | | | | | | | | | |
| 52 | 9900.0 | 10312.5 | 623.3 | 11.0 | 12.6 | -13.7 | -12.9 | 10306.3 | | 5394479.19 | | | | | | | | | | | | | | | | | | | | |
| 54 | 9900.0 | | 465.2 | 12.6 | 14.2 | -4.7 | -1.5 | | 549951.93 | | | | | | | | | | | | | | | | | | | | | |
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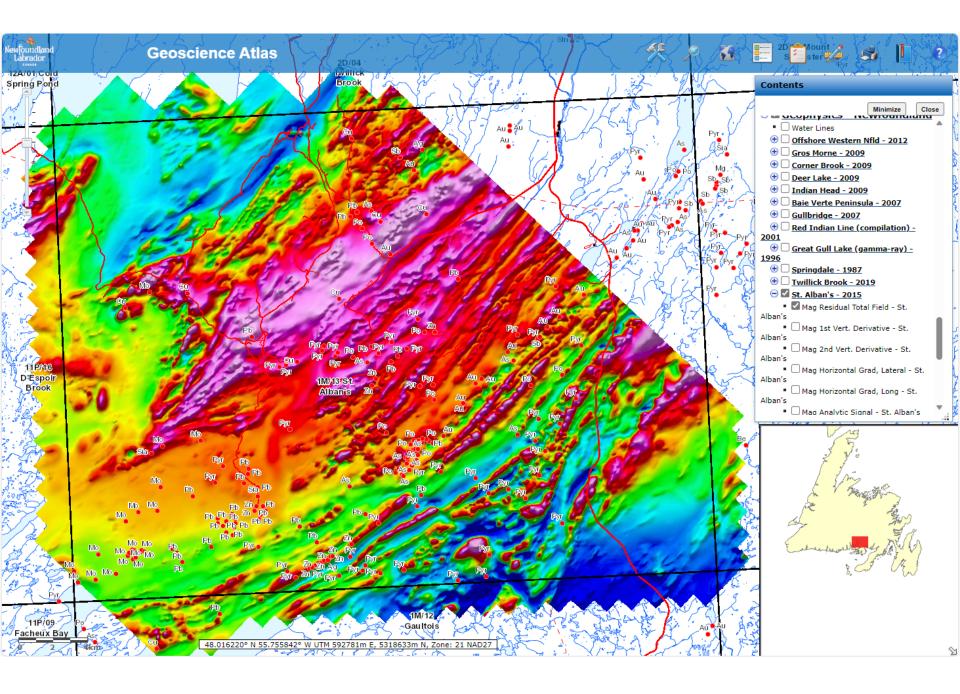
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| 4 | 9900.0 9900.0 | 9712.5 9725.0 | 400.7 372.4 | -8.6 | -7.3 -10.4 | 4.6 | 13.5 -6.1 | 9706.3 9718.4 | | 5394756.24 5394750.47 | | | | | | | | | | Line | 9900 - 1 | LF | | | | | | | | |
| 6 | 9900.0 | 9737.5 | 364.4 | -3.7 | -7.5 | -16.7 | -13.6 | 9731. | | 5394744.69 | | 180 | | | | | | | | | | | | | | | | | | |
| 7 | 9900.0 | 9750.0 | 358.2 | 0.1 | -5.6 | -10.4 | -3.6 | 9743. | | 5394738.92 | | 160 | | | | | | | | | | | | | | | | | | |
| 8 | 9900.0 9900.0 | 9762.5 9775.0 | 328.1 500.2 | -5.1 -1.8 | -9.2 -9.0 | 3.3 -3.4 | -0.1 -5.7 | 9756. 9768. | | 5394733.15 5394727.38 | | | | | | | | 1 | | | | | | | | _ | | | | - |
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| 11 | 9900.0 | 9800.0 | 379.9 | | -10.4 | -3.7 | -3.4 | 9793. | | 5394715.84 | | | | | | | | 1 | | | | | | — Qua | ad | | | | | |
| 12 13 | 9900.0 9900.0 | 9812.5 9825.0 | 375.7 371.3 | 1.3 | -10.9 -11.2 | -3.1 -4.9 | -4.0 -4.7 | 9806. 9818. | | 5394710.06 5394704.29 | | 120 | | | | | | 11 | | | | | | - Fras | ser Fil+ | er | | | | + $+$ |
| 14 | 9900.0 | 9837.5 | 364.2 | 4.2 | -11.2 | -4.5 | -4.8 | 9831. | | 5394698.52 | | | | | | | | 11 | | | | | | 1103 | Jer Fill | | | | | |
| 15 | 9900.0 | 9850.0 | 363.0 | | -12.5 | -5.0 | -7.7 | 9843. | | | | 100 | | | | | | | | | | | | | | | | | | 1 [] |
| 16 17 | 9900.0 9900.0 | 9862.5 9875.0 | 341.3 332.2 | | -12.3 -11.6 | -10.3 -13.1 | -11.7 -10.7 | 9856. 9868. | | 5394686.98 5394681.20 | | 80 | | | | | | | | | | | | | | | | | | L H |
| 18 | 9900.0 | 9887.5 | 318.8 | 11.3 | -11.0 | -13.1 -8.3 | -10.7 | 9881. | | 5394675.43 | | 0 | | | | | | | | | | | | | | | | | | |
| 19 | 9900.0 | 9900.0 | 282.9 | 13.4 | -12.4 | -3.1 | -3.2 | 9893. | 8 549563.86 | 5394669.66 | | 60 | | | | | | | | | | | | | | | | | | |
| 20 21 | 9900.0 9900.0 | 9912.5 9925.0 | 333.8 719.9 | 14.8 15.6 | -13.3 -15.5 | -3.2 -6.3 | -4.8 -8.3 | 9906.3 9918.4 | | 5394663.89 5394658.12 | | | | | | | | | | | | | | | | | | | | $ $ |
| 21 | 9900.0 | 9925.0 | 687.2 | | -15.5 | -0.3 | -8.3 | 9918. | | 5394658.12 | | 40 | | | | | | | | | | | | | | | | | | |
| 23 | 9900.0 | 9950.0 | 702.7 | 21.8 | -15.3 | -16.0 | -16.9 | 9943. | 8 549608.21 | 5394646.57 | | | | | | \square | | | | | - | | | | | | | | | |
| 24 | 9900.0 9900.0 | 9962.5 9975.0 | 1031.1 558.5 | 28.7 29.8 | -12.5 -14.2 | -17.8 | -15.0 | 9956.3 9968.4 | | 5394640.80 5394635.03 | | 20 | | | ~ | | | | | | | \sim | | | | | | | | 1 |
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| 27 | 9900.0 | 10000.0 | 428.2 | | -14.7 | | -6.0 | 9993. | 8 549652.56 | 5394623.49 | | 960 | 0 | AX | | 200 | 00 | | | $\langle \rangle$ | 10400 | | 0600 | \sim | 108 | 300 | 110 | 000 | 1 | 1200 |
| 28 | 9900.0 | 10012.5 | 401.5 | 26.0 | | | | 10006. | | 5394617.71 | | -20 | - | V | | | \triangleleft | V | | \sim | | | | | 100 | | 11 | | 1 | |
| 29 30 | 9900.0 9900.0 | 10025.0 10037.5 | 337.9 970.1 | 36.9 40.0 | -17.4 -19.5 | | -14.4 | 10018. | | 5394611.94 5394606.17 | | - | | | | | | V | | | | | | | | | | | | |
| 31 | | 10050.0 | 695.7 | 44.4 | -15.9 | -16.6 | -16.9 | 10043. | | 5394600.40 | | -40 | | | | | | | | | | | | | | | | | | |
| 32 | 9900.0 | 10062.5 | 573.1 | | -13.7 | -17.1 | -16.8 | 10056. | | 5394594.63 | | | | | | | | | | | | | | | | | | | | |
| 33 34 | | 10075.0 10087.5 | 534.8 518.6 | 52.4 57.6 | -13.1 -11.9 | -16.5 -19.2 | -17.9 -14.1 | 10068. | | 5394588.86 5394583.08 | | 6 | 1 | | | 1 | | | | | 0 | | | | | | | | | |
| 35 | 9900.0 | 10100.0 | 527.5 | 63.1 | -5.5 | -19.2 | 31.9 | 10093. | | 5394577.31 | | | | | | | | | | | | | | | | | | | | |
| 36 | | 10112.5 | 501.7 | | 1.8 | 72.7 | 112.7 | 10106. | | 5394571.54 | | | | | | | | | | | | | | | | | | | | |
| 37 38 | 9900.0 9900.0 | 10125.0 10137.5 | 497.0 486.1 | | -3.2 0.2 | 152.6 96.1 | 124.4 50.0 | 10118. | | 5394565.77 5394560.00 | | | | | | | | | | | | | | | | | | | | |
| 39 | | 10150.0 | 478.8 | | 3.3 | 3.9 | -9.3 | 10131. | | 5394554.22 | | | | | | | | | | | | | | | | | | | | |
| 40 | | 10162.5 | 475.2 | -15.4 | 7.1 | -22.5 | -21.0 | 10156. | 3 549796.70 | 5394548.45 | | | | | | | | | | | | | | | | | | | | |
| 41 42 | | 10175.0 10187.5 | 469.1 458.5 | -10.2 -7.9 | 9.4 9.1 | -19.5 -9.3 | -14.4 -4.8 | 10168. | | 5394542.68 5394536.91 | | | | | | | | | | | | | | | | | | | | |
| 42 | 9900.0 | 10187.5 | 458.5 | -7.9 | 7.7 | -9.3 | -4.8 | 10181. | | | | | | | | | | | | | | | | | | | | | | |
| 44 | 9900.0 | 10212.5 | 452.1 | -9.5 | 6.2 | 2.1 | 0.1 | 10206.3 | 3 549841.05 | 5394525.37 | | | | | | | | | | | | | | | | | | | | |
| 45 | | 10225.0 | 448.7 | -8.9 | 5.6 | -1.9 | -4.0 | 10218. | | 5394519.59 | | | | | | | | | | | | | | | | | | | | |
| 46 47 | 9900.0 9900.0 | 10237.5 10250.0 | 450.2 446.1 | -7.1 | 6.4 6.3 | -6.1 -7.9 | -7.0 -8.1 | 10231. | | 5394513.82 5394508.05 | | | | | | | | | | | | | | | | | | | | |
| 48 | 9900.0 | 10262.5 | 435.7 | -2.9 | 7.8 | -8.2 | -8.0 | 10256. | | | | | | | | | | | | | | | | | | | | | | |
| 49 | 9900.0 | 10275.0 | 427.4 | -1.2 | 8.4 | -7.7 | -8.3 | 10268. | | | | | | | | | | | | | | | | | | | | | | |
| 50 51 | 9900.0 9900.0 | 10287.5 10300.0 | 482.7 476.6 | 0.8 4.0 | 9.3 10.7 | -8.9 -11.9 | -10.4 -12.8 | 10281. | | | | | | | | | | | | | | | | | | | | | | |
| 52 | | 10312.5 | 585.9 | 7.5 | 12.6 | -13.7 | -12.9 | 10205. | | | | | | | | | | | | | | | | | | | | | | |
| 53 | | 10325.0 | 623.3 | 11.0 | 14.9 | -12.1 | -8.4 | 10318. | | 5394473.42 | | | | | | | | | | | | | | | | | | | | |
| 54 | | 10337.5 | 465.2 | 12.6 | 14.2 | -4.7 | -1.5 | 10331. | | 5394467.65 | | | | | | | | | | | | | | | | | | | | - |
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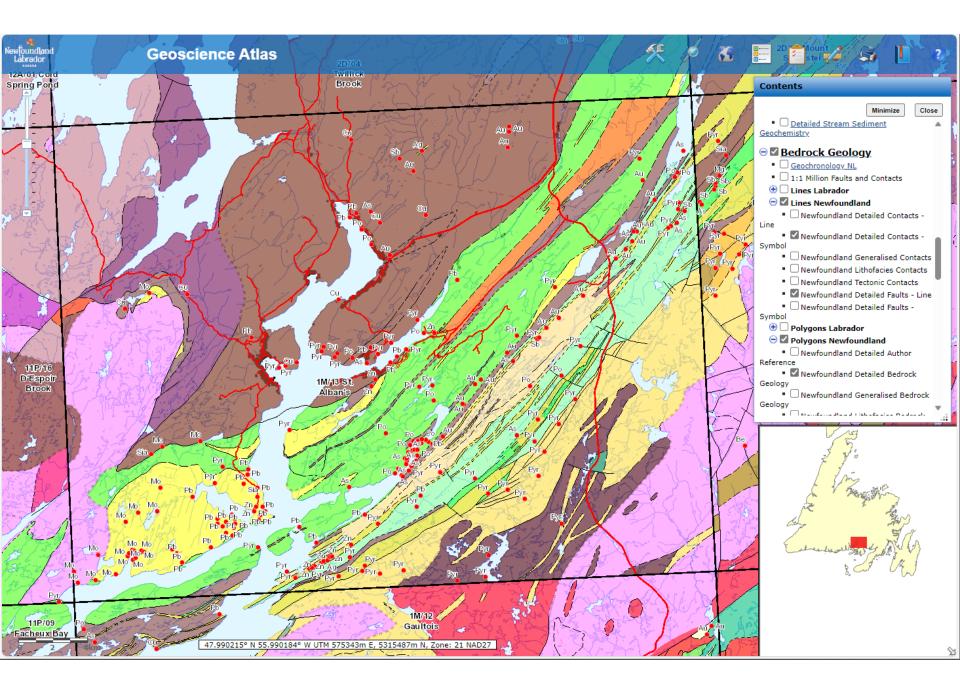
Pitfalls for VLF-EM

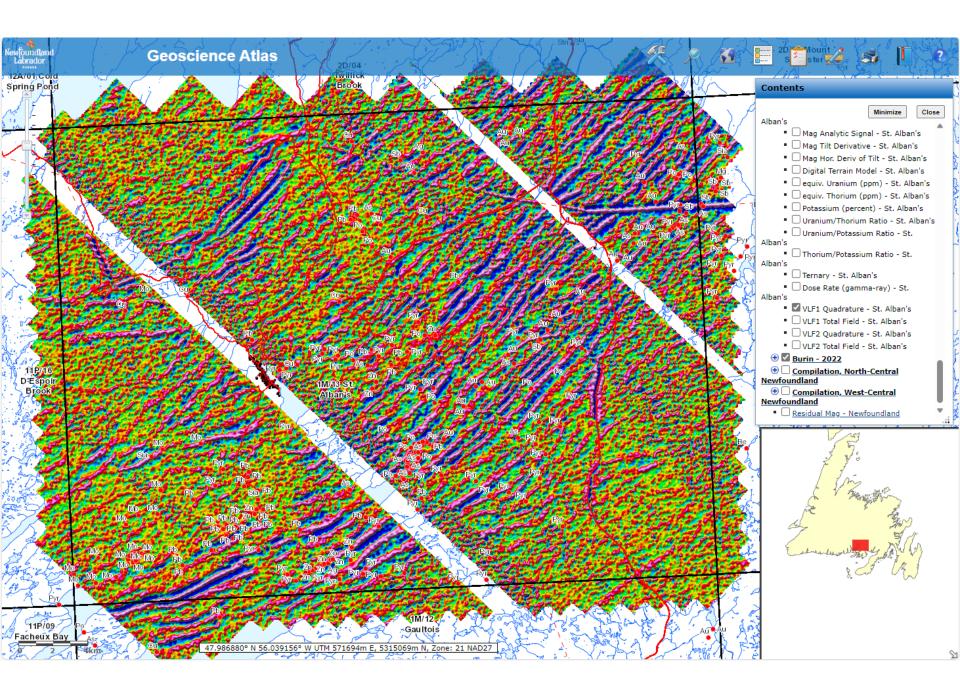
- Recording the sign (+/-) of the numbers correctly
- Switching the facing direction or orientation during survey
- Presence of cultural features power lines, cables fences, culverts, rebar, asphalt roadways, etc.
- Unforeseen causes of anomalies eg. Permafrost contacts, conductive surficial sediments

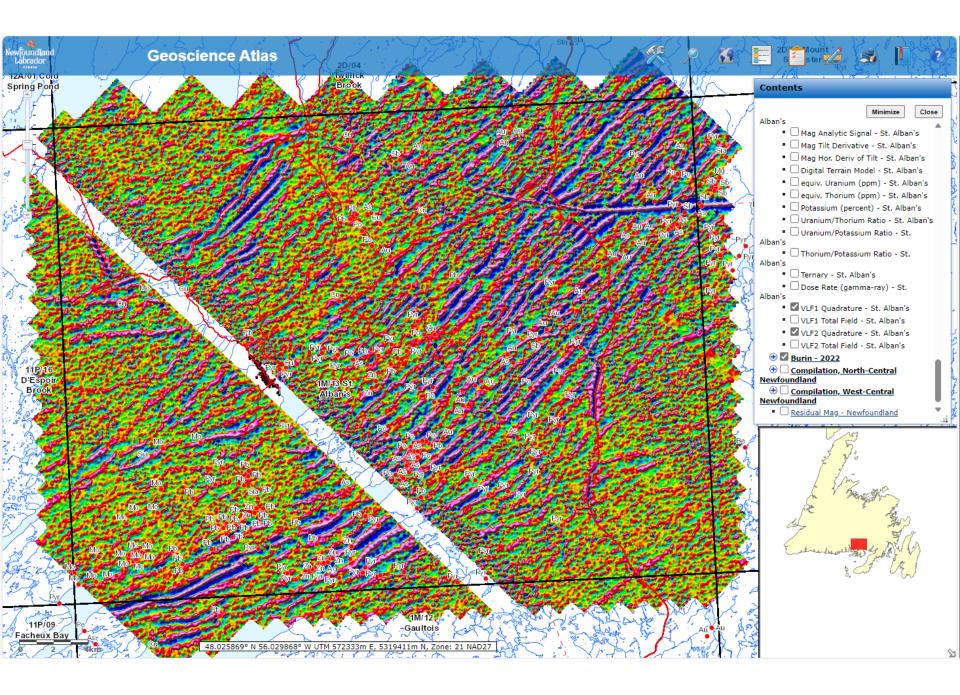
VLF-EM St. Alban's Airborne Survey

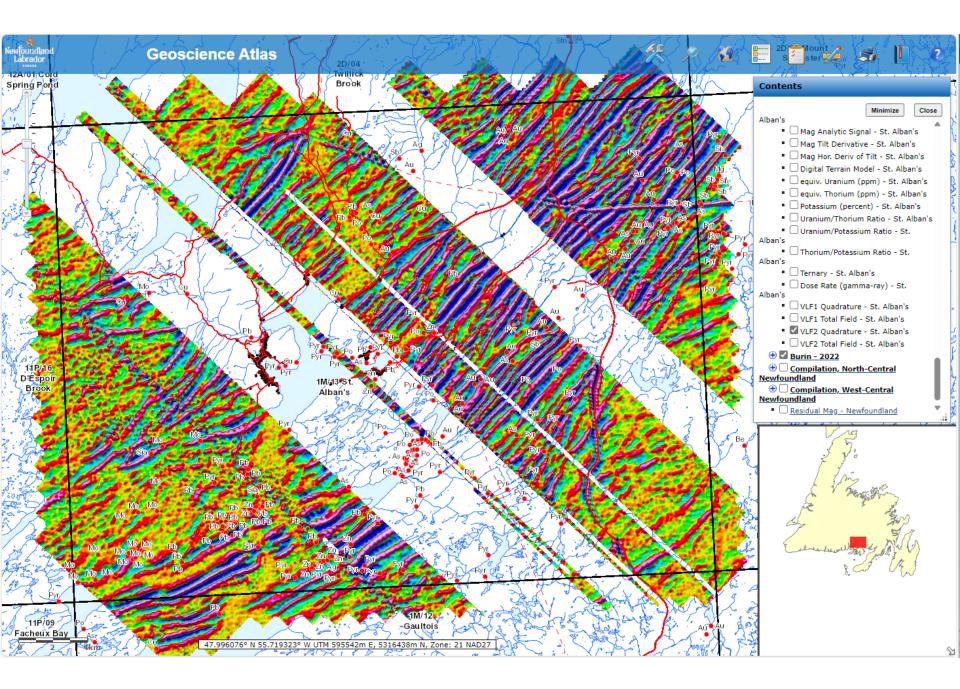


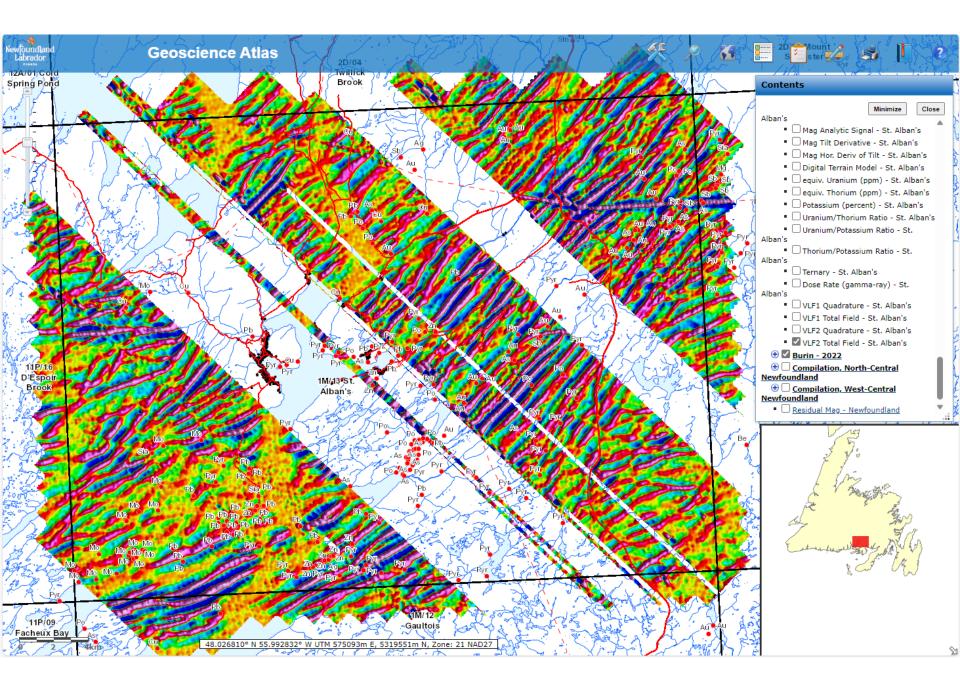


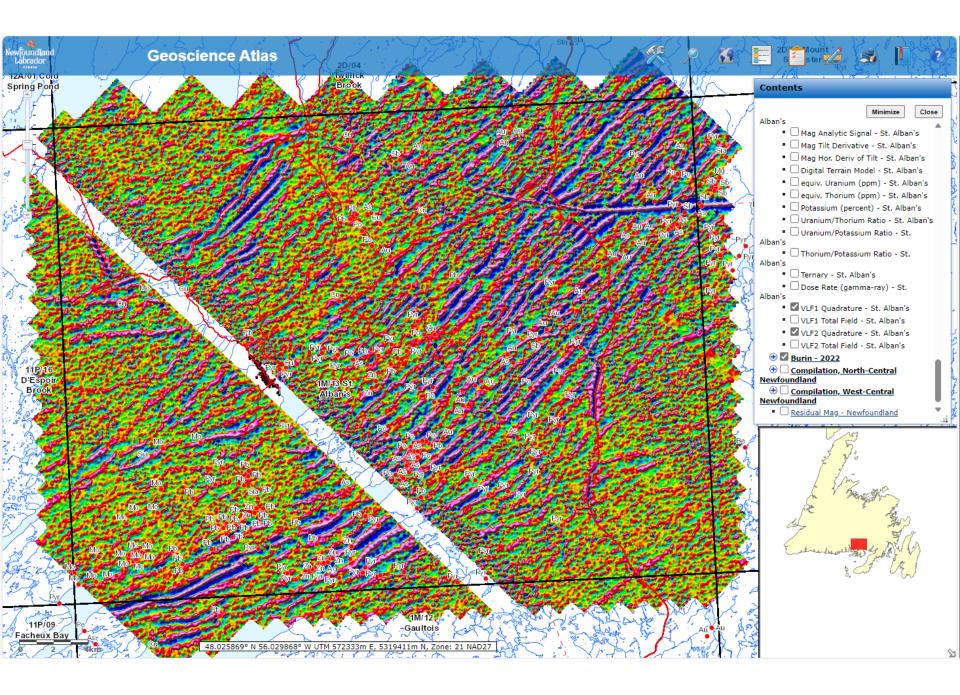


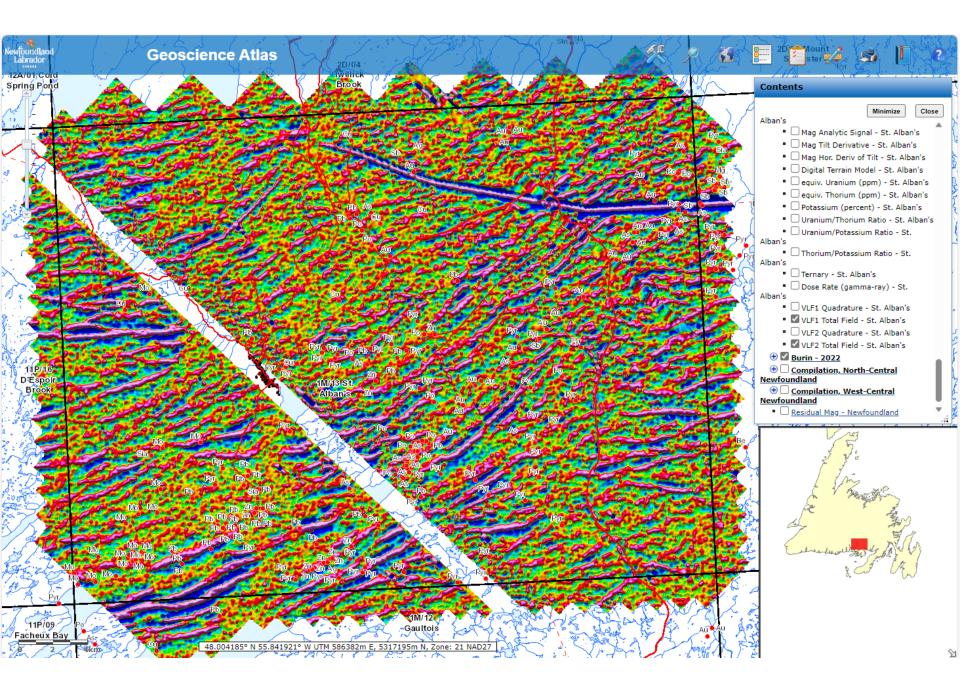


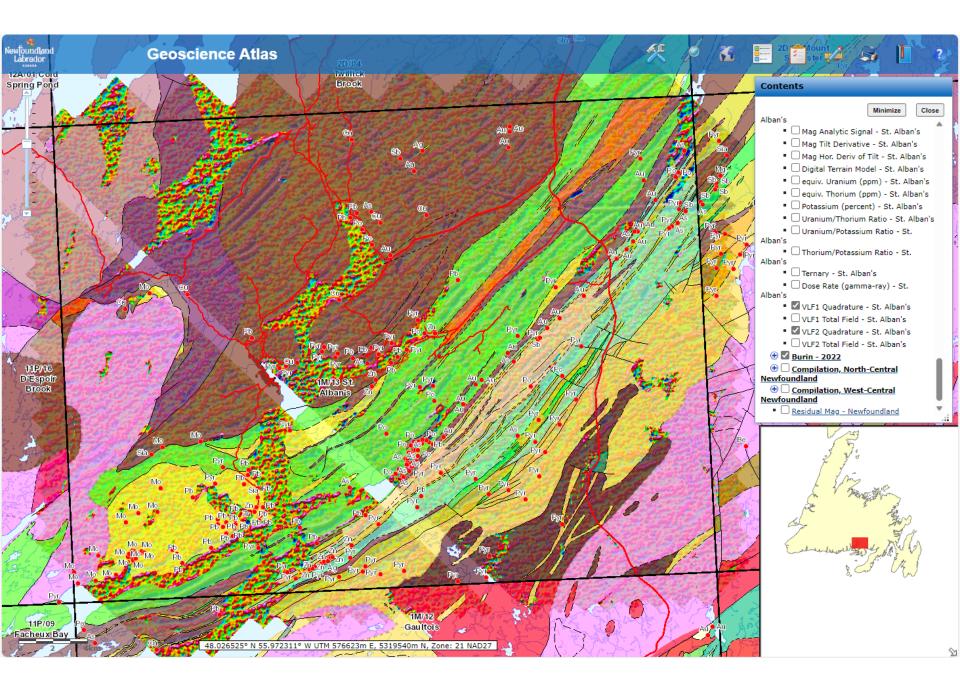


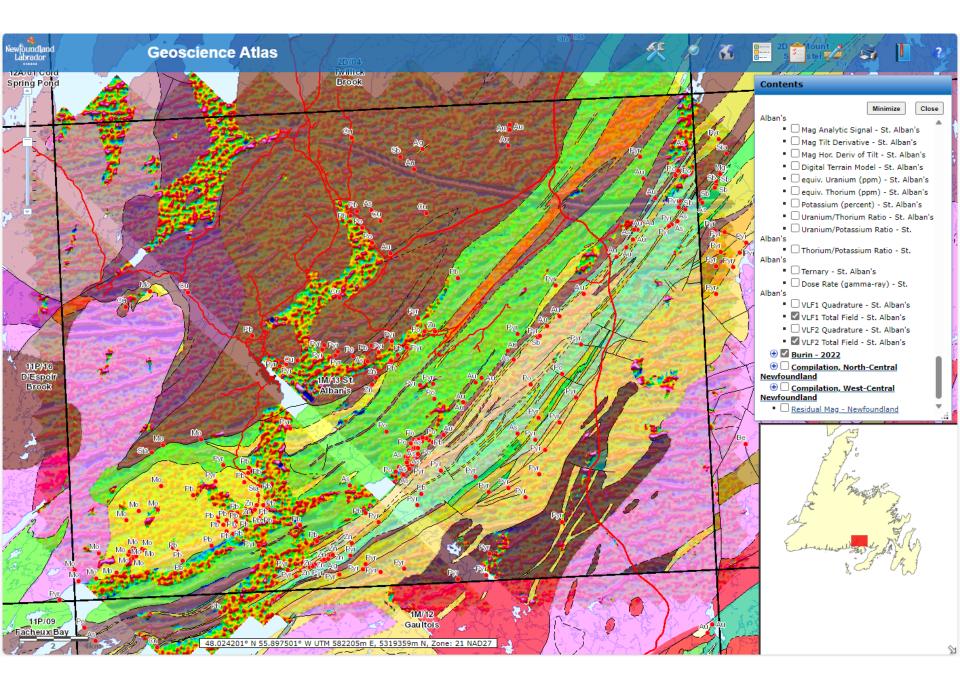




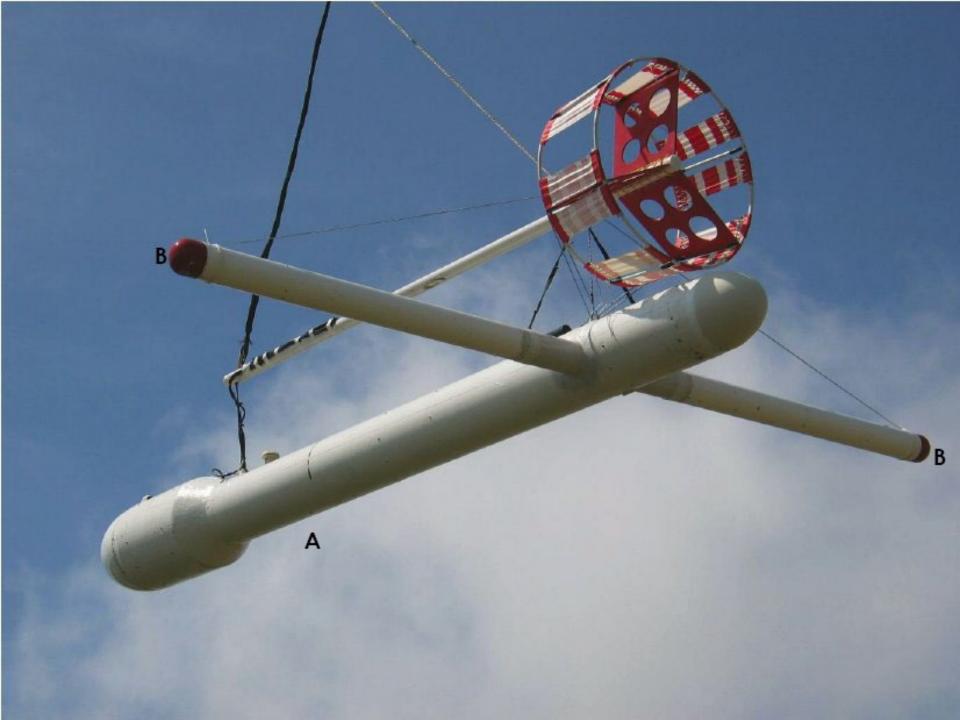


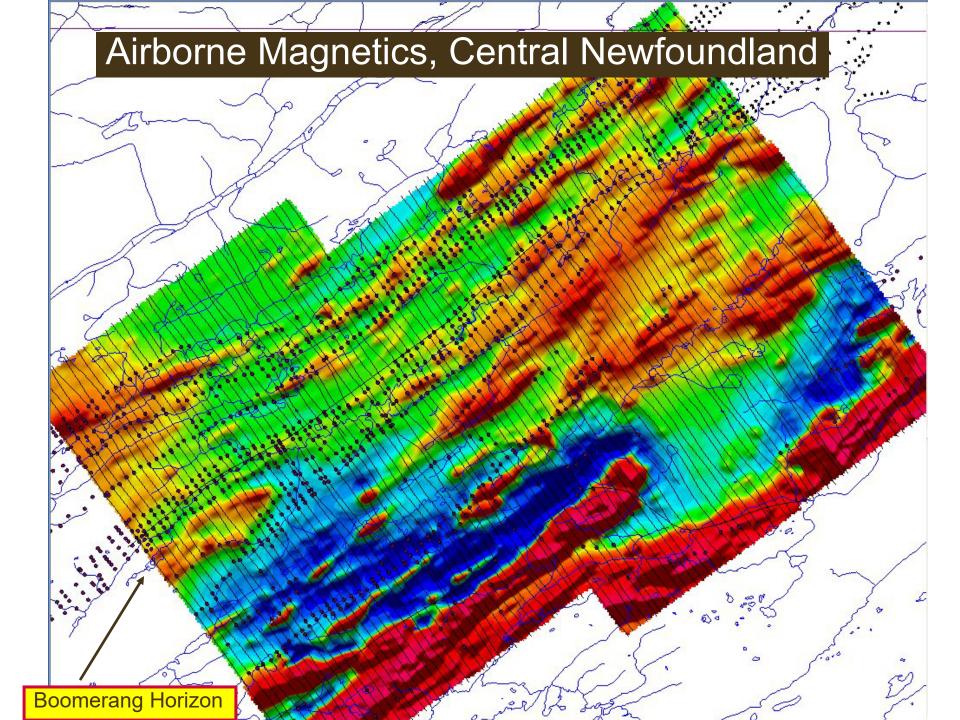




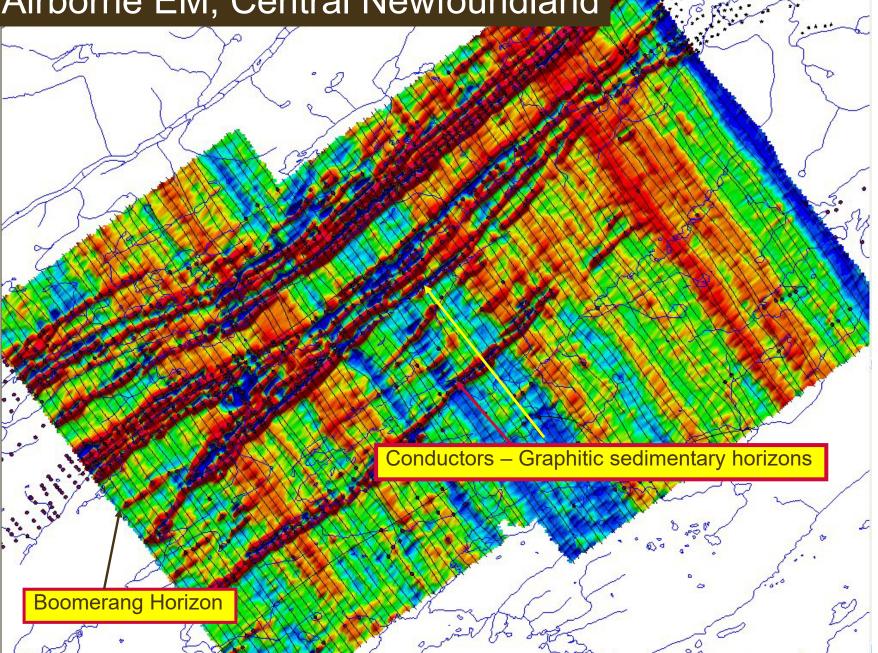








Airborne EM, Central Newfoundland



450 *Electrical properties of rocks*

Normally the sample will be equivalent to a resistance and capacitance in parallel. In some cases it may be necessary to interchange the series and parallel arms of the bridge.

5.4 Typical values of electrical constants of rocks and minerals

5.4.1 Resistivities of rocks and minerals

Of all the physical properties of rocks and minerals, electrical resistivity shows the greatest variation. While the range in density, elastic wave velocity and radioactive content is quite small, in magnetic susceptibility it may be as large as 10^5 . However, the resistivity of metallic minerals may be as small as $10^{-5} \Omega m$, that of dry, close-grained rocks like gabbro as large as $10^7 \Omega m$. The maximum possible range is even greater, from native silver ($1.6 \times 10^{-8} \Omega m$) to pure sulphur ($10^{16} \Omega m$).

A conductor is usually defined as a material of resistivity less than $10^{-5} \Omega m$, while an *insulator* is one having a resistivity greater than $10^7 \Omega m$. Between these limits lie the so-called *semiconductors*. Within this grouping the metals and graphite are all conductors; they contain a large number of free electrons whose mobility is very great. The semiconductors also carry current by mobile electrons but have fewer of them. The insulators are characterized by ionic bonding so that the valence electrons are not free to move; the charge carriers are ions which must overcome larger barrier potentials than exist either in the semiconductors or conductors.

A further difference between conductors and semiconductors is found in their respective variation with temperature. The former vary inversely with temperature and have their highest conductivities in the region of $0^{\circ}K$. The semiconductors, on the other hand, are practically insulators at low temperatures.

In a looser classification, rocks and minerals are considered to be good, intermediate and poor conductors within the following ranges:

- (a) minerals of resistivity 10^{-8} to about 1 Ω m,
- (b) minerals and rocks of resistivity 1 to $10^7 \Omega m$,
- (c) minerals and rocks of resistivity above $10^7 \Omega m$.

Group (*a*) includes the metals, graphite, the sulphides except for sphalerite, cinnabar and stibnite, all the arsenides and sulpho-arsenides except $SbAs_2$, the antimonides except for some lead compounds, the tellurides and some oxides such as magnetite, manganite, pyrolusite and ilmenite. Most oxides, ores and porous rocks containing water are intermediate conductors. The common rock-forming minerals, silicates, phosphates and the carbonates, nitrates, sulphates, borates, etc., are poor conductors.

The following tables list characteristic resistivities for various minerals and rocks. The data are from various sources, including Heiland (1940), Keller (1966), Parasnis (1956, 1966), Jakosky (1950) and Parkhomenko (1967).

The variation in resistivity of particular minerals is enormous, as can be seen from table 5.2. Among the more common minerals, pyrrhotite and graphite

Table 5.1. Resistivities of metals and elements

| | Resistivit | y (Ωm) | | Resistivity | (Ωm) |
|----------|-------------------------|----------------------|------------|------------------------------|----------------------|
| Element | Range | Average | Element | Range | Average |
| Antimony | | 4.5×10^{-7} | Molybdenum | | 5.7×10^{-8} |
| Arsenic | | 2.2×10^{-7} | Nickel | | 7.8×10^{-6} |
| Bismuth | | 1.2×10^{-6} | Platinum | | 10-7 |
| Copper | | 1.7×10^{-8} | Silver | | 1.6×10^{-8} |
| Gold | | 2.4×10^{-8} | Sulphur | $10^{7} - 10^{16}$ | 1014 |
| Graphite | $5 \times 10^{-7} - 10$ | 10^{-3} | Tellurium | $10^{-4} - 2 \times 10^{-3}$ | 10-3 |
| Iron | | 10^{-7} | Tin | | 1.1×10^{-7} |
| Lead | | 2.2×10^{-7} | Uranium | | 3×10^{-7} |
| Mercury | | 9.6×10^{-7} | Zinc | | 5.8×10^{-1} |

appear to be the most consistent good conductors, while pyrite, galena and magnetite are often poor conductors in bulk form, although the individual crystals have high conductivity. Hematite and sphalerite, in pure form, are practically insulators, but when combined with impurities may have resistivities as low as $0.1 \Omega m$. Graphite is often the connecting link in mineral zones which makes them good conductors.

Table 5.2. Resistivities of minerals

| | | Resistivity (Ω | lm) |
|--------------|---------------------------------------------------|-----------------------------------------|----------------------|
| Mineral | Formula | Range | Average |
| Argentite | Ag ₂ S | 2×10^{-3} -10 ⁴ | 1.7×10^{-3} |
| Bismuthinite | Bi_2S_3 | 18-570 | |
| Covellite | CuS | $3 \times 10^{-7} - 8 \times 10^{-5}$ | 2×10^{-5} |
| Chalcocite | Cu ₂ S | $3 \times 10^{-5} - 0.6$ | 10^{-4} |
| Chalcopyrite | CuFeS ₂ | $1.2 \times 10^{-5} - 0.3$ | 4×10^{-3} |
| Bornite | Cu ₅ FeS ₄ | $2.5 \times 10^{-5} - 0.5$ | 3×10^{-3} |
| Marcasite | FeS_2 | 10 ⁻³ -3·5 | 5×10^{-2} |
| Pyrite | FeS ₂ | $2.9 \times 10^{-5} - 1.5$ | 3×10^{-1} |
| Pyrrhotite | Fe _n S _m | $6.5 \times 10^{-6} - 5 \times 10^{-2}$ | 10^{-4} |
| Cinnabar | HgS | | 2×10^{7} |
| Molybdenite | MoS_2 | $10^{-3} - 10^{6}$ | 10 |
| Galena | PbS | $3 \times 10^{-5} - 3 \times 10^{2}$ | 2×10^{-3} |
| Millerite | NiS | | 3×10^{-7} |
| Stannite | Cu ₂ FeSnS ₂ | $10^{-3}-6 \times 10^{3}$ | |
| Stibnite | Sb_2S_3 | 105-1012 | 5×10^{6} |
| Sphalerite | ZnS | $1.5 - 10^{7}$ | 10^{2} |
| Cobaltite | CoAsS | $3.5 \times 10^{-4} - 10^{-1}$ | |
| Smaltite | CoAs ₂ | | 5×10^{-5} |
| Arsenopyrite | FeAsS | 2×10^{-5} - 15 | 10-3 |
| Niccolite | NiAs | $10^{-7}-2 \times 10^{-3}$ | 2×10^{-5} |
| Sylvanite | AgAuTe ₄ | $4 \times 10^{-6} - 2 \times 10^{-5}$ | |
| Bauxite | Al ₂ O ₃ .nH ₂ O | $2 \times 10^{2} - 6 \times 10^{3}$ | |

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| Mineral | Downald | Resistivity | (Ωm) |
|-----------------------|------------------------------------------------------|---------------------------------------------------------|--------------------|
| Mineral | Formula | Range | Average |
| Braunite | Mn ₂ O ₃ | 0.16-1.2 | |
| Cuprite | Cu ₂ O | 10^{-3} -300 | 30 |
| Chromite | FeCr ₂ O ₄ | $1 - 10^{6}$ | 6 10-2 |
| Specularite | Fe_2O_3 | $2.5 \times 10^{-3} 10^{7}$ | 6×10^{-3} |
| Hematite | Fe_2O_3 | $3.5 \times 10^{-3} - 10^{7}$ $10^{3} - 10^{7}$ | |
| Limonite | $2Fe_2O_3.3H_2O$ | $5 \times 10^{-5} - 5.7 \times 10^{3}$ | |
| Magnetite Ilmenite | Fe ₃ O ₄ FeTiO ₃ | $10^{-3}-50$ | |
| Wolframite | Fe, Mn, WO ₄ | 10^{-50} $10-10^{5}$ | |
| Manganite | MnO(OH) | 10^{-10} 10^{-2} -0.3 | |
| Pyrolusite | MnO ₂ | $5 \times 10^{-3} - 10$ | |
| Quartz | SiO ₂ | $4 \times 10^{10} - 2 \times 10^{14}$ | |
| Cassiterite | SnO_2 | $4 \times 10^{-2} \times 10^{-4}$ 4×10^{-4} | 0.2 |
| Rutile | TiO ₂ | 30-1000 | 500 |
| Uraninite | 110_{2} | 30-1000 | 500 |
| (Pitchblende) | UO_2 | 1-200 | |
| Anhydrite | CàSO ₄ | 1-200 | 10 ⁹ |
| Calcite | CaCO ₃ | | 2×10^{12} |
| Fluorite | CaF ₂ | | 8×10^{13} |
| Siderite | $Fe_2(CO_3)_3$ | | 70 |
| Rock salt | NaCl | 30-1013 | 10 |
| Sylvite | KCl | $10^{11} - 10^{12}$ | |
| Diamond | C | 10-1014 | |
| Serpentine | 0 | $2 \times 10^{2} - 3 \times 10^{3}$ | |
| Hornblende | | $2 \times 10^{2} - 10^{6}$ | |
| Mica | | $9 \times 10^{2} - 10^{14}$ | |
| Biotite | | $2 \times 10^{2} - 10^{6}$ | |
| Phlogopite | | 10 ¹¹ -10 ¹² | |
| Bitum. coal | | $0.6-10^{5}$ | |
| Coals (various) | | 10-1011 | |
| Anthracite | | $10^{-3}-2 \times 10^{5}$ | |
| Lignite | | 9-200 | |
| Fire clay | | / 100 | 30 |
| Meteoric waters | | 30–10 ³ | 50 |
| Surface waters | | | |
| (ign. rocks) | | $0.1-3 \times 10^{3}$ | |
| Surface waters | | 0 1 0 7 10 | |
| (sediments) | | 10-100 | |
| Soil waters | | | 100 |
| Natural waters | | | 100 |
| (ign. rocks) | | 0.5-150 | 9 |
| Natural waters | | | - |
| (sediments) | | 1-100 | 3 |
| Sea water | | | 0.2 |
| Saline waters, 3% | | | 0.15 |
| Saline waters, 20% | | | 0.05 |

The range of resistivities of various waters is notably smaller than for solid minerals; the actual resistivities are also lower than those of a great many minerals.

Table 5.3 lists resistivities for a variety of ores, from Parkhomenko (1967). In

general it appears that pyrrhotite in massive form has the lowest resistivity, that the resistivity of zinc ores is surprisingly low (possibly due to the presence of lead and copper fractions) and that molybdenite, chromite and iron ores have values in the range of many rocks.

Table 5.3. Resistivities of various ores

| Ore | Other minerals | Gangue | $\rho(\Omega m)$ |
|---------------------------------------------|---------------------------------------|---------------|-------------------------------------|
| Pyrite | | | |
| 18% | 2% (chalco) | 80% | 300 |
| 40 | 20% | 40 | 130 |
| 60 | 5% (ZnS) + 15% | 20 | 0.9 |
| 75 | 10% (ZnS) + 5% | 10 | 0.14 |
| 95 | 5% (ZnS) | 10 | 1.0 |
| 95 | $J_0(ZIIJ)$ | 5 | 7.0 |
| | | - | |
| Pyrrhotite | | 59% | 2.2×10^{-4} |
| 41% | | | |
| 58 | | 42 | 2.3×10^{-4} |
| 79 | | 21 | 1.4×10^{-5} |
| 82 | | 18 | 8.5×10^{-5} |
| 95 | | 5 | 1.4×10^{-5} |
| SbS ₂ in quartz | | | $4 \times 10^{3} - 3 \times 10^{7}$ |
| FeAsS 60% | FeS 20% | 20% SiO2 | 0.39 |
| FeAsS | | | $10^{-4} - 10^{-2}$ |
| Cu ₅ FeS ₄ | | | 3×10^{-3} |
| $Cu_5 FeS_4$ 40% | | 60% SiO2 | 7×10^{-2} |
| | | $00/_0 310_2$ | 2×10^4 |
| Fe, Mn, WO ₄ 80% | G 1 9 | | |
| Fe, Mn, WO ₄ | CoAsS | | $10^{3}-10^{7}$ |
| PbS, massive | | | 7×10^{-2} |
| PbS, near massive | | | 0.8 |
| PbS 50-80% | | | $10^{-2}-3$ |
| Fe ₂ O ₃ | | | 0.1-300 |
| Fe_2O_3 , massive | | | 2.5×10^{3} |
| | | | |
| Iron | | | 45 |
| $Fe_3O_4 60\%$ | | | $0.5 - 10^{2}$ |
| Fe_3O_4 from contact met. | | | |
| Diss. brown iron oxide | | 250/ | $8 \times 10^{2} - 3 \times 10^{6}$ |
| 75% brown iron oxide | | 25% | $2 \times 10^{4} - 8 \times 10^{5}$ |
| Fe ₂ O ₃ fine grained | | | 2.5×10^{3} |
| Fe ₃ O ₄ | | | $5 \times 10^{3} - 8 \times 10^{3}$ |
| Fe ₃ O ₄ in pegmatite | | | $7 \times 10^{3} - 2 \times 10^{5}$ |
| Zinc | | | |
| | 5% PbS, 15% FeS | 50% | 0.75 |
| 30% | $\frac{5}{0}$ rus, $\frac{15}{0}$ res | 50/0 | 20 |
| 70% | 3% chalco, 17% PbS, 10% FeS | | 20 |
| 80 | 10% PbS, 10% FeS | | 1.7×10^3 |
| 80 | 2% chalco, 1% | 15% | 1.3 |
| 00 | PbS, 2% FeS | 5% | 130 |
| 90 | 5 % PbS | 5/0 | 100 |

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| Ore | Other minerals | Gangue | $\rho(\Omega \mathbf{m})$ |
|----------------------------------|----------------|-----------|-------------------------------------|
| Graphitic slate | | | 0.13 |
| Graphite, massive | | | $10^{-4}-5 \times 10^{-3}$ |
| MoŜ ₂ | | | $2 \times 10^{2} - 4 \times 10^{3}$ |
| MnO ₂ colloidal ore | | | 1.6 |
| Cu ₂ S | | | 3×10^{-2} |
| CuFeS ₂ | | | $10^{-4} - 1$ |
| CuFeS ₂ 80% | 10% FeS | 10% | 0.66 |
| $CuFeS_2 90\%$ | 2% FeS | 8% SiO2 | 0.65 |
| FeCr ₂ O ₄ | 2 /0 1 00 | 0/0 5102 | 10^{3} |
| FeCr_2O_4 95% | | 5 % Serp. | 1.2×10^4 |

Tables 5.4 and 5.5 list typical values for rocks and unconsolidated formations. The ranges here are quite similar to water, which obviously is the controlling factor in many rocks.

| Table 5.4. | Resistivities | of igneous | and metamor | phic rocks |
|---------------|---------------|------------|-------------|------------|
| 2 00 10 01 11 | | | | |

| Rock type | Resistivity range (Ωm) | | |
|-------------------------------|------------------------------------------------------------------------|--|--|
| Granite | $3 \times 10^{2} - 10^{6}$ | | |
| Granite porphyry | 4.5×10^3 (wet)- 1.3×10^6 (dry) | | |
| Feldspar porphyry | 4×10^{3} (wet) | | |
| Albite | 3×10^{2} (wet)- 3.3×10^{3} (dry) | | |
| Syenite | $10^{2}-10^{6}$ | | |
| Diorite | $10^{4} - 10^{5}$ | | |
| Diorite porphyry | 1.9×10^3 (wet)- 2.8×10^4 (dry) | | |
| Porphyrite | $10-5 \times 10^4 \text{ (wet)} - 3 \cdot 3 \times 10^3 \text{ (dry)}$ | | |
| Carbonatized porphyry | 2.5×10^3 (wet)-6 $\times 10^4$ (dry) | | |
| Quartz porphyry | $3 \times 10^{2} - 9 \times 10^{5}$ | | |
| Quartz diorite | $2 \times 10^{4} - 2 \times 10^{6}$ (wet) -1.8×10^{5} (dry) | | |
| Porphyry (various) | 60-104 | | |
| Dacite | 2×10^4 (wet) | | |
| Andesite | 4.5×10^4 (wet) -1.7×10^2 (dry) | | |
| Diabase porphyry | 10^3 (wet)- 1.7×10^5 (dry) | | |
| Diabase (various) | $20-5 \times 10^7$ | | |
| Lavas | $10^{2}-5 \times 10^{4}$ | | |
| Gabbro | $10^{3} - 10^{6}$ | | |
| Basalt | $10-1.3 \times 10^{7} (dry)$ | | |
| Olivine norite | $10^{3}-6 \times 10^{4}$ (wet) | | |
| Peridotite | 3×10^3 (wet) -6.5×10^3 (dry) | | |
| Hornfels | 8×10^3 (wet) -6×10^7 (dry) | | |
| Schists (calcareous and mica) | 20-104 | | |
| Tuffs | 2×10^3 (wet)- 10^5 (dry) | | |
| Graphite schist | 10-102 | | |
| Slates (various) | $6 \times 10^{2} - 4 \times 10^{7}$ | | |
| Gneiss (various) | 6.8×10^4 (wet)-3 × 10 ⁶ (dry) | | |
| Marble | $10^2 - 2.5 \times 10^8 (dry)$ | | |
| Skarn | 2.5×10^2 (wet)- 2.5×10^8 (dry) | | |
| Quartzites (various) | $10-2 \times 10^{8}$ | | |

Table 5.5. Resistivities of sediments

| Rock type | Resistivity range (Ωm) | | |
|-------------------------|-----------------------------------------|--|--|
| Consolidated shales | $20-2 \times 10^{3}$ | | |
| Argillites | $10-8 \times 10^{2}$ | | |
| Conglomerates | $2 \times 10^{3} - 10^{4}$ | | |
| Sandstones | $1-6.4 \times 10^{8}$ | | |
| Limestones | 50-107 | | |
| Dolomite | 3.5×10^{2} - 5×10^{3} | | |
| Unconsolidated wet clay | 20 | | |
| Marls | 3-70 | | |
| Clays | 1-100 | | |
| Alluvium and sands | 10-800 | | |
| Oil sands | 4-800 | | |

Very roughly, igneous rocks have the highest resistivity, sediments the lowest, with metamorphic rocks intermediate. However, there is considerable overlapping, as in other physical properties. In addition, the resistivities of particular rock types vary directly with age and lithology, since the porosity of the rock and salinity of the contained water are affected by both. For example, the resistivity range of Precambrian volcanics is 200–5000 Ω m, while for Quaternary rocks of the same kind it is 10–200 Ω m.

The effect of water content on the bulk resistivity of rocks has been frequently mentioned and is evident from table 5.4. Further data are listed in table 5.6, where samples with variable amounts of water are shown. In all cases a small change in the percentage of water effects the resistivity enormously.

Table 5.6. Variation of rock resistivity with water content

| Rock | $\%~H_2O$ | $\rho(\Omega m)$ | Rock | $\% H_2O$ | $\rho(\Omega m)$ |
|-------------------|-----------|---------------------|----------------|-----------|-------------------------|
| Siltstone | 0.54 | 1.5×10^{4} | Pyrophyllite | 0.76 | 6×10^{6} |
| Siltstone | 0.44 | 8.4×10^{6} | Pyrophyllite | 0.72 | 5×10^{7} |
| Siltstone | 0.38 | 5.6×10^{8} | Pyrophyllite | 0.7 | 2×10^{8} |
| Coarse grain SS | 0.39 | 9.6×10^{5} | Pyrophyllite | 0 | 1011 |
| Coarse grain SS | 0.18 | 10 ⁸ | Granite | 0.31 | 4.4×10^{3} |
| Medium grain SS | 1.0 | 4.2×10^{3} | Granite | 0.19 | $1.8 \times 10^{\circ}$ |
| Medium grain SS | 1.67 | 3.2×10^{6} | Granite | 0.06 | 1.3×10 |
| Medium grain SS | 0.1 | 1.4×10^{8} | Granite | 0 | 1010 |
| Graywacke SS | 1.16 | 4.7×10^{3} | Diorite | 0.05 | 5.8×10 |
| Graywacke SS | 0.45 | 5.8×10^4 | Diorite | 0 | 6×10^{6} |
| Arkosic SS | 1.26 | 10 ³ | Basalt | 0.95 | 4×10^4 |
| Arkosic SS | 1.0 | 1.4×10^{3} | Basalt | 0.49 | 9×10^{5} |
| Organic limestone | 11 | 0.6×10^{3} | Basalt | 0.26 | 3×10^{7} |
| Dolomite | 2 | 5.3×10^{3} | Basalt | 0 | 1.3×10^{-3} |
| Dolomite | 1.3 | 6×10^{3} | Olivine-pyrox. | 0.028 | 2×10^4 |
| Dolomite | 0.96 | 8×10^{3} | Olivine-pyrox. | 0.014 | 4×10^{5} |
| Peridotite | 0.1 | 3×10^{3} | Olivine-pyrox. | 0 | $5 \cdot 6 \times 10$ |
| Peridotite | 0.03 | 2×10^{4} | | | |
| Peridotite | 0.016 | 10^{6} | | | |
| Peridotite | 0 | 1.8×10^{7} | | | |

Pitfalls for VLF-EM

- Recording the sign (+/-) of the numbers correctly
- Switching the facing direction or orientation during survey
- Presence of cultural features power lines, cables fences, culverts, rebar, asphalt roadways, etc.
- Unforeseen causes of anomalies eg. Permafrost contacts

| | Technique | Passive/ active | Physical property utilised | Source/signal |
|-------------------|--------------------------------------------------------------------|--------------------|---------------------------------------------------------------------|-------------------------------------------------------------------------------|
| \longrightarrow | Magnetics | Passive | Magnetic susceptibility/ remanence | Earth's magnetic field |
| | Gravity | Passive | Density | Earth's gravitational field |
| \longrightarrow | Continuous Wave and Time- Domain Electromagnetics (EM) | Active/ passive | Electrical conductivity/ resistivity | Hz/kHz band electromagnetic waves |
| | Resistivity Imaging/ Sounding | Active | Electrical resistivity | DC electric current |
| | Induced Polarisation | Active | Electrical resistivity/ complex resistivity and chargeability | Pulsed electric current |
| | Self potential (SP) | Passive | Redox and electrokinetic | Redox, streaming and diffusion potentials |
| | Seismic Refraction and Reflection/ Sonic | Active/ passive | Density/elasticity | Explosives, weight drops, vibrations, earthquakes, sonic transducers |
| > | Radiometrics | Active/ passive | Radioactivity | Natural or artificial radioactive sources |
| | Ground Penetrating Radar (GPR) | Active | Dielectric properties (permittivity) | Pulsed or stepped frequency microwave EM (50–2000 MHz) |
| | Wireline Logging | Active/ passive | Various | Various |