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Attachment D:	PAP#1 - ST#2 Flow Data
Attachment E:	PAP#1 - ST#2 Production Plot
Attachment F:	Drillstem Test Report on Well PAP #1 – ST#2 DST #2 (Fekete Associates Inc.)
Attachment G:	Geological Report for CIVC PAP #1 - ST#2 well Garden Hill Oilfield, Port au Port Peninsula, Newfoundland (Tectonics)

1. Introduction

Port au Port #1 - Sidetrack #2 (PAP#1 - ST#2) was drilled in the summer of 2002 to penetrate the Table Point and Aguathuna formations that were productive in Port au Port #1 (PAP#1). The intention of the operation was to produce oil from PAP#1 - ST#2 and “twin” the sidetrack with PAP#1.

The well was drilled on behalf of Canadian Imperial Venture Corporation (CIVC), the sole owner and operator of the property, by Simmons Drilling. The details of the drilling rig and contractor are as follows:

Rig Contractor: Simmons Group Inc.
Drilling Rig: Simmons Rig 31
Rig Type: National 8OUE

A plug was drilled through in the PAP#1 well, before drilling of the sidetrack commenced on July 29th, 2002. Once drilling had been conducted, two drillstem tests were run; the first on August 9th, 2002 (DST#1) and the second on August 11th, 2002 (DST#2).

DST#1 produced between 0.22 mmscf and 0.23 mmscf of gas per day from the Aguathuna and Table Point formations.

DST#2 penetrated the Table Point and Aguathuna formations and produced for 36 hours, averaging 195 barrels of oil per day and 1.2 mmscf of gas per day.

The rig was released on August 18th, 2002 and the well was suspended.

1.1 Map

Figure 1.1 displays the location of the PAP#1 wellsite on the Port au Port Peninsula.



Figure 1.1: PAP#1 Wellsite Location

1.2 General Information

The well, PAP#1 - ST#2, was drilled on Production Lease #2002-01. The Drilling Program Approval number was **DPA 2002-117-01** and the Authority to Drill a Well number was **ADW 2002-117-01-01**.

The well was drilled by sidetracking a well from the PAP#1 well, the surface location of which is N 5372856.003, E 335490.317.

1.3 Difficulties & Delays

Before the sidetrack was drilled, plugs set in PAP#1 were removed. Between July 13th, 2002 and July 18th, 2002, operations were temporarily suspended due to the absence of drill pipe.

On July 20th, 2002, approximately 20 m³ of well fluid was lost to the well bore (LCM).

The first bit that was used to drill the formation (July 31st, 2002) encountered problems and was removed, causing a short delay.

On August 3rd and 4th, 2002, 28.5 hours of downtime was incurred while the operators waited for cementers to arrive at the site.

2. Drilling Operations

2.1 Elevation

The rig floor elevation = 212.39 m above mean sea level.

2.2 Total Depth

The sidetrack window was cut at elevation 3345.62 m and the Total Depth was drilled to 3482 m.

2.3 Spud Date

The well was not “spudded”, as it was a sidetrack. However, sidetrack drilling operations commenced at 5:00 AM on July 30th, 2002.

2.4 Date Drilling Completed

Drilling was completed at 7:00 AM on August 11th, 2002 at a Total Depth of 3482 m.

2.5 Rig Release Date

The rig was released on August 18th, 2002 at 6:00 AM.

2.6 Well Status

The well was plugged and suspended.

2.7 Hole Sizes and Depths

See section 2.8: Bit Records.

2.8 Bit Records

The diameter of the bit used on July 30th, 2002 was 152.7 mm; from thereon the diameter of the drill bit was 156 mm. (A 158 mm bit was put in place on August 2nd, 2002 but never used). Bit performance records are summarized in Table 2.1.

Table 2.1: PAP#1 - ST#2 Bit Performance

Date	July 29/02	July 30/02	July 31/02	Aug 2/02	Aug 5/02	Aug 6/02	Aug10/02
Bit No.	Milling	1	2	3	3RR	4	4RR
Size (mm)	158.6	152.7	156	158	156	156	156
Mfg.	Baker	H.W	H.W.	H.W.	H.W.	H.W.	H.W.
Type	Mill	STX-30	STX-40	GT-1	GT-1	GT-1	STX-30
Serial#		TSXA6130	5004531	L24JC	L24JC	Y16JB	X1GJB
Nozzles		3x18	Open	Open	Open	Open	Open
From (mKB)	3346.69	3353.7	3364.9	3408	3310	3374	3465
To (mKB)	3353.69	3364.9	3408	3408	3374	3465	3482
Hrs on Bit	10	1.5	12.00	0	7.00	18.00	3.5
WOB (daN)	4/5		6/8	2/3	4/5	7/8	7/8
RPM	70		120	120	120	120	90
Flow (m ³ /min)	1.0		0.99	0.99	0.99	0.99	1.3
Pressure (kPa)	12000		16000	16000	14500	16000	9500
Condition		Centre buttons all missing					
Pulled For?		Bit		Plug back	Bit	Run DST	TD
Meters	7	11	43	0	64	91	17
m/hr	0.7	7.5	3.5	0.0	9.1	5.1	2.9
Cum Hrs	10	1.5					

2.9 Casing and Cementing Record

The PAP#1 - ST#2 sidetrack was open-hole (i.e. no casing or cementing).

2.10 Sidetracked Hole

PAP#1 - ST#2 is a sidetrack. No further sidetracks were drilled. PAP#1 - ST#1 was plugged and abandoned; ST#2 was plugged and suspended.

2.11 Drilling Fluid

Table 2.2 lists the properties of the drilling fluid used for each phase of drilling.

Table 2.2: Drilling Fluid Used During PAP#1 - ST#2 Drilling

Date	Drilling Fluid Density (kg/m ³)	pH	Chlorides	Calcium
July 29 th	1000	10	120	12
July 30 th	1050	10	200	180
July 31 st	1020	9	200	180
August 1 st -4 th	1030	11	200	180
August 5 th	1030	11	400	240
August 6 th	1030	10.5	200	400
August 7 th	1035	11	400	180
August 8 th	1030	11		
August 9 th	1030	11	500	200
August 10 th	1030	11	600	180
August 11 th	1045	10.5		

2.12 Fluid Disposal

No fluid disposal was recorded in the daily reports. However, 663.27 bbl of drilling mud and 1048.83 bbl of drill water were bunkered in the on-site tank farm which was subsequently disposed of by Crosbie Industrial Services during the site remediation program of May to August 2006.

2.13 Fishing Operations

No fishing operations were recorded.

2.14 Well Kicks

No well kicks were experienced during the drilling operations.

2.15 Formation Leak-Off Tests

A formation integrity (leak-off) test was conducted on July 30th, 2002 at a depth of 3364 m. The test was conducted at a pressure of 6000 kPa. There are no reports associated with the test.

A second leak-off test was conducted on August 1st, 2002 at a depth of 3373 m. The test was conducted at a pressure of 8800 kPa. There are no reports associated with the test.

2.16 Time Distribution

The daily reports produced (including hourly breakdown of activities) have been submitted separately (Attachment A).

2.17 Deviation Plot

<p>Client: Canadian Imperial Ventures Corp. Field: Garden Hill Structure: New Structure Well: New Well PAP #1 – ST#2 Borehole: UMI/API#: Date: July 27, 2002 Grid Convergence: -1.66708467° Scale Factor: 0.99993227</p> <p>Location: N 48 29 21.381, W 59 13 32.705 N5373075.623 m, E 335549.916 m Coordinate System: UTM Zone 21N- WGS84, Meters</p>	<p>Survey Computation Method: Minimum Curvature DLS Computation Method: Lubinski Vertical Section Azimuth: 3.000° Vertical Section Origin: N 0.000 m, E 0.000m TVD Reference: Borehole: 220.0 m above MSL Magnetic Declination: -21.826° Total Field Strength: 53645.745 n T Dip: 70.342° Declination Date: July 27, 2002 Magnetic Declination Model: BGGM 2002 North Reference: Grid North</p> <p>Coordinate Reference To: Wellhead (Grid)</p>
--	--

Comment	MD (m)	Incl (°)	Azim (°)	TVD (m)	VSec (m)	NS (m)	EW (m)	Closure (m)	CI Azim (°)	DLS (°/30m)
Tie-In	3352.00	5.3	341.8	3348.62	28.03	27.01	20.19	33.72	36.8	---
	3360.70	11.30	350.0	3357.22	29.24	28.23	19.91	34.55	35.2	21.04
	3370.20	15.40	357.8	3366.46	31.40	30.41	19.70	36.24	32.9	14.11
	3379.80	17.80	3.8	3375.66	34.14	33.15	19.75	38.59	30.8	9.21
	3389.20	18.20	4.2	3384.60	37.04	36.05	19.95	41.20	29.0	1.34
	3398.80	17.40	5.2	3393.74	39.98	38.97	20.19	43.89	27.4	2.68
	3408.50	17.40	3.0	3403.00	42.88	41.87	20.40	46.57	26.0	2.03
	3418.20	18.30	359.7	3412.23	45.85	44.84	20.47	49.29	24.5	4.19
	3427.80	19.90	358.6	3421.30	48.98	47.98	20.42	52.14	23.1	5.12
3437.00	22.00	357.5	3429.89	52.26	51.27	20.31	55.14	36.8	6.97	
Projection to Bit	3446.00	24.5	358.8	3438.16	55.80	54.82	20.20	58.42	35.2	8.51
	3467.10	32.60	3.9	3456.68	65.86	64.88	20.49	68.04	32.9	12.02

The well was conventionally drilled to TD @ 3482m – no further surveys.

2.18 Abandonment / Suspension Plugs

Two plugs were inserted in the well. A Baker 7-5/8" N-1 Bridge Plug was set at 3340 m and a Baker 9-5/8" N-1 Bridge Plug was set at 94 m.

2.19 Well Schematic

A schematic of the well is shown overleaf (Figure 2.1).

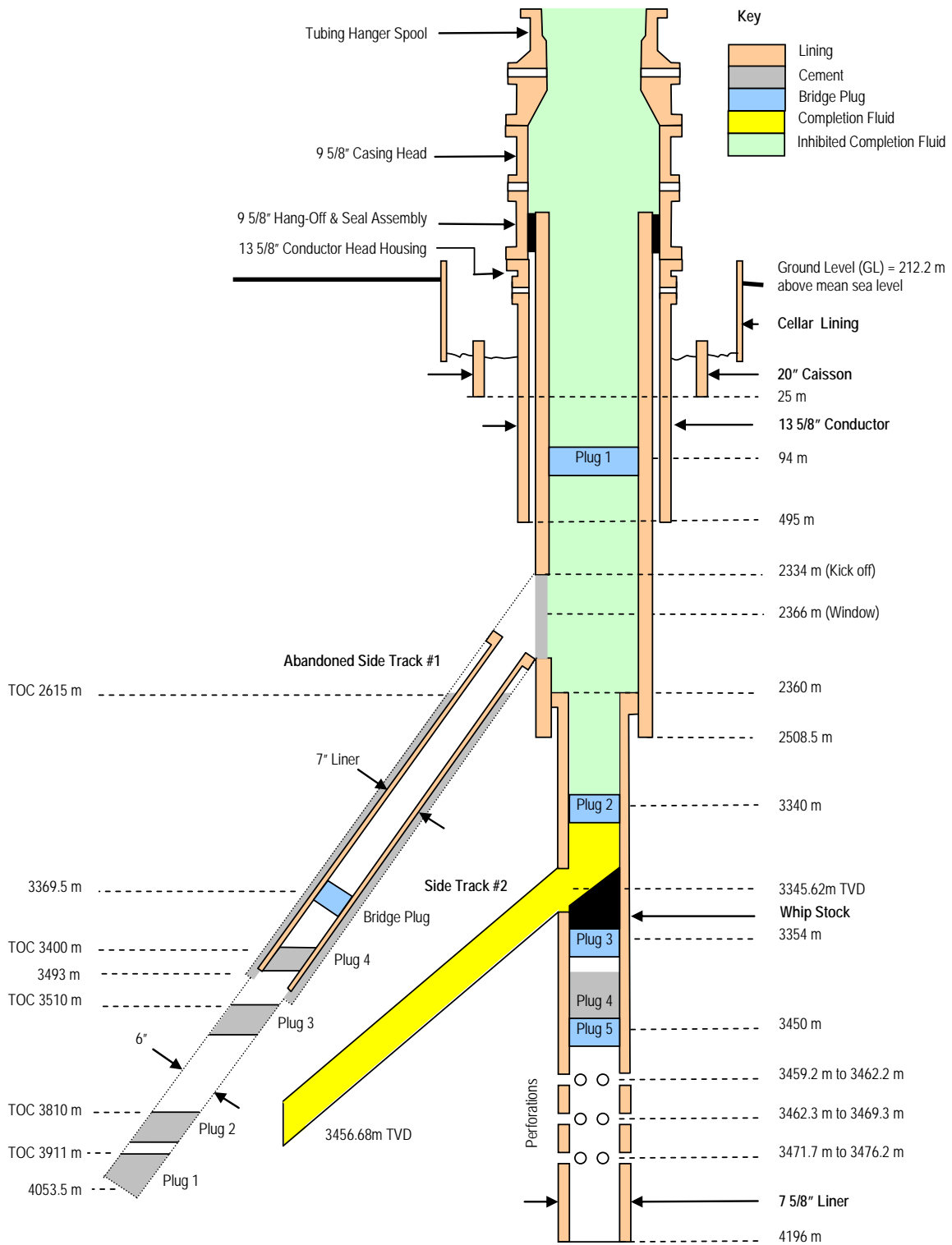


Figure 2.1: Temporary Abandonment Well Schematic for PAP#1, including PAP#1 - ST#2.

2.20 Fluid Samples

A 5.4 m³ fluid sample was taken from DST#2 on August 16th, 2002. There is no analysis of this fluid sample available.

2.21 Composite Well Record

Table 2.3 displays the composite well record.

Table 2.3: Composite Well Record for PAP#1 – ST#2

Depth	Comment	Date / Time
3346m - 3352m	152.6 mm window created for ST#2	July 28 th
3353.7m	Rate of penetration = 0.7 m/h 10 hours of drilling, 7 m drilled	July 29 th
3353.7m	Directional drilling (353° north) @ 5.64/incl Rate of penetration = 8.0 m/h 1.5 hours of drilling, 12 m drilled Hole size: 152.6 mm	July 30 th
3364.3m	Formation integrity test at 3364 m Bit changed from 152.6 mm to 165.1 mm	July 31 st
3364.9m	Directional drilling Rate of penetration = 3.5 m/h 12 hours of drilling, 43 m drilled	August 1 st
3373m	Formation leak-off test	August 1 st
3408m	Bit changed	August 2 nd
3408m - 3330m	Run kick-off cement plug	August 4 th
3310m - 3352m	Drill out cement	August 5 th
To 3352m - 3378m	Directional drilling 18 hours at 3.5 m/h 1 hour at 4 m/h	August 6 th
3374m - 3440m	Directional drilling 21.5 hours of drilling at 3.6 m/h	August 7 th
3440m - 3465m	Directional drill final 25 m 24.5 hours of drilling at 3.7 m/h	August 8 th
3465m - 3475m	Conventional drilling 2.5 hours at 4 m/h	August 10 th
3475m - 3482m	Conventional drilling 1 hour at 7 m/h	August 11 th
3340m	Baker N-1 Bridge Plug Set Pressure tested to 7000 kPa	August 16 th , 12:00 AM
94m	Baker N-1 Bridge Plug Set Pressure tested to 7000 kPa	August 17 th , 4:00 AM

3. Geology

3.1 Drill Cuttings

A full suite of cuttings was collected from 3350 m to 3480 m (see Appendix G).

Two specific sample intervals were recorded in the daily drilling reports. Samples were taken at 3354 m and 3355 m on August 5th, 2002. These samples showed 20-30% of the formation was shale. Samples were also taken on August 6th, 2002. The depth of the sample has not been recorded. The sample showed 90-95% of the formation was shale and sand.

3.2 Cores

No cores were taken during the operation.

3.3 Lithology

The following lithology log (from Attachment G) corresponds to the stratigraphic column displayed in Figure 3.1.

Table 3.1: Lithology Log Sample Descriptions, PAP#1 – ST#2

3350 m	cement (drilling out of window)
3352 m	mainly cement
3354 m	mainly cement minor shale of Goose Tickle Group
3358 m	large portion of cement Lithology: 95% shale, med-dark grey 5% sandstone, very fine grained, NVP, no shows
<i>The following samples showed regularly decreasing amounts of cement.</i>	
3360 m	95% shale a/a, non-calcareous 5% sandstone, very fine grained
3365 m	90% shale a/a 10% sandstone, a/a, highly calcareous cement
3370 m	90% shale, a/a, generally non-calcareous 10% sandstone, very fine to fine grained, generally immature, 80% quartz/20% lithic, very argillaceous in part, poorly sorted, with significant portions of chalky, calcareous matrix/cement, chips partially disaggregate when left in cold HCl.
3375 m	shale and sandstone, gen. a/a
3380 m	60% shale a/a 40% sandstone, very fine to fine grained, occasionally medium grained, mainly, quartzose, about 20% lithic fragments, well sorted, scattered poor porosity, well rounded to sub-angular grains, no shows trace siltstone grading to very fine sandstone
3385 m	70% shale, non-calcareous, grading to slightly calcareous siltstone

	<p>25% sandstone, generally a/a, very well rounded but well cemented with apparent 3-point grain junctions, trace porosity, calcareous in part</p> <p>5% limestone, white, interbedded with shale (bed boundary seen in composite grain)</p>
3390 – 3415 m	<p>90% shale, a/a</p> <p>10% sandstone a/a, speckled, salt and pepper, containing a mixture of allochems, including quartz, mica, garnet, chlorite, pyrite, and shale but no arkose</p>
3420 m	<p>80% shale a/a, slightly brown grey, non-calcareous</p> <p>20% sandstone a/a</p> <p>trace dolomitic mudstone</p> <p>trace white limestone, microcrystalline to finely crystalline</p>
3425 m	<p>90% shale a/a</p> <p>10% sandstone a/a</p>
3430 – 3435 m	<p>90% shale a/a</p> <p>10% sandstone, trace porosity, no shows minor calcite veining with light brown stain (?) and bright yellow fluorescence</p>
3440 m	<p>90% shale a/a</p> <p>10% sandstone a/a</p>
3445 m	<p>70% shale a/a</p> <p>10% sandstone a/a</p> <p>20% dolomite, brown to brown grey, crypto- to microcrystalline, faint oil stain, NVP, occasional rhombic form on edges of cuttings suggesting poor-fair (?) porosity.</p> <p>* fast drilling break at 3443 m corresponds to porosity in dolomites (see Appendix I of Attachment G)</p>
Top Table Point Formation @ 3343 m	
3450 m	<p>90% dolomite, medium to dark brown, microcrystalline, NVP, occasional dull patchy fluorescence</p> <p>10% dolomite, finely crystalline, fair to good porosity, common bitumen in pore spaces, appears to partially plug pores, occasional very dull yellow fluorescence</p> <p>trace dolomite, white, coarsely crystalline to white</p>
3453 m (bottoms up)	<p>70% dolomite, medium to dark brown, microcrystalline, mottled, NVP</p> <p>20% dolomite, brown, finely crystalline, fair intercrystalline and micro-vuggy porosity, common bitumen/dead oil residue visible in pore throats, common dull to medium yellow fluorescence. The two above lithologies are intergradational and are commonly seen on the same cutting.</p> <p>10% dolomite, white, medium to coarse grained</p> <p>N.B. By the presence of many composite</p>

	grains with microcrystalline grading to very finely or finely crystalline dolomite at the edge of the grain, it is assumed that there is a fair amount of vuggy/micro-vuggy porosity scattered in patches throughout the rock. Most of this has bitumen associated with it. Based on this the overall porosity grade of the rock may reach fair, but most of it appears to have some bitumen plugging. The presence of white sparry dolomite suggests that there may be small caverns or fracture-related voids present.
3455 m	80% dolomite, microcrystalline, a/a 10% dolomite, finely crystalline, vuggy, a/a 10% dolomite, white, sparry
3460 m	80% dolomite, tan to light brown to medium brown, very fine to finely crystalline, occasionally medium crystalline 20% tan to brown dolomite a/a, grading to medium grained euhedral rhombic crystals, inferred fair porosity, patchy bitumen residue but not as prevalent as above with many open pore throats visible. * This interval 3458 – 3465 m drilled at around 20 m/hr. while sliding with mud motor. In general, the cuttings have begun to take on a more blocky, equant appearance in this sample.
Top Aguathuna Formation @ 3458 m	
3465 m	95% dolomite, microcrystalline to finely crystalline, NVP 5% dolomite, medium grained, rhombic, blocky chips, poor inferred porosity, trace bitumen residue. trace dolomite, sucrosic, excellent porosity
3470 m	Dolomite, generally a/a (very poor sample due to abundant shale cavings – returned to rotary drilling only below 3465 m.) * drilling rate slowed to around 6 m/h in rotary drilling during this interval.
3475 m	80% dolomite, white and off-white, very fine to medium grained, occasionally coarse grained, occasionally sparry, poor to fair porosity inferred from occasional free crystal faces, no stain 20% dolomite, brown, bitumen residue (?) (cavings?) * drilling rate slowed to 3-4 m/h over this interval
3482 m TD sample	90% dolomite, white/off-white to tan to brown, occasional euhedral, rhombic dolomite with good porosity, no show, minor bitumen 10% shale/limestone interbeds (cavings?) * drilling rate slowed to 1-2 m/h over this interval.

3.4 Stratigraphic Column

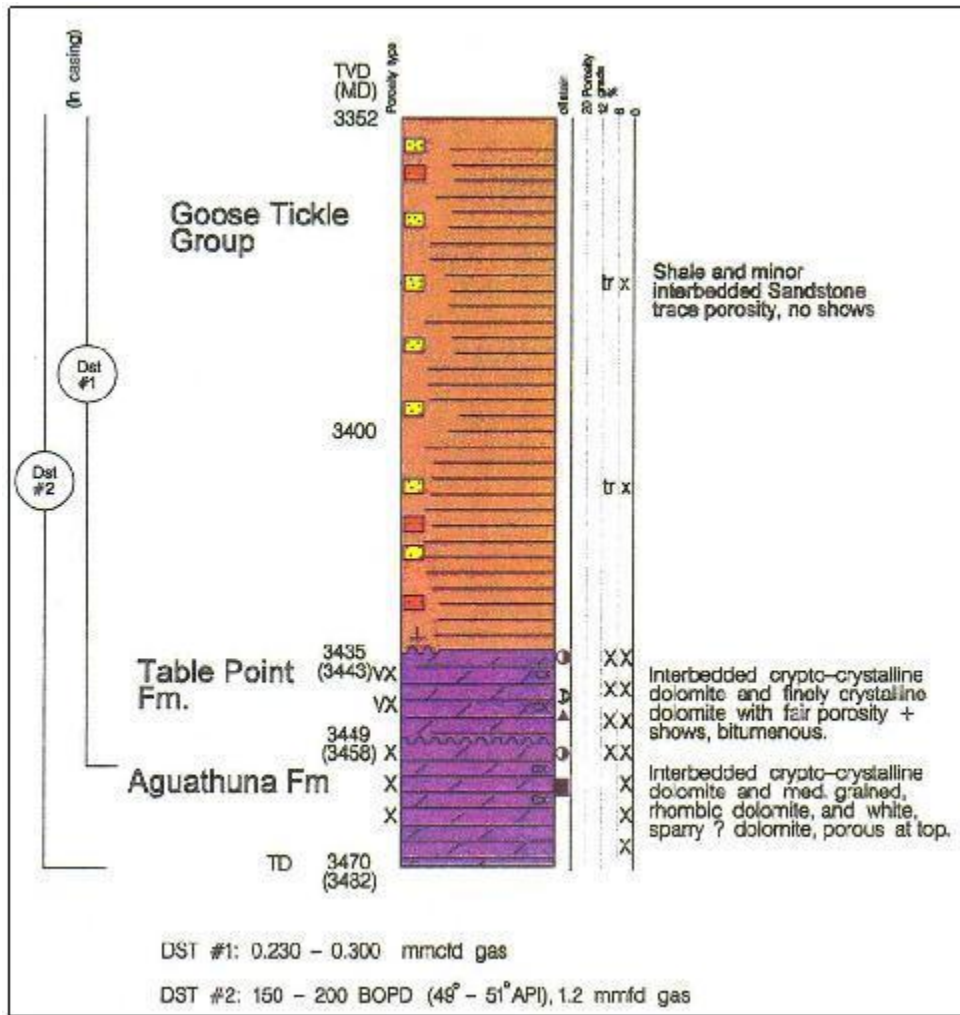


Figure 3.1: Stratigraphic Column for PAP#1 – ST#2.

3.5 Biostratigraphic Data

No biostratigraphic study was undertaken.

4. Well Evaluation

4.1 Downhole Logs

Figure 2 of Attachment G displays a portion of a real-time gamma ray log that is readily correlatable with PAP#1. In particular, the Table Point Formation is very clean and enabled prediction of the Aguathuna Formation top. It also correlated with a fast drilling break at 3443 m measured depth (MD).

Attempts to locate the entire real-time gamma ray log have been unsuccessful. This information appears to be lost.

4.2 Other Logs

Key sections of a gas log from a total gas detector set up during operations are presented in Appendix II of Attachment G.

4.3 Synthetic Seismograms

None taken.

4.4 Vertical Seismic Profiles

None taken.

4.5 Velocity Surveys

None taken.

4.6 Formation Stimulation

The formation was not stimulated.

4.7 Formation Flow Tests

Drillstem Test #1 was performed over the interval 3335-3465 m. Flow and shut-in periods of 6.8 minute flow/62.5 minute shut-in, and 56.8 minute flow/173.8 minute shut-in were performed. During the flow periods 1700.00 m of gasified mud was recovered. The test was mechanically successful. The results suggest relatively low permeability within the interval tested.

One extended (36 hour) flow test was run over part of the Table Point and Aguathuna formations (Drillstem Test #2), producing 43.1 m³ of oil and 53.3 m³ of gas. The test occurred on August 11th and 12th, 2002.

The hourly flow rate data that was taken has been submitted separately from this report. Details of the drillstem tests are included in Attachments B and C.

Attachment A: Daily Drilling Reports

Attachment B: DST#1 Port au Port (Baker Report)

Attachment C: DST#2 ST#2 Port au Port (Baker Report)

Attachment D: PAP#1 - ST#2 Flow Data

Attachment E: PAP#1 - ST#2 Production Plot

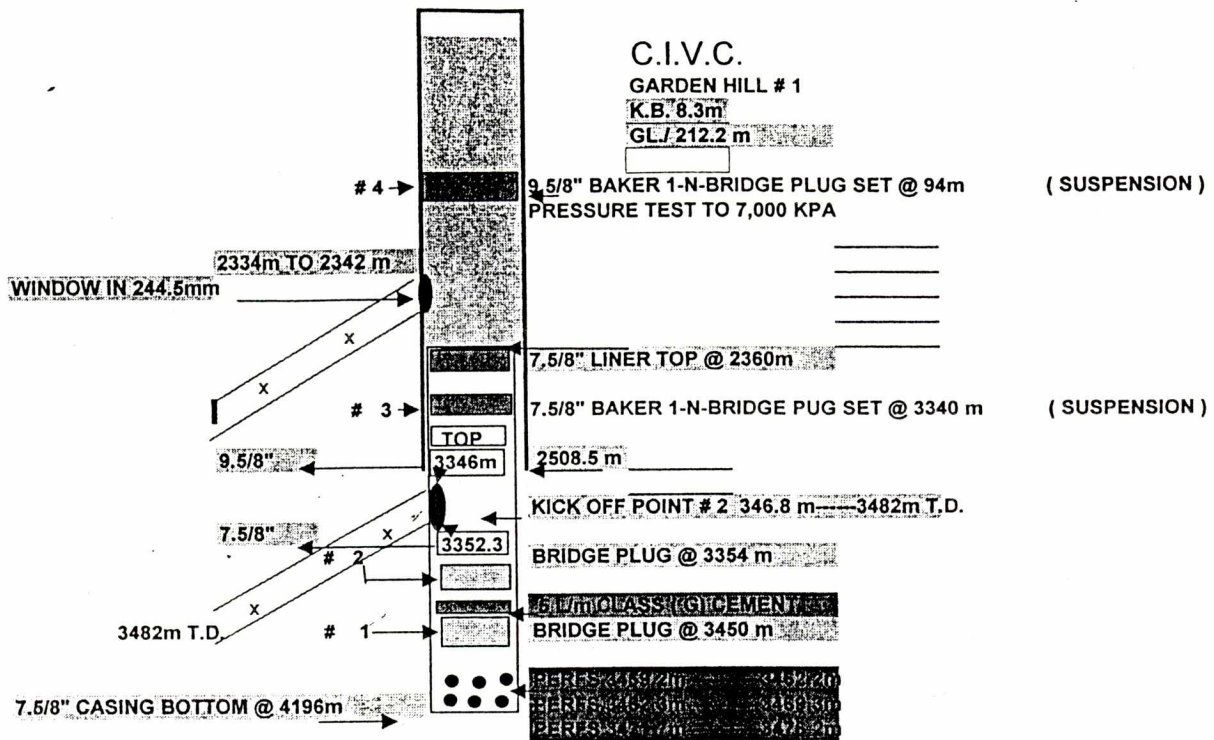
**Attachment F: Drillstem Test
Report on Well PAP #1 – ST#2 DST
#2 (Fekete Associates Inc.)**

**Attachment G: Geological Report
for CIVC PAP #1 - ST#2 well
Garden Hill Oilfield, Port au Port
Peninsula, Newfoundland
(Tectonics Inc.)**

Attachment A: Daily Drilling Reports

CANADIAN IMPERIAL VENTURE CORP. <small>IMPERIAL ENERGY SERVICES CORPORATION</small> <small>WELL DRILLING REPORT</small> <small>Garden Hill</small>		Well : garden hill ST # 2		Rig : Simmon's 31		Date : AUGS,18/002		Days Since Spud:		Report N°: 145														
		Current depth: P.B.94 m		Phase: since:		Casing size: 244.5/194		Shoe: PBTD: 94 m		F.I.T. at shoe: 8,800														
1 PENETRATION				2 BITS				DULL				3 PARAMETERS												
Type Oper.	RUN N°	DEPTH Start	OPERATION Mtrs Hours	R.O.P. m/h	CUMUL Mtrs Hours	Diameter	BIT Maker	BIT Type	IADC Code	Serial N°	Jets or TFA	CUT. STRUCT.				OTHERS				WOB daN	RPM	Flow l/min	Pres. kPa	
												I	O	D	L	B	G	O	R					
4 DRILL STRING ASSEMBLY										5 DOWN HOLE TOOLS				6 DEVIATION SURVEYS				7 MUD						
										Diam. + Type Hrs Cum.				Type N° Depth Inc. Az.				TYPE: Gel / Chem						
																		Mixed (m3) Dumped (m3) Form. Losses (m3) Surf. Losses (m3)						
																		Solids (%) Oil (%) Water (%) O/W ratio Filtrate API Filtrate HP/HT						
8 OPERATIONS & TIME ANALYSIS:										9 REMARKS														
FROM	TO	HOURS	CODE	DESCRIPTION						Conduct daily walk around inspection. Conduct safety meetings with rig crews discuss general operations. LOAD OUT SWACO TANK P.V.T.AND FLOOR CONTROLS AND CHIEMO REMOTE CHOKE AND CONTROL BIG -D RENTALS 88.9 mm HANDLING TOOLS BIG-D 50 JOINTS 88.9 mm H.W.DRILL PIPE BIG-D 15 JOINTS 88.9 mm DRILL PIPE ON D & D TRUCKING DATA-LOG EQUIPMENT SENT TO HALIFAX ON BAKER TESTER TRUCK														
6:00	18:00	12:00	D	LAY DOWN BOP,S CLEAN MUD TANKS																				
18:00	24:00	6:00	D	LAY DOWN BOP,S CLEAN MUD TANKS																				
24:00	6:00	6:00	D	LAY DOWN BOP,S CLEAN MUD TANKS INSTALL WELL HEAD DRAIN CASING DOWN 2m BELOW GROUND																				
										RIG RELEASED 08/18/002/@ 6:00 HRS.														
11 SUMMARY OF OPERATIONS										12 BASIC				10 PRODUCTS				15 PERSONNEL						
										To				Unit				Company:						
										From Formation Rock Type				In (+) / Used (-) Stock				Drilling Contractors:						
														Barite SXS				Service Contractors:						
														Bentonite SXS										
														Soda Ash SXS										
														Sapp SXS										
														Kwik Seal F SXS										
														Potassium Chlorid SXS										
														Lignite SXS										
														DeFoam X SXS										
														Poly Plus RD SXS										
														Sawdust SXS										
														Caustic Soda SXS										
														Poly Pac UL SXS										
														Lignosulphonate SXS										
														Bicarb SXS										
														Cellophane SXS										
														Mica-F SXS										
														Drilling detergent SXS										
														Kalzan SXS										
														DD 2000 Pails										
13 WELL STATUS at 06:00										14 FREIGHT ARRIVAL & DEPARTURE				15 PERSONNEL										
RIG RELEASED										HAULER FREIGHT Arrival Depart. Destination				Company:										
														Drilling Contractors:										
														Service Contractors:										
16 OPERATIONS PLANNED										19 WEA1 WIND				20 COMPANY REP.										
WELL SUSPENDED										Spe Time of Survey: 6:00 Temp: 12 deg Visibility:				TOTAL:										
										12 Knt Direction: W Barometer (Mb):				Stan Stafford										
17 SAFETY					18 COSTS																			
DRILLS:					DAILY:																			
DAYS SINCE LAST LTA: 342					CUMULATIVE: 0.0% of AFE																			

CANADIAN IMPERIAL VENTURE CORP.										Well : garden hill ST # 2		Rig : Simmon's 31		Date : AUGS,17/002		Days Since Spud:		Report N°: 144											
Current depth: P/B/3340 m										Phase: since:		Casing size: 244.5/194		Shoe: 3340 m		F.I.T. at shoe: 8,800													
Bottom hole: PBTD: 3340 m																													
1 PENETRATION										2 BITS										3 PARAMETERS									
Type Oper.	RUN N°	DEPTH Start	OPERATION Mtrs	HOURS	R.O.P. m/h	CUMUL Mtrs	HOURS	Diameter	BIT Maker	BIT Type	IADC Code	Serial N°	Jets or TFA	DULL				CUT. STRUCT.				OTHERS				WOB daN	RPM	Flow l/min	Pres. kPa
														I	O	D	L	B	G	O	R								
4 DRILL STRING ASSEMBLY										5 DOWN HOLE TOOLS					6 DEVIATION SURVEYS					7 MUD									
										Diam. + Type Hrs Cum.					Type N° Depth Inc. Az.					TYPE: Gel / Chem									
																				Mixed (m3) Den 1000 Dumped (m3) YP Form. Losses (m3) PV Surf. Losses (m3) Gel10s Solids (%) Gel10m Oil (%) Fun Vis Water (%) F/L Temp O/W ratio pH Filtrate API Fluid loss Filtrate HP/HT Chlorides Calcium									
8 OPERATIONS & TIME ANALYSIS:										9 REMARKS										10 PRODUCTS									
FROM	TO	HOURS	CODE	DESCRIPTION						REMARKS										Unit	In (+) / Used (-)	Stock							
6:00	7:30	1.50	D	TRIP OUT WITH BAKER RUNING TOOL						Conduct daily walk around inspection.										SXS									
7:30	8:00	0.50	D	LAY DOWN RUNING TOOL						Conduct safety meetings with rig crews discuss general operations.										SXS									
8:00	8:30	0.50	D	RIG SERVICE FUNCTION BLIND RAMS						FUNCTION BLIND RAMS										SXS									
8:30	13:00	4.50	D	RUN IN OPEN ENDED						FUNCTION PIPE RAMS										SXS									
13:00	14:00	1.00	D	CLEAN SUCTION TANK						INJURY INCIDENT TO SIMMONS WORKER/ NO LOST TIME										SXS									
14:00	16:00	2.00	D	REV,CIRCULATE CASING OVER TO INHIBITED WATER						TAKING SHORT CUT NOT USING WALKWAY/ ROLLED ANLIKLE ON ROCK										SXS									
16:00	24:00	8.00	D	LAY DOWN 127 mm DRILL PIPE AND 88.9 mm DRILL PIPE						DISPACE CASING TO INHIBITED WATER/ 130 m/3										SXS									
24:00	4:00	4.00	D	LAY DOWN 88.9 mm DRILL PIPE						60/L KD-40 CORROSION INHIBITOR										SXS									
4:00	6:00	2.00	D	RUN 244.5 mm BAKER BRIDGE PLUG SET @ 94 m (PRESSURE TEST 7,000 KPA OK.)						X-CIDE 102 W BACTERICIDE 1/2 BBL. SODIUM SUFLFATE ANHYDROUS 5 SX										SXS									
										SET BAKER 244.5 mm N-BRIDGE PLUG @ 94 m PRESSURE TEST TO 7,000 KPA OK.										SXS									
11 SUMMARY OF OPERATIONS										12 BASIC To										14 FREIGHT ARRIVAL & DEPARTURE					15 PERSONNEL				
WELL SUSPENED WITH (2) BAKER N-BRIDGE PLUGS										From Formation Rock Type										HAULER FREIGHT Arrival Depart. Destination					Company: 3 Drilling Contractors: 16 Service Contractors: 2				
13 WELL STATUS at 06:00										16 OPERATIONS PLANNED										19 WEAT WIND Spe Time of Survey: 6:00 Temp: 14 deg Visibility: Barometer (Mb):					TOTAL: 21				
LAY DOWN KELLY AND 88.9 mm PIPE										RIG OUT BOPS IN STALL WELL HEAD										Direction: S/W					20 COMPANY REP. Stan Stafford				
17 SAFETY										18 COSTS																			
DRILLS: DAYS SINCE LAST LTA.										DAILY: CUMULATIVE: 341 0.0% of AFE																			



- # 1 BRIDGE PLUG SET ON DRILL PIPE 07 / 25 / 002
 PRESSURE TEST TO 13,500 KPA OK.
- # 2 BRIDGE PLUG SET ON DRILL PIPE 07 / 27002
 ANCHOR FOR WHIP STOCK KICK OFF
- # 3 BRIDGE PLUG SET ON DRILL PIPE 08 / 16002
- # 4 BRIDGE PLUG SET ON DRILL PIPE 08 / 17. 002
- # 3 PRESSURE TESTED TO 7,000 KPA OK.
- # 4 PRESSURE TESTED TO 7,000 KPA OK.

STAN.STAFFORD

CANADIAN IMPERIAL VENTURE CORP.										Well : garden hill ST # 2		Rig : Simmon's 31		Date : AUGS,16/002		Days Since Spud:		Report N°: 143										
										Current depth: 3482m		Phase: since:		Casing size: 244.5/194		Shoe: PBDT: 3354		F.L.T. at shoe: 8,800										
1 PENETRATION								2 BITS					DULL					3 PARAMETERS										
Type	RUN N°	DEPTH Start	OPERATION Mtrs	Hours	R.O.P. m/h	CUMUL Mtrs	Hours	Diameter	BIT Maker	BIT Type	IADC Code	Serial N°	Jets or TFA	CUT. STRUCT.				OTHERS				WOB daN	RPM	Flow l/min	Pres. kPa			
Oper.														I	O	D	L	B	G	O	R							
4 DRILL STRING ASSEMBLY													5 DOWN HOLE TOOLS			6 DEVIATION SURVEYS					7 MUD							
													Diam. + Type Hrs Cum. .			Type N° Depth Inc. Az.					TYPE: Gel / Chem							
																					Mixed (m3) Den 1060 Dumped (m3) YP Form. Losses (m3) PV Surf. Losses (m3) Gel10s Solids (%) Gel10m Oil (%) Fun Vis 46 Water (%) F/L Temp O/W ratio pH 11 Filtrate API Fluid loss 10 Filtrate HP/HT Chlorides Calcium							
8 OPERATIONS & TIME ANALYSIS:													9 REMARKS											10 PRODUCTS				
FROM	TO	HOURS	CODE	DESCRIPTION																				Unit	In (+) / Used (-)	Stock		
6:00	12:00	6:00	D	TRIP OUT WITH D.S.T.# 2									Conduct daily walk around inspection.											SXS				
12:00	13:30	1:50	D	TRIP OUT WITH D.S.T.# 2									Conduct safety meetings with rig crews discuss general operations.											SXS				
13:30	15:30	2:00	D	LAY DOWN D.S.T. TOOLS									FUNCTION BLIND RAMS											SXS				
15:30	16:00	0:50	D	MAKE UP 7.5/8" BRIDGE PLUG RUN 88 9mm H.W PIPE									FUNCTION PIPERAMS											SXS				
16:00	17:00	1:00	D	RUN IN WITH BRIDGE PLUG									RELEASED MARITIME TESTERS @ 18:00 HRS.											SXS				
17:00	18:00	1:00	D	SLIP AND CUT DRILLING LINE									FLUID SAMPLE FROM D.S.T.# 2: 5.4 m ³ VERY LIGHT OIL											SXS				
18:00	24:00	5:50	D	RUN IN WITH 7.7/8" BIRDGE PLUG									400 SX PULPRO ON SITE @ 16:00 HRS.											SXS				
24:00	1:30	1:50	D	SET 7.5/8" BRIDGE PLUG @ 3340 m (PRESSURE TEST TO 7,000 KPA)									SWACO TANK P.V.T.QUIT WORKING, UNABLE TO REPAIR ON SITE											SXS				
1:00	6:00	5:00	D	TRIP OUT WITH RUNNING TOOL (WET PIPE)									RUN BAKER 7.5/8: 1-N BIRDGE PLUG SET @ 3340 m PRESSURE TEST BRIDGE PLUG TO 7,000 KPA SURFACE PRESSURE WITH DRILLING MUD OK.SET ON 08/16/002/@ 130 am PORTS IN RUNING TOOL PLUGGED/ TRIP OUT WITH WET: TRIP											SXS				
													12 BASIC To								Lignosulphonate SXS Bicarb SXS Cellophane SXS Mica-F SXS Drilling detergent SXS Kalzan SXS DD 2000 SXS							
													From Formation Rock Type															
11 SUMMARY OF OPERATIONS													14 FREIGHT ARRIVAL & DEPARTURE											15 PERSONNEL				
TO RUN SUSPENSION BIRDGE PLUG													HAULER				FREIGHT				Arrival Depart. Destination				Company: 3 Drilling Contractors: 16 Service Contractors: 1			
13 WELL STATUS at 06:00																								TOTAL: 20				
TRIP OUT WITH RUNNING TOOL																								20 COMPANY REP. Stan Stafford				
16 OPERATIONS PLANNED													19 WEAT WIND Spe Time of Survey: 6:00 Temp: 15 deg Visibility: 14 Knt Direction: S/W Barometer (Mb):															
TO RUN SUSPENSION BIRDGE PLUG																												
17 SAFETY						18 COSTS																						
DRILLS:						DAILY:																						
DAYS SINCE LAST LTA: 340						CUMULATIVE: 0.0% of AFE																						

CANADIAN IMPERIAL VENTURE CORP.				Well: garden hill ST # 2		Rig: Simmon's 31		Date: AUGS,14/002		Days Since Spud:		Report N°: 141																	
Current depth: 3482 m				Phase: since:				Casing size: 244.5/194		Shoe: 3354		F.I.T. at shoe: 8,800																	
1 PENETRATION				2 BITS				3 DULL				3 PARAMETERS																	
Type Oper.	RUN N°	DEPTH Start	OPERATION Mtrs Hours	R.O.P. m/h	CUMUL Mtrs Hours	Diameter	BIT Maker	BIT Type	IADC Code	Serial N°	Jets or TFA	CUT. STRUCT.				OTHERS				WOB daN	RPM	Flow l/min	Pres. kPa						
												I	O	D	L	B	G	O	R										
4 DRILL STRING ASSEMBLY						5 DOWN HOLE TOOLS						6 DEVIATION SURVEYS						7 MUD											
						Diam. + Type Hrs Cum.						Type N° Depth Inc. Az.						TYPE: Gel / Chem											
																		Mixed (m3) Dumped (m3) Form. Losses (m3) Surf. Losses (m3) Solids (%) Oil (%) Water (%) O/W ratio Filtrate API Filtrate HP/HT						Den YP PV Gel10s Gel10m Fun Vis F/L Temp pH Fluid loss Chlorides Calcium					
8 OPERATIONS & TIME ANALYSIS:												9 REMARKS																	
FROM	TO	HOURS	CODE	DESCRIPTION								Conduct daily walk around inspection. Conduct safety meetings with rig crews discuss general operations. RELEASE M.I.SWACO MUD MAN.																	
6.00	6.00	24.00	D	WELL SHUT IN ON FINAL SHUT IN																									
												10 PRODUCTS																	
												Unit In (+) / Used (-) Stock																	
												Barite Bentonite Soda Ash Sapp Kwik Seal F Potassium Chlorid Lignite DeFoam X Poly Plus RD Sawdust Caustic Soda Poly Pac UL Lignosulphonate Bicarb Cellophane Mica-F Drilling detergent Kalzan DD 2000																	
11 SUMMARY OF OPERATIONS												12 BASIC																	
48 HR, SHUT IN ON D.S.T.												To Formation Rock Type																	
13 WELL STATUS at 06:00												14 FREIGHT ARRIVAL & DEPARTURE																	
WELL SHUT ON 48 HR/SHUT IN												HAULER FREIGHT Arrival Depart. Destination																	
16 OPERATIONS PLANNED												15 PERSONNEL																	
PULL D.S.T. RUN BAKER I-N BRIDGE PLUGS												Company: 3 Drilling Contractors: 16 Service Contractors: 3																	
												TOTAL: 22																	
17 SAFETY												18 COSTS																	
DRILLS: DAYS SINCE LAST LTA: 338												DAILY: CUMULATIVE: 0.0% of AFE																	
												19 WEAT WIND Spe Time of Survey: 6:00 Temp: 14 deg Visibility: 5 Knt Direction: W Barometer (Mb):																	
												20 COMPANY REP. Stan Stafford																	

CANADIAN IMPERIAL VENTURE CORP.										Well: garden hill ST # 2		Rig: Simmon's 31		Date: AUGS.13/002		Days Since Spud:		Report N°: 140						
INSBORO DRILLING CORP. Garden Hill										Current depth: 3482 m		Phase: since:		Casing size: Bottom hole:		Shoe: PBT.D: 3354		F.I.T. at shoe: 8,800						
1 PENETRATION										2 BITS					3 PARAMETERS									
Type Oper.	RUN N°	DEPTH Start	OPERATION Mtrs	HOURS	R.O.P. m/h	CUMUL Mtrs	HOURS	Diameter	BIT Maker	BIT Type	IADC Code	Serial N°	Jets or TFA	DULL				WOB daN		RPM	Flow l/min	Pres. kPa		
														I	O	D	L	B	G	O	R			
4 DRILL STRING ASSEMBLY										5 DOWN HOLE TOOLS			6 DEVIATION SURVEYS					7 MUD						
										Diam. + Type Hrs Cum.			Type N° Depth Inc. Az.					TYPE: Gel / Chem						
																		Mixed (m3) Den 1030 Dumped (m3) YP Form. Losses (m3) PV Surf. Losses (m3) Gel10s Solids (%) Gel10m Oil (%) Fun Vis 46 Water (%) F/L Temp O/W ratio pH 10 Filtrate API Fluid loss 10 Filtrate HP/HT Chlorides Calcium						
8 OPERATIONS & TIME ANALYSIS:										9 REMARKS														
FROM	TO	HOURS	CODE	DESCRIPTION						Conduct daily walk around inspection. Conduct safety meetings with rig crews discuss general operations. FUNCTION REMOTE CHOKE														
6:00	6:00	12:00	D	FLOW WELL THROUGH PRODUCTION SEPERATOR ON FLOW # 3																				
6:00	6:30	0:50	D	FLOW WELL THROUGH PRODUCTION SEPERATOR ON FLOW # 3																				
6:30	6:00	11:50	D	WELL SHUT IN ON 48 HR, SHUT IN (FINAL)																				
										12 BASIC To			10 PRODUCTS					Unit In (+) / Used (-) Stock						
										From Formation Rock Type			Barite SXS Bentonite SXS Soda Ash SXS Sapp SXS Kwik Seal F SXS Potassium Chlorid SXS Lignite SXS DeFoam X SXS Poly Plus RD SXS Sawdust SXS Caustic Soda SXS Poly Pac UL SXS Lignosulphonate SXS Bicarb SXS Cellophane SXS Mica-F SXS Drilling detergent SXS Kalzan SXS DD 2000 Pails											
11 SUMMARY OF OPERATIONS										14 FREIGHT ARRIVAL & DEPARTURE														
RUN D.S.T TO EVALUATE FORMATION										HAULER			FREIGHT		Arrival	Depart.	Destination		15 PERSONNEL					
13 WELL STATUS at 06:00										WELL ON 48-HR. SHUT IN (final)														
16 OPERATIONS PLANNED										FINISH SHUT IN TRIP OUT WITH D.S.T. TOOLS														
17 SAFETY										18 COSTS														
DRILLS: DAYS SINCE LAST LTA. 337										DAILY: CUMULATIVE: 0.0% of AFE														
										19 WEAT WIND Spe Time of Survey: 6:00 Temp: 10 deg Visibility: 11 Knt Direction: S/E Barometer (Mb):					TOTAL: 21									
										20 COMPANY REP. Stan Stafford														

CANADIAN IMPERIAL VENTURE CORP. <small>CONSTRUCTION DRILLING REPORT</small> Garden Hill	Well : garden hill ST # 2	Rig : Simmon's 31	Date : AUG12./002	Days Since Spud:	Report N°: 139
	Current depth: 3482 m T.D.	Phase: since:	Casing size: 244.5/194	Shoe: 3354	F.I.T. at shoe: 8,800

1 PENETRATION				2 BITS				DULL				3 PARAMETERS													
Type Oper.	RUN N°	DEPTH Start	OPERATION Mtrs Hours	R.O.P. m/h	CUMUL. Mtrs	Hours	Diameter	BIT Maker	BIT Type	IADC Code	Serial N°	Jets or TFA	CUT. STRUCT.				OTHERS				WOB daN	RPM	Flow l/min	Pres. kPa	
													I	O	D	L	B	G	O	R					

4 DRILL STRING ASSEMBLY				5 DOWN HOLE TOOLS			6 DEVIATION SURVEYS			7 MUD				
				Diam. + Type	Hrs	Cum.	Type	N°	Depth	Inc.	Az.	TYPE: Gel / Chem		
												Mixed (m3)	Den	1045
												Dumped (m3)	YP	3.5
												Form. Losses (m3)	PV	1.2
												Surf. Losses (m3)	Gel10s	

8 OPERATIONS & TIME ANALYSIS:				9 REMARKS											
FROM	TO	HOURS	CODE	DESCRIPTION											
6.00	6.00	24.00	D	RUN D.S.T. # 2 RUN FLOW # 1 # 2 # 3 FOR D.S.T FLOW REPORT SEE PRODUCTION (FLOW REPORT) FAX											
				Conduct daily walk around inspection. Conduct safety meetings with rig crews discuss general operations. RUN D.S.T. # 2 TO EVALUATE FORMATTION											
				10 PRODUCTS											
					Unit	In (+) / Used (-)	Stock	Lignosulphonate					SXS		
								Bicarb					SXS		
								Cellophane					SXS		
								Mica-F					SXS		
								Drilling detergent					SXS		
								Kalzan					SXS		
								DD 2000					Pails		

11 SUMMARY OF OPERATIONS				14 FREIGHT ARRIVAL & DEPARTURE				15 PERSONNEL				
DRILL TO T.D. RUN D.S.T. TO EVALUATE FORMATION				HAULER	FREIGHT	Arrival	Depart.	Destination	Company:	3		
13 WELL STATUS at 06:00									Drilling Contractors:	16		
RUN D.S.T.									Service Contractors:	4		

16 OPERATIONS PLANNED				19 WEAT WIND				TOTAL:				
FLOW WELL TO EVALUATE FORMATION				Spe Time of Survey:	6.00	Temp:	13 deg	Visibility:	23			
				15 Knt	Direction:	S/W	Barometer (Mb):					

17 SAFETY		18 COSTS		20 COMPANY REP.	
DRILLS:	BOP DRILL	DAILY:		Stan Stafford	
DAYS SINCE LAST LTA:	326	CUMULATIVE:	0.0% of AFE		

CANADIAN IMPERIAL VENTURE CORP.										Well : garden hill ST # 2		Rig : Simmon's 31		Date : AUG.11/002		Days Since Spud:		Report N°: 138									
										Current depth: 3482 T.D.		Phase:		Casing size: 244.5/194		Shoe:		F.I.T. at shoe:									
												since:		Bottom hole:		PBTD: 3354		8,800									
1 PENETRATION										2 BITS				DULL				3 PARAMETERS									
Type Oper.	RUN N°	DEPTH Start	OPERATION Mtrs	HOURS	R.O.P. m/h	CUMUL Mtrs	HOURS	Diameter	BIT Maker	BIT Type	IADC Code	Serial N°	Jets or TFA	CUT. STRUCT.				OTHERS				WOB daN	RPM	Flow l/min	Pres. kPa		
DRILL	RR # 4	3465	16	5.50	2.9	17	25.00	156	H.W.	STX-30	537	X1GJB	000	I	O	D	L	B	G	O	R	7/8	90	1.3	95.00		
4 DRILL STRING ASSEMBLY										5 DOWN HOLE TOOLS				6 DEVIATION SURVEYS				7 MUD									
										Diam. + Type Hrs Cum.				Type N° Depth Inc. Az.				TYPE: Gel / Chem									
																		Mixed (m3) Dumped (m3) Form. Losses (m3) Surf. Losses (m3) Solids (%) Oil (%) Water (%) O/W ratio Filtrate API Filtrate HP/HT				Den 1045 YP PV Gel10s Gel10m Fun Vis 46 F/L Temp pH 10.5 Fluid loss Chlorides Calcium					
8 OPERATIONS & TIME ANALYSIS:										9 REMARKS																	
FROM	TO	HOURS	CODE	DESCRIPTION						Conduct daily walk around inspection. Conduct safety meetings with rig crews discuss general operations.																	
6:00	7:00	1:00	D	DRILL 156 mm HOLE (3475 m--- 3482 m						FUNCTION BLIND RAMS FUNCTION REMOTE CHOKE																	
7:00	8:30	1:50	D	CIRCULATE BOTTOMS UP						REMARKS																	
8:30	9:00	0:50	D	BOP/DRILL						ON TRIP OUT TO RUN D.S.T.# 2																	
9:00	10:30	1:50	D	TRIP WORK TIGHT HOLE @ 3450 m AND @ 3346m WINDOW						TIGHT HOLE @ 3450 m PUMP OUT 2 SINGLES																	
10:30	11:00	0:50	D	RIG SERVICE, FUNCTION TEST ANNULAR PREVENTER						WORK THROUGH WINDOW TIGHT SPOT																	
11:00	12:30	1:50	D	CIRCULATE CONDITION HOLE						RUN IN CIRCULATE CONDITION HOLE																	
12:30	17:30	5:00	D	TRIP OUT TO PICK UP D.S.T TOOLS						TRIP OUT NO HOLE PROBLEMS																	
17:30	19:00	1:50	D	MAKE UP D.S.T # 2						12 BASIC To																	
19:00	24:00	5:00	D	RUN IN WITH D.S.T # 2						From Formation Rock Type																	
24:00	2:00	2:00	D	RUN IN WITH D.S.T # 2																							
2:00	6:00	4:00	D	RUN D.S.T # 2																							
										10 PRODUCTS																	
										Unit In (+) / Used (-) Stock																	
										Barite SXs Bentonite SXs +15 Soda Ash SXs Sapp SXs Kwik Seal F SXs Potassium Chlorid SXs Lignite SXs DeFoam X SXs Poly Plus RD SXs Sawdust SXs Caustic Soda SXs Poly Pac UL SXs Lignosulphonate SXs Bicarb SXs Cellophane SXs Mica-F SXs Drilling detergent SXs Kalzan SXs DD 2000 Pails																	
11 SUMMARY OF OPERATIONS										14 FREIGHT ARRIVAL & DEPARTURE																	
DRILL TO T.D. RUN D.S.T. TO EVALUATE FORMATOIN										HAULER				FREIGHT				Arrival		Depart.		Destination		15 PERSONNEL			
13 WELL STATUS at 06:00										Company: 4																	
RUN D.S.T # 2										Drilling Contractors: 16																	
16 OPERATIONS PLANNED										Service Contractors: 4																	
RUN D.S.T.# 2 EVALUATE										TOTAL: 24																	
17 SAFETY										19 WEAT WIND Spc Time of Survey: 6:00 Temp: 8 deg Visibility: 2000m																	
DRILLS:										13 Knt				Direction: E				Barometer (Mb):				20 COMPANY REP.					
DAYS SINCE LAST LTA. 326										Stan Stafford																	
18 COSTS										0.0% of AFE																	
DAILY:																											
CUMULATIVE:																											



Well: garden hill ST # 2 Rig: Simmon's 31 Date: AUG./10/002 Days Since Spud: Report N°: 137
 Current depth: 3481 Phase: since: Casing size: 244.5/194 Shoe: Bottom hole: PBTD: 3354 F.I.T. at shoe: 8,800

1 PENETRATION						2 BITS						3 PARAMETERS												
Type	RUN N°	DEPTH Start	OPERATION Mtrs	R.O.P. Hours	CUMUL. Hours	Diameter	BIT Maker	BIT Type	IADC Code	Serial N°	Jets or TFA	DULL CUT. STRUCT.				OTHERS				WOB daN	RPM	Flow U/min	Pres. kPa	
DRILL	RR # 4	3465	16	5.50	2.9	25.00	156	H.W.	STX-30	537	X1GJB	OOO	I	O	D	L	B	G	O	R	7/8	90	1.3	95.00

4 DRILL STRING ASSEMBLY						5 DOWN HOLE TOOLS			6 DEVIATION SURVEYS					7 MUD			
156mm BIT/ BIT/SUB, 50/ 88.9mm H.W. 78/88.9mm DRILL PIPE 127mm DRILL PIPE						Diam. + Type	Hrs	Cum.	Type	N°	Depth	Inc.	Az.	TYPE:		Gel / Chem	

8 OPERATIONS & TIME ANALYSIS:					9 REMARKS	10 PRODUCTS				
FROM	TO	HOURS	CODE	DESCRIPTION	Conduct daily walk around inspection. Conduct safety meetings with rig crews discuss general operations. FUNCTION TEST BLIND RAMS FUNCTION TEST HYDRIL FUNCTION TEST REMOTE CHOKE		Unit	In (+) / Used (-)	Stock	
6:00	10:30	4.50	D	TRIP OUT WITH D.S.T TOOL # 1		Conduct daily walk around inspection. Conduct safety meetings with rig crews discuss general operations. FUNCTION TEST BLIND RAMS FUNCTION TEST HYDRIL FUNCTION TEST REMOTE CHOKE	Mixed (m3)	SXS		Den 1045
10:30	11:00	0.50	D	RIG SERVICE FUNCTION BLIND RAMS			Dumped (m3)	SXS		YP 3
11:00	14:30	3.50	D	HANDLE TEST TOOLS READ RECORDERS			Form. Losses (m3)	SXS		PV 17
14:30	15:00	0.50	D	MAKE UP BIT AND B.H.A			Surf. Losses (m3)	SXS		Gel10s 3
15:00	16:00	1.00	D	SLIP AND CUT DRILLING LINE			Solids (%)	SXS		Gel10m
16:00	21:00	5.00	D	RUN IN WITH BIT			Oil (%)	SXS		Fun Vis 44
21:00	22:00	1.00	D	DRILL 156 mm HOLE (3465 m-----3470 m)			Water (%)	SXS		F/L Temp
22:00	22:30	1.50	D	CIRCULATE UP SAMPLE			O/W ratio	SXS		pH 11
22:30	24:00	0.50	D	DRILL 156 mm HOLE (3470 m -----3471 m)			Filtrate API	SXS		Fluid loss 9
24:00	1:00	1.00	D	DRILL 156 mm HOLE (3471 m-----3475 m)			Filtrate HP/HT	SXS		Chlorides 600
1:00	2:30	1.50	D	CIRCULATE UP SAMPLE				SXS		Calcium 180
2:30	3:00	0.50	D	W O O				SXS		
3:00	6:00	3.00	D	DRILL AHEAD				SXS		

11 SUMMARY OF OPERATIONS
 DRILL TO T.D. RUN D.S.T. TO EVALUATE FORMATOIN

13 WELL STATUS at 06:00				14 FREIGHT ARRIVAL & DEPARTURE				15 PERSONNEL	
DRILL AHEAD WITH 156 mm BIT				HAULER	FREIGHT	Arrival	Depart.	Destination	Company:

16 OPERATIONS PLANNED				17 SAFETY				18 COSTS		19 WEA1 WIND		20 COMPANY REP.				
DRILL TO 3482 m RUN D.S.T.				DRILLS:	DAYS SINCE LAST LTA:	325	DAILY:	CUMULATIVE:	0.0% of AFE	Spe Time of Survey:	6:00	Temp:	12 deg	Visibility:	TOTAL:	Stan Stafford



Well: **garden hill ST # 2** Rig: **Simmon's 31** Date: **AUG.9/002** Days Since Spud: Report No: **136**
 Current depth: **3465 m** Phase: since: Casing size: **244.5/194** Shoe: F.I.T. at shoe: **8,800**
 Bottom hole: **PBTD: 3354**

1 PENETRATION							2 BITS							3 PARAMETERS										
Type	RUN N°	DEPTH	OPERATION		R.O.P.	CUMUL	Diameter	BIT Maker	BIT Type	IADC Code	Serial N°	Jets or TFA	DULL CUT. STRUCT.				OTHERS			WOB	RPM	Flow	Pres.	
Oper.		Start	Mtrs	Hours	m/h	Mtrs	Hours						I	O	D	L	B	G	O	R	daN		l/min	kPa

4 DRILL STRING ASSEMBLY							5 DOWN HOLE TOOLS			6 DEVIATION SURVEYS				7 MUD				
D.S.T.STRING 120 mm							Diam. + Type	Hrs	Cum.	Type	N°	Depth	Inc.	Az.	TYPE: Gel / Chem			

8 OPERATIONS & TIME ANALYSIS:					9 REMARKS	10 PRODUCTS			
FROM	TO	HOURS	CODE	DESCRIPTION	Conduct daily walk around inspection. Conduct safety meetings with rig crews discuss general operations. D.S.T. # 1 FORMATION TABLE TOP/AGUATHUNA 3465 m— 3336 m 5:45 10/MIN P.F. N.G.T.S 5:55 60 MIN S/IN 7:00 V OPEN G.T.S. ON V.OPEN G.T.S. 7:12 250 KPA/ MAX. 7:17 220 KPA 7:20 200 KPA 7:30 60 KPA 7:32 15 KPA GAS RATE 220—230 M.C.F.D. 2/BBLs WATER @ 110,000 P.P.M.,NO MUD TO SURFACE	Unit	In (+) / Used (-)	Stock	
6:00	8:30	2.50	D	MAKE UP D.S.T.TOOL # 1		Mixed (m3)	Den	1030	
8:30	9:00	0.50	D	RIG SERVICE SET UP BREAKS		Dumped (m3)	YP	12	
9:00	15:30	6.50	D	RUN IN WITH D.S.T. # 1		Form. Losses (m3)	PV	1	
15:30	21:00	5.50	D	RUN D.S.T.# 1		Surf. Losses (m3)	Gel10s		
21:00	24:00	3.00	D	UNSET PACKER DROP BAR TRY SHESR PUMP OUT PIN UNABLE TO		Solids (%)	Gel10m		
24:00	1:00	1:00	D	SHEAR PUMP OUT PRESSURE PIN REVERSE CIRCULATE OUT D S T FLUID		Oil (%)	Fun Vis		
1:00	3:30	2.50	D	CIRCULATE TO CONTROL GAS CUT DRILLING MUD		Water (%)	F/L Temp		
3:30	6:00	2.50	D	TRIP OUT WITH D.S.T. TOOLS		O/W ratio	pH	11	
						Filtrate API	Fluid loss	11	
					Filtrate HP/HT	Chlorides	500		
						Calcium	200		

11 SUMMARY OF OPERATIONS					12 BASIC To		14 FREIGHT ARRIVAL & DEPARTURE				15 PERSONNEL				
DIRECTION DRILL TO T.D. RUN D.S.T. FOR EVALUATE FORMATOIN					From	To	Formation	Rock Type	Hauler	Freight	Arrival	Depart.	Destination	Company:	2

13 WELL STATUS at 06:00					TRIP OUT WITH D.S.T.TOOLS						Drilling Contractors: 16	
16 OPERATIONS PLANNED					RUN BOTTOM HOLE D.S.T.						Service Contractors: 4	

17 SAFETY					18 COSTS		19 WEA1 WIND Spe Time of Survey: 6:00 Temp: 11 deg Visibility: 8 Knt Direction: E Barometer (Mb):				TOTAL: 22	
DRILLS: DAYS SINCE LAST LTA: 324					DAILY: CUMULATIVE: 0.0% of AFE						20 COMPANY REP. Stan Stafford	



GREEN HILL
DRILLING & MINING

Well : garden hill ST # 2 Rig : Simmon's 31 Date : AUG.6/002 Days Since Spud: Report N°: 133
 Current depth: 3378m Phase: since: Casing size: 244.5/194 Shoe: F.I.T. at shoe: 8,800
 Bottom hole: PBTD: 3354

1 PENETRATION							2 BITS				3 DULL										3 PARAMETERS				
Type Oper.	RUN N°	DEPTH Start	OPERATION Mtrs	Hours	R.O.P. m/h	CUMUL Mtrs	Hours	Diameter	BIT Maker	BIT Type	IADC Code	Serial N°	Jets or TFA	CUT. STRUCT.				OTHERS				WOB daN	RPM	Flow l/min	Pres. kPa
														I	O	D	L	B	G	O	R				
3-RR	3	3352m	64	18.00	3.5	64	18.00	156mm	H.W.	GT-1		L24-JC	OPEN	2	5	1						4/5	120	.99	14,500
DI/R	4	3374	4	1.00	4.0																	4/5	120	.99	15,000

4 DRILL STRING ASSEMBLY										5 DOWN HOLE TOOLS			6 DEVIATION SURVEYS				7 MUD					
156.7mm BIT MUD MOTOR 2/ MONNELS COLLARS, 3/ 88.9mm H.W. 120mm JARS, 47 88.9mm DRILL PIPE 127mm DRILL PIPE 1 83 DEGRESS										Diam. + Type	Hrs	Cum.	Type	N°	Depth	Inc.	Az.	TYPE:		Gel / Chem		
													D/D	3	3360.8	11.3	351.5	Mixed (m3)	Den	1030		
																		Dumped (m3)	YP	5		
																		Form. Losses (m3)	PV	10		
																		Surf. Losses (m3)	Gel10s			
																		Solids (%)	Gel10m			
																		Oil (%)	Fun Vis	44		
																		Water (%)	F/L Temp			
																		O/W ratio	pH	10.5		
																		Filtrate API	Fluid loss	11		
																		Filtrate HP/FT	Chlorides	200		
																			Calcium	400		

8 OPERATIONS & TIME ANALYSIS:					9 REMARKS									
FROM	TO	HOURS	CODE	DESCRIPTION	Conduct daily walk around inspection. Conduct safety meetings with rig crews discuss general operations. TRIP FOR BIT @ 3374 m DIRECTION DRILL TO 3374 m WITH THOOOTH BIT RR-# 3 DIRECTION SURVEY @ 3360.8 m 11.8 DEGRESS 15 m FROM BIT AZIm 351.5 SAMPLES SHOW 90-95% SHALE AND SAND FUNCTION BLIND RAMS FUNCTION PIPE RAMS									
6:00	9:30	3.50	D	TIME DRILL CATCH SAMPLES (2m)										
9:30	12:00	2.50	D	DIRECTION DRILL AHEAD WITH 1000 KPA/ DIFF.										
12:00	15:00	4.00	D	DIRECTION DRILL AHEAD WITH 1000 KPA/ DIFF.										
15:00	22:00	6.00	D	TRIP OUT WITH BIT FLOW CHECK @ 3213m @ 1740 m @ 1215 m										
22:00	22:30	0.50	D	CHANGE BIT SERVICE M.W.D.										
22:30	24:00	1.50	D	RUN IN WITH BIT # 4 TO 1215 M										
24:00	1:00	1.00	D	SLIP AND CUT DRILLING LINE										
1:00	4:00	3.00	D	RUN IN WITH BIT # 4 TO 1215 M										
4:00	5:00	1.00	D	RUN CHECK SURVEY										
5:00	6:00	1.00	D	DIRECTION DRILL AHEAD WITH 1000 KPA/ DIFF.										

11 SUMMARY OF OPERATIONS					12 BASIC To									
From	Formation	Rock Type												
24:00														

13 WELL STATUS at 06:00					14 FREIGHT ARRIVAL & DEPARTURE										15 PERSONNEL		
DIRECTION DRILL AHEAD					HAULER	FREIGHT	Arrival	Depart.	Destination	Company: 2							
										Drilling Contractors: 16							
										Service Contractors: 3							

16 OPERATIONS PLANNED					17 SAFETY										18 COSTS			19 WEA1 WIND			20 COMPANY REP.							
DIRECTION DRILL TO T.D / TRIP OUT FOR D.S.T.					DRILLS:					DAILY:					CUMULATIVE:					Spt Time of Survey: 6.00			Temp: 8 deg			Visibility: 3000		
					DAYS SINCE LAST LTA: 321					0.0% of AFE					6 Knt			Direction: S/W			Barometer (Mb):			TOTAL: 21				
																					Stan Stafford							



Well: **garden hill ST # 2** Rig: **Simmon's 31** Date: **AUG.4/002** Days Since Spud: Report No: **131**

Current depth: **3408 m** Phase: since: Casing size: **244.5/194** Shoe: Bottom hole: **PBTD: 3354** F.I.T. at shoe: **8,800**

1 PENETRATION						2 BITS						3 PARAMETERS											
Type Oper.	RUN N°	DEPTH Start	OPERATION Mtrs	R.O.P. Hours	CUMUL Mtrs	Diameter	BIT Maker	BIT Type	IADC Code	Serial N°	Jets or TFA	DULL CUT. STRUCT.				OTHERS				WOB daN	RPM	Flow l/min	Pres. kPa
												I O D L				B G O R							

4 DRILL STRING ASSEMBLY						5 DOWN HOLE TOOLS			6 DEVIATION SURVEYS				7 MUD				
						Diam. + Type	Hrs	Cum.	Type	N°	Depth	Inc.	Az.	TYPE: Gel / Chem			

8 OPERATIONS & TIME ANALYSIS:					9 REMARKS	10 PRODUCTS						
FROM	TO	HOURS	CODE	DESCRIPTION	Conduct daily walk around inspection. Conduct safety meetings with rig crews discuss general operations. FUNCTION 127mm PIPE RAMS RAN KICK OFF CEMENT PLUG FROM 3408 m—3330 m WITH 11 TONNES (CLASS G) CEMENT+ 10/L TONNE D80 2/L TONNE D801 AT 2100 KG/m ³ DISPLACE WITH 18.9 m ³ DRILLING MUD PLUG INPLACE AT 17:00 HRS. PULL UP TO 3330m RIG AND BACK WASH WITH RIG PUMP WHEN DISPLACING HIT PRESSURE SPIKE @ 18.9 m ³ AWAY BLEED PRESSURE OF PULL UP TO 3330 m AND BACK WASH ON BOTTOMS UP 3-4 m ³ CEMENT RETURNS					Unit	In (+) / Used (-)	Stock
6:00	13:00	7.00	D	WAIT ON CEMENTERS		CEMENT SAMPLES SET UP VEARY HARD RUN IN CHECK FOR KICK OFF CEMENT PLUG TOP PLUG TOP @ 3310 m WITH 10/DAN.08/04/002/ @ 7:20 AM.					SXS	
13:00	15:30	2.50	D	RIG UP SCLUMBERGER CMENTERS HOLD SAFETY MEETING						SXS		
15:30	17:00	1.50	D	RUN KICK OFF CEMENT PLUG						SXS		
17:00	17:30	0.50	D	PULL UP TO 3330 m						SXS		
17:30	18:00	0.50	D	REV,CIRCULATE OUT CEMENT (3--4 m ³						SXS		
18:00	19:00	1.00	D	PULL TO 3025 m CIRCULATE CIRCULATE CONDITION MUD						SXS		
19:00	6:00	11.00	D	CIRCULATE W.O.C. KICK OFF PLUG						SXS		
		24.00									SXS	

11 SUMMARY OF OPERATIONS					12 BASIC To				14 FREIGHT ARRIVAL & DEPARTURE				15 PERSONNEL				
DIRECTION DRILL OFF KICK OF PLUG					From	Formation	Rock Type		HAULER	FREIGHT	Arrival	Depart.	Destination		Company:		

13 WELL STATUS at 06:00					16 OPERATIONS PLANNED				19 WEAT WIND				20 COMPANY REP.					
W.O.C. KICK OFF PLUG					RUN IN CHECK PLUG TOP				HAULER	FREIGHT	Arrival	Depart.	Destination		TOTAL:		Stan Stafford	

17 SAFETY					18 COSTS					19 WEAT WIND					20 COMPANY REP.				
DRILLS: SAFETY MEETING CEMENTING DAYS SINCE LAST LTA: 319					DAILY: CUMULATIVE: 0.0% of AFE					Spe Time of Survey: 6.00 Temp: 11 deg Visibility: 16 Knt Direction: E Barometer (Mb):					TOTAL: 21 Stan Stafford				



Well: **garden hill ST # 2** Rig: **Simmon's 31** Date: **AUG./3/002** Days Since Spud: Report No: **130**

Current depth: **3408 m** Phase: since: Casing size: **244.5/194** Shoe: Bottom hole: **PBTD: 3354** F.I.T. at shoe: **8,800**

1 PENETRATION				2 BITS				DULL				3 PARAMETERS												
Type	RUN No	DEPTH Start	OPERATION Mtrs Hours	R.O.P. m/h	CUMUL Mtrs	Hours	Diameter	BIT Maker	BIT Type	IADC Code	Serial No	Jets or TFA	CUT. STRUCT.				OTHERS				WOB daN	RPM	Flow U/min	Pres. kPa
Oper.													I	O	D	L	B	G	O	R				

4 DRILL STRING ASSEMBLY				5 DOWN HOLE TOOLS			6 DEVIATION SURVEYS				7 MUD						
				Diam. + Type	Hrs	Cum.	Type	No	Depth	Inc.	Az.	TYPE: Gel / Chem					
												Mixed (m3)				Den	1030
												Dumped (m3)				YP	
												Form. Losses (m3)				PV	
												Surf. Losses (m3)				Gel10s	
												Solids (%)				Gel10m	
												Oil (%)				Fun Vis	42
												Water (%)				F/L Temp	
												O/W ratio				pH	
												Filtrate API				Fluid loss	14
												Filtrate HP/HT				Chlorides	
																Calcium	

8 OPERATIONS & TIME ANALYSIS:				9 REMARKS				
FROM	TO	HOURS	CODE	DESCRIPTION				
6:00	8:30	2.50	D	RUN IN HOLE OPEN END	Conduct daily walk around inspection. Conduct safety meetings with rig crews discuss general operations. FUNCTION PIPE RAMS FUNCTION REMOTE CHOKE FUNCTION HYDRIL MAKE 4/WIPER TRIPS			
8:30	12:00	3.50	D	CIRCULATE WAIT ON CEMENTERS				
12:00	24:00	12.00	D	CIRCULATE WAIT ON CEMENTERS				
24:00	6:00	6.00	D	CIRCULATE WAIT ON CEMENTERS				
		24.00						

11 SUMMARY OF OPERATIONS				12 BASIC			
TO RUN PLUG BACK PLUG TO CORRECTE DIRECTION HOLE PROBLEMS				From	Formation	Rock Type	To

13 WELL STATUS at 06:00				14 FREIGHT ARRIVAL & DEPARTURE				15 PERSONNEL				
CIRCULATE WAIT ON CEMENTERS				HAULER	FREIGHT	Arrival	Depart.	Destination	Company:	2		
									Drilling Contractors:	16		
									Service Contractors:	1		

16 OPERATIONS PLANNED				17 SAFETY				18 COSTS				19 WEA1 WIND				20 COMPANY REP.					
RUN PLUG BACK CEMENT PLUG @ 3408 m				DRILLS:	DAYS SINCE LAST LTA:	318	DAILY:	CUMULATIVE:	0.0% of AFE	Spe Time of Survey:	6.00	Temp:	10 deg	Visibility:	Barometer (Mb):	TOTAL:	19	Stan Stafford			
									9 Knt												



Well : garden hill ST # 2 Rig : Simmon's 31 Date : AUG 2/002 Days Since Spud: Report N°: 129
 Current depth: 3408 Phase: since: Casing size: 244.5/194 Shoe: F.I.T. at shoe: 8,800
 Bottom hole: PBTD: 3354m

1 PENETRATION				2 BITS				3 PARAMETERS																										
Type Oper.	RUN N°	DEPTH Start	OPERATION Mtrs Hours	R.O.P. m/h	CUMUL Mtrs Hours	Diameter	BIT Maker	BIT Type	IADC Code	Serial N°	Jets or TFA	DULL					CUT. STRUCT.					OTHERS					WOB daN	RPM	Flow l/min	Pres. kPa				
DR/D	RR-3	3408	0 0.00	0.0	0 0.00	158mm	H.W	GT-1		L24JC	0.000	I	O	D	L	B	G	O	R															

4 DRILL STRING ASSEMBLY										5 DOWN HOLE TOOLS			6 DEVIATION SURVEYS					7 MUD				
156mm BIT MOTOR SUB, 2 MONNELS, 3 H.W., JARS, 47 H.W., 76 88 9mm DRILL PIPE, X/O SUB, 127 mm DRILL PIPE										Diam. + Type	Hrs	Cum.	Type	N°	Depth	Inc.	Az.	TYPE: Gel / Chem				

8 OPERATIONS & TIME ANALYSIS:				9 REMARKS										10 PRODUCTS				
FROM	TO	HOURS	CODE	DESCRIPTION										In (+) / Used (-) Stock				
6:00	12:00	6:00	D	RUN IN WITH BIT # 3 AND DIRECTION TOOLS										Mixed (m3)	Den	1030		
12:00	13:30	1:30	D	RUN IN WITH BIT # 3 AND DIRECTION TOOLS										Dumped (m3)	YP			
13:30	14:00	0:50	D	BREAK CIRCULATION (ORIENT TOLL)										Form. Losses (m3)	PV			
14:00	17:00	3:00	D	TIME DRILL TRY TO START NEW HOLE (KEEP SLIDING)										Surf. Losses (m3)	Gel 10s			
17:00	23:30	6:50	D	TRIP OUT WITH BIT # 3 AND DIRECTION TOOLS										Solids (%)	Gel 10m			
23:30	24:00	0:50	D	RIG SERVICE FUNCTION BLIND RAMS										Oil (%)	Fun Vis	50		
24:00	1:00	1:00	D	LAY DOWN DIRECTION TOOLS										Water (%)	F/L Temp			
1:00	3:30	2:50	D	RUN IN OPEN ENDED DRILL PIPE										O/W ratio	pH	11		
3:30	4:30	1:00	D	SLIP AND CUT DRILLING LINE										Filtrate API	Fluid loss	14		
4:30	6:00	1:50	D	RUN IN OPEN ENDED DRILL PIPE										Filtrate HP/HT	Chlorides	200		
				FUNCTION BLIND RAMS FUNCTION PIPE RRAMS										Calcium		180		
				12 BASIC To														
				From Formation					Rock Type									

11 SUMMARY OF OPERATIONS										14 FREIGHT ARRIVAL & DEPARTURE					15 PERSONNEL				
										HAULER	FREIGHT	Arrival	Depart.	Destination	Company:				

13 WELL STATUS at 06:00															Drilling Contractors: 16				
RUN IN OPEN ENDED WITH DRILL PIPE															Service Contractors: 0				

16 OPERATIONS PLANNED										17 WEAT WIND					TOTAL:				
CIRCULATE WAIT ON CEMENTERS RUN PLUG BACK CEMENT PLUG										Spe	Time of Survey:	6:00	Temp:	7 deg	Visibility:				

17 SAFETY					18 COSTS					20 COMPANY REP.									
DRILLS:					DAILY:					8 Knt					Direction: N				
DAYS SINCE LAST LTA: 317					CUMULATIVE: 0.0% of AFE					Barometer (Mb):					Stan Stafford				



ONSHORE OIL & GAS DRILLING REPORT
Garden Hill

Well: garden hill ST # 2 Rig: Simmon's 31 Date: AUGS,1/002 Days Since Spud: Report N°: 128
 Current depth: 3408m Phase: Casing size: 244.5/194 Shoe: F.I.T. at shoe:
 since: Bottom hole: PBTD: 3354m 8,800 Kpa

1 PENETRATION										2 BITS					DULL										3 PARAMETERS			
Type	RUN N°	DEPTH Start	OPERATION		R.O.P. m/h	CUMUL		Diameter	BIT Maker	BIT Type	IADC Code	Serial N°	Jets or TFA	CUT. STRUCT.					OTHERS					WOB daN	RPM	Flow l/min	Pres. kPa	
DR/D	2	3364.9	Mtrs	Hours	3.5	Mtrs	Hours	156mm	H.W.	STX40	617	5004531	0.000	I	O	D	L	B	G	O	R	6/8	120	.99	16,000			

4 DRILL STRING ASSEMBLY										5 DOWN HOLE TOOLS			6 DEVIATION SURVEYS					7 MUD			
156mm BIT MOTOR SUB, 2 MONNELS, 3 H W., JARS, 47 H W., 76 88 9mm DRILL PIPE, X/O SUB, 127 mm DRILL PIPE										Diam. + Type	Hrs	Cum.	Type	N°	Depth	Inc.	Az.	TYPE:		Gel / Chem	
										120mm/ JARS	13.50	13.50	DR	1	3352	5.3	341.8	Mixed (m3)	Den	1030	
																		Dumped (m3)	YP	3	
																		Form. Losses (m3)	PV	15	
																		Surf. Losses (m3)	Gel10s	62"	
																		Solids (%)	Gel10m		
																		Oil (%)	Fun Vis	30	
																		Water (%)	F/L Temp	14	
																		O/W ratio	pH	11	
																		Filtrate API	Fluid loss	14	
																		Filtrate HP/HT	Chlorides	200	
																			Calcium	180	

8 OPERATIONS & TIME ANALYSIS:					9 REMARKS										10 PRODUCTS			
FROM	TO	HOURS	CODE	DESCRIPTION	Conduct daily walk around inspection. Conduct safety meetings with rig crews discuss general operations. RUN LEAK OFF TEST TO FORMATION @ 3373 m (8,800 KPA) FUNCTION TEST 127 mm PIPE RAMS TIME DRILL FROM 3406 m TO TRY TO MOVE BIT AWAY FROM CASING OUT IN TO FORMATION TRIP OUT TO CHANGE BIT AND SET BENTHOSE TO 1.83 DECESS DIRECTION HOLE SLIDING DOWN A LONG SIDE 7.5/8" CASING SAMPLES RUNNING 80-90 % CEMENT SENDING OUT BKER ATLAS WIRE LINE UNIT TO DAY										Unit	In (+) / Used (-)	Stock	
6:00	7:00	1.00	D	REAM FROM 3354m---3364m											Barite	SXS		
7:00	7:30	0.50	D	RIG SERVICE FUNCTION H C R VAVLVE											Bentonite	SXS		
7:30	9:00	1.50	D	DRILL FROM 3367m---3375.5m											Soda Ash	SXS		
9:00	9:30	0.50	D	CIRCULATE HOLE TO RUN LEAK OFF TEST											Sapp	SXS	+11	9
9:30	10:00	0.50	D	RUN FORMATION LEAK OFF TEST @ 3373 m (8,800 KPA OK.											Kwik Seal F	SXS		
10:00	11:00	1.00	D	DRILL FROM 3373.5m---3383.2 m											Potassium Chlorid	SXS		
11:00	12:00	1.00	D	DIRECTION SURVEYS											Lignite	SXS		
12:00	17:00	5.00	D	DRILL FROM 3383m---3406m											DeFoam X	SXS		
17:00	21:30	4.50	D	TIME DRILL TRY TO KICK DIRECTION HOLE OUT											Poly Plus RD	SXS		
21:30	23:00	1.50	D	CIRCULATE BOTTOMS UP											Sawdust	SXS		
23:00	24:00	1.00	D	TRIP OUT WITH DIRECTION TOOLS AND BIT # 2											Caustic Soda	SXS		
24:00	5:00	5.00	D	TRIP OUT WITH DIRECTION TOOLS AND BIT # 2											Poly Pac UL	SXS		
5:00	6:00	1.00	D	CHANGE BIT SET BENTHOSE TO 1.83 DECESS											Lignosulphonate	SXS		
															Bicarb	SXS		
															Cellophane	SXS		
															Mica-F	SXS		
															Drilling detergent	SXS		
															Kalzan	SXS		
															DD 2000	Pails		

11 SUMMARY OF OPERATIONS					12 BASIC To										14 FREIGHT ARRIVAL & DEPARTURE				15 PERSONNEL			
DIRECTION DRILL TO T.D. RUN OPEN HOLE D.S.T.					From	Formation	Rock Type	HAULER	FREIGHT	Arrival	Depart.	Destination	Company:									
												Drilling Contractors:	16									
												Service Contractors:	5									

13 WELL STATUS at 06:00					16 OPERATIONS PLANNED										19 WEATWIND				TOTAL:			
RUN IN WITH THOOH BIT AND DIRECTION TOOLS					RUN IN WITH THOOH BIT AND 1.83 DEGREE BENTHOSE TRY TO STEER HOLE AWAY F/CSG.										Spe	Time of Survey:	Temp:	7 deg	Visibility:			
															9 Knt	6.00	Direction:	N	Barometer (Mb):			
															20 COMPANY REP.							

17 SAFETY					18 COSTS										TOTAL:			
DRILLS:					DAILY:					CUMULATIVE:					24			
DAYS SINCE LAST LTA: 316										0.0% of AFE					Stan Stafford			



Well: **garden hill ST # 2** Rig: **Simmon's 31** Date: **JULY 30/002** Days Since Spud: **127**
 Report N°: **127**
 Current depth: **3353.7m** Phase: since: Casing size: **244.5/194** Shoe: **PBTD: 3354**
 Bottom hole: F.I.T. at shoe:

1 PENETRATION								2 BITS					DULL								3 PARAMETERS				
Type	RUN N°	DEPTH Start	OPERATION Mtrs	R.O.P. Hours	CUMUL Mtrs	Hours	Diameter	BIT Maker	BIT Type	IADC Code	Serial N°	Jets or TFA	CUT. STRUCT.				OTHERS				WOB daN	RPM	Flow l/min	Pres. kPa	
DRLG	1	3353.7	12	1.50	8.0	12	1.50	152.7m	H.W.	STX-30	537	TSXA6130	3X18	I	O	D	L	B	G	O	R				

4 DRILL STRING ASSEMBLY										5 DOWN HOLE TOOLS				6 DEVIATION SURVEYS					7 MUD				
1 152.7mm BIT MOTOR SUB, 2 MONNELS, 3 H.W., JARS, 47 H.W., 76 88 9mm DRILL PIPE, X/O SUB, 127 mm DRILL PIPE										Diam. + Type		Hrs	Cum.	Type	N°	Depth	Inc.	Az.	TYPE: Gel / Chem				
										121mm	JARS			DIRC						Mixed (m3)	Den	1050	
										121mm	MOTOR										Dumped (m3)	YP	7.5
																		Form. Losses (m3)	PV	20			
																		Surf. Losses (m3)	Gel10s				

8 OPERATIONS & TIME ANALYSIS:										9 REMARKS										10 PRODUCTS						
FROM	TO	HOURS	CODE	DESCRIPTION																In (+) / Used (-)		Stock				
6:00	6:30	0.50	D	MILL 152.6mm WINDOW						Conduct daily walk around inspection.																
6:30	8:00	1.50	D	CIRCULATE AND REAM WINDOW						Conduct safety meetings with rig crews discuss general operations.																
8:00	9:30	1.50	D	CIRCULATE BOTTOMS UP						FINISH MILLING THROUGH 7.5/8" CASING AT 6:30 AM																
9:30	15:00	5.50	D	TRIP OUT WITH WHIP STOCK MILL						REAM 152.6 mm WINDOW WITH 156.5 mm TOP STRING HOLE OPENER																
15:00	15:30	0.50	D	LAY DOWN MILLING TOOLS						FUNCTION BLIND RAMS FUNCTION 127 mm PIPE RAMS																
15:30	16:30	1.00	D	SLIP ANS CUT DRLG LINE						ON TRIP IN WITH DIRECTION TOOLS/ TIGHT SPOT @ 2870 m TO 280 m																
16:30	17:00	0.50	D	RIG SERVICE/ FUNCTION BLIND RAMS						KELLY UP CIRCULATE AND WORK THROUGH TIGHT SPOT																
17:00	19:00	2.00	D	MAKE UP DIRECTION TOOLS (FUNCTION TEST M W D.						WORK THROUGH TIGHT SPOT @ 3190 m @ 3334 m																
19:00	21:30	2.50	D	RUN IN WITH DIRECTION TOOLS						BENTHOSE SET @ 1.83/ DEGREES																
21:30	22:00	0.50	D	LAY DOWN 12 JOINTS 127 mm PIPE						PROBLEMS RUNNING IN HOLE WITH 1.83/ DEGREES																
22:00	22:30	0.50	D	FILL DRILL PIPE FUNCTION M W D.						FORMATION LEAK OFF TEST 6,000 KPA @ 3364 m																
22:30	024.00	1.50	D	RUN IN WITH 127 mm DRILL PIPE						12 BASIC G To																
024.00	0:30	0.50	D	FUNCTION TEST M W D						From																
0:30	1:30	1.00	D	RUN IN WITH DIRECTION TOOLS						Formation																
1:30	2:00	0.50	D	CIRCULATE THROUGH TIGHT SPOT @ 2870 m--2880 m						Rock Type																
2:00	2:30	0.50	D	RUN IN HOLE																						
2:30	3:00	0.50	D	CIRCULATE THROUGH TIGHT SPOT @ 3190 m																						
3:00	3:30	0.50	D	RUN IN HOLE																						
3:30	4:00	0.50	D	CIRCULATE THROUGH TIGHT SPOT @ 334 m																						
4:00	4:30	0.50	D	DIRECTION DRILL 152.6mm HOLE																						
4:30	5:00	0.50	D	FORMATION INTERGRITY TEST @ 3364 m (6000 KPA)																						
5:00	6:00	1.00	D	DIRECTION DRILL 152.6mm HOLE																						
		24.00																								

11 SUMMARY OF OPERATIONS										14 FREIGHT ARRIVAL & DEPARTURE										15 PERSONNEL			
DIRECTION DRILL 152.6mm HOLE										HAULER		FREIGHT		Arrival	Depart.	Destination		Company: 2					
																		Drilling Contractors: 15					
																		Service Contractors: 5					

13 WELL STATUS at 06:00										16 OPERATIONS PLANNED										17 SAFETY			
DIRECTION DRILL										DIRECTION DRILL 152.6mm HOLE IN TO TOP ZONE										DRILLS: SAFETY MEETING			
																				DAYS SINCE LAST LTA: 314			
																				18 COSTS			
																				DAILY: 0.0% of AFE			
																				CUMULATIVE:			

19 WEATHWIND										20 COMPANY REP.									
Spe Time of Survey: 6:00					Temp: 9 deg					Visibility:					TOTAL: 22				
11 Knt					Direction: E					Barometer (Mb):					Stan Stafford				

	CANADIAN IMPERIAL VENTURE CORPORATION ONSECRE/DAILY DRILLING REPORT Garden Hill	Well: garden hill ST # 2	Rig: Simmon's 31	Date: JULY 29/002	Days Since Spud:	Report N°: 126
	Current depth: 3353.7	Phase: since:	Casing size: 244.5/194	Shoe: 3354m	F.I.T. at shoe:	

1 PENETRATION										2 BITS					3 PARAMETERS															
Type	RUN N°	DEPTH Start	OPERATION Mtrs	Hours	R.O.P. m/h	CUMUL Mtrs	Hours	Diameter	BIT Maker	BIT Type	IADC Code	Serial N°	Jets or TFA	CUT. STRUCT.					OTHERS					WOB daN	RPM	Flow l/min	Pres. kPa			
MILL	1	3346.69	7	10.00	0.7	7	10.00	158.6mm	BAKER	MILL			0.000	I	O	D	L	B	G	O	R						4/5	70	1.00	12000

4 DRILL STRING ASSEMBLY
 TORQUE MASTER ANCHOR/ WHIP STOCK /STARTER MILL/ LOWER WATER MELON MILL
 UPER WATER MELON MILL/ U.B.H.O. SUB,

5 DOWN HOLE TOOLS			6 DEVIATION SURVEYS					7 MUD		
Diam. + Type	Hrs	Cum.	Type	N°	Depth	Inc.	Az.	TYPE: Gel / Chem		
								Mixed (m3)	Den	1000
								Dumped (m3)	YP	3
								Form. Losses (m3)	PV	6
								Surf. Losses (m3)	Gel10s	
								Solids (%)	Gel10m	
								Oil (%)	Fun Vis	
								Water (%)	F/L Temp	
								O/W ratio	pH	10
								Filtrate API	Fluid loss	11
								Filtrate HP/HT	Chlorides	120
									Calcium	12

8 OPERATIONS & TIME ANALYSIS:

FROM	TO	HOURS	CODE	DESCRIPTION
6:00	12:00	6.00	D	RUN IN WITH MILL BIT AND WHIP STOCK TOOLS
12:00	14:00	2.00	D	RUN IN WITH MILL BIT AND WHIP STOCK TOOLS
14:00	16:30	2.50	D	RIG IN BAKER ATLAS WIRE LINE RUN GYRO SURVEY (ORIENT)
16:30	19:30	3.50	D	SET ANCHOR AND WHIP STOCK TOOL
19:30	6:00	10.00	D	MILL 152.6mm WINDOW IN 7.5/8" CASING
		24.00		

9 REMARKS
 Conduct daily walk around inspection.
 Conduct safety meetings with rig crews discuss general operations.

START MUDING UP WHEN STARTING TO MILL WINDOW

PROBLEMS RUNNING GYRO SURVEY TOOL THROUGH H.W.DRILL PIPE
 PULL OUT REMOVE BOTTOM STAB, SPRING
 RE RUN OK.
 REMOTE CHOKE INSTALLED AND FUNCTION TESTED
 07/29/002 OK.

RUN GYRO SURVEY TO ORIENT WHIP STOCK TOOL @ 3334.1m
 WHIP STOCK SET @ 353/DEGESS NORTH/ @ 5.64/ INCL.
 BOTTOM @ 3352.3 m/ WINDOW TOP @ 3346.69 m

12 BASIC

From	Formation	Rock Type

11 SUMMARY OF OPERATIONS
 CUT 152.6mm WINDOW IN 7.5/8" CASING AT 3354 m
 FOR DIRECTION DRILLING

13 WELL STATUS at 06:00 MILL WINDOW IN 7.5/8" CASING FOR DIRECTION DRILLING

16 OPERATIONS PLANNED
 CUT 152.4mm WINDOW IN CASING

17 SAFETY
 DRILLS:
 DAYS SINCE LAST LTA: 313

18 COSTS
 DAILY:
 CUMULATIVE: 0.0% of AFE

14 FREIGHT ARRIVAL & DEPARTURE

HAULER	FREIGHT	Arrival	Depart.	Destination

19 WEATWIND Spe Time of Survey: 6:00 Temp: 9 deg Visibility: 2000m
 8 Knt Direction: N/E Barometer (Mb):

10 PRODUCTS	Unit	In (+) / Used (-)	Stock
Barite	SXS		
Bentonite	SXS	+240	
Soda Ash	SXS	+9	
POLYACUL	SXS	+20	
POLYPAC-R	SXS	+3	
Potassium Chlorid	SXS		
Lignite	SXS		
DeFoam X	SXS		
Poly Plus RD	SXS		
Sawdust	SXS		
Caustic Soda	SXS	+6	
Poly Pac UL	SXS		
Lignosulphonate	SXS		
Bicarb	SXS		
Cellophane	SXS		
Mica-F	SXS		
Drilling detergent	SXS		
Kalzan	SXS		
DD 2000	Pails		

15 PERSONNEL
 Company: 2
 Drilling Contractors: 16
 Service Contractors: 5

20 COMPANY REP.
 TOTAL: 23
 Stan Stafford

1 PENETRATION						2 BITS						DULL						3 PARAMETERS					
Type Oper.	RUN N°	DEPTH Start	OPERATION Mtrs	R.O.P. Hours	CUMUL. Mtrs	Diameter	BIT Maker	BIT Type	IADC Code	Serial N°	Jets or TFA	CUT. STRUCT.				OTHERS				WOB daN	RPM	Flow l/min	Pres. kPa
												I	O	D	L	B	G	O	R				

4 DRILL STRING ASSEMBLY						5 DOWN HOLE TOOLS			6 DEVIATION SURVEYS					7 MUD	
						Diam. + Type	Hrs	Cum.	Type	N°	Depth	Inc.	Az.	TYPE: Gel / Chem	
														Mixed (m3)	Den
														Dumped (m3)	YP
														Form. Losses (m3)	PV
														Surf. Losses (m3)	Gel10s
														Solids (%)	Gel10m
														Oil (%)	Fun Vis
														Water (%)	F/L Temp
														O/W ratio	pH
														Filtrate API	Fluid loss
														Filtrate HP/HT	Chlorides
															Calcium

8 OPERATIONS & TIME ANALYSIS:				
FROM	TO	HOURS	CODE	DESCRIPTION
6:00	9:30	3.50	D	TRIP OUT WITH BIT AND STRING MILL
9:30	11:30	1.00	D	RIG UP BAKER ATLAS WIRE LINE TRUCK RUN 6.1/8" GAUGE RING RUN TO 3365m
11:30	13:30	2.00	D	MAKE UP 158.7mm BAKER N-1 BRIDGE PLUG ON W/LINE RUN UNABLE GET IN TO LINER TOP
13:30	14:00	0.50	D	MAKE UP 158.7mm BAKER N-1 BRIDGE PLUG ON 88.9mm DRILL PIPE
			D	MAKE BAKER N-1 BRIDGE PLUG UP ON DRILL PIPE RUN HOLE SET N-1 BAKER BRIDGE
14:00	20:00	5.00	D	RUN IN WITH 158.7mm BIRDGE PLUG ON 88.9mm DRILL PIPE
20:00	20:30	0.50	D	SET 158.7mm BRIDGE PLUG @ 3354m
20:30	2:00	7.50	D	TRIP OUT WITH RUNNING TOOL
2:00	2:30	0.50	D	LOAD OUT RUNNING TOOL
2:30	5:00	2.50	D	MAKE UP WHIP STOCK ASSY,
5:00	6:00	1.00	D	RUN IN WITH WHIP STOCK TOOLS
		24.00		

9 REMARKS
 Conduct daily walk around inspection.
 Conduct safety meetings with rig crews discuss general operations.
 RUN 6.1/8. GAUGE RING IN 7.5/8. CASING TO 3367m OK.
 RUN BAKER N-1 BIRDGE PLUG ON WIRE LINE UNABLE TO GET IN TO 7.5/8. LINER TOP
 TRIP OUT/MAKE UP BAKER N-1 158.7mm BIRDGE PLUG ON DRILL PIPE AND RUN IN HOLE SET 158.7mm BIRDGE PLUG AT 3354m OK.

10 PRODUCTS				In (+) / Used (-)	Stock
Barite	SXS				
Bentonite	SXS				
Soda Ash	SXS				
Sapp	SXS				
Kwik Seal F	SXS				
Potassium Chlorid	SXS				
Lignite	SXS				
DeFoam X	SXS				
Poly Plus RD	SXS				
Sawdust	SXS				
Caustic Soda	SXS				
Poly Pac UL	SXS				
Lignosulphonate	SXS				
Bicarb	SXS				
Cellophane	SXS				
Mica-F	SXS				
Drilling detergent	SXS				
Kalzan	SXS				
DD 2000	Pails				

11 SUMMARY OF OPERATIONS
 RUN IN CUT WINDOW IN 7.5/8. CASING AT 3354m

13 WELL STATUS at 06:00
 RUN IN WITH WHIP STOCK TOOLS

16 OPERATIONS PLANNED
 SET WHIP STOCK MILL WINDOW IN 7.5/8. CASING

17 SAFETY
 DRILLS:
 DAYS SINCE LAST LTA: **312**

18 COSTS
 DAILY:
 CUMULATIVE: **0.0% of AFE**

12 BASIC To

From	Formation	Rock Type

14 FREIGHT ARRIVAL & DEPARTURE

HAULER	FREIGHT	Arrival	Depart.	Destination

19 WEATWIND Spe Time of Survey: **6.00** Temp: **11 deg** Visibility: **2.00**
16 Knt Direction: **E** Barometer (Mb): **1013**

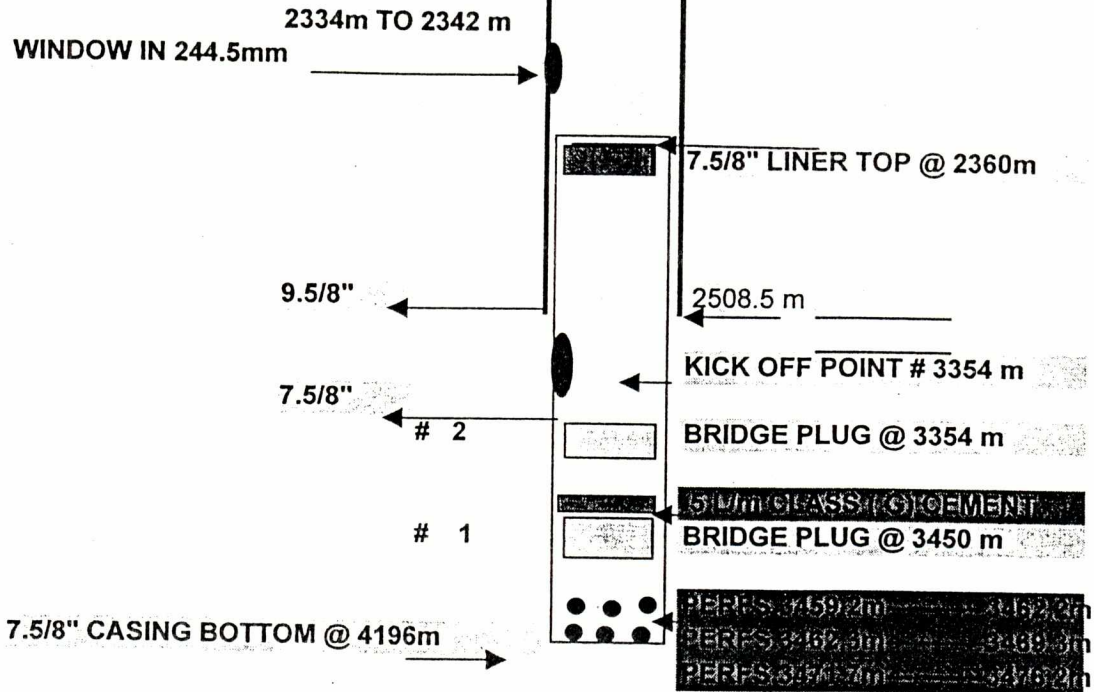
15 PERSONNEL
 Company: **2**
 Drilling Contractors: **16**
 Service Contractors: **5**

TOTAL: 23
20 COMPANY REP.
Stan Stafford

C.I.V.C.

GARDEN HILL # 1

K.B. 8.3m



1 BRIDGE PLUG SET ON DRILL PIPE 07/ 25 /002
PRESSURE TEST TO 13,500 KPA OK.

2 BRIDGE PLUG SET ON DRILL PIPE 07 / 27002

STAN.STAFFORD



CANADIAN IMPERIAL VENTURE CORPORATION
ONSHORE DAILY DRILLING REPORT
Garden Hill

Well : **garden hill # 1** Rig : **Simmon's 31** Date : **JULY 25/002** Days Since Spud:
 Current depth: **P.B.T.D./3450 m** Phase:
 Casing size: **244.5/194mm** Shoe: **3450m** Report N°: **122**
 Bottom hole: **PBTD: 3450m** F.I.T. at shoe:

1 PENETRATION						2 BITS				DULL								3 PARAMETERS					
Type	RUN N°	DEPTH Start	OPERATION Mtrs	R.O.P. Hours	CUMUL Mtrs	Diameter	BIT Maker	BIT Type	IADC Code	Serial N°	Jets or TFA	CUT. STRUCT.				OTHERS				WOB daN	RPM	Flow l/min	Pres. kPa
Oper.												I	O	D	L	B	G	O	R				

4 DRILL STRING ASSEMBLY						5 DOWN HOLE TOOLS			6 DEVIATION SURVEYS					7 MUD			
						Diam. + Type	Hrs	Cum.	Type	N°	Depth	Inc.	Az.	TYPE: Gel / Chem			

8 OPERATIONS & TIME ANALYSIS:					DESCRIPTION
FROM	TO	HOURS	CODE		
6:00	7:00	1.00	D		RUN GAUGE RINGS
7:30	7:30	0.50	D		RIG SERVICE FUNCTION BLIND RAMS
7:30	8:30	1.00	D		MAKE UP BAKER 158.7mm BRIDGE PLUG
8:30	17:00	8.00	D		STRAP IN WITH BAKER N-1 BRIDGE PLUG
17:00	18:00	1.00	D		DROP BALL PRESSURE SET BAKER N-1 BRIDGE PLUG SHEAR OFF N-1 BRIDGE PLUG
18:00	18:30	0.50	D		PRESSURE TEST CSG. AND BAKER N-1 BRIDGE PLUG 13,500 KPA/ 8/MINS OK.
18:30	0:30	6.50	D		TRIP OUT WITH SETTING TOOLS
00:30	0:00	5.50	D		RIG IN BAKER ATLAS WIRE LINE WITH CEMENT BALIER MIX CEMENT RUN BALIER IN HOLE DUMP CEMENT ON BAKER N-1 BRIDGE PLUG @ 3450 m 2/ RUNS WITH CMENT BAILER
		24.00			# 1 RUN WITH CEMENT BAILER MISS RUN (CEMENT IN WHEN BACK AT SURFACE RUN # 2 # 3 WITH CEMENT BAILER CAP BRIDGE PLUG WITH 5/LIN/ CLASS (G) CEMENT (AT 3450 m)
					SWACO P.V.T.IN TANKS HOOD UP AND WORKING FLOW SHOW WORKING

9 REMARKS											
Conduct daily walk around inspection. Conduct safety meetings with rig crews discuss general operations.											
RUN 165.1mm GAUGE RING ON WIRE LINE UNABLE TO GET PAST 7.5/8" LINER TOP @ 2360 m PULL OUT CHANGE GAUGE RING TO 152.8 mm RUN IN UNABLE TO GET PAST 2434 m PULL OUT RIG AND RUN BAKER N-1 158.75 mm BRIDGE PLUG ON DRILL PIPE											
SET BAKER 158.7mmN-1 BRIDGE PLUG @ 3450m WITH 14000 KPA SHEAR OFF WITH 8,000 DAN. CLOSE 127 mm PIPE RAMS PESSURE TEST CASING AND BAKER N-1 BRIDGE PULG TO 13,500 KPA FOR 8/MINS OK.*** TRIP OUT WITH 127mm PIPE AND 88.9 mm PIPE											
12 BASIC To						From					
Formation						Rock Type					

10 PRODUCTS		Unit	In (+) / Used (-)	Stock
Barite	8XS			
Bentonite	8XS			
Soda Ash	8XS			
Sapp	8XS			
Kwik Seal F	8XS			
Potassium Chloride	8XS			
Lignite	8XS			
DeFoam X	8XS			
Poly Plus RD	8XS			
Sawdust	8XS			
Caustic Soda	8XS			
Poly Pac UL	8XS			
Lignosulphonate	8XS			
Bicarb	8XS			
Cellophane	8XS			
Mica-F	8XS			
Drilling detergent	8XS			
Kalzan	8XS			
DD 2000	8XS			
Pails				

11 SUMMARY OF OPERATIONS
RUN IN SET BRIDGE PLUGS TO ISOLATE BOTTOM ZONES

13 WELL STATUS at 06:00

16 OPERATIONS PLANNED
 RUN 158.7 mm BAKER N-1 BRIDGE PLUG ON DRILL PIPE

17 SAFETY
 DRILLS:
 DAYS SINCE LAST LTA: **310**

18 COSTS in CAN\$
 DAILY:
 CUMULATIVE: **0.0%** of AFE

14 FREIGHT ARRIVAL & DEPARTURE				
HAULER	FREIGHT	Arrival	Depart.	Destination

19 WEA' WIND Sp Time of Survey: 6:00 Temp: 5 deg Visibility: **CLEAR**
 9 Knt Direction: N/W Barometer (Mb):

15 PERSONNEL
 Company: **3**
 Drilling Contractors: **8**
 Service Contractors: **4**

TOTAL: **13**
 20 COMPANY REP. **Stan Stafford**

	CANADIAN IMPERIAL VENTURE CORPORATION	Well : garden hill # 1	Rig : Simmon's 31	Date : JULY 24/002	Days Since Spud:	Report N°: 121
	IMPERIAL VENTURE CORP.	ONSHORE DAILY DRILLING REPORT Garden Hill	Current depth: 4196	Phase:	Casing size: 244.5/197	Shoe:
		since:		Bottom hole:		PBDT:

1 PENETRATION								2 BITS				DULL								3 PARAMETERS					
Type Oper.	RUN N°	DEPTH Start	OPERATION Mtrs	Hours	R.O.P. m/h	CUMUL Mtrs Hours		Diameter	BIT Maker	BIT Type	IADC Code	Serial N°	Jets or TFA	CUT. STRUCT.				OTHERS				WOB daN	RPM	Flow l/min	Pres. kPa
														I	O	D	L	B	G	O	R				
MILL	1	2347.8																							

4 DRILL STRING ASSEMBLY												5 DOWN HOLE TOOLS			6 DEVIATION SURVEYS					7 MUD			
												Diam. + Type	Hrs	Cum.	Type	N°	Depth	Inc.	Az.	TYPE: Gel / Chem			
																				Mixed (m3)	Den		
																				Dumped (m3)	YP		
																				Form. Losses (m3)	PV		
																				Surf. Losses (m3)	Gel10s		
																				Solids (%)	Gel10m		
																				Oil (%)	Fun Vis		
																				Water (%)	F/L Temp		
																				O/W ratio	pH		
																				Filtrate API	Fluid loss		
																				Filtrate HP/HT	Chloride		
																					Calcium		

8 OPERATIONS & TIME ANALYSIS:					9 REMARKS												10 PRODUCTS																																																															
FROM	TO	HOURS	CODE	DESCRIPTION																																																																												
6:00	8:00	2.00	D	FINISH OUT WITH HURRICANE PACKER	Conduct daily walk around inspection. Conduct safety meetings with rig crews discuss general operations. RUN IN WITH 166MM MILL CIRCULATE AND REAM 7.5/8" CSG. 2435 m TO 2437 m (TABLE TORQUE @ 2434m WASH THROUGH SPOTS @ 2721 m TO 2747 m WASH THROUGH SPOTS @ 3110 m TO 3130 m RUN IN WITH 6.5" GAUGE RING ON WIRE LING UNABLE TO GET IN TO 7.5/8" LINER TOP @ 2360 m PULL OUT, RUN WITH 6.1/8" GAUGE RING NOTE: CORRECTION TO REPORT 120, JULY 24, IRREGULTRITIES PICKED UP ON CC 1												<table border="1" style="width:100%; border-collapse: collapse;"> <thead> <tr> <th>Unit</th> <th>In (+) / Used (-)</th> <th>Stock</th> </tr> </thead> <tbody> <tr><td>Barite</td><td>sxs</td><td></td></tr> <tr><td>Bentonite</td><td>sxs</td><td></td></tr> <tr><td>Soda Ash</td><td>sxs</td><td></td></tr> <tr><td>Sapp</td><td>sxs</td><td></td></tr> <tr><td>Kwik Seal F</td><td>sxs</td><td></td></tr> <tr><td>Potassium Chloride</td><td>sxs</td><td></td></tr> <tr><td>Lignite</td><td>sxs</td><td></td></tr> <tr><td>DeFoam X</td><td>sxs</td><td></td></tr> <tr><td>Poly Plus RD</td><td>sxs</td><td></td></tr> <tr><td>Sawdust</td><td>sxs</td><td></td></tr> <tr><td>Caustic Soda</td><td>sxs</td><td></td></tr> <tr><td>Poly Pac UL</td><td>sxs</td><td></td></tr> <tr><td>Lignosulphonate</td><td>sxs</td><td></td></tr> <tr><td>Bicarb</td><td>sxs</td><td></td></tr> <tr><td>Cellophane</td><td>sxs</td><td></td></tr> <tr><td>Mica-F</td><td>sxs</td><td></td></tr> <tr><td>Drilling detergent</td><td>sxs</td><td></td></tr> <tr><td>Kalzan</td><td>sxs</td><td></td></tr> <tr><td>DD 2000</td><td>Pails</td><td></td></tr> </tbody> </table>				Unit	In (+) / Used (-)	Stock	Barite	sxs		Bentonite	sxs		Soda Ash	sxs		Sapp	sxs		Kwik Seal F	sxs		Potassium Chloride	sxs		Lignite	sxs		DeFoam X	sxs		Poly Plus RD	sxs		Sawdust	sxs		Caustic Soda	sxs		Poly Pac UL	sxs		Lignosulphonate	sxs		Bicarb	sxs		Cellophane	sxs		Mica-F	sxs		Drilling detergent	sxs		Kalzan	sxs		DD 2000	Pails	
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8:00	8:30	0.50	D	LAY DOWN HURRICANE PACKER																																																																												
8:30	9:30	1.00	D	HOIST 88.9mm H.W.																																																																												
9:30	10:30	1.00	D	MAKE UP 6.68mm MILLS																																																																												
10:30	14:30	3.00	D	RUN IN WITH 127 mm DRILL PIPE TO 2437 m																																																																												
14:30	16:30	3.00	D	CIRCULATE AND REAM 7.5/8" CASING FROM 2435 m TO 2437m																																																																												
16:30	17:00	1.50	D	RUN IN WITH PIPE																																																																												
17:00	18:30	1.50	D	WASH THROUGH SPOT @ 2721 m TO 2747 m																																																																												
18:30	19:00	0.50	D	TRIP IN																																																																												
19:00	20:00	1.00	D	WAH THROUGH SPOTS @ 3110 m 3130 m																																																																												
20:00	20:30	0.50	D	TRIP IN																																																																												
20:30	22:00	1.50	D	CIRCULATE BOTTOMS UP																																																																												
22:00	4:30	5.50	D	TRIP OUT WITH MILLS																																																																												
4:30	6:00	1.50	D	RIG IN BAKER ATLAS WIRE LINE RUN GAUGE RINGS																																																																												
24.00																																																																																

11 SUMMARY OF OPERATIONS	RUN IN SET BRIDGE PLUGS TO ISOLATE BOTTOM ZONES
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13 WELL STATUS at 06:00	RUN 6 1/8 GAUGE RING ON WIRE LINE
16 OPERATIONS PLANNED	TRY TO RUN GAUGE RING ON WIRE LINE AND RUN BRIDGE PLUGS

17 SAFETY	18 COSTS	19 WEA WIND	Sp Time of Survey: 6:00	Temp: 9 deg	Visibility: CLEAR	20 COMPANY REP.
DRILLS:	in CAN\$	HAULER	0 Knt	Direction: 0 deg	Barometer (Mb):	Stan Stafford
DAYS SINCE LAST LTA: 309	DAILY: CUMULATIVE: 0.0% of AFE	FREIGHT	Arrival	Depart.	Destination	TOTAL: 25

15 PERSONNEL	
Company:	3
Drilling Contractors:	18
Service Contractors:	6
TOTAL:	25

	CANADIAN IMPERIAL VENTURE CORPORATION	Well : garden hill # 1	Rig : Simmon's 31	Date : JULY24 002	Days Since Spud:	Report N°: 120
	ONSHORE DAILY DRILLING REPORT Garden Hill	Current depth: 4196	Phase: since:	Casing size: 244/197	Shoe: PBDT:	F.I.T. at shoe:

1 PENETRATION								2 BITS				DULL								3 PARAMETERS					
Type Oper.	RUN N°	DEPTH Start	OPERATION Mtrs	Hours	R.O.P. m/h	CUMUL Mtrs	Hours	Diameter	BIT Maker	BIT Type	IADC Code	Serial N°	Jets or TFA	CUT. STRUCT.				OTHERS				WOB daN	RPM	Flow l/min	Pres. kPa
														I	O	D	L	B	G	O	R				
MILL	1	2347.8																							

4 DRILL STRING ASSEMBLY				5 DOWN HOLE TOOLS			6 DEVIATION SURVEYS				7 MUD				
				Diam. + Type	Hrs	Cum.	Type	N°	Depth	Inc.	Az.	TYPE: Gel / Chem			
												Mixed (m3)	Den		
												Dumped (m3)	YP		
												Form. Losses (m3)	PV		
												Surf. Losses (m3)	Gel10s		
												Solids (%)	Gel10m		
												Oil (%)	Fun Vis		
												Water (%)	F/L Temp		
												O/W ratio	pH		
												Filtrate API	Fluid loss		
												Filtrate HP/HT	Chloride		
													Calcium		

8 OPERATIONS & TIME ANALYSIS:				
FROM	TO	HOURS	CODE	DESCRIPTION
6:00	9:30	3.50	D	TRIP OUT WITH MILLS
9:30	10:00	1.50	D	RIG SERVICE FUNCTION PIPE RAMS
10:00	10:30	0.50	D	LAY DOWN MILLING TOOLS
10:30	12:00	1.50	D	RIG UP BAKER ATLAS WIRE LINE RUN JUNK BASKET AND GAUGE RING
12:00	13:00	1.00	D	RUN CCL/ TOOL UNABLE TO GET IN TO LINER TOP @ 2360 m
13:00	16:30	3.50	D	RUN 5.7/8" GAUGE RING AND BASKET TO 3459 m
16:30	17:30	1.00	D	SLIP AND CUT DRILLING LINE
17:30	18:30	1.00	D	RUN IN 16 STANDS H.W.DRILL PIPE
18:30	2:00	6.50	D	MAKE UP HURRICANE PACKER AND STRAP IN WITH 127 mm DRILL PIPE PICK UP SINGLES
2:00	3:00	1.00	D	SET HURRICANE PACKER TEST 244.5 mm CASING TO 13,525 KPA 10/MINS OK.
3:00	6:00	3.00	D	TRIP OUT WITH HURRICANE PACKER
		24.00		

9 REMARKS
 Conduct daily walk around inspection.
 Conduct safety meetings with rig crews discuss general operations.

RUN IN WITH 6.1/8" GAUGE RING ON WIRE LINE BRIDGE OF AT 2437 m
 PULL OUT WITH GAUGE RING RUN IN WITH CCL. ONLY
 UNABLE TO GET IN TO THE 7.5/8" LINER PULL OUT
 RUN IN WITH 5.7/8" GAUGE RING WHEN,T TO 3458.5 m
 WITH NO PROBLEMS/ RUN CCL. FROM 3458m TO SURACES

THE CCL. SHOWS THE 7/5/8" CASING IS DAMAGED @ 2750 m
 THE CCL. SHOWS THE 9.5/8" CASING IS DAMAGED @ 1583 m
 1262 m 1431 m TO 1432 m @ 1795 m 1704 m 1898 m
 SET HURRICANE PAKER @ 236.00 m PRESSURE TEST 244.5mm CASING TO 13,525 KPA 10/MINS OK.

MUD TANKS IN VEARY POOR CONDITION VALVE AND AND SKIMER LEAKING FROM ONE TANK TO THE NEXT TANK
 UNABLE TO HOLED ANY PRE-MIX MUD.

12 BASIC To			
From	Formation	Rock Type	

11 SUMMARY OF OPERATIONS
 RUN IN SET BRIDGE PLUGS ISOLATE BOTTOM ZONES

13 WELL STATUS at 06:00 TRIP OUT WITH HURRICANE PACKER

16 OPERATIONS PLANNED
 RUN IN WITH HURRICANE PACKER TO PRESSURE TEST 244.5mm CASING

17 SAFETY
 DRILLS:
 DAYS SINCE LAST LTA: 308

18 COSTS in CANS
 DAILY:
 CUMULATIVE: 0.0% of AFE

19 WEA* WIND Sp Time of Survey: 6:00 Temp: 7 deg Visibility: RAIN
 21 Knt Direction: NW Barometer (Mb):

10 PRODUCTS			
	Unit	In (+) / Used (-)	Stock
Barite	sxs		
Bentonite	sxs		
Soda Ash	sxs		
Sapp	sxs		
Kwik Seal F	sxs		
Potassium Chloride	sxs		
Lignite	sxs		
DeFoam X	sxs		
Poly Plus RD	sxs		
Sawdust	sxs		
Caustic Soda	sxs		
Poly Pac UL	sxs		
Lignosulphonate	sxs		
Bcarb	sxs		
Cellophane	sxs		
Mica-F	sxs		
Drilling detergent	sxs		
Kalzan	sxs		
DD 2000	Pails		

15 PERSONNEL
 Company:
 Drilling Contractors:
 Service Contractors:

TOTAL:
20 COMPANY REP.
 Stan Stafford

	CANADIAN IMPERIAL VENTURE CORPORATION	Well : garden hill # 1	Rig : Simmon's 31	Date : JULY 22/002	Days Since Spud:	Report N°: 118
	ONSHORE DAILY DRILLING REPORT	Current depth: 4196	Phase: since:	Casing size: 244/197	Shoe:	F.I.T. at shoe:
Garden Hill						

1 PENETRATION								2 BITS						DULL						3 PARAMETERS					
Type Oper.	RUN N°	DEPTH Start	OPERATION Mtrs	Hours	R.O.P. m/h	CUMUL Mtrs	Hours	Diameter	BIT Maker	BIT Type	IADC Code	Serial N°	Jets or TFA	CUT. STRUCT.				OTHERS				WOB daN	RPM	Flow l/min	Pres. kPa
														I	O	D	L	B	G	O	R				

4 DRILL STRING ASSEMBLY

TAPERD MILL BIT/SUB 6.50" STRING MILL, JARS, 3.50" H.W.

5 DOWN HOLE TOOLS				6 DEVIATION SURVEYS				7 MUD							
Diam. + Type	Hrs	Cum.		Type	N°	Depth	Inc.	Az.				TYPE:	Gel / Chem		
														Mixed (m3)	Den
														Dumped (m3)	YP
														Form, Losses (m3)	PV
														Surf. Losses (m3)	Gel10s
														Solids (%)	Gel10m
														Oil (%)	Fun Vis
														Water (%)	F/L Temp
														O/W ratio	pH
														Filtrate API	Fluid loss
														Filtrate HP/HT	Chlorides
															Calcium

8 OPERATIONS & TIME ANALYSIS:

FROM	TO	HOURS	CODE	DESCRIPTION
8:00	9:00	3.00	D	RUN IN WITH 7.5/8" CASING SCRAPER
9:00	10:00	1.00	D	WORK CASING SCRAPER UP AND DOWN @ 3450m TO 3455 m AND 3355m TO 3360 m
10:00	15:00	5.00	D	TRIP OUT WITH CASING SCRAPER
15:00	15:30	0.50	D	BREAK DOWN SCRAPER
15:30	21:00	5.50	D	RIG IN BAKER ATLAS WIRE LINE/ AND WAIT FOR WIRE LINE EQUIPMENT FROM CORNERBROOK
21:00	024:00	3.00	D	RUN IN GAUGE RING ON WIRE LINE/ STUCK IN 7.5/8 LINER TOP 2363 m
024:00	1:00	1.00	D	WORK GAUGE RING AND BASKET UP AND DOWN FEE AFTER /2 HRS.
1:00	6:00	5.00	D	RIG OUT WIRE LINE
				RUN IN WITH 6.50" MILLS AND JARS.
		24.00		

9 REMARKS

Conduct daily walk around inspection.
Conduct safety meetings with rig crews discuss general operations.

WORK CASING SCRAPER THROUGH 7.5/8" CASING
NO TIGHT SPOTS
FUNCTION BLIND RAMS
RUN IN WITH 6.1/8" GAUGE RING ON

LARGE STEEL RING 8" LONG AND SMLL STEEL BALL IN WIRE LINE
JUNK BASKET
THE STEEL RING LOOKS LIKE PART OF THE 7.5/8" LINER TOP

12 BASIC To

From	Formation	Rock Type

10 PRODUCTS

Unit	In (+) / Used (-)	Stock
Barite	sxs	
Bentonite	sxs	
Soda Ash	sxs	
Sapp	sxs	
Kwik Seal F	sxs	
Potassium Chloride	sxs	
Lignite	sxs	
DeFoam X	sxs	
Poly Plus RD	sxs	
Sawdust	sxs	
Causlic Soda	sxs	
Poly Pac UL	sxs	
Lignosulphonate	sxs	
Bicarb	sxs	
Celkophane	sxs	
Mica-F	sxs	
Drilling detergent	sxs	
Kalzan	sxs	
DD 2000	Pa/s	

11 SUMMARY OF OPERATIONS

RUN IN SET BRIDGE PLUGS ISOLATE BOTTOM ZONES

13 WELL STATUS at 06:00

RUN IN WITH MILLS

16 OPERATIONS PLANNED REAM TOP OF 7.5/8: LINNER WITH MILLS
RUN WIRE LINE GAUGE RING AND BRIDGE PLUGS

17 SAFETY

DRILLS:
DAYS SINCE LAST LTA: 306

18 COSTS in CANS

DAILY:
CUMULATIVE: 0.0% of AFE

14 FREIGHT ARRIVAL & DEPARTURE

HAULER	FREIGHT	Arrival	Depart.	Destination

19 WEA' WIND Sp Time of Survey: 6:00 Temp: 9 deg Visibility: O/CAST
25 Knt Direction: SW Barometer (Mb):

15 PERSONNEL

Company:
Drilling Contractors:
Service Contractors:

20 COMPANY REP.
Stan Stafford

CANADIAN IMPERIAL VENTURE CORP.		CANADIAN IMPERIAL VENTURE CORPORATION		Well : garden hill # 1		Rig : Simmon's 31		Date : JULY 19/002		Days Since Spud:		Report N°: 115											
ONSHORE DAILY DRILLING REPORT				Current depth: 2349		Phase:		Casing size: 244/192.5		Shoe:		F.I.T. at shoe:											
Garden Hill						since:		Bottom hole:		PBT.D:													
1 PENETRATION				2 BITS				DULL				3 PARAMETERS											
Type Oper.	RUN N°	DEPTH Start	OPERATION Mtrs Hours	R.O.P. m/h	CUMUL Mtrs Hours	Diameter	BIT Maker	BIT Type	IADC Code	Serial N°	Jets or TFA	CUT. STRUCT.				OTHERS				WOB daN	RPM	Flow l/min	Pres. kPa
MILL	1	2347.8m	1.4 17.50	70.0	1.4 17.50							I	O	D	L	B	G	O	R				
4 DRILL STRING ASSEMBLY						5 DOWN HOLE TOOLS			6 DEVIATION SURVEYS				7 MUD										
203.9mm WASH OVER SHOE/WASH OVER PIPE/ X/O SUB. BOOT BASKET/ BIT SUB/ BUMPER SUB, JARS/ 9 JOINTS 127mm H.W. DRILL PIPE / B.H.A.98.49 m						Diam. + Type Hrs Cum.			Type N° Depth Inc. Az.				TYPE: Gel / Chem										
8 OPERATIONS & TIME ANALYSIS:													Mixed (m3) Dumped (m3) Form. Losses (m3) Surf. Losses (m3) Solids (%) Oil (%) Water (%) OW ratio Filtrate API Filtrate HP/HT				Den YP PV Gel10s Gel10m Fun Vis F/L Temp pH Fluid loss Chloride Calcium						
FROM	TO	HOURS	CODE	DESCRIPTION																			
6:00	6:30	0.50	D	RUN IN H.W. DRILL PIPE WITH MILL SHOE																			
6:30	7:30	1.00	D	SLIP AND CUT DRILLING LINE																			
7:30	8:30	1.00	D	TRIP IN WITH MILL SHOE																			
8:30	9:00	0.50	D	HELD BOP DRILL WHEN TRIPPING																			
9:00	11:30	2.50	D	RUN IN WITH MILL																			
11:30	12:00	0.50	D	WASH DOWN TO FM.PACKER																			
12:00	12:30	0.50	D	RIG SERVICES (FUNCTION 127mm PIPE RAMS)																			
12:30	6:00	17.50	D	MILL ON ML. PACKER @ 2347.8m																			
									9 REMARKS								10 PRODUCTS						
									Conduct daily walk around inspection. Conduct safety meetings with rig crews discuss general operations.								Unit In (+) / Used (-) Stock						
									HELD BOP DRILL WITH RIG CREW WHEN TRIPPING								Barite sxs Bentonite sxs Soda Ash sxs Sapp sxs Kwik Seal F sxs Potassium Chloride sxs Lignite sxs DeFoam X sxs Poly Plus RD sxs Sawdust sxs Caustic Soda sxs Poly Pac UL sxs Lignosulphonate sxs Bicarb sxs Cellophane sxs Mica-F sxs Drilling detergent sxs Kalzan sxs DD 2000 Pails						
									FUNCTION PIPE RAMS														
									MILL FM PACKER FROM 2347.8m----2349.25 m														
									CUT 1.4 m														
						12 BASIC To																	
						From			Formation				Rock Type										
11 SUMMARY OF OPERATIONS																							
MILL OUT ML PACKER ABANDON BOTTOM ZONE																							
13 WELL STATUS at 08:00									14 FREIGHT ARRIVAL & DEPARTURE				15 PERSONNEL										
MILL ON ML PACKER @ 2349.25 m						HAULER			FREIGHT				Arrival Depart. Destination				Company: 2 Drilling Contractors: 16 Service Contractors: 1						
16 OPERATIONS PLANNED																							
FINISH MILLING ML/PACKER PUSH TO TOP OF 7.5/8" @ 2360 m																							
17 SAFETY						18 COSTS			19 WEA' WIND				20 COMPANY REP.										
DRILLS: 302 DAYS SINCE LAST LTA: 302						in CAN\$ DAILY: CUMULATIVE: 0.0% of AFE			Sp Time of Survey: 6:00 10 Knt				Temp: 9 deg Direction: N/W Barometer (Mb):				TOTAL: 19 Stan Stafford						

1 PENETRATION								2 BITS				DULL								3 PARAMETERS					
Type Oper.	RUN N°	DEPTH Start	OPERATION Mtrs Hours		R.O.P. m/h	CUMUL Mtrs Hours		Diameter	BIT Make	BIT Type	IADC Code	Serial N°	Jets or TFA	CUT. STRUCT.				OTHERS				WOB daN	RPM	Flow l/min	Pres. kPa
MILL	1	2316												I	O	D	L	B	G	O	R				

4 DRILL STRING ASSEMBLY 215.9mm WASH OVER SHOE/WASH OVER PIPE/ X/O SUB. BOOT BASKET/ BIT SUB/ BUMPER SUB, JARS/ 9 JOINTS 127mm H.W. DRILL PIPE / B.H.A.98.49 m												5 DOWN HOLE TOOLS Diam. + Type Hrs Cum.				6 DEVIATION SURVEYS Type N° Depth Inc. Az.				7 MUD TYPE: Gel / Chem			
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8 OPERATIONS & TIME ANALYSIS:					9 REMARKS Conduct daily walk around inspection. Conduct safety meetings with rig crews discuss general operations. 115 JOINTS 88.9mm DRILL PIPE ON LOCATION @ 19:00/ HRS. BAKER MILLING TOOLS ON LOCATION @ 3:00 AM. SWACO PIT LEVELERS ON WITH BAKER TOOLS																	
FROM	TO	HOURS	CODE	DESCRIPTION																		
6:00	18:00	12.00	SF	WAIT ON 3.50" DRILL PIPE AND MILLING TOOLS																		
18:00				PICK UP 127mm H.W. DRILL PIPE AND 127mm DRILL PIPE																		
	22:00	4.00	D	UNLOAD 88.9mm DRILL PIPE 115 JOINTS																		
22:00	3:00	5.00	D	TRIP OUT WITH 127mm DRILL PIPE																		
3:00	4:00	1.00	D	UNLOAD BAKER MILLING TOOLS																		
4:00	5:30	1.50	D	MAKE UP MILLING SHOE AND SHORT WAS OVER PIPE AND BUMPER SUB,AND JARS.																		
5:30	6:00	0.50	D	RUN HOLE WITH MILL SHOE [STRAP IN]																		
					12 BASIC		To															
					From	Formation	Rock Type															

11 SUMMARY OF OPERATIONS MILL OUT ML PACKER ABANDON BOTTOM ZONE												10 PRODUCTS				Unit	In (+) / Used (-)	Stock
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13 WELL STATUS at 06:00 TRIP IN WITH MILL SHOE												14 FREIGHT ARRIVAL & DEPARTURE				15 PERSONNEL					
16 OPERATIONS PLANNED RUN IN TO MILL ON M.L. PACKER @ 2316m												HAULER	FREIGHT			Arrival	Depart.	Destination		Company:	2
																	Drilling Contractors:	16			
																	Service Contractors:	1			

17 SAFETY				18 COSTS in CAN\$				19 WEA* WIND Sp Time of Survey: 6:00 Temp: 11 deg Visibility: O/CAST				TOTAL: 19			
DRILLS: DAYS SINCE LAST LTA: 301				DAILY: CUMULATIVE: 0.0% of AFE				8 Knt Direction: S Barometer (Mb):				20 COMPANY REP. Stan Stafford			

	CANADIAN IMPERIAL VENTURE CORPORATION	Well : garden hill # 1	Rig : Simmon's 31	Date : JULY 17/002	Days Since Spud:	Report N°: 113
	ONSHORE DAILY DRILLING REPORT	Garden Hill	Current depth:	Phase: since:	Casing size: 244/177	Shoe:
				Bottom hole:	PBTD:	

1 PENETRATION										2 BITS					DULL					3 PARAMETERS					
Type	RUN	DEPTH	OPERATION		R.O.P.	CUMUL		Diameter	BIT	BIT	IADC	Serial	Jets or	CUT. STRUCT.				OTHERS				WOB	RPM	Flow	Pres.
Oper.	N°	Start	Mtrs	Hours	m/h	Mtrs	Hours		Maker	Type	Code	N°	TFA	I	O	D	L	B	G	O	R	daN		l/min	kPa

4 DRILL STRING ASSEMBLY										5 DOWN HOLE TOOLS			6 DEVIATION SURVEYS					7 MUD			
										Diam. + Type	Hrs	Cum.	Type	N°	Depth	Inc.	Az.	TYPE:		Gel / Chem	
																		Mixed (m3)		Den	
																		Dumped (m3)		YP	
																		Form. Losses (m3)		PV	
																		Surf. Losses (m3)		Gel10s	

8 OPERATIONS & TIME ANALYSIS:					9 REMARKS										10 PRODUCTS			
FROM	TO	HOURS	CODE	DESCRIPTION											Unit	In (+) /	Used (-)	Stock
8:00	6:00	24.00	SF	WAIT ON 3.50" DRILL PIPE AND MILLING TOOLS	Conduct daily walk around inspection. Conduct safety meetings with rig crews discuss general operations. VERY HIGH WINDS OVER NIGHT										Barite	sxs		
		24.00													Bentonite	sxs		
					12 BASIC		To						Lignosulphonate	sxs				
					From	Formation	Rock Type						Bicarb	sxs				
													Cellophane	sxs				
													Mica-F	sxs				
													Drilling detergent	sxs				
													Kalzan	sxs				
													DD 2000	Pails				

11 SUMMARY OF OPERATIONS										14 FREIGHT ARRIVAL & DEPARTURE					15 PERSONNEL				
										HAULER	FREIGHT		Arrival	Depart.	Destination	Company:	2		
															Drilling Contractors:	16			
															Service Contractors:				

13 WELL STATUS at 06:00					16 OPERATIONS PLANNED										17 WEA				TOTAL:					
WAIT ON 3.50" DRILL PIPE AND MILLING TOOLS					PICK UP 3.50" DRILL PIPE AND MILLING TOOLS..										20 Time of Survey:	6:00	Temp:	12 deg	Visibility:	O/C/CAST	18			
															20 Knt		Direction:	S/E	Barometer (Mb):		20 COMPANY REP.			
																			Stan Stafford					

17 SAFETY					18 COSTS					19 WEAT					20 COMPANY REP.			
DRILLS:					in CAN\$													
DAYS SINCE LAST LTA:					DAILY:					20 Time of Survey:					TOTAL:			
301					CUMULATIVE:					6:00					18			
					0.0% of AFE					Temp:					Stan Stafford			
										12 deg								
										Direction:								
										Barometer (Mb):								

1 PENETRATION								2 BITS				DULL				3 PARAMETERS									
Type Oper.	RUN N°	DEPTH Start	OPERATION Mtrs Hours		R.O.P. m/h	CUMUL Mtrs Hours		Diameter	BIT Maker	BIT Type	IADC Code	Serial N°	Jets or TFA	CUT. STRUCT.				OTHERS				WOB daN	RPM	Flow l/min	Pres. kPa
														I	O	D	L	B	G	O	R				

4 DRILL STRING ASSEMBLY								5 DOWN HOLE TOOLS				6 DEVIATION SURVEYS				7 MUD			
								Diam. + Type Hrs Cum.				Type N° Depth Inc. Az.				TYPE: Gel / Chem			

8 OPERATIONS & TIME ANALYSIS:					DESCRIPTION	9 REMARKS
FROM	TO	HOURS	CODE			
6:00	6:00	24.00	SF		WAIT ON 3.50" DRILL PIPE AND MILLING TOOLS	Conduct daily walk around inspection. Conduct safety meetings with rig crews discuss general operations.

10 PRODUCTS				Unit	In (+) / Used (-)	Stock
Barite			sxs			
Bentonite			sxs			
Soda Ash			sxs			
Sapp			sxs			
Kwik Seal F			sxs			
Potassium Chloride			sxs			
Lignite			sxs			
DeFoam X			sxs			
Poly Plus RD			sxs			
Sawdust			sxs			
Caustic Soda			sxs			
Poly Pac UL			sxs			
Lignosulphonate			sxs			
Bicarb			sxs			
Cellophane			sxs			
Mica-F			sxs			
Drilling detergent			sxs			
Kalzan			sxs			
DD 2000			sxs			

11 SUMMARY OF OPERATIONS					14 FREIGHT ARRIVAL & DEPARTURE				15 PERSONNEL		
					HAULER	FREIGHT	Arrival	Depart.	Destination	Company:	2
13 WELL STATUS at 06:00					WAIT ON 3.50" DRILL PIPE AND MILLING TOOLS					Drilling Contractors:	13
16 OPERATIONS PLANNED					PICK UP 3.50" DRILL PIPE AND MILLING TOOLS..					Service Contractors:	

17 SAFETY		18 COSTS in CAN\$		19 WEA* WIND Sp Time of Survey: 6:00 Temp: 9 deg Visibility: CLEAR		20 COMPANY REP.	
DRILLS:		DAILY:		33 Knt	Direction: E	Barometer (Mb):	
DAYS SINCE LAST LTA:	300	CUMULATIVE:	0.0% of AFE			TOTAL: 15	
						Stan Stafford	

1 PENETRATION								2 BITS					DULL					3 PARAMETERS							
Type	RUN N°	DEPTH Start	OPERATION		R.O.P. m/h	CUMUL		Diameter	BIT Maker	BIT Type	IADC Code	Serial N°	Jets or TFA	CUT. STRUCT.				OTHERS				WOB daN	RPM	Flow l/min	Pres. kPa
Oper.			Mtrs	Hours		Mtrs	Hours							I	O	D	L	B	G	O	R				

4 DRILL STRING ASSEMBLY			

5 DOWN HOLE TOOLS			6 DEVIATION SURVEYS			
Diam. + Type	Hrs	Cum.	Type	N°	Depth	Inc. Az.

7 MUD	
TYPE:	Gel / Chem
Mixed (m3)	Den
Dumped (m3)	YP
Form. Losses (m3)	PV
Surf. Losses (m3)	Gel10s
Solids (%)	Gel10m
Oil (%)	Fun Vis
Water (%)	F/L Temp
O/W ratio	pH
Filtrate API	Fluid los
Filtrate HP/HT	Chloride
	Calcium

8 OPERATIONS & TIME ANALYSIS:				
FROM	TO	HOURS	CODE	DESCRIPTION
6:00	6:00	24.00	SF	WAIT ON 3.50" DRILL PIPE AND MILLING TOOLS
		24.00		

9 REMARKS
 Conduct daily walk around inspection.
 Conduct safety meetings with rig crews discuss general operations.

WHEN MILLING ML PACKER AND IT IS FREE AND GOSE TO BOTTOM DO WE NEED TO FISH IT OUT

12 BASIC To	
From	Formation Rock Type

10 PRODUCTS			
	Unit	In (+) / Used (-)	Stock
Barite	sxs		
Bentonite	sxs		
Soda Ash	sxs		
Sapp	sxs		
Kwik Seal F	sxs		
Potassium Chloride	sxs		
Lignite	sxs		
DeFoam X	sxs		
Poly Plus RD	sxs		
Sawdust	sxs		
Caustic Soda	sxs		
Poly Pac UL	sxs		
Lignosulphonate	sxs		
Bicarb	sxs		
Cellophane	sxs		
Mica-F	sxs		
Drilling detergent	sxs		
Kalzan	sxs		
DD 2000	Pails		

11 SUMMARY OF OPERATIONS

13 WELL STATUS at 06:00
 WAIT ON 3.50" DRILL PIPE AND MILLING TOOLS

16 OPERATIONS PLANNED
 PICK UP 3.50" DRILL PIPE AND MILLING TOOLS..

17 SAFETY
 DRILLS:
 DAYS SINCE LAST LTA: 299

18 COSTS in CANS
 DAILY:
 CUMULATIVE: 0.0% of AFE

14 FREIGHT ARRIVAL & DEPARTURE				
HAULER	FREIGHT	Arrival	Depart.	Destination

19 WEA* WIND Sp Time of Survey: 6:00 Temp: 14 deg Visibility: O/C/AST
 2 Knt Direction: S/W Barometer (Mb):

15 PERSONNEL
 Company: 2
 Drilling Contractors: 13
 Service Contractors:
TOTAL: 15

20 COMPANY REP.
 Stan Stafford

1 PENETRATION								2 BITS				DULL								3 PARAMETERS					
Type Oper.	RUN N°	DEPTH Start	OPERATION Mtrs	Hours	R.O.P. m/h	CUMUL Mtrs Hours		Diameter	BIT Maker	BIT Type	IADC Code	Serial N°	Jets or TFA	CUT. STRUCT.				OTHERS				WOB daN	RPM	Flow l/min	Pres. kPa
														I	O	D	L	B	G	O	R				

4 DRILL STRING ASSEMBLY												5 DOWN HOLE TOOLS			6 DEVIATION SURVEYS					7 MUD																				
												Diam. + Type	Hrs	Cum.	Type	N°	Depth	Inc.	Az.	TYPE: Gel / Chem																				
																				Mixed (m3)	Den	Dumped (m3)	YP	Form. Losses (m3)	PV	Surf. Losses (m3)	Gel10s	Solids (%)	Gel10m	Oil (%)	Fun Vis	Water (%)	F/L Temp	O/W ratio	pH	Filtrate API	Fluid los:	Filtrate HP/HT	Chloride	Calcium

8 OPERATIONS & TIME ANALYSIS:					9 REMARKS												10 PRODUCTS																																																															
FROM	TO	HOURS	CODE	DESCRIPTION	Conduct daily walk around inspection. Conduct safety meetings with rig crews discuss general operations.														In (+) /	Stock																																																												
8:00	8:00	24.00	SF	WAIT ON 3.50" DRILL PIPE AND MILLING TOOLS													Unit	Used (-)	Stock																																																													
		24.00															Barite	sxs			Bentonite	sxs			Soda Ash	sxs			Sapp	sxs			Kwik Seal F	sxs			Potassium Chloride	sxs			Lignite	sxs			DeFoam X	sxs			Poly Plus RD	sxs			Sawdust	sxs			Caustic Soda	sxs			Poly Pac UL	sxs			Lignosulphonate	sxs			Bicarb	sxs			Cellophane	sxs			Mica-F	sxs		

11 SUMMARY OF OPERATIONS					14 FREIGHT ARRIVAL & DEPARTURE					15 PERSONNEL			
13 WELL STATUS at 06:00 WAIT ON 3.50" DRILL PIPE AND MILLING TOOLS					HAULER	FREIGHT	Arrival	Depart.	Destination	Company: Drilling Contractors: Service Contractors:			
16 OPERATIONS PLANNED PICK UP 3.50" DRILL PIPE AND MILLING TOOLS..									TOTAL:				
17 SAFETY DRILLS: DAYS SINCE LAST LTA: 299		18 COSTS DAILY: CUMULATIVE:			19 WEA* WIND Sp Time of Survey: 6:00 Temp: 11 deg Visibility: RAIN: 16 Knt Direction: E Barometer (Mb):				20 COMPANY REP. Stan Stafford				
		in CAN\$											
		0.0% of AFE											

1 PENETRATION								2 BITS				DULL				3 PARAMETERS									
Type Oper.	RUN N°	DEPTH Start	OPERATION Mtrs	Hours	R.O.P. m/h	CUMUL Mtrs	Hours	Diameter	BIT Maker	BIT Type	IADC Code	Serial N°	Jets or TFA	CUT. STRUCT.				OTHERS				WOB daN	RPM	Flow l/min	Pres. kPa
														I	O	D	L	B	G	O	R				

4 DRILL STRING ASSEMBLY								5 DOWN HOLE TOOLS				6 DEVIATION SURVEYS				7 MUD											
								Diam. + Type				Hrs				Cum.				TYPE:				Gel / Chem			
																				Mixed (m3)				Den YP			

8 OPERATIONS & TIME ANALYSIS:					9 REMARKS	10 PRODUCTS																																																															
FROM	TO	HOURS	CODE	DESCRIPTION																																																																	
6:00				RUN IN WITH OVER SHOT ON 127mm DRILL PIPE	<p>Conduct daily walk around inspection. Conduct safety meetings with rig crews discuss general operations.</p> <p>SHEAR PACKER WITH 4,000 LBS SHEAR ANCHOR WITH 40,000 LBS, WHEN AT SURFACE WITH F.H.PACKER THE F.W.G. PLUG THAT WAS SET IN THE ON/OFF @ 2316m IS MISSING RECOVER 208.5mm F.H.PACKER AND EXPANSION JOINT AND BAKER ML. ORODUCTION ANCHOR /AND 2/JOINTS 88.9mm TUBING</p> <p>WHERE DO WE SEND F.H. PACKER TO BE SERVICED AND ON /OFF TOOL</p> <p>PRESSURE TEST 127mm PIPE RAMS # 1 # 2 KILL LINE VALVES H.C.R. LOW 3500 KPA HIGH 17,250 KPA 10/MINS EACH OK. PRESSURE TEST HYDRIL TO 7,000 KPA HELD BOP DRILL WITH RIG CREW</p>	<table border="1" style="width:100%; border-collapse: collapse;"> <tr> <th>Unit</th> <th>In (+) / Used (-)</th> <th>Stock</th> </tr> <tr><td>Banite</td><td>sxs</td><td></td></tr> <tr><td>Bentonite</td><td>sxs</td><td></td></tr> <tr><td>Soda Ash</td><td>sxs</td><td></td></tr> <tr><td>Sapp</td><td>sxs</td><td></td></tr> <tr><td>Kwik Seal F</td><td>sxs</td><td></td></tr> <tr><td>Potassium Chloride</td><td>sxs</td><td></td></tr> <tr><td>Lignite</td><td>sxs</td><td></td></tr> <tr><td>DeFoam X</td><td>sxs</td><td></td></tr> <tr><td>Poly Plus RD</td><td>sxs</td><td></td></tr> <tr><td>Sawdust</td><td>sxs</td><td></td></tr> <tr><td>Caustic Soda</td><td>sxs</td><td></td></tr> <tr><td>Poly Pac UL</td><td>sxs</td><td></td></tr> <tr><td>Lignosulphonate</td><td>sxs</td><td></td></tr> <tr><td>Bicarb</td><td>sxs</td><td></td></tr> <tr><td>Cellophane</td><td>sxs</td><td></td></tr> <tr><td>Mica-F</td><td>sxs</td><td></td></tr> <tr><td>Drilling detergent</td><td>sxs</td><td></td></tr> <tr><td>Kalzan</td><td>sxs</td><td></td></tr> <tr><td>DD 2000</td><td>Pails</td><td></td></tr> </table>				Unit	In (+) / Used (-)	Stock	Banite	sxs		Bentonite	sxs		Soda Ash	sxs		Sapp	sxs		Kwik Seal F	sxs		Potassium Chloride	sxs		Lignite	sxs		DeFoam X	sxs		Poly Plus RD	sxs		Sawdust	sxs		Caustic Soda	sxs		Poly Pac UL	sxs		Lignosulphonate	sxs		Bicarb	sxs		Cellophane	sxs		Mica-F	sxs		Drilling detergent	sxs		Kalzan	sxs		DD 2000	Pails	
Unit	In (+) / Used (-)	Stock																																																																			
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Kalzan	sxs																																																																				
DD 2000	Pails																																																																				
18:00	18:00	12.00	D	WAS OVER SHOT ON TO PACKER/ SHEAR PACKER/ PULL UP SHEAR ANCHOR/ TRIP OUT OF HOLE WITH F.H. PACKER AND ANCHOR LAY DOWN F.H. PACKER AND BOTTOM ASSY,																																																																	
	21:00	3.00	D	RUN IN 10 STANDS PICK UP 244.5mm HURRICANE PACKER SET @ 15m PRESSURE TEST 127mm PIPE RAMS AND SPOOL BE LOW PIPE RAMS LOW 3500 KPA HIGH 17,250 KPA 10/MINS EACH OK.																																																																	
	21:00	8.00	D	PULL HURRICANE PACKER LAY IT DOWN LAY DOWN 47 JOINTS 127mm DRILL PIPE RUN HOLE WITH 196 JOINTS 127mm DRILL PIPE AND IN STALL CASING PROTECTOR RUBBERS ON EVERY SEC/ JOINT OF DRILL PIPE																																																																	
	5:00	1.00	SF																																																																		
24.00																																																																					

11 SUMMARY OF OPERATIONS					14 FREIGHT ARRIVAL & DEPARTURE				15 PERSONNEL			
PICK UP 88.9mm H.W.DRILL PIPE TO MILL ML. PACKER @ 2360m					HAULER FREIGHT Arrival Depart. Destination				Company: 2			
									Drilling Contractors: 13			
									Service Contractors:			

13 WELL STATUS at 06:00					16 OPERATIONS PLANNED				19 WEA WIND				20 COMPANY REP.			
WAIT ON 3.50" DRILL STRING					RUN IN WITH 88.9mm H.W.DRILLPIPE AND MILL TO MILL PACKER M.L. PACKER				Sp Time of Survey: 6:00 Temp: 12 deg Visibility: O/CAST				TOTAL: 15			
					4 km/h Direction: SW Barometer (Mb):				Stan Stafford							

17 SAFETY					18 COSTS				
DRILLS: DAYS SINCE LAST LTA: 299					in CAN\$ DAILY: CUMULATIVE: 0.0% of AFE				



CANADIAN IMPERIAL VENTURE CORPORATION
 ONSHORE DAILY DRILLING REPORT
 Garden Hill

Well : **garden hill # 1** Rig : **Simmon's 31** Date : **JULY 12/02** Days Since Spud:
 Current depth: Phase: since: Casing size: Shoe: F.I.T. at shoe:
 Bottom hole: PBTD:

1 PENETRATION						2 BITS						DULL						3 PARAMETERS					
Type Oper.	RUN N°	DEPTH Start	OPERATION Mtrs	R.O.P. Hours	CUMUL Mtrs	Diameter	BIT Maker	BIT Type	IADC Code	Serial N°	Jets or TFA	CUT. STRUCT.				OTHERS				WOB daN	RPM	Flow l/min	Pres. kPa
												I	O	D	L	B	G	O	R				

4 DRILL STRING ASSEMBLY			
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5 DOWN HOLE TOOLS			6 DEVIATION SURVEYS					7 MUD	
Diam. + Type	Hrs	Cum.	Type	N°	Depth	Inc.	Az.	TYPE: Gel / Chem	

8 OPERATIONS & TIME ANALYSIS:				
FROM	TO	HOURS	CODE	DESCRIPTION
6:00	14:00	8.00	D	LAY DOWN 88.9mm TUBING AND SPOOL 3/8" INJECTION LINE
			D	REMOVE CAMERON INJECTOR CLAMPS
14:00	16:00	2.00	D	LOAD OUT F.I.CANADA POWER TONGS RIG IMPORT TOOL EQUIPMENT
16:00	6:00	14.00	D	PICK UP 127mm DRILL PIPE RUN IN WITH OVER SHOT TO RECOVER F/H/ PACKER
		24.00		

9 REMARKS									
Conduct daily walk around inspection.									
Conduct safety meetings with rig crews discuss general operations.									
TOTAL TUBING PULLED FROM HOLE 241 JOINTS									
TOTAL CAMERON INJECTOR CLAMPS/244									
TOTAL KEEPER PINS FOT CLAMPS 288									
TUBING WILL NEED TO BE INSPECTED/BEFOR IT IS RUB BACK IN HOLE									
10 PRODUCTS					Unit	In (+) / Used (-)	Stock		
Barite		sxs							
Bentonite		sxs							
Soda Ash		sxs							
Sapp		sxs							
Kwik Seal F		sxs							
Potassium Chloride		sxs							
Lignite		sxs							
DeFoam X		sxs							
Poly Plus RD		sxs							
Sawdust		sxs							
Caustic Soda		sxs							
Poly Pac UL		sxs							
Lignosulphonate		sxs							
Bicarb		sxs							
Cellophane		sxs							
Mica-F		sxs							
Drilling detergent		sxs							
Kalzan		sxs							
DD 2000		Pails							

11 SUMMARY OF OPERATIONS
 RUN IN WITH 127mm DRILL PIPE WITH OVER SHOT TO RECOVER F.H. PACKER

13 WELL STATUS at 06:00
 PICK UP 127mm DRILL PIE

16 OPERATIONS PLANNED
 RUN IN WITH OVER SHOT WASH ON TO PACKER FISHING NECK/ PULL PACKER OUT

17 SAFETY
 DRILLS:
 DAYS SINCE LAST LTA: 3

18 COSTS in CAN\$
 DAILY:
 CUMULATIVE: 0.0% of AFE

12 BASIC To				
From	Formation	Rock Type		

14 FREIGHT ARRIVAL & DEPARTURE

HAULER	FREIGHT	Arrival	Depart.	Destination
--------	---------	---------	---------	-------------

19 WEA* WIND Sp Time of Survey: 6.00 9 DEG Visibility: O/CAST:
 0.11 Knt Direction: N/WEST Barometer (Mb):

15 PERSONNEL
 Company: 2
 Drilling Contractors: 11
 Service Contractors: 2
 TOTAL: 15
 20 COMPANY REP. Stan Stafford

Attachment B: DST #1 Port au Port (Baker Report)



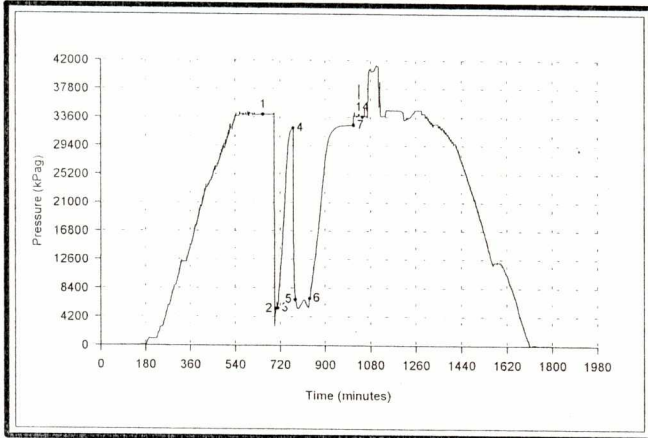
PORT AU PORT 1

Baker Oil Tools

DST# 1

Formation: AGUATHUNA
 Interval - from: 3335.00 to: 3465.00 m

Recorder# 80142 at 3340.00 m



Test Date: 2002-08-08
 Test Type: CASING PACKER
 Tester Name: BRIAN MAGNUS
 Drill Pipe O.D.: 102.00 mm
 Drill Collar I.D.: 0.00 mm
 Drill Collar Length: 471.25 m
 Hole Size: 0.00 mm

Blow Description:

No air blow.

Strong air blow immediately then decreasing throughout. Gas to surface immediately.

Remarks:

Mechanically successful test. Results suggest relatively low permeability within the interval tested.

Maximum Btm Hole Temperature @ FSI: 55.3 C

		Pressure (kPag)	Time (min)	Extrapolated Pressure (kPag)
1	Initial Hydrostatic	34000		
2	Start of 1st Flow	5384		
3	End of 1st Flow	5443	6.8	
4	End of 1st Shut-in	31991	62.5	
5	Start of 2nd Flow	6702		
6	End of 2nd Flow	6877	56.8	
7	End of 2nd Shut-in	32444	173.8	32866.8
14	Final Hydrostatic	33702		

Liquid Recovery of 1700.00 m

Test was reversed out.

Recovery	Description	Salinity
1700.00 m	GASIFIED MUD	

PORT AU PORT 1

DST #: 1
Recorder: 80242

Pressure (kPag) at Critical Points:

2:	46	6:	6658
3:	4067	7:	8484
5:	4226		

Recovery recorder



PORT AU PORT 1

DST #: 1
Recorder: 80142

Pressure (kPag) at Critical Points:

1: 34000	4: 31991	7: 32444
2: 5384	5: 6702	14: 33702
3: 5443	6: 6877	



PORT AU PORT 1

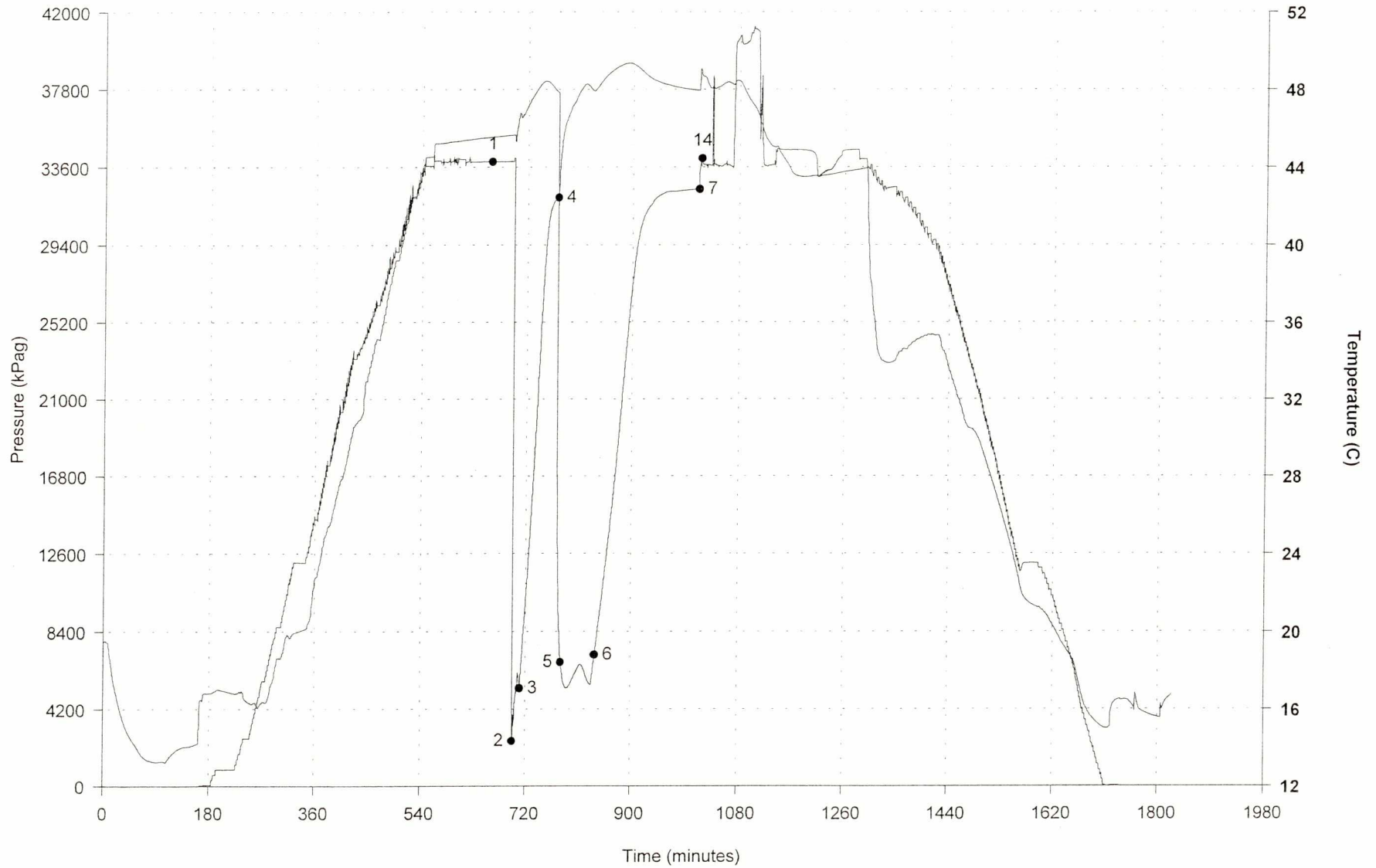
DST #: 1

Recorder: 80121

Pressure (kPag) at Critical Points:

1: 33899	4: 31964	7: 32411
2: 2469	5: 6743	14: 34073
3: 5342	6: 7146	

Other outside gauge

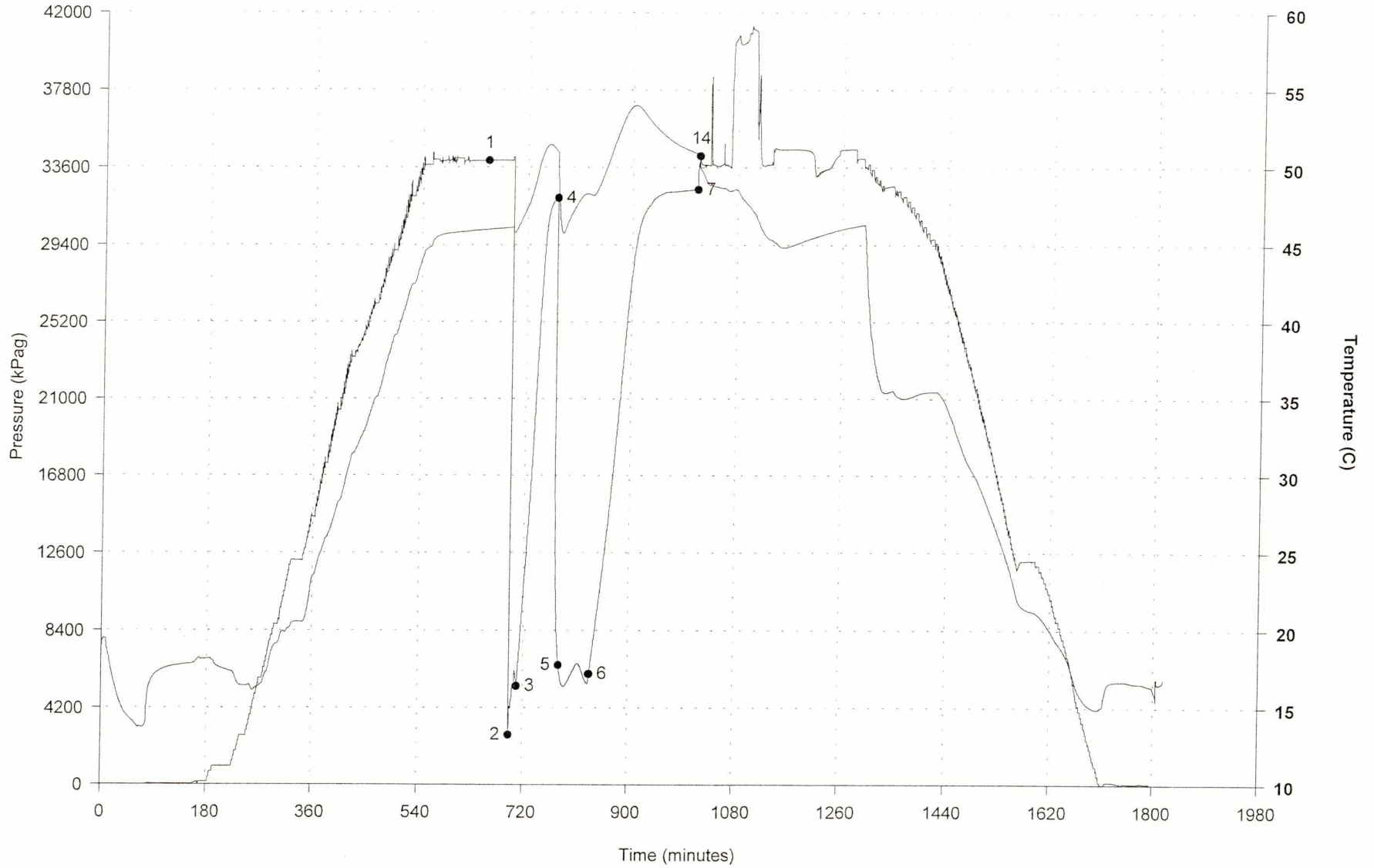


PORT AU PORT 1

DST #: 1
Recorder: 80129

Pressure (kPag) at Critical Points:
1: 33955 4: 31942 7: 32396
2: 2728 5: 6526 14: 34222
3: 5392 6: 6046

Other outside gauge

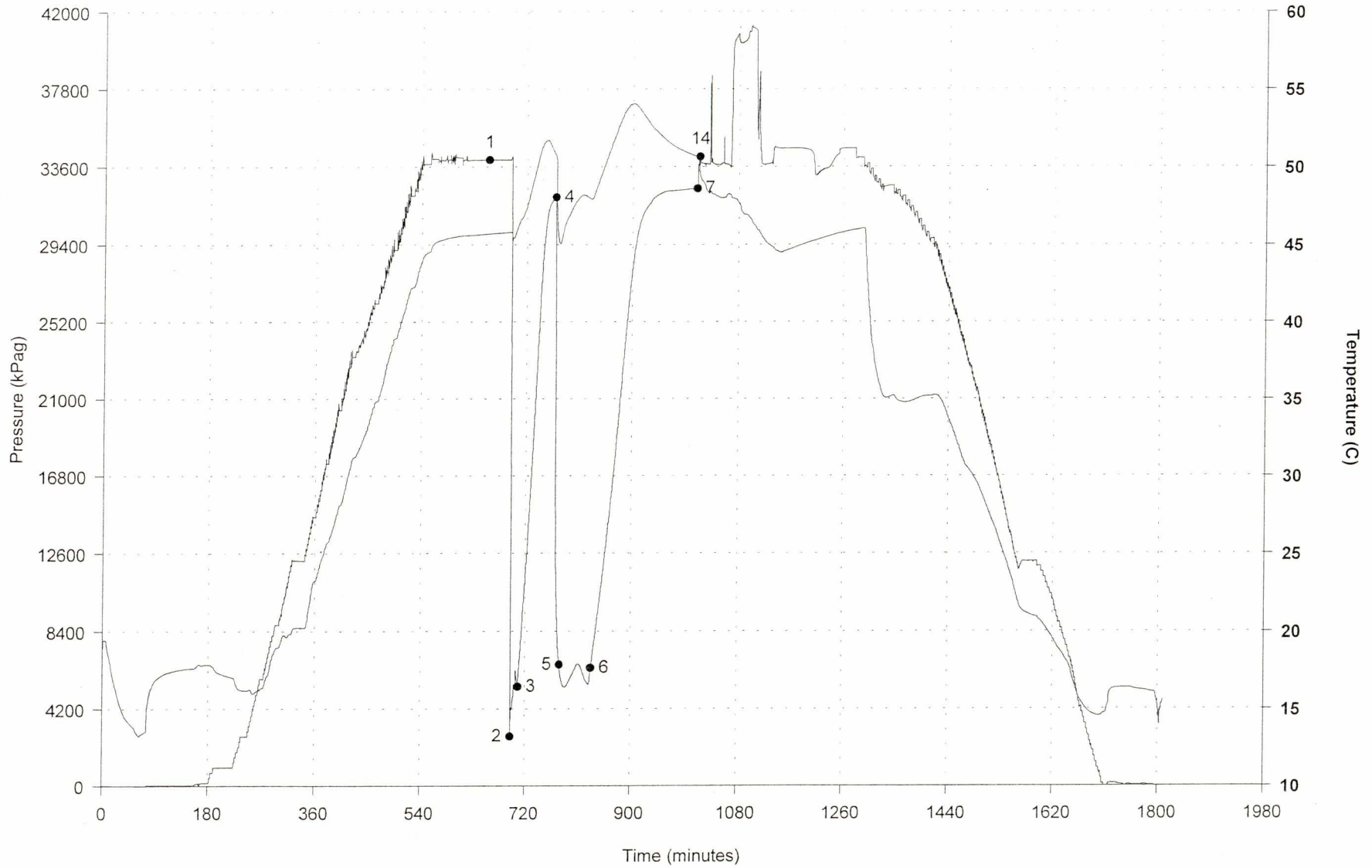


PORT AU PORT 1

DST #: 1
Recorder: 80383

Pressure (kPag) at Critical Points:
 1: 33971 4: 31962 7: 32416
 2: 2708 5: 6603 14: 34141
 3: 5416 6: 6424

Above interval



PORT AU PORT 1

DST# 1 Recorder 80142

Build-up and Flow Curve Increments

Flow# 1

Chart Label	Time (min)	Pressure (kPag)
2	0.0	5384
	0.5	5425
	1.0	5317
	1.5	5303
	2.0	5360
	2.5	5696
	3.0	6030
	3.5	6354
	4.0	6207
	4.5	6012
	5.0	5875
	5.5	5747
	6.0	5608
	6.5	5501
	3	6.8

Shutin# 1

Chart Label	Time (min)	Delta P (kPag)	Pressure (kPag)	Abscissa (T+dT)/dT	Pressure ² (kPag ² /10 ⁶)	Used for Extrap
	0.0		5443		29.6213	
	1.0	446	5888	7.7500	34.6700	
	2.0	938	6381	4.3750	40.7130	
	3.0	1421	6863	3.2500	47.1070	
	4.0	1898	7340	2.6875	53.8819	
	5.0	2374	7817	2.3500	61.1059	
	6.0	2850	8293	2.1250	68.7673	
	7.0	3326	8768	1.9643	76.8795	
	8.0	3802	9245	1.8438	85.4656	
	9.0	4281	9724	1.7500	94.5496	
	10.0	4761	10204	1.6750	104.1115	
	11.0	5243	10685	1.6136	114.1786	
	12.0	5733	11175	1.5625	124.8822	
	13.0	6227	11669	1.5192	136.1689	
	14.0	6728	12170	1.4821	148.1180	
	15.0	7239	12682	1.4500	160.8234	
	16.0	7756	13199	1.4219	174.2066	
	17.0	8286	13729	1.3971	188.4796	
	18.0	8826	14269	1.3750	203.5999	
	19.0	9377	14820	1.3553	219.6217	
	20.0	9942	15385	1.3375	236.6906	
	21.0	10521	15963	1.3214	254.8305	
	22.0	11113	16555	1.3068	274.0791	
	23.0	11721	17164	1.2935	294.5948	
	24.0	12348	17790	1.2812	316.4865	
	25.0	12988	18431	1.2700	339.6878	
	26.0	13644	19086	1.2596	364.2878	
	27.0	14318	19761	1.2500	390.4980	
	28.0	15007	20449	1.2411	418.1745	
	29.0	15704	21146	1.2328	447.1694	
	30.0	16409	21852	1.2250	477.4910	
	31.0	17115	22557	1.2177	508.8363	
	32.0	17816	23259	1.2109	540.9621	
	33.0	18509	23951	1.2045	573.6573	
	34.0	19193	24636	1.1985	606.9120	
	35.0	19864	25307	1.1929	640.4419	
	36.0	20516	25959	1.1875	673.8586	
	37.0	21145	26587	1.1824	706.8908	

Note: Increment listing is filtered to include critical data only. Complete time/pressure data are available in electronic or printed format.

PORT AU PORT 1

DST# 1 Recorder 80142

Build-up and Flow Curve Increments

Shutin# 1

Chart Label	Time (min)	Delta P (kPag)	Pressure (kPag)	Abscissa (T+dT)/dT	Pressure ² (kPag ² /10 ⁶)	Used for Extrap
	38.0	21747	27189	1.1776	739.2487	
	39.0	22323	27766	1.1731	770.9432	
	40.0	22869	28312	1.1687	801.5609	
	41.0	23375	28818	1.1646	830.4654	
	42.0	23823	29266	1.1607	856.4824	
	43.0	24218	29660	1.1570	879.7201	
	44.0	24573	30015	1.1534	900.9205	
	45.0	24888	30331	1.1500	919.9577	
	46.0	25159	30602	1.1467	936.4580	
	47.0	25394	30836	1.1436	950.8672	
	48.0	25589	31032	1.1406	962.9573	
	49.0	25750	31193	1.1378	972.9923	
	50.0	25883	31326	1.1350	981.2976	
	51.0	25994	31436	1.1324	988.2507	
	52.0	26087	31530	1.1298	994.1223	
	53.0	26168	31611	1.1274	999.2410	
	54.0	26236	31679	1.1250	1003.5425	
	55.0	26294	31737	1.1227	1007.2105	
	56.0	26341	31783	1.1205	1010.1650	
	57.0	26383	31825	1.1184	1012.8406	
	58.0	26418	31861	1.1164	1015.1091	
	59.0	26455	31898	1.1144	1017.4765	
	60.0	26488	31931	1.1125	1019.5783	
	61.0	26517	31959	1.1107	1021.3811	
	62.0	26542	31985	1.1089	1023.0291	
4	62.5	26548	31991	1.1080	1023.4097	

Flow# 2

Chart Label	Time (min)	Pressure (kPag)
5	0.0	6702
	0.8	6482
	1.5	6297
	2.2	6123
	3.0	5974
	3.8	5846

Shutin# 2

Chart Label	Time (min)	Delta P (kPag)	Pressure (kPag)	Abscissa (T+dT)/dT	Pressure ² (kPag ² /10 ⁶)	Used for Extrap
	0.0		6877		47.2918	
	1.8	462	7339	37.2857	53.8645	
	3.5	922	7799	19.1429	60.8227	
	5.2	1380	8257	13.0952	68.1804	
	7.0	1839	8716	10.0714	75.9686	
	8.8	2302	9179	8.2571	84.2561	

Note: Increment listing is filtered to include critical data only. Complete time/pressure data are available in electronic or printed format.

PORT AU PORT 1

DST# 1 Recorder 80142

Build-up and Flow Curve Increments

Flow# 2

Shutin# 2

Chart Label	Time (min)	Pressure (kPag)
	4.5	5741
	5.2	5654
	6.0	5585
	6.8	5530
	7.5	5488
	8.2	5454
	9.0	5432
	9.8	5420
	10.5	5419
	11.2	5424
	12.0	5438
	12.8	5461
	13.5	5489
	14.2	5524
	15.0	5562
	15.8	5603
	16.5	5645
	17.2	5691
	18.0	5739
	18.8	5788
	19.5	5840
	20.2	5890
	21.0	5941
	21.8	5991
	22.5	6040
	23.2	6089
	24.0	6138
	24.8	6186
	25.5	6233
	26.2	6281
	27.0	6330
	27.8	6379
	28.5	6429
	29.2	6479
	30.0	6531
	30.8	6582
	31.5	6624
	32.2	6653

Chart Label	Time (min)	Delta P (kPag)	Pressure (kPag)	Abscissa (T+dT)/dT	Pressure ² (kPag ² /10 ⁶)	Used for Extrap
	10.5	2768	9645	7.0476	93.0272	
	12.2	3239	10116	6.1837	102.3391	
	14.0	3715	10592	5.5357	112.1901	
	15.8	4201	11078	5.0317	122.7199	
	17.5	4695	11572	4.6286	133.9138	
	19.2	5195	12072	4.2987	145.7246	
	21.0	5706	12583	4.0238	158.3199	
	22.8	6226	13102	3.7912	171.6749	
	24.5	6755	13632	3.5918	185.8222	
	26.2	7296	14173	3.4190	200.8713	
	28.0	7849	14726	3.2679	216.8511	
	29.8	8412	15289	3.1345	233.7496	
	31.5	8988	15865	3.0159	251.7001	
	33.2	9575	16452	2.9098	270.6610	
	35.0	10175	17052	2.8143	290.7729	
	36.8	10791	17668	2.7279	312.1606	
	38.5	11423	18300	2.6494	334.8731	
	40.2	12072	18949	2.5776	359.0648	
	42.0	12739	19616	2.5119	384.7784	
	43.8	13420	20297	2.4514	411.9780	
	45.5	14114	20991	2.3956	440.6373	
	47.2	14819	21696	2.3439	470.7192	
	49.0	15522	22399	2.2959	501.7251	
	50.8	16219	23096	2.2512	533.4126	
	52.5	16905	23782	2.2095	565.5978	
	54.2	17579	24456	2.1705	598.1058	
	56.0	18238	25115	2.1339	630.7407	
	57.8	18874	25751	2.0996	663.1217	
	59.5	19485	26361	2.0672	694.9253	
	61.2	20068	26945	2.0367	726.0129	
	63.0	20620	27497	2.0079	756.0811	
	64.8	21138	28015	1.9807	784.8165	
	66.5	21614	28491	1.9549	811.7168	
	68.2	22051	28928	1.9304	836.8257	
	70.0	22447	29324	1.9071	859.8883	
	71.8	22802	29679	1.8850	880.8349	
	73.5	23117	29994	1.8639	899.6489	
	75.2	23387	30264	1.8439	915.9026	

Note: Increment listing is filtered to include critical data only. Complete time/pressure data are available in electronic or printed format.

PORT AU PORT 1

DST# 1 Recorder 80142

Build-up and Flow Curve Increments

Flow# 2

Chart Label	Time (min)	Pressure (kPag)
	33.0	6670
	33.8	6676
	34.5	6671
	35.2	6655
	36.0	6629
	36.8	6594
	37.5	6549
	38.2	6497
	39.0	6437
	39.8	6372
	40.5	6304
	41.2	6234
	42.0	6163
	42.8	6094
	43.5	6024
	44.2	5959
	45.0	5894
	45.8	5839
	46.5	5788
	47.2	5738
	48.0	5698
	48.8	5666
	49.5	5629
	50.2	5603
	51.0	5585
	51.8	5568
	52.5	5719
	53.2	5927
	54.0	6135
	54.8	6340
	55.5	6543
	56.2	6743
6	56.8	6877

Shutin# 2

Chart Label	Time (min)	Delta P (kPag)	Pressure (kPag)	Abscissa (T+dT)/dT	Pressure ² (kPag ² /10 ⁶)	Used for Extrap
	77.0	23622	30498	1.8247	930.1583	
	78.8	23827	30704	1.8063	942.7276	
	80.5	23999	30876	1.7888	953.3396	
	82.2	24147	31024	1.7720	962.4800	
	84.0	24273	31150	1.7560	970.3335	
	85.8	24382	31259	1.7405	977.1151	
	87.5	24480	31357	1.7257	983.2607	
	89.2	24567	31444	1.7115	988.7492	
	91.0	24645	31522	1.6978	993.6498	
	92.8	24713	31590	1.6846	997.9142	
	94.5	24775	31652	1.6720	1001.8560	
	96.2	24878	31755	1.6597	1008.3752	
	98.0	24973	31850	1.6480	1014.4209	
	99.8	25044	31921	1.6366	1018.9209	
	101.5	25097	31974	1.6256	1022.3289	
	103.2	25134	32011	1.6150	1024.7265	
	105.0	25175	32052	1.6048	1027.3413	
	106.8	25217	32094	1.5948	1030.0379	
	108.5	25253	32129	1.5853	1032.3030	
	110.2	25283	32160	1.5760	1034.2613	
	112.0	25302	32179	1.5670	1035.5100	
	113.8	25332	32209	1.5582	1037.4216	
	115.5	25359	32236	1.5498	1039.1637	*
	117.2	25384	32261	1.5416	1040.7935	*
	119.0	25407	32284	1.5336	1042.2488	*
	120.8	25423	32300	1.5259	1043.2992	*
	122.5	25438	32315	1.5184	1044.2698	*
	124.2	25447	32323	1.5111	1044.8066	*
	126.0	25450	32327	1.5040	1045.0592	*
	127.8	25449	32326	1.4971	1044.9654	*
	129.5	25450	32327	1.4903	1045.0241	*
	131.2	25452	32329	1.4838	1045.1654	*
	133.0	25455	32332	1.4774	1045.3533	*
	134.8	25458	32335	1.4712	1045.5513	*
	136.5	25462	32339	1.4652	1045.8011	*
	138.2	25466	32343	1.4593	1046.0923	*
	140.0	25472	32348	1.4536	1046.4222	*
	141.8	25477	32354	1.4480	1046.7803	*

Note: Increment listing is filtered to include critical data only. Complete time/pressure data are available in electronic or printed format.

PORT AU PORT 1

DST# 1 Recorder 80142

Build-up and Flow Curve Increments

Shutin# 2

Chart Label	Time (min)	Delta P (kPag)	Pressure (kPag)	Abscissa (T+dT)/dT	Pressure ² (kPag ² /10 ⁶)	Used for Extrap
	143.5	25483	32360	1.4425	1047.1413	*
	145.2	25488	32365	1.4372	1047.4944	*
	147.0	25494	32371	1.4320	1047.8864	*
	148.8	25500	32376	1.4269	1048.2317	*
	150.5	25505	32382	1.4219	1048.5823	*
	152.2	25511	32388	1.4171	1048.9746	*
	154.0	25516	32393	1.4123	1049.3173	*
	155.8	25521	32398	1.4077	1049.6524	*
	157.5	25528	32405	1.4032	1050.0990	*
	159.2	25533	32410	1.3987	1050.3851	*
	161.0	25537	32414	1.3944	1050.6688	*
	162.8	25542	32419	1.3902	1050.9780	*
	164.5	25546	32423	1.3860	1051.2718	*
	166.2	25550	32427	1.3820	1051.5245	*
	168.0	25555	32432	1.3780	1051.8315	*
	169.8	25559	32435	1.3741	1052.0608	*
	171.5	25562	32439	1.3703	1052.3054	*
	173.2	25566	32443	1.3665	1052.5711	*
7	173.8	25567	32444	1.3655	1052.6225	*

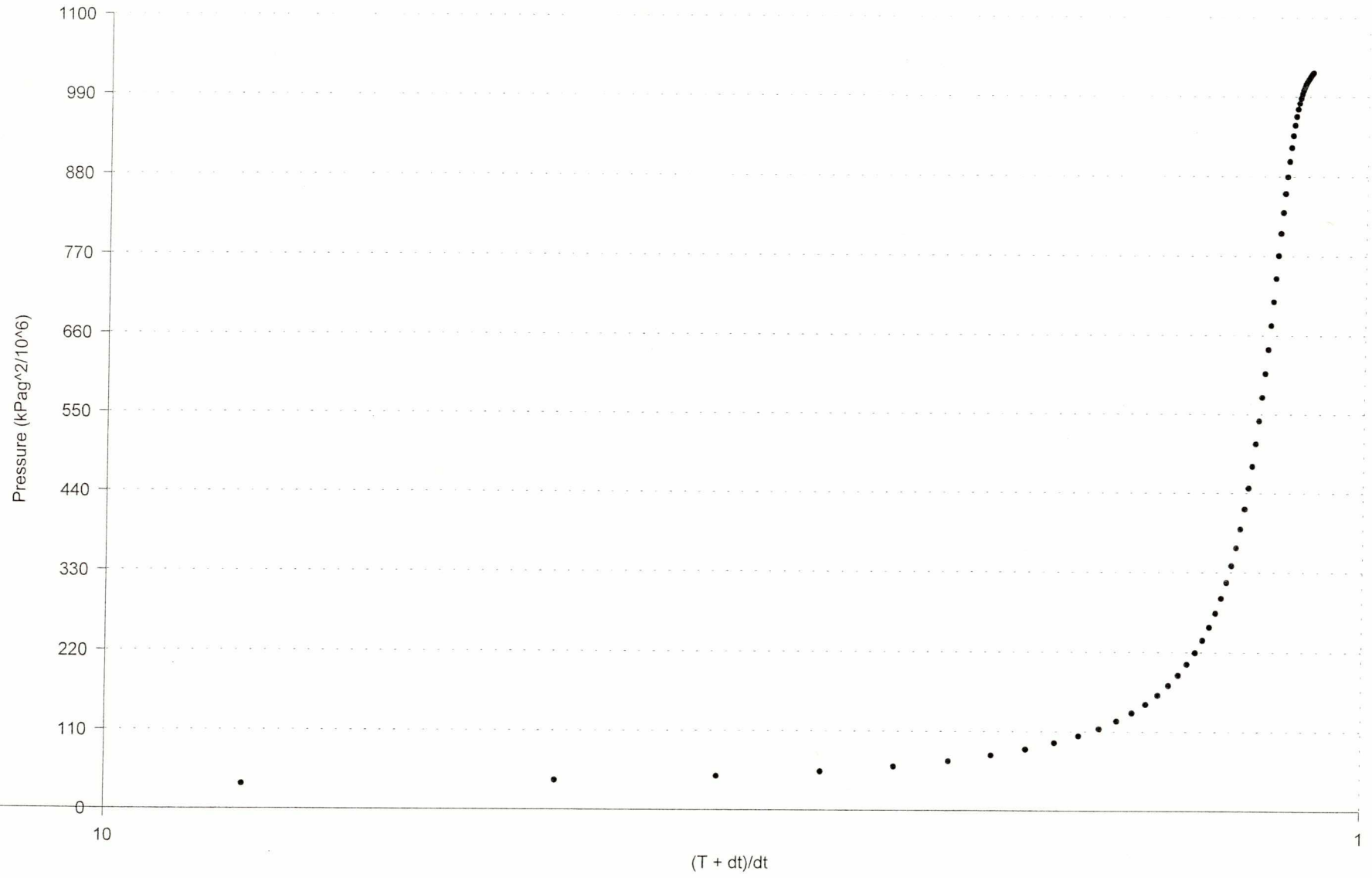
Horner Extrapolation

Shut-in#	Extrapolated Pressure (kPag)	Extrapolated Slope (kPag/cycle)
2	32866.8	205.20964

Note: Increment listing is filtered to include critical data only. Complete time/pressure data are available in electronic or printed format.

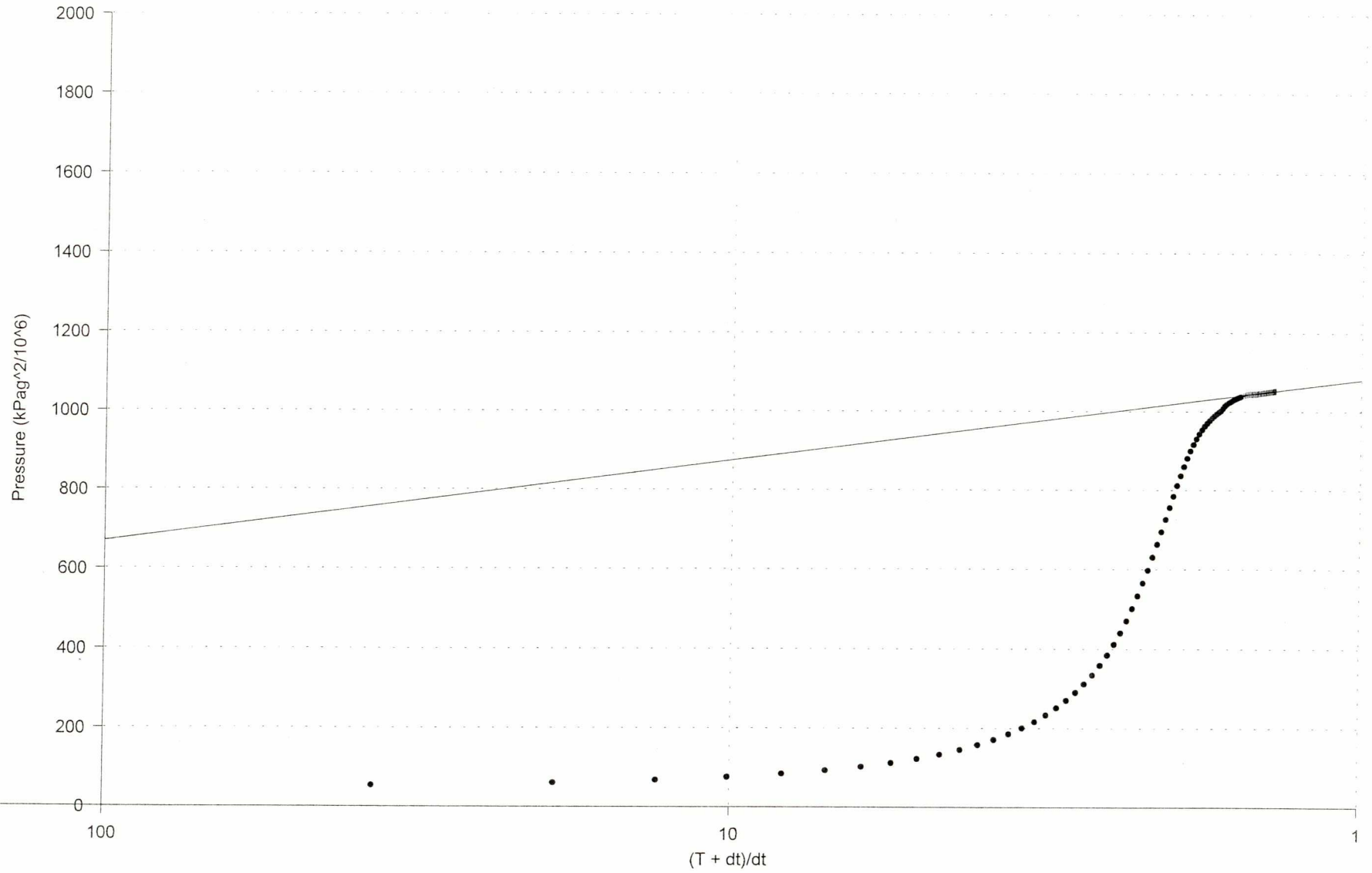
PORT AU PORT 1
DST #: 1
Recorder: 80142

Shut-in #1



PORT AU PORT 1
DST #: 1
Recorder: 80142

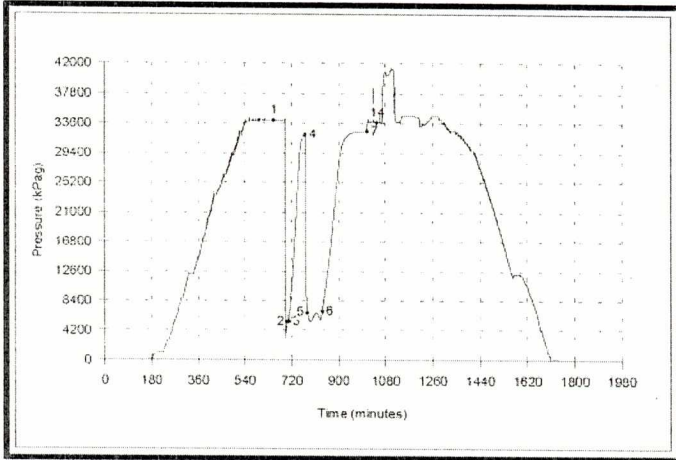
Shut-in #2
Slope = 205.21 kPag²/10⁶/cycle
Extrapolated Pressure = 32866.84 kPag



Baker Oil Tools

Formation: AGUATHUNA
Interval - from: 3335.00 to: 3465.00 m

Recorder# 80142 at 3340.00 m



Test Date: 2002-08-08
Test Type: CASING PACKER
Tester Name: BRIAN MAGNUS
Drill Pipe O.D.: 102.00 mm
Drill Collar I.D.: 0.00 mm
Drill Collar Length: 471.25 m
Hole Size: 0.00 mm

Blow Description:

No air blow.

Strong air blow immediately then decreasing throughout. Gas to surface immediately.

Remarks:

Mechanically successful test. Results suggest relatively low permeability within the interval tested.

Maximum Btm Hole Temperature @ FSI: 55.3 C

		Pressure (kPag)	Time (min)	Extrapolated Pressure (kPag)
1	Initial Hydrostatic	34000		
2	Start of 1st Flow	5384		
3	End of 1st Flow	5443	6.8	
4	End of 1st Shut-in	31991	62.5	
5	Start of 2nd Flow	6702		
6	End of 2nd Flow	6877	56.8	
7	End of 2nd Shut-in	32444	173.8	32866.8
14	Final Hydrostatic	33702		

Liquid Recovery of 1700.00 m

Test was reversed out.

Recovery	Description	Salinity
1700.00 m	GASIFIED MUD	

PORT AU PORT 1

DST #. 1

Recorder: 80242

Pressure (kPag) at Critical Points:

2:	46	6:	6658
3:	4067	7:	8484
5:	4226		

Recovery recorder



PORT AU PORT 1

DST # 1

Recorder: 80142

Pressure (kPag) at Critical Points:

1: 34000	4: 31991	7: 32444
2: 5384	5: 6702	14: 33702
3: 5443	6: 6877	

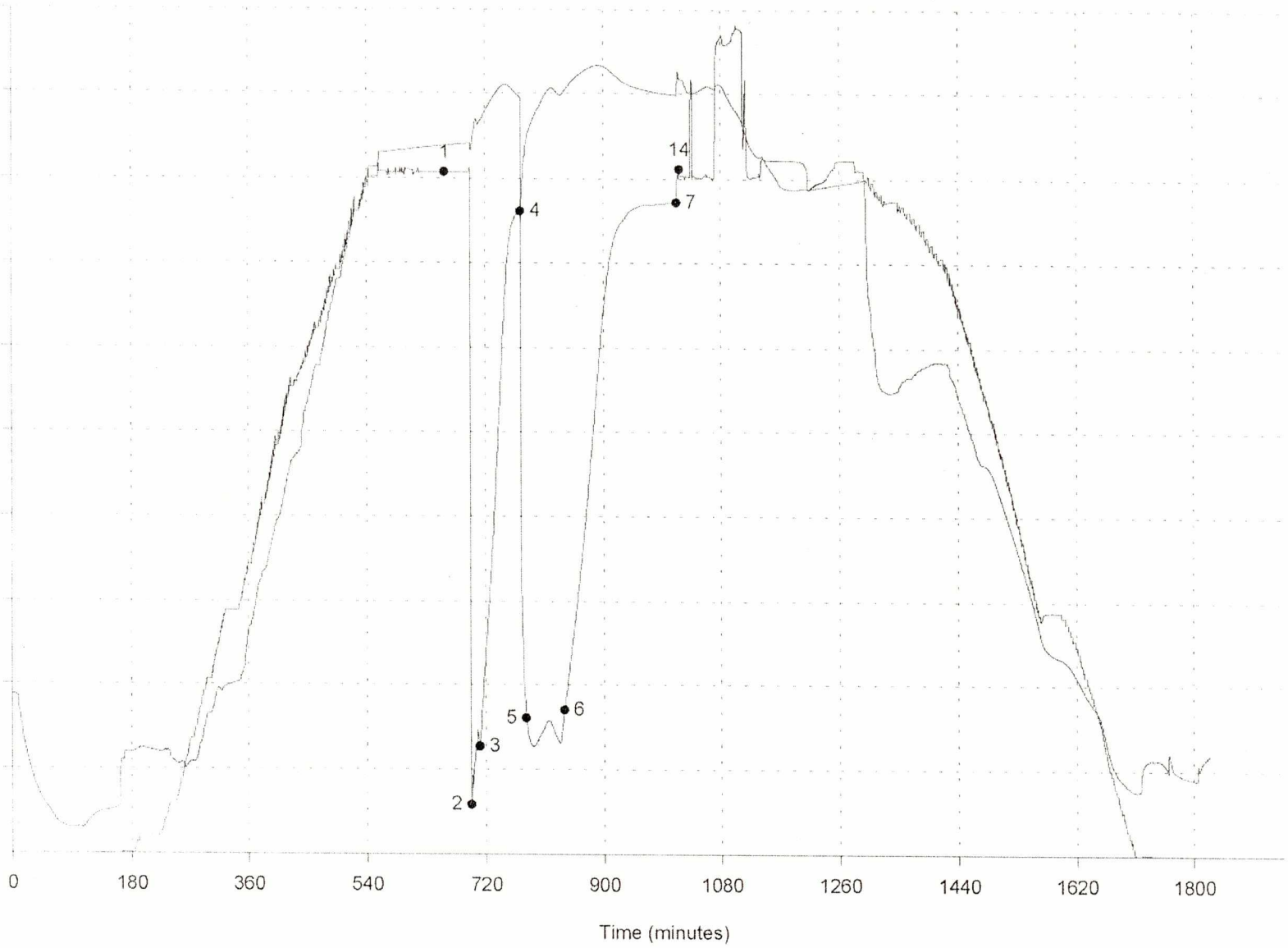


PORT AU PORT 1

DST #: 1
Recorder: 80121

Pressure (kPag) at Critical Point
1: 33899 4: 31964 7: 32411
2: 2469 5: 6743 14: 34073
3: 5342 6: 7146

Other outside gauge



PORT AU PORT 1

DST #: 1

Recorder: 80129

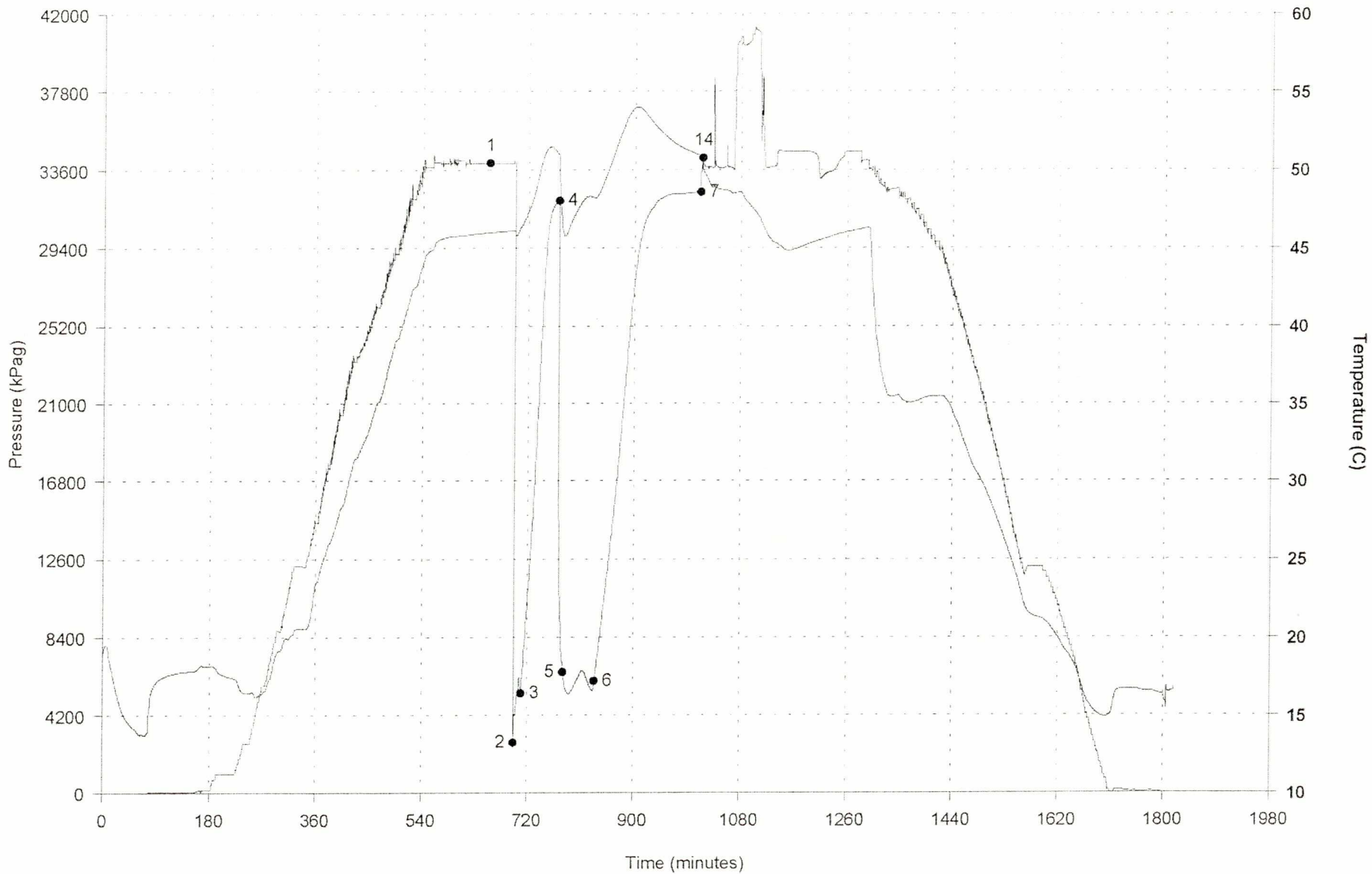
Pressure (kPag) at Critical Points:

1: 33955 4: 31942 7: 32396

2: 2728 5: 6526 14: 34222

3: 5392 6: 6046

Other outside gauge

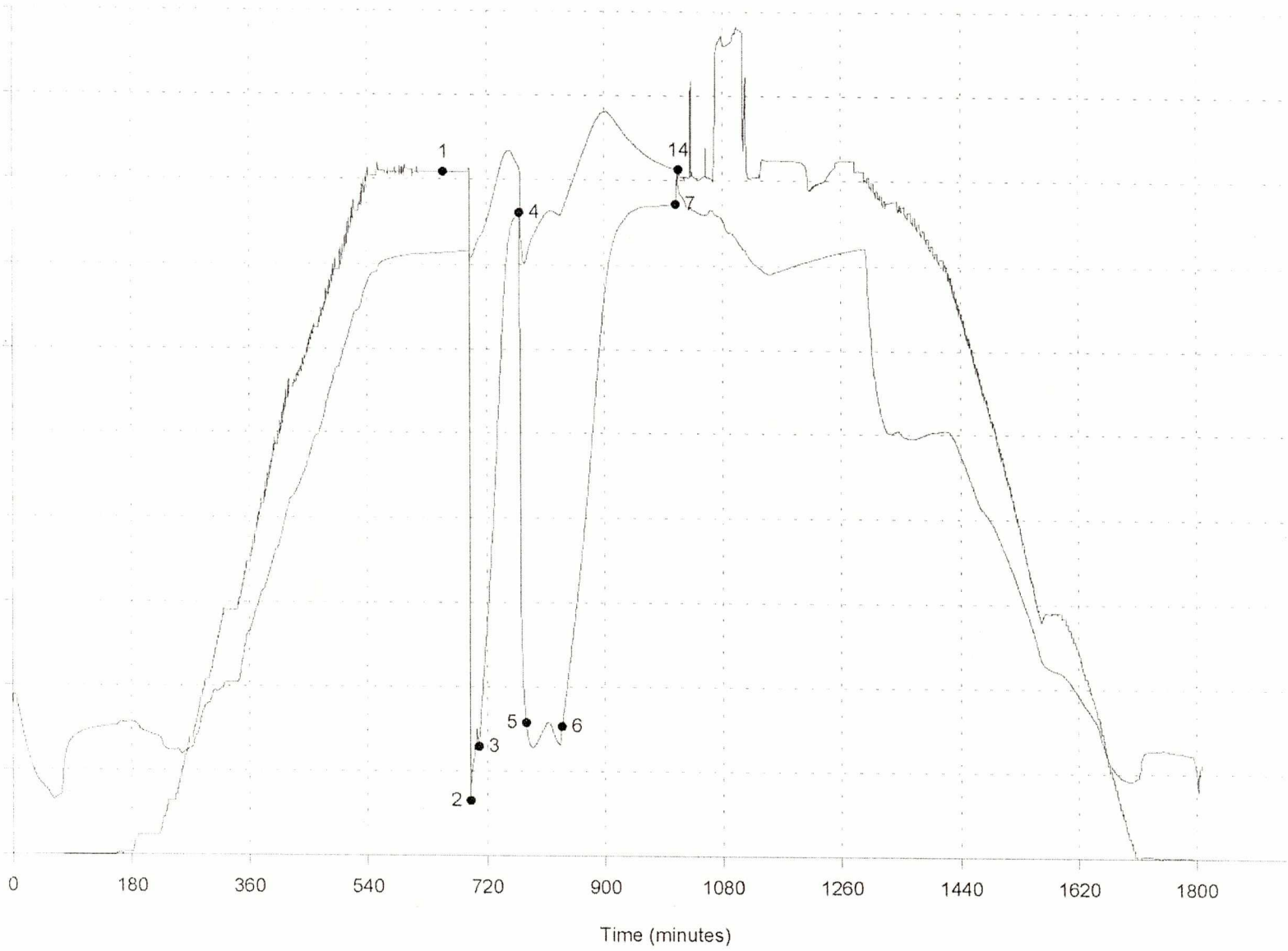


PORT AU PORT 1

DST #: 1
Recorder: 80383

Pressure (kPag) at Critical Point
1: 33971 4: 31962 7: 32416
2: 2708 5: 6603 14: 34141
3: 5416 6: 6424

Above interval



PORT AU PORT 1

DST#1 Recorder 80142

Build-up and Flow Curve Increments

Flow# 1

Chart Label	Time (min)	Pressure (kPag)	
2	0.	5384	
	0.	5425	
	1.	5317	
	1.	5303	
	2.	5360	
	2.	5696	
	3.	6030	
	3.	6354	
	4.	6207	
	4.	6012	
	5.	5875	
	5.	5747	
	6.	5608	
	6.	5501	
	3	6.	5443

Shutin# 1

Chart Label	Time (min)	Delta P (kPag)	Pressure (kPag)	Abscissa (T+dT)/dT	Pressure ² (kPag ² /10 ⁶)	Used for Extrap
	0.0		5443		29.6213	
	1.0	446	5888	7.7500	34.6700	
	2.0	938	6381	4.3750	40.7130	
	3.0	1421	6863	3.2500	47.1070	
	4.0	1898	7340	2.6875	53.8819	
	5.0	2374	7817	2.3500	61.1059	
	6.0	2850	8293	2.1250	68.7673	
	7.0	3326	8768		76.8795	
	8.0	3802	9245		85.4656	
	9.0	4281	9724		94.5496	
	10.0	4761	10204		104.1115	
	11.0	5243	10685		114.1786	
	12.0	5733	11175		124.8822	
	13.0	6227	11669		136.1689	
	14.0	6728	12170		148.1180	
	15.0	7239	12682		160.8234	
	16.0	7756	13199		174.2066	
	17.0	8286	13729		188.4796	
	18.0	8826	14269		203.5999	
	19.0	9377	14820		219.6217	
	20.0	9942	15385		236.6906	
	21.0	10521	15963		254.8305	
	22.0	11113	16555		274.0791	
	23.0	11721	17164		294.5948	
	24.0	12348	17790		316.4865	
	25.0	12988	18431		339.6878	
	26.0	13644	19086		364.2878	
	27.0	14318	19761		390.4980	
	28.0	15007	20449		418.1745	
	29.0	15704	21146		447.1694	
	30.0	16409	21852		477.4910	
	31.0	17115	22557		508.8363	
	32.0	17816	23259		540.9621	
	33.0	18509	23951		573.6573	
	34.0	19193	24636		606.9120	
	35.0	19864	25307		640.4419	
	36.0	20516	25959		673.8586	
	37.0	21145	26587		706.8908	

Note: Increment listing is filtered to include critical data only. Complete time/pressure data are available in electronic or printed format.

DST#1 Recorder 80142

Build-up and Flow Curve Increments

Shutin# 1

Chart Label	Time (min)	Delta P (kPag)	Pressure (kPag)	Abscissa (T+dT)/dT	Pressure ² (kPag ² /10 ⁴ 6)	Used for Extrap
	38.0	21747	27189		739.2487	
	39.0	22323	27766		770.9432	
	40.0	22869	28312		801.5609	
	41.0	23375	28818		830.4654	
	42.0	23823	29266		856.4824	
	43.0	24218	29660		879.7201	
	44.0	24573	30015		900.9205	
	45.0	24888	30331		919.9577	
	46.0	25159	30602		936.4580	
	47.0	25394	30836		950.8672	
	48.0	25589	31032		962.9573	
	49.0	25750	31193		972.9923	
	50.0	25883	31326		981.2976	
	51.0	25994	31436		988.2507	
	52.0	26087	31530		994.1223	
	53.0	26168	31611		999.2410	
	54.0	26236	31679		1003.5425	
	55.0	26294	31737		1007.2105	
	56.0	26341	31783		1010.1650	
	57.0	26383	31825		1012.8406	
	58.0	26418	31861		1015.1091	
	59.0	26455	31898		1017.4765	
	60.0	26488	31931		1019.5783	
	61.0	26517	31959		1021.3811	
	62.0	26542	31985		1023.0291	
4	62.5	26548	31991		1023.4097	

Flow# 2

Chart Label	Time (min)	Pressure (kPag)
5	0.0	6702
	0.8	6482
	1.5	6297
	2.2	6123
	3.0	5974
	3.8	5846

Shutin# 2

Chart Label	Time (min)	Delta P (kPag)	Pressure (kPag)	Abscissa (T+dT)/dT	Pressure ² (kPag ² /10 ⁴ 6)	Used for Extrap
	0.0		6877		47.2918	
	1.8	462	7339	37.2857	53.8645	
	3.5	922	7799	19.1429	60.8227	
	5.2	1380	8257	13.0952	68.1804	
	7.0	1839	8716	10.0714	75.9686	
	8.8	2302	9179	8.2571	84.2561	

Note: Increment listing is filtered to include critical data only. Complete time/pressure data are available in electronic or printed format.

PORT AU PORT 1

DST#1 Recorder 80142

Build-up and Flow Curve Increments

Flow# 2

Shutin# 2

Chart Label	Time (min)	Pressure (kPag)
	4.5	5741
	5.2	5654
	6.0	5585
	6.8	5530
	7.5	5488
	8.2	5454
	9.0	5432
	9.8	5420
	10.5	5419
	11.2	5424
	12.0	5438
	12.8	5461
	13.5	5489
	14.2	5524
	15.0	5562
	15.8	5603
	16.5	5645
	17.2	5691
	18.0	5739
	18.8	5788
	19.5	5840
	20.2	5890
	21.0	5941
	21.8	5991
	22.5	6040
	23.2	6089
	24.0	6138
	24.8	6186
	25.5	6233
	26.2	6281
	27.0	6330
	27.8	6379
	28.5	6429
	29.2	6479
	30.0	6531
	30.8	6582
	31.5	6624
	32.2	6653

Chart Label	Time (min)	Delta P (kPag)	Pressure (kPag)	Abscissa (T+dT)/dT	Pressure ² (kPag ² /10 ⁶)	Used for Extrap
	10.5	2768	9645	7.0476	93.0272	
	12.2	3239	10116	6.1837	102.3391	
	14.0	3715	10592	5.5357	112.1901	
	15.8	4201	11078	5.0317	122.7199	
	17.5	4695	11572	4.6286	133.9138	
	19.2	5195	12072	4.2987	145.7246	
	21.0	5706	12583	4.0238	158.3199	
	22.8	6226	13102	3.7912	171.6749	
	24.5	6755	13632	3.5918	185.8222	
	26.2	7296	14173	3.4190	200.8713	
	28.0	7849	14726	3.2679	216.8511	
	29.8	8412	15289	3.1345	233.7496	
	31.5	8988	15865	3.0159	251.7001	
	33.2	9575	16452	2.9098	270.6610	
	35.0	10175	17052	2.8143	290.7729	
	36.8	10791	17668	2.7279	312.1606	
	38.5	11423	18300	2.6494	334.8731	
	40.2	12072	18949	2.5776	359.0648	
	42.0	12739	19616	2.5119	384.7784	
	43.8	13420	20297	2.4514	411.9780	
	45.5	14114	20991	2.3956	440.6373	
	47.2	14819	21696	2.3439	470.7192	
	49.0	15522	22399	2.2959	501.7251	
	50.8	16219	23096	2.2512	533.4126	
	52.5	16905	23782	2.2095	565.5978	
	54.2	17579	24456	2.1705	598.1058	
	56.0	18238	25115	2.1339	630.7407	
	57.8	18874	25751	2.0996	663.1217	
	59.5	19485	26361	2.0672	694.9253	
	61.2	20068	26945	2.0367	726.0129	
	63.0	20620	27497	2.0079	756.0811	
	64.8	21138	28015		784.8165	
	66.5	21614	28491		811.7168	
	68.2	22051	28928		836.8257	
	70.0	22447	29324		859.8883	
	71.8	22802	29679		880.8349	
	73.5	23117	29994		899.6489	
	75.2	23387	30264		915.9026	

Note: Increment listing is filtered to include critical data only. Complete time/pressure data are available in electronic or printed format.

PORT AU PORT 1

DST#1 Recorder 80142

Build-up and Flow Curve Increments

Flow# 2

Chart Label	Time (min)	Pressure (kPag)
	33.0	6670
	33.8	6676
	34.5	6671
	35.2	6655
	36.0	6629
	36.8	6594
	37.5	6549
	38.2	6497
	39.0	6437
	39.8	6372
	40.5	6304
	41.2	6234
	42.0	6163
	42.8	6094
	43.5	6024
	44.2	5959
	45.0	5894
	45.8	5839
	46.5	5788
	47.2	5738
	48.0	5698
	48.8	5666
	49.5	5629
	50.2	5603
	51.0	5585
	51.8	5568
	52.5	5719
	53.2	5927
	54.0	6135
	54.8	6340
	55.5	6543
	56.2	6743
6	56.8	6877

Shutin# 2

Chart Label	Time (min)	Delta P (kPag)	Pressure (kPag)	Abscissa (T+dT)/dT	Pressure ² (kPag ² /10 ⁶)	Used for Extrap
	77.0	23622	30498		930.1583	
	78.8	23827	30704		942.7276	
	80.5	23999	30876		953.3396	
	82.2	24147	31024		962.4800	
	84.0	24273	31150		970.3335	
	85.8	24382	31259		977.1151	
	87.5	24480	31357		983.2607	
	89.2	24567	31444		988.7492	
	91.0	24645	31522		993.6498	
	92.8	24713	31590		997.9142	
	94.5	24775	31652		1001.8560	
	96.2	24878	31755		1008.3752	
	98.0	24973	31850		1014.4209	
	99.8	25044	31921		1018.9209	
	101.5	25097	31974		1022.3289	
	103.2	25134	32011		1024.7265	
	105.0	25175	32052		1027.3413	
	106.8	25217	32094		1030.0379	
	108.5	25253	32129		1032.3030	
	110.2	25283	32160		1034.2613	
	112.0	25302	32179		1035.5100	
	113.8	25332	32209		1037.4216	
	115.5	25359	32236		1039.1637	*
	117.2	25384	32261		1040.7935	*
	119.0	25407	32284		1042.2488	*
	120.8	25423	32300		1043.2992	*
	122.5	25438	32315		1044.2698	*
	124.2	25447	32323		1044.8066	*
	126.0	25450	32327		1045.0592	*
	127.8	25449	32326		1044.9654	*
	129.5	25450	32327		1045.0241	*
	131.2	25452	32329		1045.1654	*
	133.0	25455	32332		1045.3533	*
	134.8	25458	32335		1045.5513	*
	136.5	25462	32339		1045.8011	*
	138.2	25466	32343		1046.0923	*
	140.0	25472	32348		1046.4222	*
	141.8	25477	32354		1046.7803	*

Note: Increment listing is filtered to include critical data only. Complete time/pressure data are available in electronic or printed format.

PORT AU PORT 1

DST#1 Recorder 80142

Build-up and Flow Curve Increments

Shutin# 2

Chart Label	Time (min)	Delta P (kPag)	Pressure (kPag)	Abscissa (T+dT)/dT	Pressure ² (kPag ² /10 ⁴ 6)	Used for Extrap
	143.5	25483	32360		1047.1413	*
	145.2	25488	32365		1047.4944	*
	147.0	25494	32371		1047.8864	*
	148.8	25500	32376		1048.2317	*
	150.5	25505	32382		1048.5823	*
	152.2	25511	32388		1048.9746	*
	154.0	25516	32393		1049.3173	*
	155.8	25521	32398		1049.6524	*
	157.5	25528	32405		1050.0990	*
	159.2	25533	32410		1050.3851	*
	161.0	25537	32414		1050.6688	*
	162.8	25542	32419		1050.9780	*
	164.5	25546	32423		1051.2718	*
	166.2	25550	32427		1051.5245	*
	168.0	25555	32432		1051.8315	*
	169.8	25559	32435		1052.0608	*
	171.5	25562	32439		1052.3054	*
	173.2	25566	32443		1052.5711	*
7	173.8	25567	32444		1052.6225	*

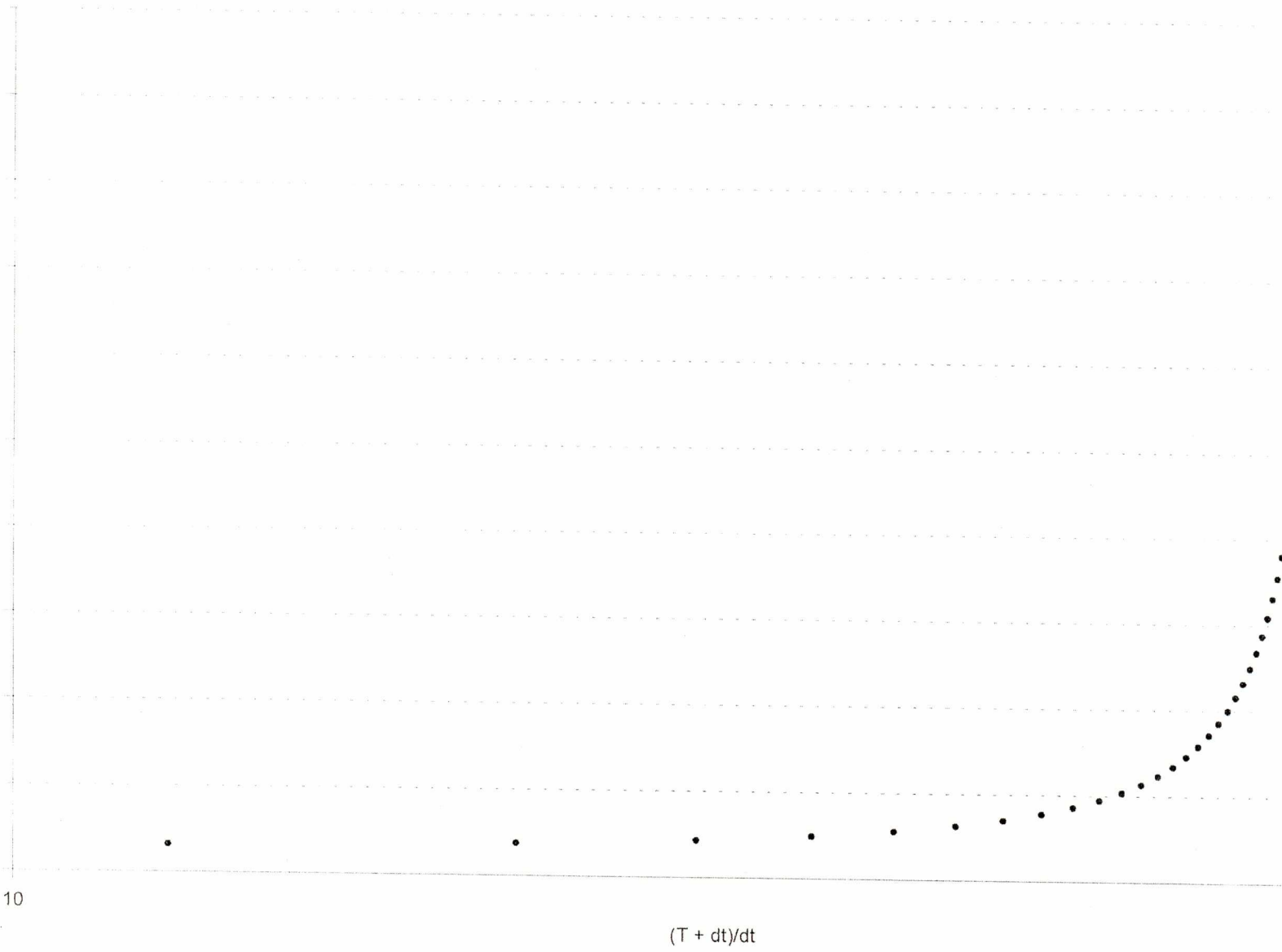
Horner Extrapolation

Shut-in#	Extrapolated Pressure (kPag)	Extrapolated Slope (kPag/cycle)
2	32866.8	205.20964

PORT AU PORT 1

DST #: 1
Recorder: 80142

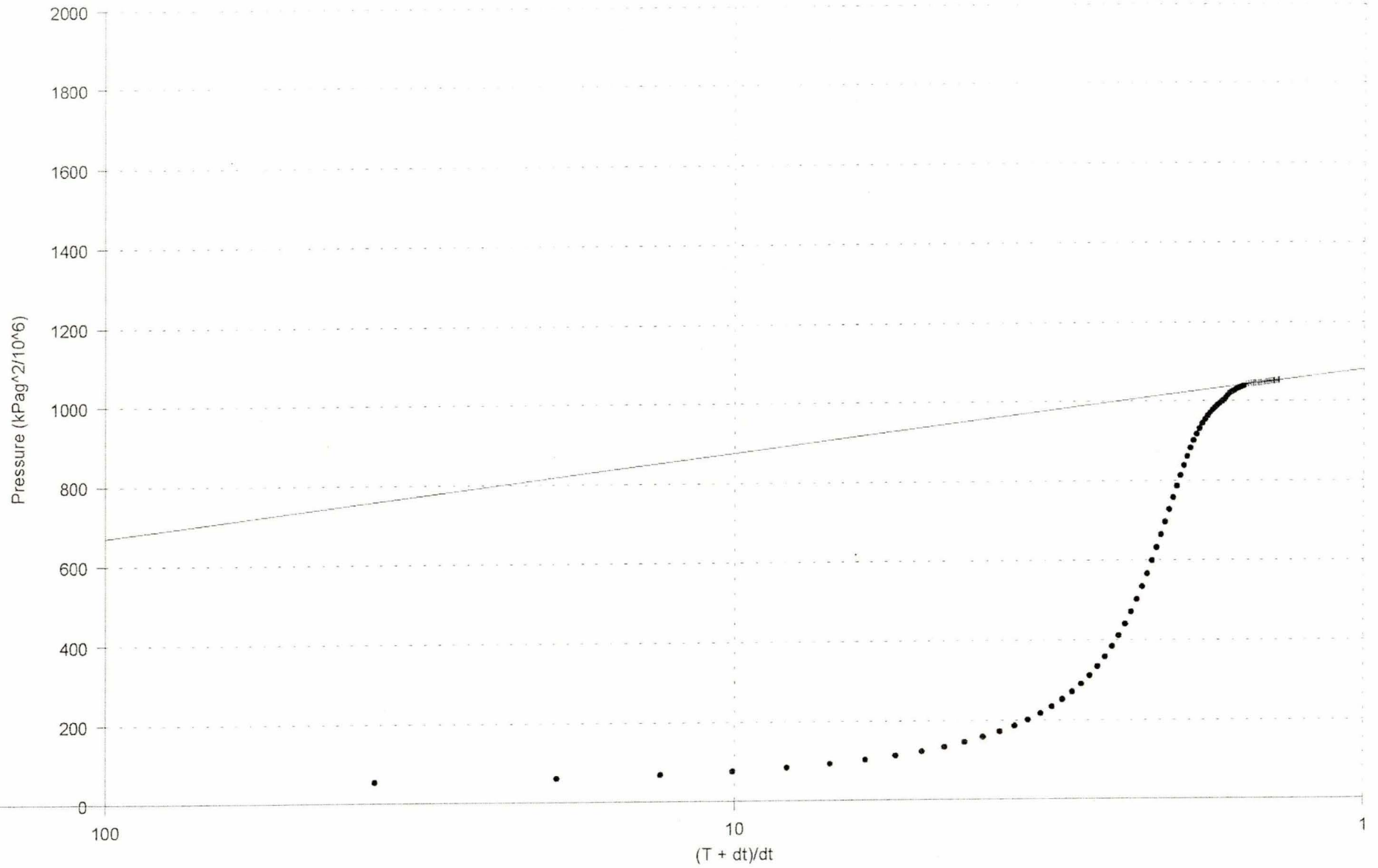
Shut-in



PORT AU PORT 1

DST # 1
Recorder: 80142

Shut-in #2
Slope = 205.21 kPag²/10⁶/cycle
Extrapolated Pressure = 32866.84 kPag



Attachment C: DST#2 ST#2 Port au Port (Baker Report)



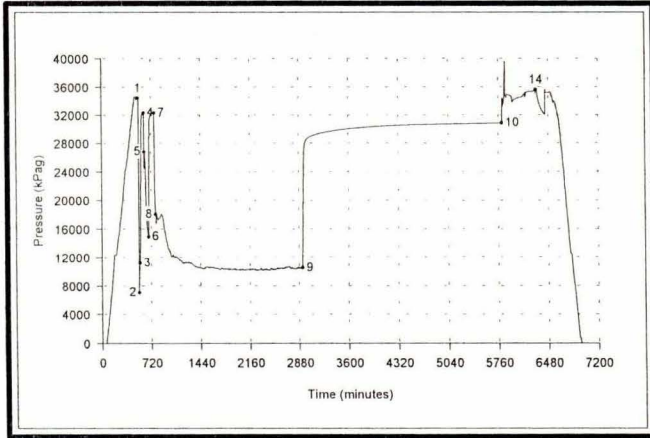
CDN IMPERIAL PORT AU PORT #1
48.490/59.226
DST# 2

Baker Oil Tools

Formation: **AGUATHUNA**
 Interval - from: **3335.00** to: **3482.00 m**

Recorder# 80121 at 3340.00 m

Test Date: **2002-08-11**
 Test Type: **CASING PACKER**
 Tester Name: **BRIAN MAGNUS**
 Drill Pipe O.D.: **102.00 mm**
 Drill Collar I.D.: **60.00 mm**
 Drill Collar Length: **471.25 m**
 Hole Size: **156.00 mm**



Maximum Btm Hole Temperature @ FSI: 49.0 C

		Pressure (kPag)	Time (min)	Extrapolated Pressure (kPag)
1	Initial Hydrostatic	34414		
2	Start of 1st Flow	7063		
3	End of 1st Flow	11163	16.2	
4	End of 1st Shut-in	32298	60.8	32610.7
5	Start of 2nd Flow	26784		
6	End of 2nd Flow	14897	60.5	
7	End of 2nd Shut-in	32272	88.5	32534.1
8	Start of 3rd Flow	18034		
9	End of 3rd Flow	10496	2146.5	
10	End of 3rd Shut-in	30848	2879.5	31342.6
14	Final Hydrostatic	35572		

Liquid Recovery of 1566.00 m

Test was reversed out.

Recovery	Description	Salinity
1566.00 m	CONDENSATE	

Blow Description:

Weak air blow increasing to strong in 4 minutes then steady throughout. No gas to surface.

Gas to surface immediately with fluid to surface in 90 minutes.

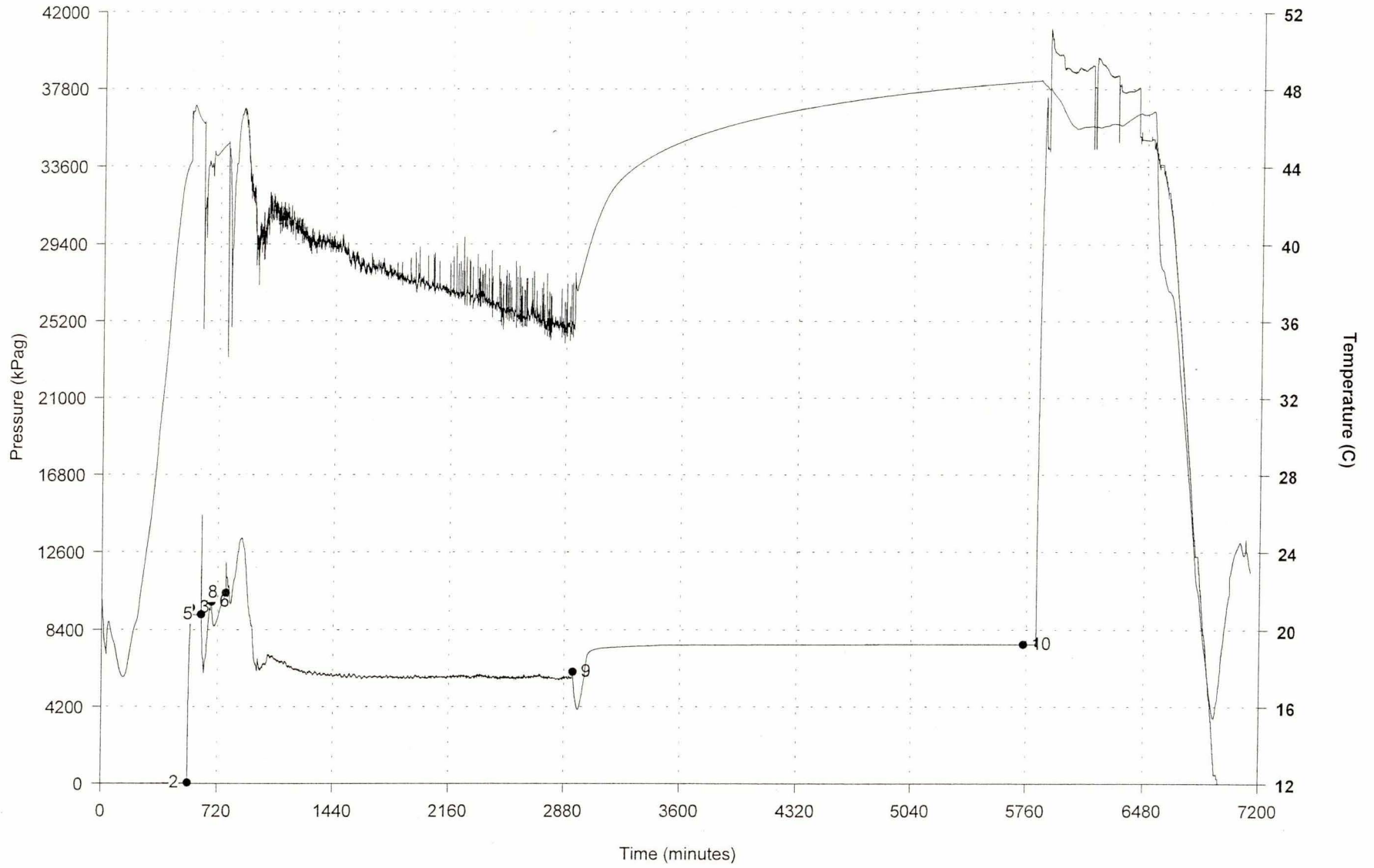
Remarks:

Mechanically successful test. Results suggest relatively high permeability within the interval tested. All surface equipment was pressure tested to 16 mPa prior to opening the tool. Flow rates taken by Maritime Testers at the separator. The fluid to surface started out as drilling mud then turned to a light oil (50.8 API) shortly after. The recovered fluid was determined by reverse circulating to the separator and back calculating the linear height.

CDN IMPERIAL PORT AU PORT #1
 48.490/59.226
 DST #: 2
 Recorder: 80242

Pressure (kPag) at Critical Points:
 2: 45 6: 9912 10: 7613
 3: 9588 8: 10394
 5: 9227 9: 6125

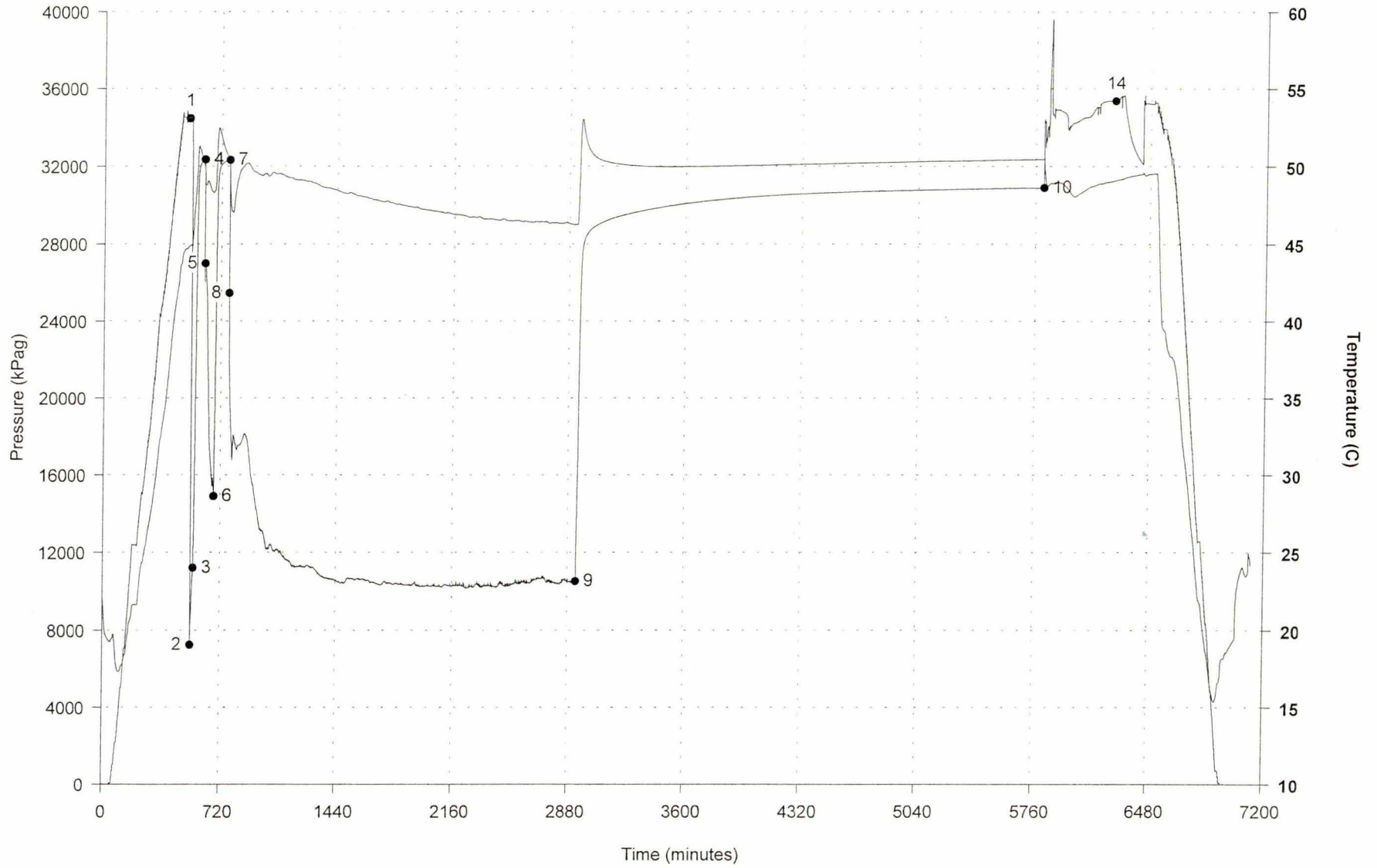
Recovery recorder



CDN IMPERIAL PORT AU PORT #1
 48.490/59.226
 DST #: 2
 Recorder: 80142

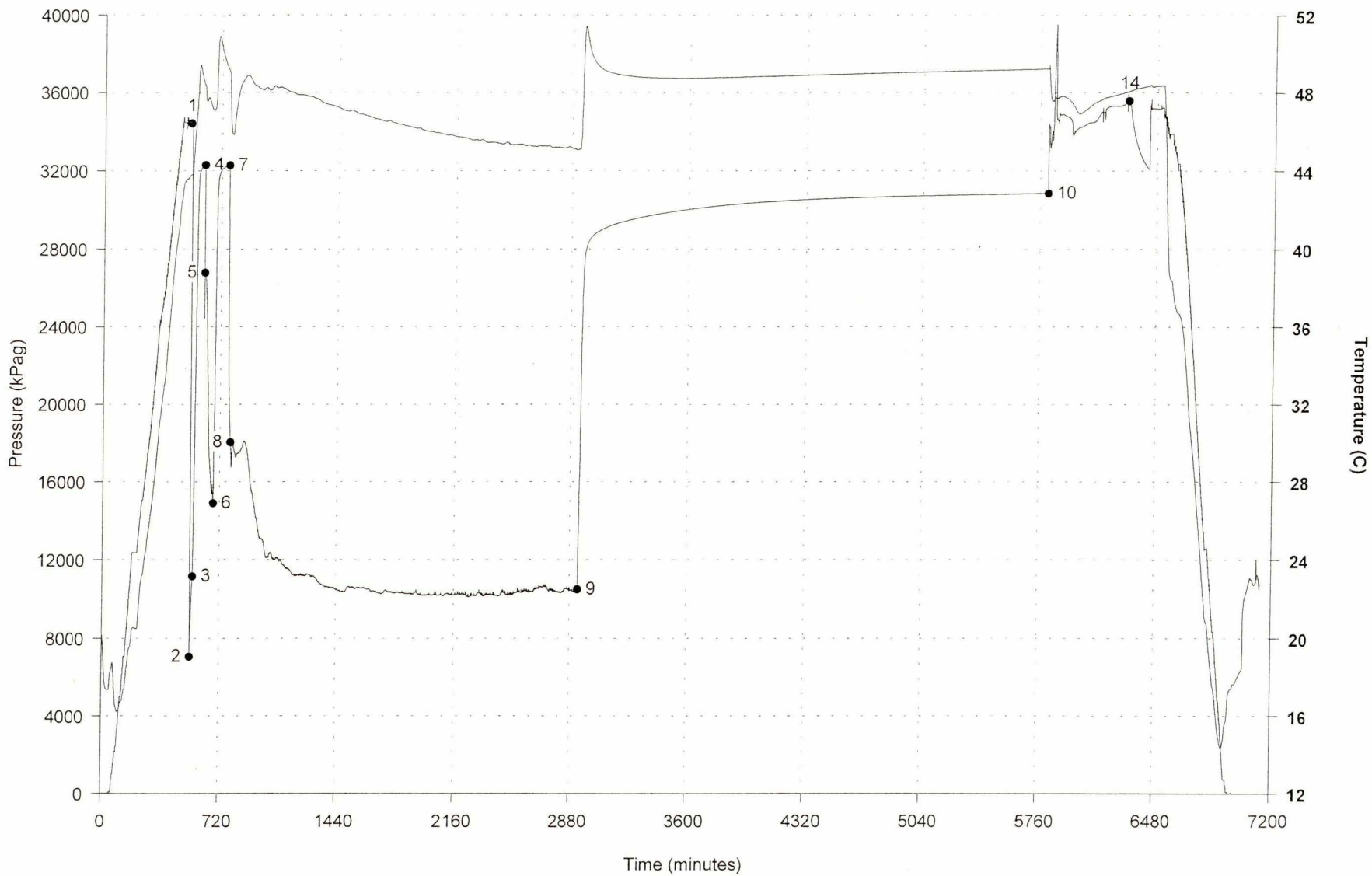
1: 34464	4: 32347	7: 32323	10: 30897
2: 7247	5: 26988	8: 25455	14: 35361
3: 11202	6: 14896	9: 10522	

Other electronic gauge



CDN IMPERIAL PORT AU PORT #1
 48.490/59.226
 DST #. 2
 Recorder: 80121

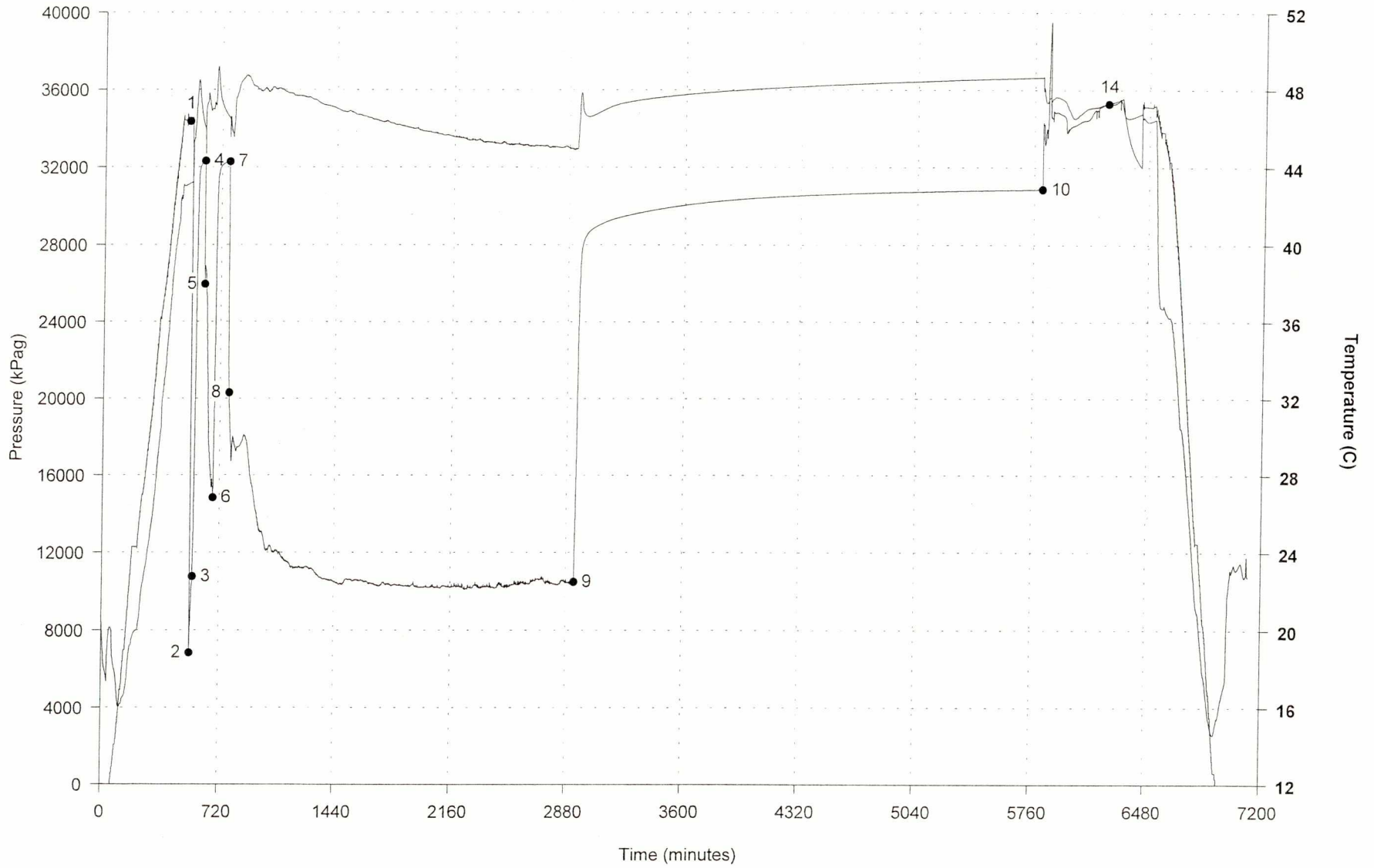
1: 34414	4: 32298	7: 32272	10: 30848
2: 7063	5: 26784	8: 18034	14: 35572
3: 11163	6: 14897	9: 10496	



CDN IMPERIAL PORT AU PORT #1
48.490/59.226
DST #: 2
Recorder: 80383

1: 34359	4: 32314	7: 32288	10: 30868
2: 6827	5: 25952	8: 20292	14: 35271
3: 10754	6: 14828	9: 10484	

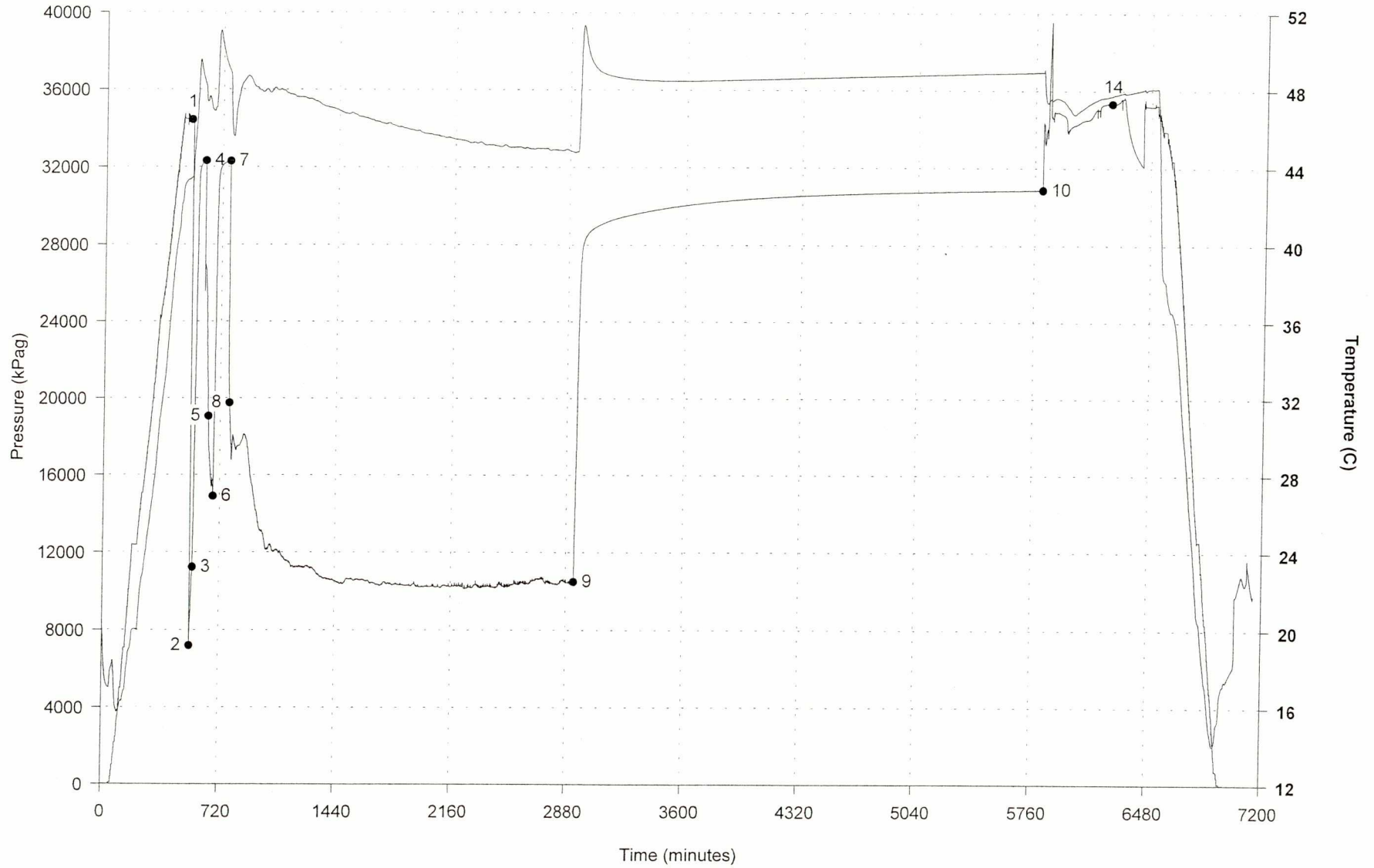
Above interval



CDN IMPERIAL PORT AU PORT #1
 48.490/59.226
 DST #: 2
 Recorder: 80129

1: 34432	4: 32317	7: 32293	10: 30868
2: 7190	5: 19054	8: 19754	14: 35326
3: 11230	6: 14889	9: 10497	

Other electronic gauge



CDN IMPERIAL PORT AU PORT #1
48.490/59.226
DST# 2
Recorder 80121

Build-up and Flow Curve Increments

Flow# 1

Chart Label	Time (min)	Pressure (kPag)
2	0.0	7063
	0.5	7815
	1.0	7857
	1.5	8007
	2.0	8136
	2.5	8275
	3.0	8351
	3.5	8386
	4.0	8438
	4.5	8516
	5.0	8582
	5.5	8723
	6.0	8858
	6.5	8975
	7.0	9094
	7.5	9229
	8.0	9418
	8.5	9633
	9.0	9802
	9.5	9943
3	10.0	10065
	10.5	10191
	11.0	10313
	11.5	10417
	12.0	10525
	12.5	10629
	13.0	10721
	13.5	10803
14.0	10889	
14.5	10959	
15.0	11029	
15.5	11097	
16.0	11149	
16.2	11163	

Shutin# 1

Chart Label	Time (min)	Delta P (kPag)	Pressure (kPag)	Abscissa (T+dT)/dT	Used for Extrap
	0.0		11163		
	1.0	877	12039	17.2500	
	2.0	1649	12811	9.1250	
	3.0	2429	13592	6.4167	
	4.0	3235	14397	5.0625	
	5.0	4073	15236	4.2500	
	6.0	4946	16109	3.7083	
	7.0	5861	17024	3.3214	
	8.0	6819	17981	3.0312	
	9.0	7825	18988	2.8056	
	10.0	8869	20032	2.6250	
	11.0	9955	21118	2.4773	
	12.0	11076	22239	2.3542	
	13.0	12225	23388	2.2500	
	14.0	13383	24545	2.1607	
	15.0	14526	25688	2.0833	
	16.0	15628	26790	2.0156	
	17.0	16643	27806	1.9559	
	18.0	17533	28696	1.9028	
	19.0	18293	29456	1.8553	
	20.0	18922	30084	1.8125	
	21.0	19415	30578	1.7738	
	22.0	19787	30950	1.7386	
	23.0	20063	31226	1.7065	
	24.0	20267	31430	1.6771	
	25.0	20414	31577	1.6500	
	26.0	20521	31684	1.6250	
	27.0	20606	31768	1.6019	
	28.0	20671	31834	1.5804	
	29.0	20721	31884	1.5603	
	30.0	20763	31925	1.5417	
	31.0	20802	31964	1.5242	
	32.0	20834	31997	1.5078	
	33.0	20863	32026	1.4924	
	34.0	20888	32050	1.4779	
	35.0	20910	32073	1.4643	
	36.0	20930	32093	1.4514	
	37.0	20947	32110	1.4392	

Note: Increment listing is filtered to include critical data only. Complete time/pressure data are available in electronic or printed format.

CDN IMPERIAL PORT AU PORT #1
48.490/59.226
DST# 2
Recorder 80121

Build-up and Flow Curve Increments

Shutin# 1

Chart Label	Time (min)	Delta P (kPag)	Pressure (kPag)	Abscissa (T+dT)/dT	Used for Extrap
	38.0	20961	32124	1.4276	
	39.0	20977	32140	1.4167	
	40.0	20991	32154	1.4062	
	41.0	21004	32167	1.3963	
	42.0	21015	32178	1.3869	*
	43.0	21027	32190	1.3779	*
	44.0	21036	32199	1.3693	*
	45.0	21046	32209	1.3611	*
	46.0	21056	32218	1.3533	*
	47.0	21065	32228	1.3457	*
	48.0	21072	32235	1.3385	*
	49.0	21078	32240	1.3316	*
	50.0	21085	32248	1.3250	*
	51.0	21090	32253	1.3186	*
	52.0	21096	32259	1.3125	*
	53.0	21102	32265	1.3066	*
	54.0	21106	32268	1.3009	*
	55.0	21111	32273	1.2955	*
	56.0	21116	32279	1.2902	*
	57.0	21121	32284	1.2851	*
	58.0	21124	32287	1.2802	*
	59.0	21129	32291	1.2754	*
	60.0	21133	32296	1.2708	*
4	60.8	21135	32298	1.2675	*

Flow# 2

Chart Label	Time (min)	Pressure (kPag)
5	0.0	26784
	1.0	26918
	2.0	26944
	3.0	26908
	4.0	26846
	5.0	26777
	6.0	26734
	7.0	26685

Shutin# 2

Chart Label	Time (min)	Delta P (kPag)	Pressure (kPag)	Abscissa (T+dT)/dT	Used for Extrap
	0.0		14897		
	1.0	911	15808	77.7500	
	2.0	1862	16759	39.3750	
	3.0	2815	17712	26.5833	
	4.0	3799	18696	20.1875	
	5.0	4827	19724	16.3500	
	6.0	5901	20798	13.7917	
	7.0	7026	21923	11.9643	

Note: Increment listing is filtered to include critical data only. Complete time/pressure data are available in electronic or printed format.

CDN IMPERIAL PORT AU PORT #1
48.490/59.226
DST# 2
Recorder 80121

Build-up and Flow Curve Increments

Flow# 2

Chart Label	Time (min)	Pressure (kPag)
	8.0	26634
	9.0	26329
	10.0	26007
	11.0	25802
	12.0	25642
	13.0	25510
	14.0	25377
	15.0	25324
	16.0	25012
	17.0	24185
	18.0	23398
	19.0	23275
	20.0	22678
	21.0	22177
	22.0	21792
	23.0	21493
	24.0	21099
	25.0	20655
	26.0	20066
	27.0	19549
	28.0	19153
	29.0	18898
	30.0	18314
	31.0	17904
	32.0	17592
	33.0	17435
	34.0	17276
	35.0	17210
	36.0	17120
	37.0	16967
	38.0	16813
	39.0	16703
	40.0	16599
	41.0	16453
	42.0	16335
	43.0	16206
	44.0	16063
	45.0	15925

Shutin# 2

Chart Label	Time (min)	Delta P (kPag)	Pressure (kPag)	Abscissa (T+dT)/dT	Used for Extrap
	8.0	8199	23096	10.5938	
	9.0	9395	24292	9.5278	
	10.0	10596	25493	8.6750	
	11.0	11741	26638	7.9773	
	12.0	12795	27692	7.3958	
	13.0	13717	28614	6.9038	
	14.0	14491	29388	6.4821	
	15.0	15110	30007	6.1167	
	16.0	15582	30479	5.7969	
	17.0	15931	30828	5.5147	
	18.0	16184	31081	5.2639	
	19.0	16367	31264	5.0395	
	20.0	16502	31399	4.8375	
	21.0	16604	31502	4.6548	
	22.0	16685	31582	4.4886	
	23.0	16749	31646	4.3370	
	24.0	16802	31699	4.1979	
	25.0	16842	31739	4.0700	
	26.0	16882	31779	3.9519	
	27.0	16917	31814	3.8426	
	28.0	16948	31845	3.7411	
	29.0	16975	31872	3.6466	
	30.0	17000	31897	3.5583	
	31.0	17022	31919	3.4758	
	32.0	17042	31939	3.3984	
	33.0	17062	31959	3.3258	
	34.0	17079	31976	3.2574	
	35.0	17096	31993	3.1929	
	36.0	17110	32007	3.1319	
	37.0	17124	32021	3.0743	
	38.0	17137	32034	3.0197	
	39.0	17150	32047	2.9679	
	40.0	17161	32058	2.9188	
	41.0	17172	32069	2.8720	
	42.0	17182	32079	2.8274	
	43.0	17192	32089	2.7849	
	44.0	17200	32097	2.7443	
	45.0	17209	32106	2.7056	

Note: Increment listing is filtered to include critical data only. Complete time/pressure data are available in electronic or printed format.

CDN IMPERIAL PORT AU PORT #1
48.490/59.226
DST# 2
Recorder 80121

Build-up and Flow Curve Increments

Flow# 2

Chart Label	Time (min)	Pressure (kPag)
	46.0	15781
	47.0	15619
	48.0	15488
	49.0	15389
	50.0	15399
	51.0	15415
	52.0	15499
	53.0	15666
	54.0	15772
	55.0	15765
	56.0	15509
	57.0	15337
	58.0	15239
	59.0	15117
	60.0	15009
6	60.5	14897

Shutin# 2

Chart Label	Time (min)	Delta P (kPag)	Pressure (kPag)	Abscissa (T+dT)/dT	Used for Extrap
	46.0	17217	32114	2.6685	
	47.0	17225	32122	2.6330	
	48.0	17232	32129	2.5990	
	49.0	17238	32135	2.5663	
	50.0	17245	32142	2.5350	*
	51.0	17251	32148	2.5049	*
	52.0	17258	32155	2.4760	*
	53.0	17263	32160	2.4481	*
	54.0	17268	32165	2.4213	*
	55.0	17274	32171	2.3955	*
	56.0	17279	32176	2.3705	*
	57.0	17283	32180	2.3465	*
	58.0	17288	32185	2.3233	*
	59.0	17292	32189	2.3008	*
	60.0	17296	32194	2.2792	*
	61.0	17301	32198	2.2582	*
	62.0	17305	32202	2.2379	*
	63.0	17309	32206	2.2183	*
	64.0	17312	32209	2.1992	*
	65.0	17316	32213	2.1808	*
	66.0	17319	32216	2.1629	*
	67.0	17322	32219	2.1455	*
	68.0	17326	32223	2.1287	*
	69.0	17328	32225	2.1123	*
	70.0	17331	32228	2.0964	*
	71.0	17334	32232	2.0810	*
	72.0	17337	32234	2.0660	*
	73.0	17340	32237	2.0514	*
	74.0	17342	32239	2.0372	*
	75.0	17345	32242	2.0233	*
	76.0	17348	32245	2.0099	*
	77.0	17350	32247	1.9968	*
	78.0	17353	32250	1.9840	*
	79.0	17355	32252	1.9715	*
	80.0	17358	32255	1.9594	*
	81.0	17359	32256	1.9475	*
	82.0	17362	32259	1.9360	*
	83.0	17364	32261	1.9247	*

Note: Increment listing is filtered to include critical data only. Complete time/pressure data are available in electronic or printed format.

CDN IMPERIAL PORT AU PORT #1
48.490/59.226
DST# 2
Recorder 80121

Build-up and Flow Curve Increments

Shutin# 2

Chart Label	Time (min)	Delta P (kPag)	Pressure (kPag)	Abscissa (T+dT)/dT	Used for Extrap
7	84.0	17366	32263	1.9137	*
	85.0	17368	32265	1.9029	*
	86.0	17370	32267	1.8924	*
	87.0	17372	32269	1.8822	*
	88.0	17374	32271	1.8722	*
	88.5	17375	32272	1.8672	*

Flow# 3

Chart Label	Time (min)	Pressure (kPag)
8	0.0	18034
	18.2	17904
	36.5	17281
	54.8	17502
	73.0	17796
	91.2	18026
	109.5	17182
	127.8	15778
	146.0	14959
	164.2	14098
	182.5	13148
	200.8	13044
	219.0	12309
	237.2	12130
	255.5	12342
	273.8	12036
	292.0	12130
	310.2	12030
	328.5	11758
	346.8	11604
	365.0	11493
	383.2	11240
	401.5	11206
	419.8	11252
	438.0	11245
	456.2	11191

Shutin# 3

Chart Label	Time (min)	Delta P (kPag)	Pressure (kPag)	Abscissa (T+dT)/dT	Used for Extrap
	0.0		10496		
	24.2	16124	26621	92.6804	
	48.5	17795	28292	46.8402	
	72.8	18134	28630	31.5601	
	97.0	18314	28811	23.9201	
	121.2	18440	28936	19.3361	
	145.5	18542	29039	16.2801	
	169.8	18636	29132	14.0972	
	194.0	18719	29216	12.4601	
	218.2	18791	29287	11.1867	
	242.5	18852	29349	10.1680	
	266.8	18908	29404	9.3346	
	291.0	18960	29456	8.6400	
	315.2	19009	29506	8.0523	
	339.5	19056	29552	7.5486	
	363.8	19101	29597	7.1120	
	388.0	19144	29640	6.7300	
	412.2	19185	29682	6.3930	
	436.5	19225	29722	6.0934	
	460.8	19264	29760	5.8253	
	485.0	19300	29796	5.5840	
	509.2	19335	29832	5.3657	
	533.5	19369	29866	5.1673	
	557.8	19402	29898	4.9861	
	582.0	19433	29930	4.8200	
	606.2	19464	29960	4.6672	

Note: Increment listing is filtered to include critical data only. Complete time/pressure data are available in electronic or printed format.

CDN IMPERIAL PORT AU PORT #1
48.490/59.226
DST# 2
Recorder 80121

Build-up and Flow Curve Increments

Flow# 3

Chart Label	Time (min)	Pressure (kPag)
	474.5	11284
	492.8	11229
	511.0	11190
	529.2	11065
	547.5	10875
	565.8	10754
	584.0	10640
	602.2	10645
	620.5	10611
	638.8	10595
	657.0	10508
	675.2	10443
	693.5	10413
	711.8	10384
	730.0	10636
	748.2	10611
	766.5	10588
	784.8	10581
	803.0	10562
	821.2	10576
	839.5	10537
	857.8	10525
	876.0	10405
	894.2	10389
	912.5	10337
	930.8	10285
	949.0	10332
	967.2	10418
	985.5	10397
	1003.8	10340
	1022.0	10335
	1040.2	10349
	1058.5	10317
	1076.8	10285
	1095.0	10269
	1113.2	10264
	1131.5	10283
	1149.8	10367

Shutin# 3

Chart Label	Time (min)	Delta P (kPag)	Pressure (kPag)	Abscissa (T+dT)/dT	Used for Extrap
	630.5	19493	29990	4.5262	
	654.8	19521	30018	4.3956	
	679.0	19548	30045	4.2743	
	703.2	19574	30071	4.1614	
	727.5	19600	30096	4.0560	
	751.8	19624	30120	3.9574	
	776.0	19647	30144	3.8650	
	800.2	19670	30166	3.7782	
	824.5	19692	30188	3.6965	
	848.8	19713	30210	3.6194	
	873.0	19734	30230	3.5467	
	897.2	19753	30250	3.4778	
	921.5	19773	30269	3.4126	
	945.8	19791	30288	3.3508	
	970.0	19809	30305	3.2920	*
	994.2	19826	30322	3.2361	*
	1018.5	19843	30339	3.1829	*
	1042.8	19858	30355	3.1321	*
	1067.0	19874	30370	3.0836	*
	1091.2	19889	30385	3.0373	*
	1115.5	19903	30400	2.9931	*
	1139.8	19916	30412	2.9506	*
	1164.0	19929	30425	2.9100	*
	1188.2	19942	30439	2.8710	*
	1212.5	19954	30451	2.8336	*
	1236.8	19966	30463	2.7977	*
	1261.0	19978	30474	2.7631	*
	1285.2	19989	30486	2.7298	*
	1309.5	19999	30496	2.6978	*
	1333.8	20010	30507	2.6669	*
	1358.0	20020	30517	2.6372	*
	1382.2	20030	30527	2.6084	*
	1406.5	20040	30536	2.5807	*
	1430.8	20049	30545	2.5539	*
	1455.0	20058	30554	2.5280	*
	1479.2	20066	30563	2.5030	*
	1503.5	20075	30572	2.4787	*
	1527.8	20083	30580	2.4552	*

Note: Increment listing is filtered to include critical data only. Complete time/pressure data are available in electronic or printed format.

CDN IMPERIAL PORT AU PORT #1
48.490/59.226
DST# 2
Recorder 80121

Build-up and Flow Curve Increments

Flow# 3

Shutin# 3

<i>Chart Label</i>	<i>Time (min)</i>	<i>Pressure (kPag)</i>
	1168.0	10235
	1186.2	10206
	1204.5	10208
	1222.8	10246
	1241.0	10208
	1259.2	10230
	1277.5	10194
	1295.8	10220
	1314.0	10173
	1332.2	10295
	1350.5	10251
	1368.8	10217
	1387.0	10250
	1405.2	10283
	1423.5	10270
	1441.8	10219
	1460.0	10126
	1478.2	10140
	1496.5	10187
	1514.8	10195
	1533.0	10368
	1551.2	10277
	1569.5	10198
	1587.8	10233
	1606.0	10284
	1624.2	10247
	1642.5	10202
	1660.8	10179
	1679.0	10373
	1697.2	10243
	1715.5	10274
	1733.8	10240
	1752.0	10323
	1770.2	10371
	1788.5	10375
	1806.8	10373
	1825.0	10419
	1843.2	10369

<i>Chart Label</i>	<i>Time (min)</i>	<i>Delta P (kPag)</i>	<i>Pressure (kPag)</i>	<i>Abscissa (T+dT)/dT</i>	<i>Used for Extrap</i>
	1552.0	20091	30588	2.4325	*
	1576.2	20100	30596	2.4105	*
	1600.5	20107	30603	2.3891	*
	1624.8	20114	30611	2.3684	*
	1649.0	20121	30618	2.3482	*
	1673.2	20129	30625	2.3287	*
	1697.5	20135	30631	2.3097	*
	1721.8	20142	30639	2.2913	*
	1746.0	20148	30645	2.2733	*
	1770.2	20155	30651	2.2559	*
	1794.5	20161	30658	2.2389	*
	1818.8	20167	30663	2.2224	*
	1843.0	20173	30669	2.2063	*
	1867.2	20179	30675	2.1907	*
	1891.5	20184	30681	2.1754	*
	1915.8	20189	30686	2.1605	*
	1940.0	20195	30692	2.1460	*
	1964.2	20201	30697	2.1319	*
	1988.5	20206	30702	2.1181	*
	2012.8	20211	30708	2.1046	*
	2037.0	20216	30713	2.0914	*
	2061.2	20221	30718	2.0786	*
	2085.5	20226	30722	2.0661	*
	2109.8	20230	30727	2.0538	*
	2134.0	20235	30732	2.0418	*
	2158.2	20240	30736	2.0301	*
	2182.5	20244	30741	2.0187	*
	2206.8	20249	30745	2.0075	*
	2231.0	20254	30750	1.9965	*
	2255.2	20258	30754	1.9858	*
	2279.5	20262	30758	1.9753	*
	2303.8	20266	30762	1.9651	*
	2328.0	20270	30767	1.9550	*
	2352.2	20274	30771	1.9452	*
	2376.5	20279	30775	1.9355	*
	2400.8	20282	30779	1.9261	*
	2425.0	20286	30783	1.9168	*
	2449.2	20290	30786	1.9077	*

Note: Increment listing is filtered to include critical data only. Complete time/pressure data are available in electronic or printed format.

CDN IMPERIAL PORT AU PORT #1
48.490/59.226
DST# 2
Recorder 80121

Build-up and Flow Curve Increments

Flow# 3

Chart Label	Time (min)	Pressure (kPag)
	1861.5	10369
	1879.8	10530
	1898.0	10557
	1916.2	10614
	1934.5	10632
	1952.8	10667
	1971.0	10483
	1989.2	10480
	2007.5	10422
	2025.8	10361
	2044.0	10324
	2062.2	10470
	2080.5	10552
	2098.8	10481
	2117.0	10411
	2135.2	10458
9	2146.5	10496

Shutin# 3

Chart Label	Time (min)	Delta P (kPag)	Pressure (kPag)	Abscissa (T+dT)/dT	Used for Extrap
	2473.5	20294	30790	1.8988	*
	2497.8	20298	30794	1.8901	*
	2522.0	20301	30798	1.8815	*
	2546.2	20305	30801	1.8731	*
	2570.5	20309	30805	1.8649	*
	2594.8	20312	30809	1.8568	*
	2619.0	20316	30812	1.8489	*
	2643.2	20320	30816	1.8411	*
	2667.5	20323	30820	1.8335	*
	2691.8	20326	30823	1.8259	*
	2716.0	20330	30826	1.8186	*
	2740.2	20333	30830	1.8113	*
	2764.5	20336	30833	1.8042	*
	2788.8	20340	30836	1.7972	*
	2813.0	20344	30840	1.7903	*
	2837.2	20346	30843	1.7836	*
	2861.5	20350	30846	1.7770	*
10	2879.5	20352	30848	1.7721	*

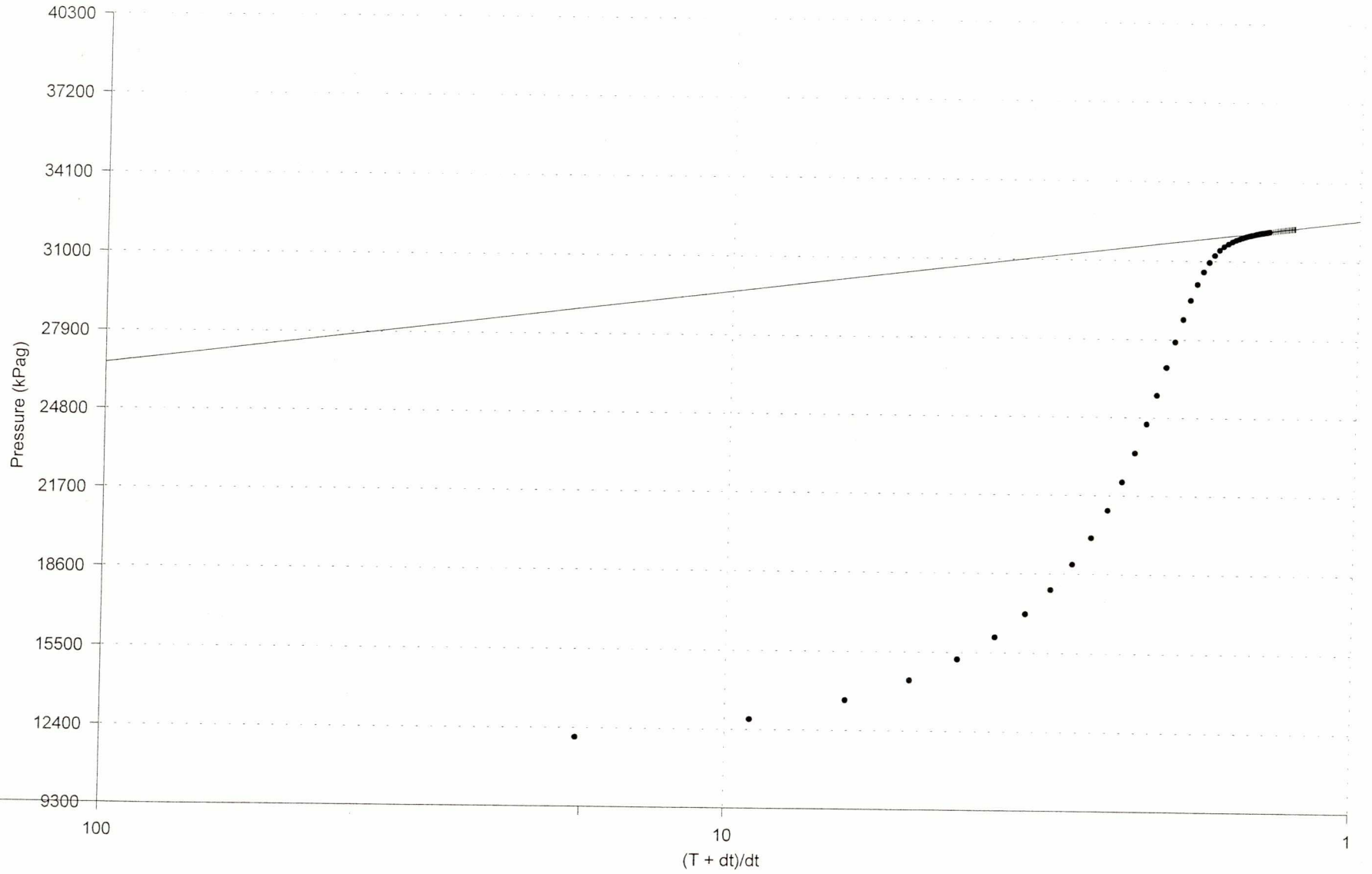
Horner Extrapolation

Shut-in#	Extrapolated Pressure (kPag)	Extrapolated Slope (kPag/cycle)
1	32610.7	2998.85797
2	32534.1	956.47939
3	31342.6	1971.93978

Note: Increment listing is filtered to include critical data only. Complete time/pressure data are available in electronic or printed format.

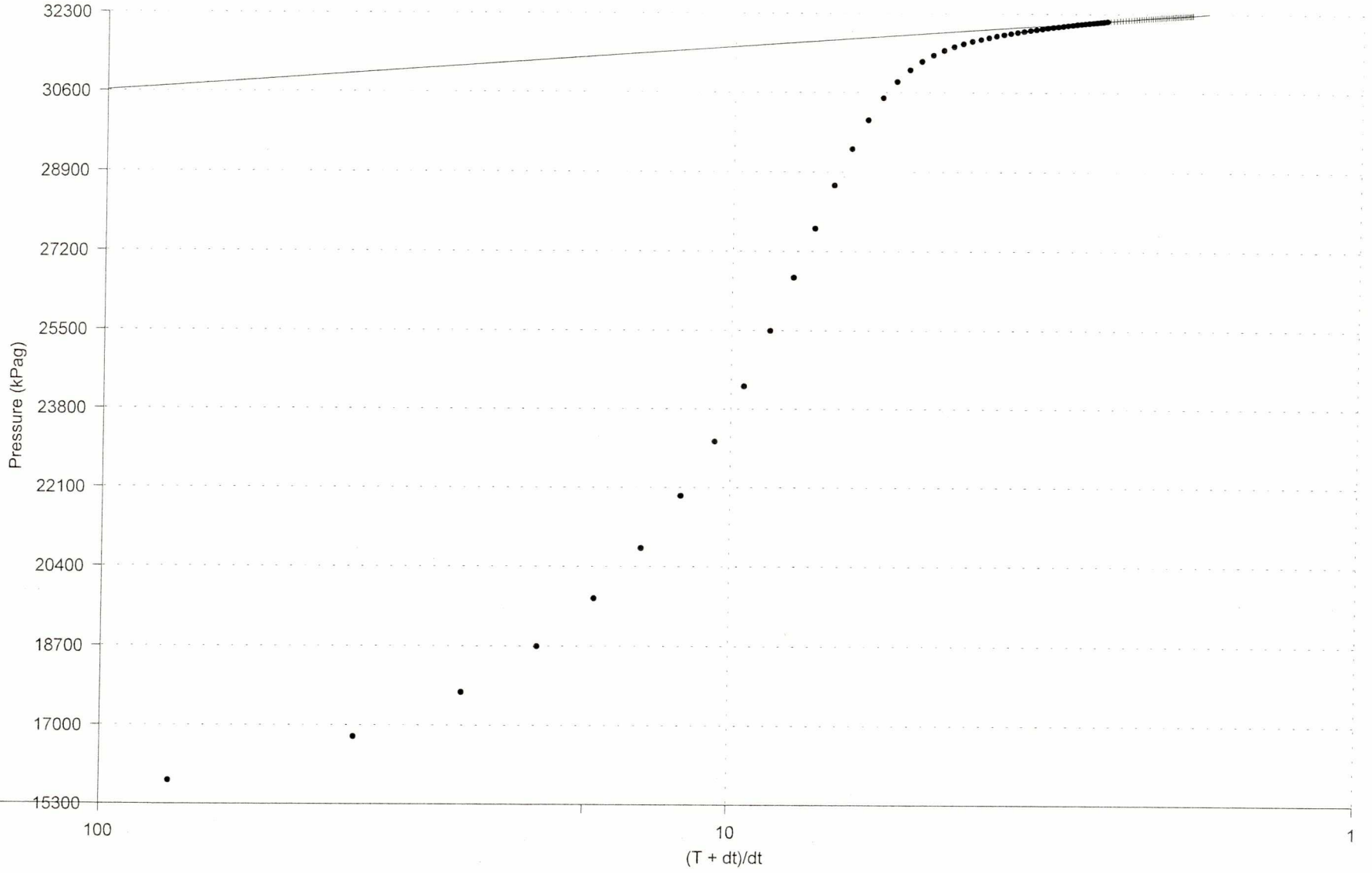
CDN IMPERIAL PORT AU PORT #1
48.490/59.226
DST #: 2
Recorder: 80121

Shut-in #1
Slope = 2998.86 kPag/cycle
Extrapolated Pressure = 32610.66 kPag



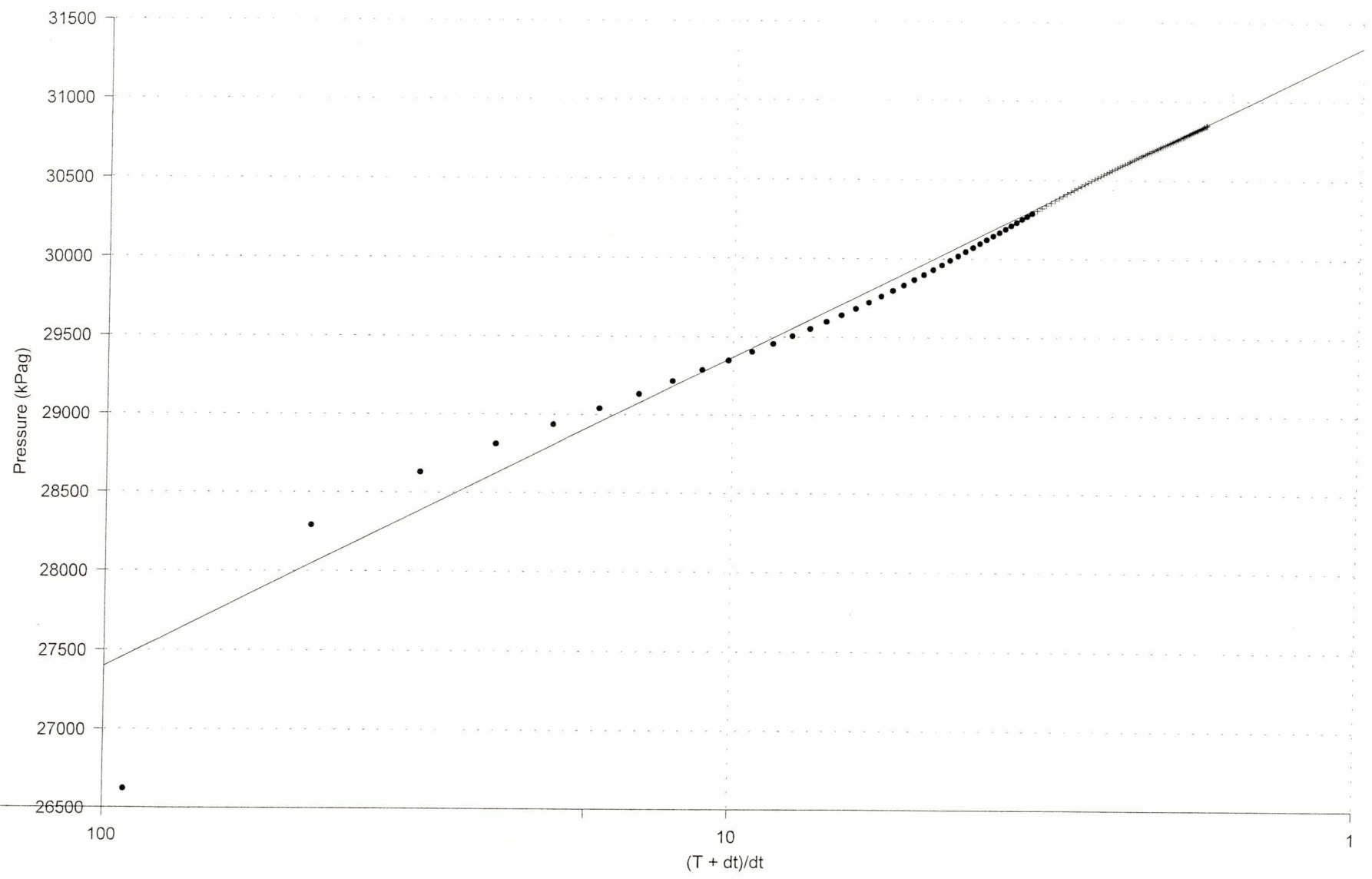
CDN IMPERIAL PORT AU PORT #1
48.490/59.226
DST #: 2
Recorder: 80121

Shut-in #2
Slope = 956.48 kPag/cycle
Extrapolated Pressure = 32534.11 kPag



CDN IMPERIAL PORT AU PORT #1
48.490/59.226
DST #: 2
Recorder: 80121

Shut-in #3
Slope = 1971.94 kPag/cycle
Extrapolated Pressure = 31342.56 kPag



Kil CDN IMPERIAL PORT AU PORT #1

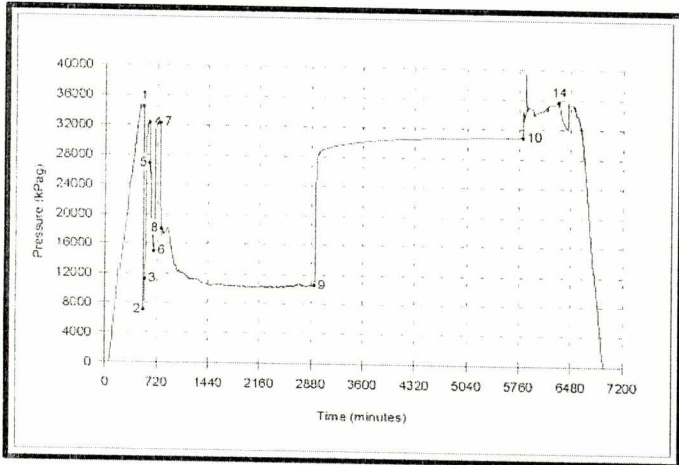
"HUGHES 48.490/59.226

Baker Oil Tools

LJO I rr ^

Formation: AGUATHUNA
Interval - from: 3335.00 to: 3482.00 m

Recorder# 80121 at 3340.00 m



Test Date: 2002-08-11
Test Type: CASING PACKER
Tester Name: BRIAN MAGNUS
Drill Pipe O.D.: 102.00 mm
Drill Collar I.D.: 60.00 mm
Drill Collar Length: 471.25 m
Hole Size: 156.00 mm

Blow Description:

Weak air blow increasing to strong in 4 minutes then steady throughout. No gas to surface.

Gas to surface immediately with fluid to surface in 90 minutes.

Remarks:

Mechanically successful test. Results suggest relatively high permeability within the interval tested. All surface equipment was pressure tested to 16 mPa prior to opening the tool. Flow rates taken by Maritime Testers at the separator. The fluid to surface started out as drilling mud then turned to a light oil (50.8 API) shortly after. The recovered fluid was determined by reverse circulating to the separator and back calculating the linear height.

Maximum Btm Hole Temperature @ FSI: 49.0 C

Pressure (kPag)	Time (min)	Extrapolated Pressure (kPag)	(min)
1	Initial Hydrostatic	34414	2
7063	3 End of 1st Flow	11163	16.2
32298	60.8	32610.7	5
26784	6 End of 2nd Flow		
14897	60.5	32272	88.5
32534.1	8 Start of 3rd Flow	18034	9
10496	2146.5		
30848	2879.5	31342.6	14
35572			

Liquid Recovery of 1566.00 m

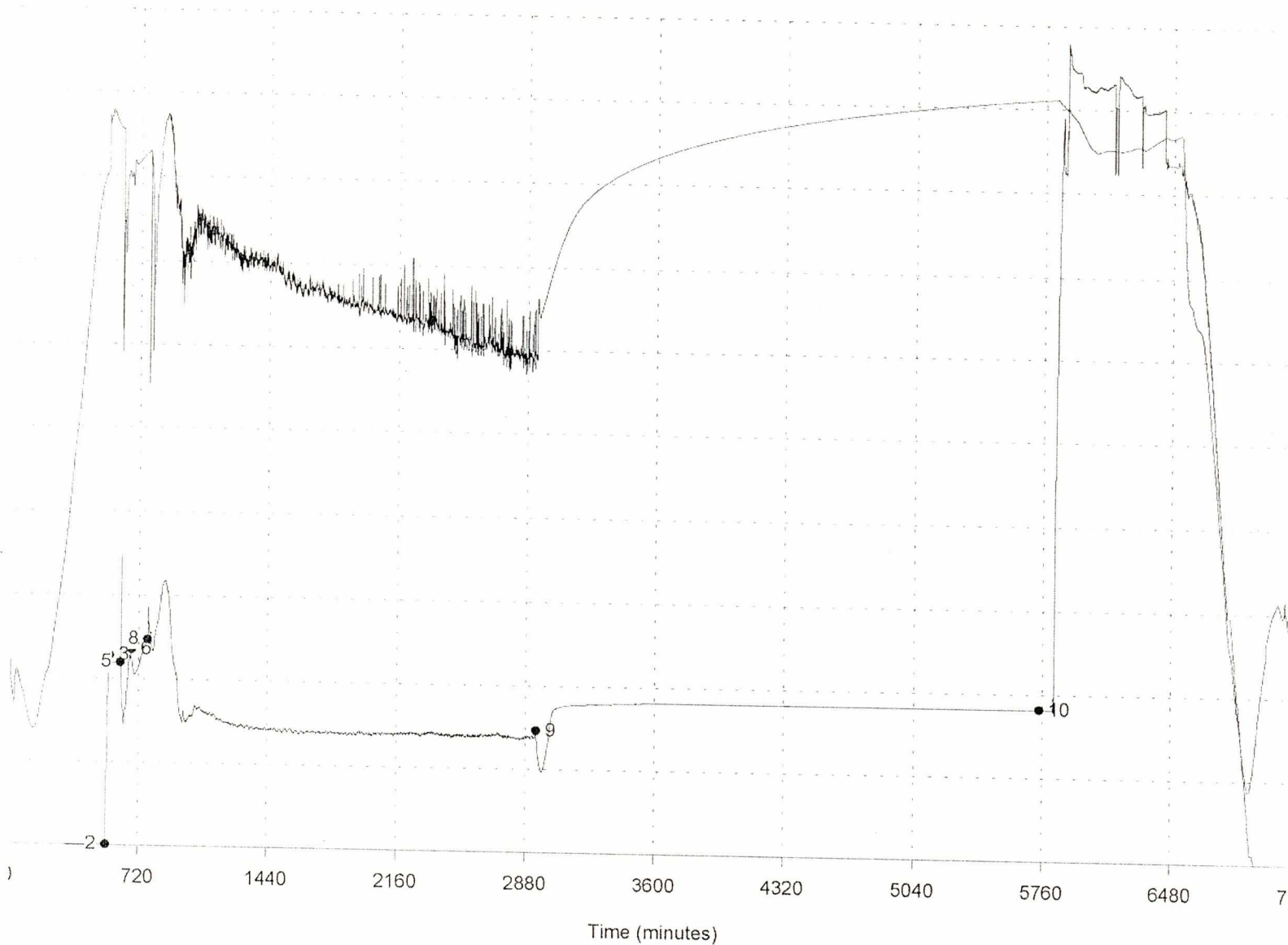
Test was reversed out.

Recovery	Description	Salinity
1566.00 m	CONDENSATE	

CDN IMPERIAL PORT AU PORT #1
48.490/59.226
DST #: 2
Recorder: 80242

Pressure (kPag) at Critical Points
2: 45 6: 9912 10: 7613
3: 9588 8: 10394
5: 9227 9: 6125

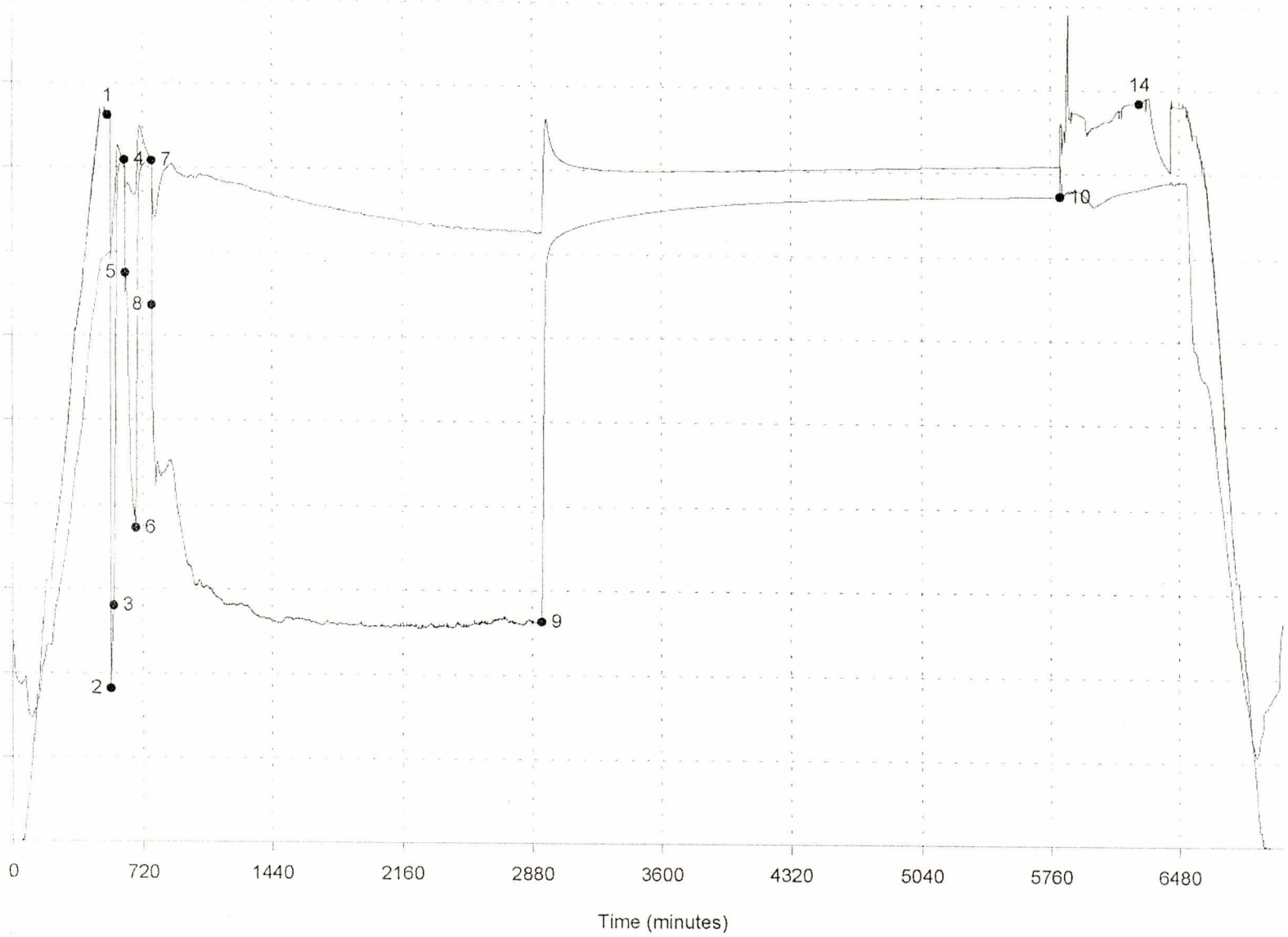
Recovery recorder



CDN IMPERIAL PORT AU PORT #1
48.490/59.226
DST #. 2
Recorder: 80142

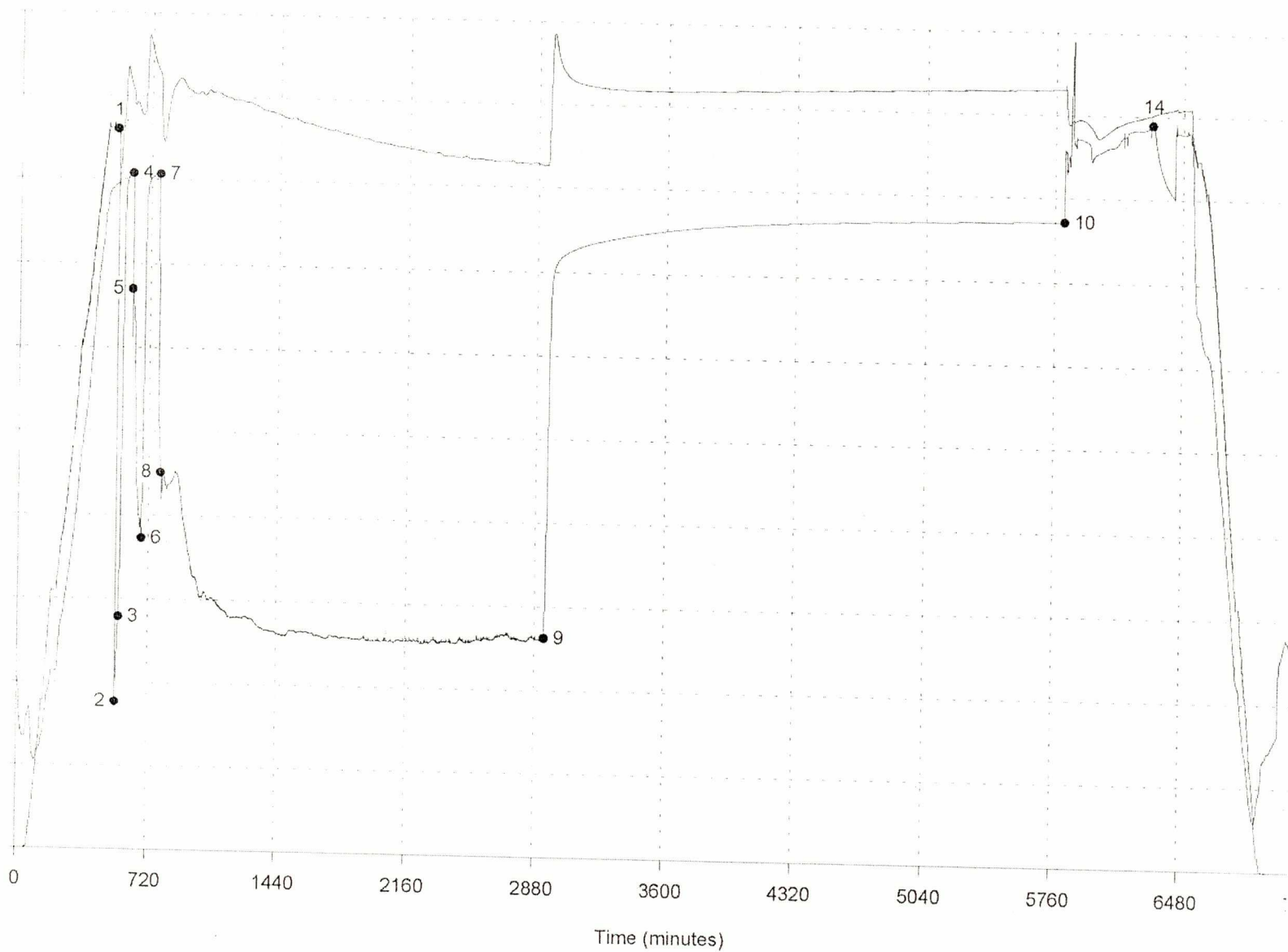
1: 34464	4: 32347	7: 32323	10: 308
2: 7247	5: 26988	8: 25455	14: 353
3: 11202	6: 14896	9: 10522	

Other electronic gauge



CDN IMPERIAL PORT AU PORT #1
48.490/59.226
DST #: 2
Recorder: 80121

1: 34414	4: 32298	7: 32272	10: 3084
2: 7063	5: 26784	8: 18034	14: 355
3: 11163	6: 14897	9: 10496	



CDN IMPERIAL PORT AU PORT #1

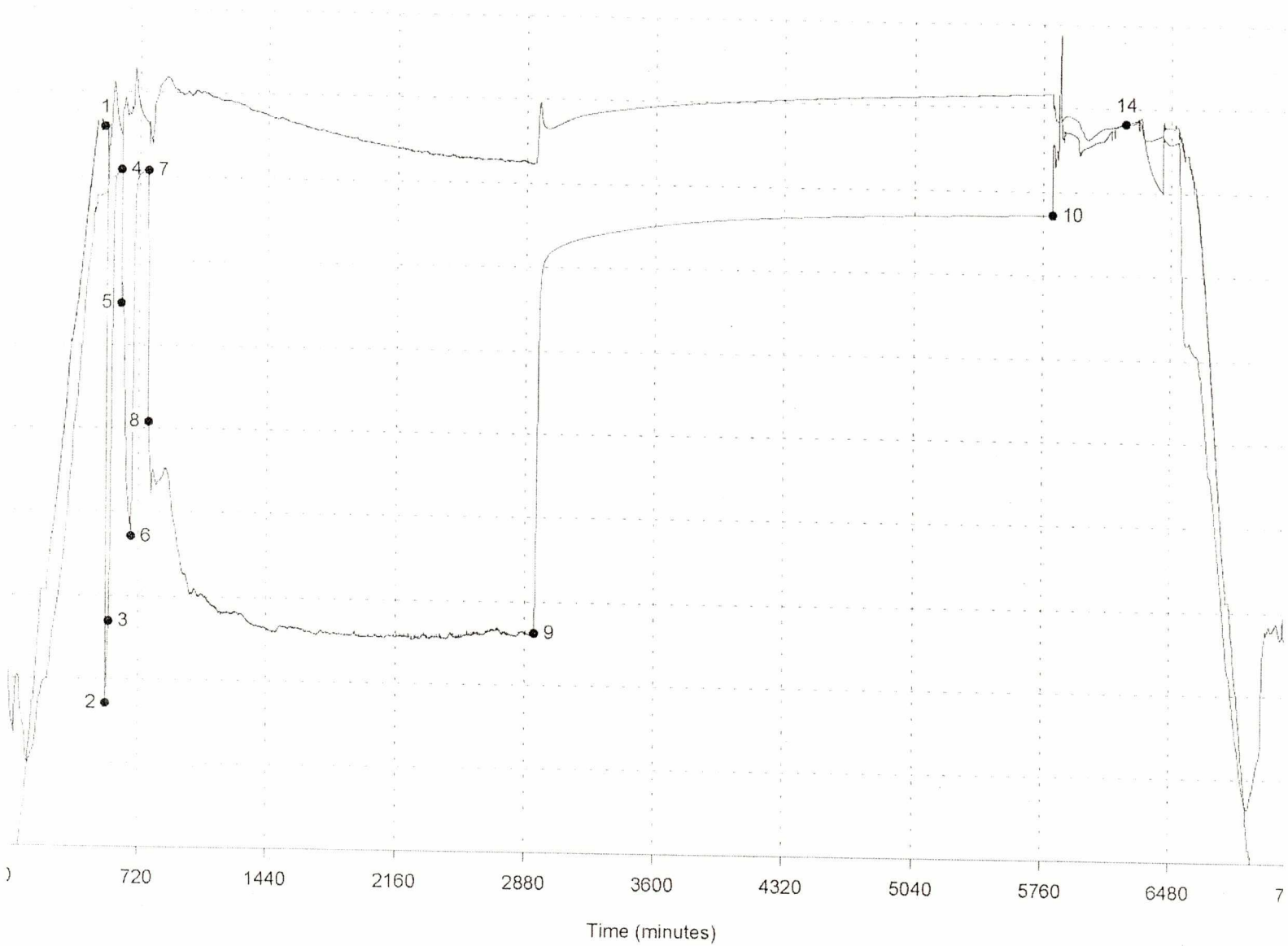
48.490/59.226

DST #: 2

Recorder: 80383

1: 34359	4: 32314	7: 32288	10: 3086
2: 6827	5: 25952	8: 20292	14: 3527
3: 10754	6: 14828	9: 10484	

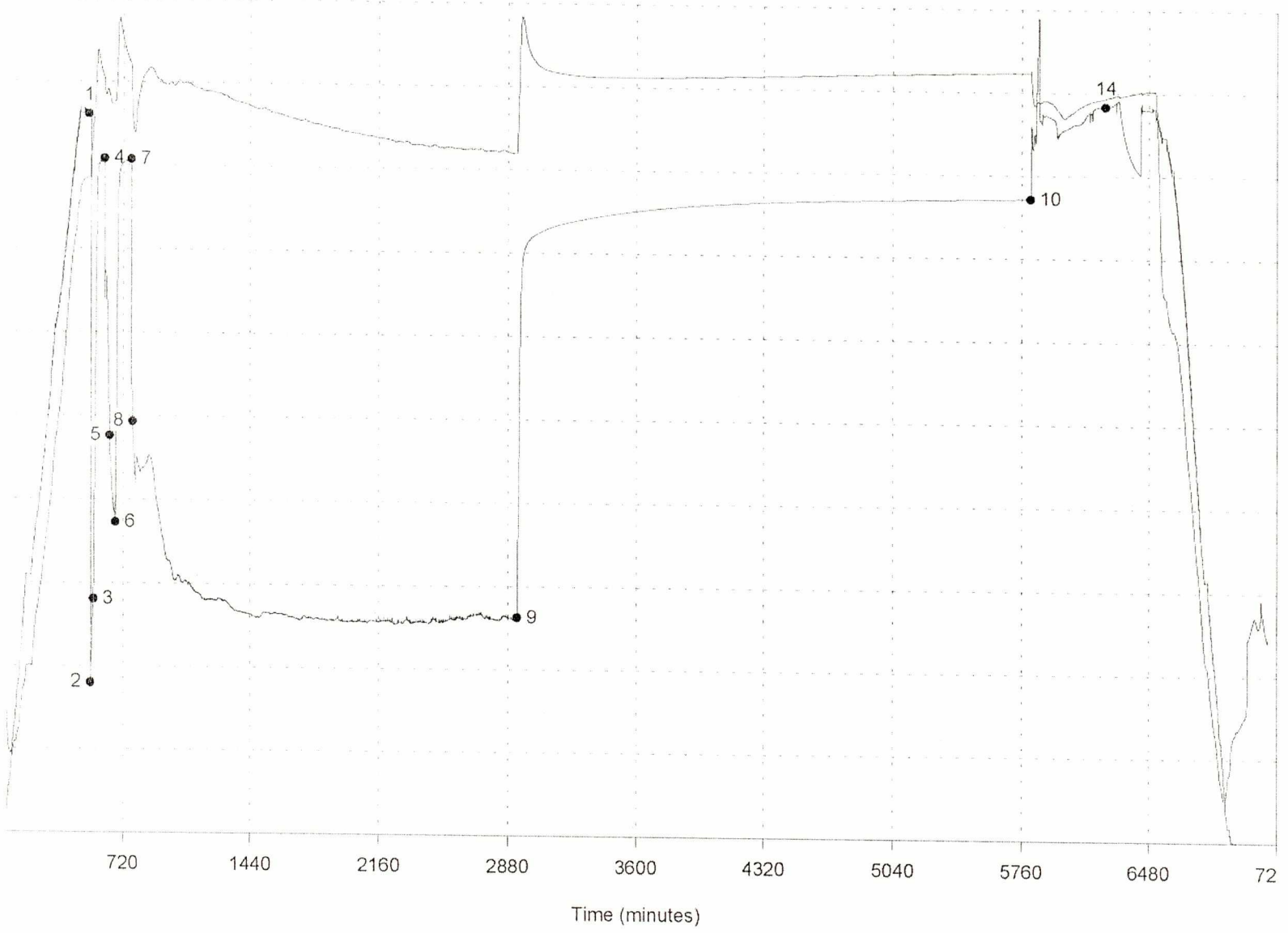
Above interval



DN IMPERIAL PORT AU PORT #1
3.490/59.226
ST #: 2
ecorder: 80129

1: 34432	4: 32317	7: 32293	10: 30868
2: 7190	5: 19054	8: 19754	14: 35326
3: 11230	6: 14889	9: 10497	

Other electronic gauge



CDN IMPERIAL PORT AU PORT #1
48.490/59.226
DST#2
Recorder 80121

Build-up and Flow Curve Increments

Flow# 1

Chart Label	Time (min)	Pressure (kPag)
2	0.0	7063
	0.5	7815
	1.0	7857
	1.5	8007
	2.0	8136
	2.5	8275
	3.0	8351
	3.5	8386
	4.0	8438
	4.5	8516
	5.0	8582
	5.5	8723
	6.0	8858
	6.5	8975
	7.0	9094
	7.5	9229
	8.0	9418
	8.5	9633
	9.0	9802
	9.5	9943
3	10.0	10065
	10.5	10191
	11.0	10313
	11.5	10417
	12.0	10525
	12.5	10629
	13.0	10721
	13.5	10803
14.0	10889	
14.5	10959	
15.0	11029	
15.5	11097	
16.0	11149	
16.2	11163	

Shutin# 1

Chart Label	Time (min)	Delta P (kPag)	Pressure (kPag)	Abscissa (T+dT)/dT	Used for Extrap
	0.0		11163		
	1.0	877	12039	17.2500	
	2.0	1649	12811	9.1250	
	3.0	2429	13592	6.4167	
	4.0	3235	14397	5.0625	
	5.0	4073	15236	4.2500	
	6.0	4946	16109	3.7083	
	7.0	5861	17024	3.3214	
	8.0	6819	17981	3.0312	
	9.0	7825	18988	2.8056	
	10.0	8869	20032	2.6250	
	11.0	9955	21118	2.4773	
	12.0	11076	22239	2.3542	
	13.0	12225	23388	2.2500	
	14.0	13383	24545	2.1607	
	15.0	14526	25688	2.0833	
	16.0	15628	26790	2.0156	
	17.0	16643	27806	1.9559	
	18.0	17533	28696	1.9028	
	19.0	18293	29456	1.8553	
	20.0	18922	30084	1.8125	
	21.0	19415	30578	1.7738	
	22.0	19787	30950	1.7386	
	23.0	20063	31226	1.7065	
	24.0	20267	31430	1.6771	
	25.0	20414	31577	1.6500	
	26.0	20521	31684	1.6250	
	27.0	20606	31768	1.6019	
	28.0	20671	31834	1.5804	
	29.0	20721	31884	1.5603	
	30.0	20763	31925	1.5417	
	31.0	20802	31964	1.5242	
	32.0	20834	31997	1.5078	
	33.0	20863	32026	1.4924	
	34.0	20888	32050	1.4779	
	35.0	20910	32073	1.4643	
	36.0	20930	32093	1.4514	
	37.0	20947	32110	1.4392	

Note: Increment listing is filtered to include critical data only. Complete time/pressure data are available in electronic or printed format.

CDN IMPERIAL PORT AU PORT #1
48.490/59.226
DST#2
Recorder 80121

Build-up and Flow Curve Increments

Shutin# 1

Chart Label	Time (min)	Delta P (kPag)	Pressure (kPag)	Abscissa (T+dT)/dT	Used for Extrap
	38.0	20961	32124	1.427	
	39.0	20977	32140	1.416	
	40.0	20991	32154	1.406	
	41.0	21004	32167	1.3963	
	42.0	21015	32178	1.386	*
	43.0	21027	32190	1.377	*
	44.0	21036	32199	1.3693	*
	45.0	21046	32209	1.3611	*
	46.0	21056	32218	1.3533	*
	47.0	21065	32228	1.345	*
	48.0	21072	32235	1.3385	*
	49.0	21078	32240	1.331	*
	50.0	21085	32248	1.325	*
	51.0	21090	32253	1.318	*
	52.0	21096	32259	1.3125	*
	53.0	21102	32265	1.306	*
	54.0	21106	32268	1.300	*
	55.0	21111	32273	1.2955	*
	56.0	21116	32279	1.290	*
	57.0	21121	32284	1.2851	*
	58.0	21124	32287	1.280	*
	59.0	21129	32291	1.275	*
	60.0	21133	32296	1.2708	*
4	60.8	21135	32298	1.2675	*

Flow# 2

Chart Label	Time (min)	Pressure (kPag)
5	0.0	26784
	1.0	26918
	2.0	26944
	3.0	26908
	4.0	26846
	5.0	26777
	6.0	26734
	7.0	26685

Shutin# 2

Chart Label	Time (min)	Delta P (kPag)	Pressure (kPag)	Abscissa (T+dT)/dT	Used for Extrap
	0.0		14897		
	1.0	911	15808	77.7500	
	2.0	1862	16759	39.3750	
	3.0	2815	17712	26.5833	
	4.0	3799	18696	20.1875	
	5.0	4827	19724	16.3500	
	6.0	5901	20798	13.7917	
	7.0	7026	21923	11.9643	

Note: Increment listing is filtered to include critical data only. Complete time/pressure data are available in electronic or printed format.

CDN IMPERIAL PORT AU PORT #1
48.490/59.226
DST#2
Recorder 80121

Build-up and Flow Curve Increments

Flow# 2

Chart Label	Time (min)	Pressure (kPag)
	8.0	26634
	9.0	26329
	10.0	26007
	11.0	25802
	12.0	25642
	13.0	25510
	14.0	25377
	15.0	25324
	16.0	25012
	17.0	24185
	18.0	23398
	19.0	23275
	20.0	22678
	21.0	22177
	22.0	21792
	23.0	21493
	24.0	21099
	25.0	20655
	26.0	20066
	27.0	19549
	28.0	19153
	29.0	18898
	30.0	18314
	31.0	17904
	32.0	17592
	33.0	17435
	34.0	17276
	35.0	17210
	36.0	17120
	37.0	16967
	38.0	16813
	39.0	16703
	40.0	16599
	41.0	16453
	42.0	16335
	43.0	16206
	44.0	16063
	45.0	15925

Shutin# 2

Chart Label	Time (min)	Delta P (kPag)	Pressure (kPag)	Abscissa (T+dT)/dT	Used for Extrap
	8.0	8199	23096	10.5938	
	9.0	9395	24292	9.5278	
	10.0	10596	25493	8.6750	
	11.0	11741	26638	7.9773	
	12.0	12795	27692	7.3958	
	13.0	13717	28614	6.9038	
	14.0	14491	29388	6.4821	
	15.0	15110	30007	6.1167	
	16.0	15582	30479	5.7969	
	17.0	15931	30828	5.5147	
	18.0	16184	31081	5.2639	
	19.0	16367	31264	5.0395	
	20.0	16502	31399	4.8375	
	21.0	16604	31502	4.6548	
	22.0	16685	31582	4.4886	
	23.0	16749	31646	4.3370	
	24.0	16802	31699	4.1979	
	25.0	16842	31739	4.0700	
	26.0	16882	31779	3.9519	
	27.0	16917	31814	3.8426	
	28.0	16948	31845	3.7411	
	29.0	16975	31872	3.6466	
	30.0	17000	31897	3.5583	
	31.0	17022	31919	3.4758	
	32.0	17042	31939	3.3984	
	33.0	17062	31959	3.3258	
	34.0	17079	31976	3.2574	
	35.0	17096	31993	3.1929	
	36.0	17110	32007	3.1319	
	37.0	17124	32021	3.0743	
	38.0	17137	32034	3.0197	
	39.0	17150	32047	2.9679	
	40.0	17161	32058	2.9188	
	41.0	17172	32069	2.8720	
	42.0	17182	32079	2.8274	
	43.0	17192	32089	2.7849	
	44.0	17200	32097	2.7443	
	45.0	17209	32106	2.7056	

Note: Increment listing is filtered to include critical data only. Complete time/pressure data are available in electronic or printed format.

CDN IMPERIAL PORT AU PORT #1
48.490/59.226
DST#2
Recorder 80121

Build-up and Flow Curve Increments

Flow# 2

Chart Label	Time (min)	Pressure (kPag)
	46.0	15781
	47.0	15619
	48.0	15488
	49.0	15389
	50.0	15399
	51.0	15415
	52.0	15499
	53.0	15666
	54.0	15772
	55.0	15765
	56.0	15509
	57.0	15337
	58.0	15239
	59.0	15117
	60.0	15009
6	60.5	14897

Shutin# 2

Chart Label	Time (min)	Delta P (kPag)	Pressure (kPag)	Abscissa (T+dT)/dT	Used for Extrap
	46.0	17217	32114	2.6685	
	47.0	17225	32122	2.6330	
	48.0	17232	32129	2.5990	
	49.0	17238	32135	2.5663	
	50.0	17245	32142	2.5350	*
	51.0	17251	32148	2.5049	*
	52.0	17258	32155	2.4760	*
	53.0	17263	32160	2.4481	*
	54.0	17268	32165	2.4213	*
	55.0	17274	32171	2.3955	*
	56.0	17279	32176	2.3705	*
	57.0	17283	32180	2.3465	*
	58.0	17288	32185	2.3233	*
	59.0	17292	32189	2.3008	*
	60.0	17296	32194	2.2792	*
	61.0	17301	32198	2.2582	*
	62.0	17305	32202	2.2379	*
	63.0	17309	32206	2.2183	*
	64.0	17312	32209	2.1992	*
	65.0	17316	32213	2.1808	*
	66.0	17319	32216	2.1629	*
	67.0	17322	32219	2.1455	*
	68.0	17326	32223	2.1287	*
	69.0	17328	32225	2.1123	*
	70.0	17331	32228	2.0964	*
	71.0	17334	32232	2.0810	*
	72.0	17337	32234	2.0660	*
	73.0	17340	32237	2.0514	*
	74.0	17342	32239	2.0372	*
	75.0	17345	32242	2.0233	*
	76.0	17348	32245	2.0099	*
	77.0	17350	32247	1.9968	*
	78.0	17353	32250	1.9840	*
	79.0	17355	32252	1.9715	*
	80.0	17358	32255	1.9594	*
	81.0	17359	32256	1.9475	*
	82.0	17362	32259	1.9360	*
	83.0	17364	32261	1.9247	*

Note: Increment listing is filtered to include critical data only. Complete time/pressure data are available in electronic or printed format.

CDN IMPERIAL PORT AU PORT #1
48.490/59.226
DST#2
Recorder 80121

Build-up and Flow Curve Increments

Shutin# 2

Chart Label	Time (min)	Delta P (kPag)	Pressure (kPag)	Abscissa (T+dT)/dT	Used for Extrap
7	84.0	17366	32263	1.913	*
	85.0	17368	32265	1.902	*
	86.0	17370	32267	1.892	*
	87.0	17372	32269	1.882	*
	88.0	17374	32271	1.872	*
	88.5	17375	32272	1.867	*

Flow# 3

Shutin# 3

Chart Label	Time (min)	Pressure (kPag)
8	0.0	18034
	18.2	17904
	36.5	17281
	54.8	17502
	73.0	17796
	91.2	18026
	109.5	17182
	127.8	15778
	146.0	14959
	164.2	14098
	182.5	13148
	200.8	13044
	219.0	12309
	237.2	12130
	255.5	12342
	273.8	12036
	292.0	12130
	310.2	12030
	328.5	11758
	346.8	11604
	365.0	11493
	383.2	11240
	401.5	11206
	419.8	11252
	438.0	11245
	456.2	11191

Chart Label	Time (min)	Delta P (kPag)	Pressure (kPag)	Abscissa (T+dT)/dT	Used for Extrap
	0.0		10496		
	24.2	16124	26621	92.6804	
	48.5	17795	28292	46.8402	
	72.8	18134	28630	31.5601	
	97.0	18314	28811	23.9201	
	121.2	18440	28936	19.3361	
	145.5	18542	29039	16.2801	
	169.8	18636	29132	14.0972	
	194.0	18719	29216	12.4601	
	218.2	18791	29287	11.1867	
	242.5	18852	29349	10.1680	
	266.8	18908	29404	9.3346	
	291.0	18960	29456	8.6400	
	315.2	19009	29506	8.0523	
	339.5	19056	29552	7.5486	
	363.8	19101	29597	7.1120	
	388.0	19144	29640	6.7300	
	412.2	19185	29682	6.3930	
	436.5	19225	29722	6.0934	
	460.8	19264	29760	5.8253	
	485.0	19300	29796	5.5840	
	509.2	19335	29832	5.3657	
	533.5	19369	29866	5.1673	
	557.8	19402	29898	4.9861	
	582.0	19433	29930	4.8200	
	606.2	19464	29960	4.6672	

Note: Increment listing is filtered to include critical data only. Complete time/pressure data are available in electronic or printed format.

CDN IMPERIAL PORT AU PORT #1
48.490/59.226
DST#2
Recorder 80121

Build-up and Flow Curve Increments

Flow# 3

Chart Label	Time (min)	Pressure (kPag)
	474.5	11284
	492.8	11229
	511.0	11190
	529.2	11065
	547.5	10875
	565.8	10754
	584.0	10640
	602.2	10645
	620.5	10611
	638.8	10595
	657.0	10508
	675.2	10443
	693.5	10413
	711.8	10384
	730.0	10636
	748.2	10611
	766.5	10588
	784.8	10581
	803.0	10562
	821.2	10576
	839.5	10537
	857.8	10525
	876.0	10405
	894.2	10389
	912.5	10337
	930.8	10285
	949.0	10332
	967.2	10418
	985.5	10397
	1003.8	10340
	1022.0	10335
	1040.2	10349
	1058.5	10317
	1076.8	10285
	1095.0	10269
	1113.2	10264
	1131.5	10283
	1149.8	10367

Shutin# 3

Chart Label	Time (min)	Delta P (kPag)	Pressure (kPag)	Abscissa (T+dT)/dT	Used for Extrap
	630.5	19493	29990	4.5262	
	654.8	19521	30018	4.3956	
	679.0	19548	30045	4.2743	
	703.2	19574	30071	4.1614	
	727.5	19600	30096	4.0560	
	751.8	19624	30120	3.9574	
	776.0	19647	30144	3.8650	
	800.2	19670	30166	3.7782	
	824.5	19692	30188	3.6965	
	848.8	19713	30210	3.6194	
	873.0	19734	30230	3.5467	
	897.2	19753	30250	3.4778	
	921.5	19773	30269	3.4126	
	945.8	19791	30288	3.3508	
	970.0	19809	30305	3.2920	*
	994.2	19826	30322	3.2361	*
	1018.5	19843	30339	3.1829	*
	1042.8	19858	30355	3.1321	*
	1067.0	19874	30370	3.0836	*
	1091.2	19889	30385	3.0373	*
	1115.5	19903	30400	2.9931	*
	1139.8	19916	30412	2.9506	*
	1164.0	19929	30425	2.9100	*
	1188.2	19942	30439	2.8710	*
	1212.5	19954	30451	2.8336	*
	1236.8	19966	30463	2.7977	*
	1261.0	19978	30474	2.7631	*
	1285.2	19989	30486	2.7298	*
	1309.5	19999	30496	2.6978	*
	1333.8	20010	30507	2.6669	*
	1358.0	20020	30517	2.6372	*
	1382.2	20030	30527	2.6084	*
	1406.5	20040	30536	2.5807	*
	1430.8	20049	30545	2.5539	*
	1455.0	20058	30554	2.5280	*
	1479.2	20066	30563	2.5030	*
	1503.5	20075	30572	2.4787	*
	1527.8	20083	30580	2.4552	*

Note: Increment listing is filtered to include critical data only. Complete time/pressure data are available in electronic or printed format.

CDN IMPERIAL PORT AU PORT #1
48.490/59.226
DST#2
Recorder 80121

Build-up and Flow Curve Increments

Flow# 3

Chart Label	Time (min)	Pressure (kPag)
	1168.0	10235
	1186.2	10206
	1204.5	10208
	1222.8	10246
	1241.0	10208
	1259.2	10230
	1277.5	10194
	1295.8	10220
	1314.0	10173
	1332.2	10295
	1350.5	10251
	1368.8	10217
	1387.0	10250
	1405.2	10283
	1423.5	10270
	1441.8	10219
	1460.0	10126
	1478.2	10140
	1496.5	10187
	1514.8	10195
	1533.0	10368
	1551.2	10277
	1569.5	10198
	1587.8	10233
	1606.0	10284
	1624.2	10247
	1642.5	10202
	1660.8	10179
	1679.0	10373
	1697.2	10243
	1715.5	10274
	1733.8	10240
	1752.0	10323
	1770.2	10371
	1788.5	10375
	1806.8	10373
	1825.0	10419
	1843.2	10369

Shutin# 3

Chart Label	Time (min)	Delta P (kPag)	Pressure (kPag)	Abscissa (T+dT)/dT	Used for Extrap
	1552.0	20091	30588	2.4325	*
	1576.2	20100	30596	2.4105	*
	1600.5	20107	30603	2.3891	*
	1624.8	20114	30611	2.3684	*
	1649.0	20121	30618	2.3482	*
	1673.2	20129	30625	2.3287	*
	1697.5	20135	30631	2.3097	*
	1721.8	20142	30639	2.2913	*
	1746.0	20148	30645	2.2733	*
	1770.2	20155	30651	2.2559	*
	1794.5	20161	30658	2.2389	*
	1818.8	20167	30663	2.2224	*
	1843.0	20173	30669	2.2063	*
	1867.2	20179	30675	2.1907	*
	1891.5	20184	30681	2.1754	*
	1915.8	20189	30686	2.1605	*
	1940.0	20195	30692	2.1460	*
	1964.2	20201	30697	2.1319	*
	1988.5	20206	30702	2.1181	*
	2012.8	20211	30708	2.1046	*
	2037.0	20216	30713	2.0914	*
	2061.2	20221	30718	2.0786	*
	2085.5	20226	30722	2.0661	*
	2109.8	20230	30727	2.0538	*
	2134.0	20235	30732	2.0418	*
	2158.2	20240	30736	2.0301	*
	2182.5	20244	30741	2.0187	*
	2206.8	20249	30745	2.0075	*
	2231.0	20254	30750	1.9965	*
	2255.2	20258	30754	1.9858	*
	2279.5	20262	30758	1.9753	*
	2303.8	20266	30762	1.9651	*
	2328.0	20270	30767	1.9550	*
	2352.2	20274	30771	1.9452	*
	2376.5	20279	30775	1.9355	*
	2400.8	20282	30779	1.9261	*
	2425.0	20286	30783	1.9168	*
	2449.2	20290	30786	1.9077	*

Note: Increment listing is filtered to include critical data only. Complete time/pressure data are available in electronic or printed format.

CDN IMPERIAL PORT AU PORT #1
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DST#2
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Build-up and Flow Curve Increments

Flow# 3

Chart Label	Time (min)	Pressure (kPag)
	1861.5	10369
	1879.8	10530
	1898.0	10557
	1916.2	10614
	1934.5	10632
	1952.8	10667
	1971.0	10483
	1989.2	10480
	2007.5	10422
	2025.8	10361
	2044.0	10324
	2062.2	10470
	2080.5	10552
	2098.8	10481
	2117.0	10411
	2135.2	10458
9	2146.5	10496

Shutin# 3

Chart Label	Time (min)	Delta P (kPag)	Pressure (kPag)	Abscissa (T+dT)/dT	Used for Extrap
	2473.5	20294	30790	1.8988	*
	2497.8	20298	30794	1.8901	*
	2522.0	20301	30798	1.8815	*
	2546.2	20305	30801	1.8731	*
	2570.5	20309	30805	1.8649	*
	2594.8	20312	30809	1.8568	*
	2619.0	20316	30812	1.8489	*
	2643.2	20320	30816	1.8411	*
	2667.5	20323	30820	1.8335	*
	2691.8	20326	30823	1.8259	*
	2716.0	20330	30826	1.8186	*
	2740.2	20333	30830	1.8113	*
	2764.5	20336	30833	1.8042	*
	2788.8	20340	30836	1.7972	*
	2813.0	20344	30840	1.7903	*
	2837.2	20346	30843	1.7836	*
	2861.5	20350	30846	1.7770	*
10	2879.5	20352	30848	1.7721	*

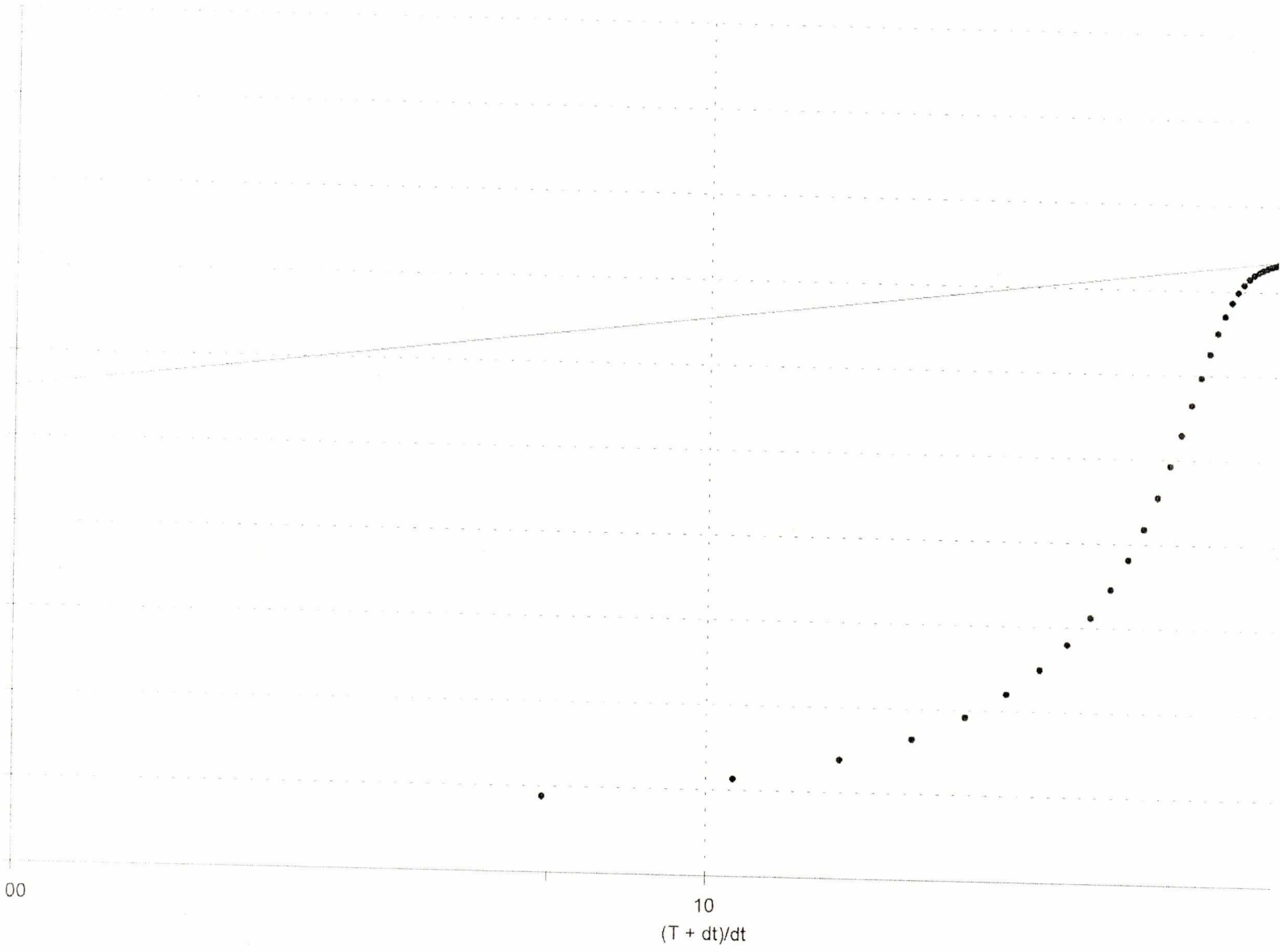
Horner Extrapolation

Shut-in#	Extrapolated Pressure (kPag)	Extrapolated Slope (kPag/cycle)
1	32610.7	2998.85797
2	32534.1	956.47939
3	31342.6	1971.93978

Note: Increment listing is filtered to include critical data only. Complete time/pressure data are available in electronic or printed format.

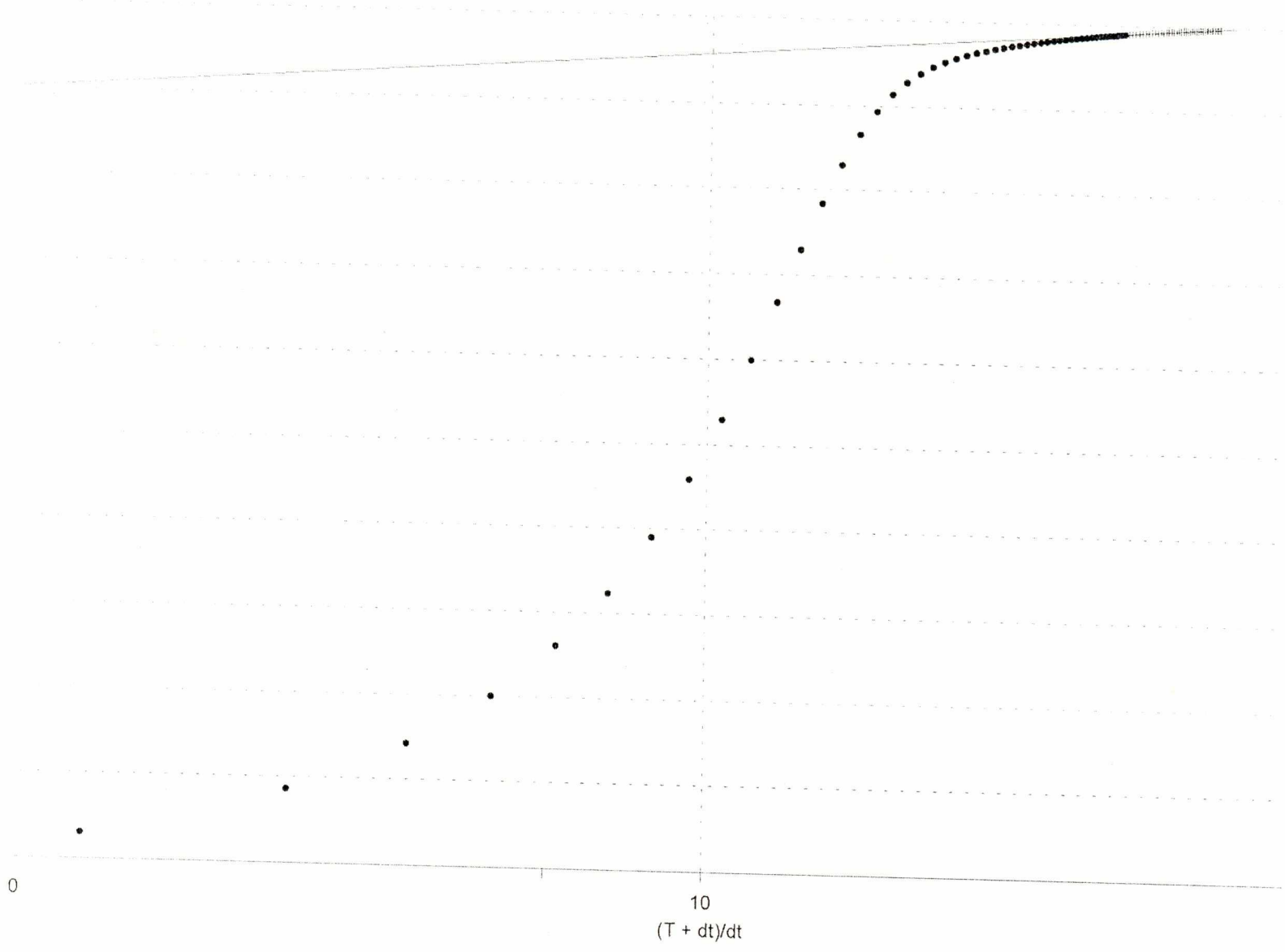
CDN IMPERIAL PORT AU PORT #1
48.490/59.226
DST #: 2
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Shut-in #1
Slope = 2998.86 kPag/cycle
Extrapolated Pressure = 32610.66 kPa



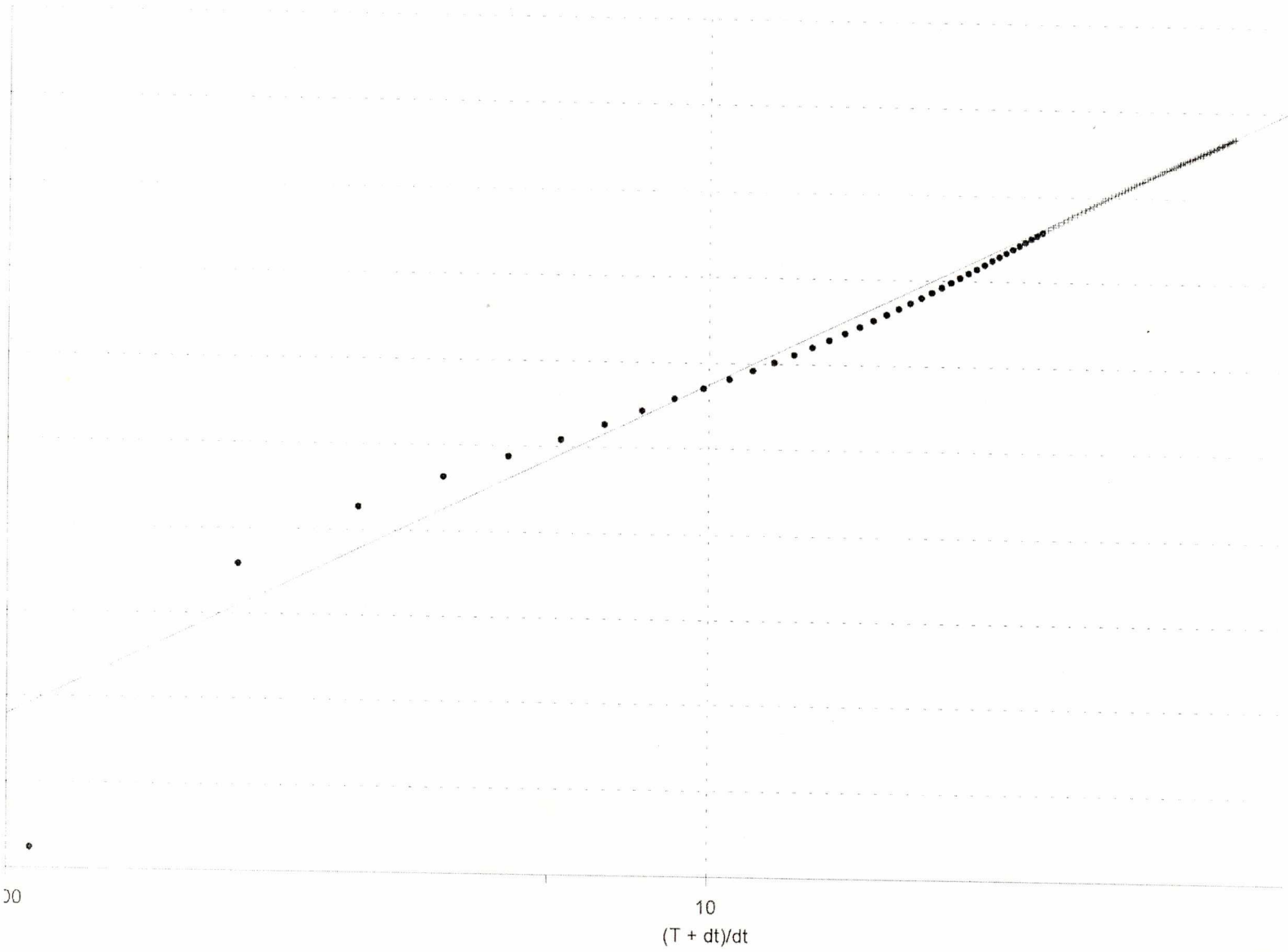
CDN IMPERIAL PORT AU PORT #1
48.490/59.226
DST #: 2
Recorder: 80121

Shut-in #2
Slope = 956.48 kPag/cycle
Extrapolated Pressure = 32534.11 kPa



CDN IMPERIAL PORT AU PORT #1
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Shut-in #3
Slope = 1971.94 kPag/cycle
Extrapolated Pressure = 31342.56 kPa



Attachment D: ST #2 Flow Data

FieldNotes

Field Measurements

Date	Time	C	Size	Pres	Pres	Temp	Pres	Pres	Orifice	Temp	Rate	Gas1	Oil Cum	Gain	Mud Cum	Gain	API 1	Salinity	pH	Mud Cut	Calc	Calc
																					Inc	Inc
yyyy/mm/dd	hh:mm:ss	mm	kPa(g)	kPa(g)	°C	kPa(g)	kPa	mm	°C	10 ³ m ³ /d	10 ³ m ³	m ³	m ³	m ³	m ³	* API	ppm	%				

1	2002/08/10	19:30:00																				
2		21:30:00																				
3	2002/08/11	02:15:00																				
4		02:30:00																				
6		02:36:00																				
6		02:37:00																				
7		02:48:00																				
8		02:52:00																				
8		03:52:00																				
10		03:57:00																				
11		04:00:00	50.20		5.00	11.0																
12		04:15:00	50.20		5.00	11.0																
13		04:30:00	50.20		5.00	11.0																
14		04:45:00	50.20		30.00	12.0																
16		04:52:00	50.20		52.00	13.0																
16		04:52:00																				

2002/08/10 19:30:00 To 2002/08/11 06:22:00

Gas		Cum.	10 ³ m ³
Oil	0.000	Cum.	0.000 m ³
MUD	0.000	Cum.	0.000 m ³

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FieldNotes

Field Measurements

Date	Time	C	Size	Pres	Pres	Temp	Pres	Pres	Orifice	Temp	Rate	Gas1	Cum.	Measured	Oil	Gain	Mud Cum	Gain	API	Salinity	pH	Mud Cut	Calc	Calc		
																							Inc	Inc		
yyyy/mm/dd	hh:mm:ss		mm	kPa(g)	kPa(g)	°C	kPa(g)	kPa	mm	°C	10 ³ m ³ /d	10 ³ m ³	m ³	m ³	m ³	m ³	m ³	m ³	° API	ppm	%					
2002/08/11	06:22:00																									
	06:23:00																									
	06:30:00		60.80			0.06																				
	07:00:00		50.80			0.06																				
	07:30:00		50.80			14.00	14.0	14.06	4.23	34.83	13.00	6.362	2.681	0.000	0.000									6.00		
	07:40:00																									
	07:50:00																									
	08:00:00		50.80			260.00	12.0																			
	08:18:00																									
	08:20:00																									
	08:25:00																									
	08:25:00																									
	08:29:00																									
	08:30:00		12.70			410.00	13.0	296.00	47.31	60.80	43.80	63.418	4.114	0.000	0.000										0.00	
	08:40:00																									
	08:50:00																									
	08:50:00																									
	09:00:00		18.06			2365.00	14.0	172.00	36.11	60.80	36.80	62.718	5.323	1.760	1.760	0.040	0.040	48.70							0.00	
	09:30:00		18.06			1720.00	14.0	267.00	18.82	60.80	32.80	41.380	6.304	3.420	1.660	0.090	0.060								2.82	
	09:41:00																									
	09:45:00																									
	10:00:00		18.06			1130.00	14.0	207.00	17.83	60.80	31.00	38.281	7.144	4.640	1.220	0.140	0.060	48.80							3.84	
	10:30:00		18.06			1060.00	13.0	166.00	16.84	60.80	29.00	34.670	7.812													
	11:00:00		18.06			1405.00	12.0	183.00	14.84	60.80	29.00	36.060	8.637	6.880	1.310	0.290	0.080								4.38	
	11:30:00		18.06			1330.00	12.0	183.00	14.84	60.80	28.00	36.140	8.389													
	12:00:00		18.06			1296.00	12.0	178.00	16.44	60.80	24.00	36.100	10.101	7.140	1.180	0.240	0.040	48.80							3.88	
	12:30:00		18.06			1260.00	13.0	186.00	16.89	60.80	22.00	36.980	10.841													
	13:00:00		18.06			1277.00	12.0	183.00	16.43	60.80	20.00	37.402	11.806	8.480	1.320	0.480	0.242								18.48	
	13:20:00																									
	13:30:00		18.06			1288.00	12.0	245.00	61.79	34.83	26.00	33.623	12.344													

2002/08/11 06:22:00 To 2002/08/12 06:00:00
 Gas 35.138 Cum. 35.138 10³m³
 Oil 29.890 Cum. 29.890 m³
 MUD 1.525 Cum. 1.525 m³

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FieldNotes

Field Measurements

Date	Time	C Size	Pres	Pres	Temp	Pres	Pres	Orifice1	Temp	Rate	Gas1	Cum. Gas1	Measured Oil	Oil Cum	Gain	Measured Mud1	Mud Cum	Gain	API 1	Salinity	pH	Mud Cut	Calc	Calc
																							Inc	Inc
yyyy/mm/dd	hh:mm:ss	mm	kPa(g)	kPa(g)	°C	kPa(g)	kPa	mm	°C	10 ⁻³ m ³ /h	10 ⁻³ m ³	m ³	m ³	m ³	m ³	m ³	m ³	° API	ppm		%			
2002/08/11	14:00:00	18.06		1277.00	12.0	246.89	43.82	34.83	23.89	36.21	13.054		8.880	1.420		0.670	0.180	48.60				11.26		
	14:30:00	18.06		1266.00	12.0	246.00	44.32	34.83	25.00	36.86	13.657													
	15:00:00	18.06		1220.00	12.0	234.00	42.08	34.83	27.00	29.38	14.264		11.060	1.180		0.790	0.120					8.23		
	15:30:00	18.06		1180.00	12.0	241.00	46.07	34.83	27.00	36.74	14.810													
	16:00:00	18.06		1200.00	12.0	248.00	46.06	34.83	27.00	32.11	15.566		12.320	1.260		0.820	0.030	50.30				2.91		
	16:30:00	18.06		1220.00	12.0	266.00	47.81	34.83	27.00	32.34	16.237													
	17:00:00	18.06		1266.00	12.0	241.00	44.57	34.83	26.00	30.62	16.853		13.740	1.420		0.840	0.830					2.08		
	17:30:00	18.06		1376.00	12.0	262.00	51.78	34.83	26.00	34.11	17.567													
	18:00:00	18.06		1326.00	12.0	262.00	47.80	34.83	27.00	32.64	18.262		16.140	1.400		0.820	0.670	50.10				4.76		
	18:30:00	18.06		1352.00	12.0	246.21	48.00	34.83	27.00	32.73	18.843													
	19:00:00	18.06		1228.00	12.0	248.00	48.80	34.83	27.00	32.72	19.626		16.410	1.270		1.070	0.147					10.06		
	19:30:00	18.06		1226.00	12.0	236.30	48.80	34.83	26.00	32.24	20.302													
	20:00:00	18.06		1246.00	12.0	236.30	48.80	34.83	26.00	32.24	20.974		17.890	1.390		1.100	0.030	50.50				2.68		
	20:30:00	18.06		1200.00	12.0	260.20	47.80	34.83	26.00	32.23	21.646													
	21:00:00	18.06		1300.00	11.0	243.00	54.78	34.83	26.00	34.28	22.338		18.060	1.260		1.100	0.060					4.43		
	21:30:00	18.06		1400.00	11.0	243.00	53.78	34.83	26.00	33.86	23.040													
	22:00:00	18.06		1390.00	11.0	243.00	54.78	34.83	26.00	34.28	23.700		20.330	1.280		1.233	0.067	60.40				4.87		
	22:30:00	18.06		1400.00	11.0	260.00	60.26	34.83	26.00	36.42	24.487													
	23:00:00	18.06		1328.00	11.0	243.00	62.26	34.83	26.00	36.70	25.250		21.370	1.040		1.248	0.010					1.61		
	23:30:00	18.06		1400.00	11.0	243.00	66.27	34.83	23.00	34.87	26.001													
2002/08/12	00:00:00	18.06		1360.00	11.0	236.00	62.29	34.83	24.00	33.18	26.767		22.620	1.240		1.262	0.073	60.20				1.00		
	00:30:00	18.06		1346.00	11.0	220.00	66.28	34.83	24.00	33.77	27.464													
	01:00:00	18.06		1316.00	11.0	221.00	66.63	34.83	24.00	33.54	28.103		23.810	1.290		1.368	0.097					7.83		
	01:30:00	18.06		1286.00	11.0	220.00	64.78	34.83	24.00	33.61	28.801													
	02:00:00	18.06		1280.00	11.0	248.00	60.80	34.83	24.00	33.24	29.487		26.030	1.120		1.370	0.011	60.30				0.96		
	02:30:00	18.06		1310.00	11.0	241.00	62.04	34.83	24.00	33.33	30.181													
	03:00:00	18.06		1340.00	11.0	234.00	63.78	34.83	24.00	33.62	30.868		28.330	1.300		1.430	0.060					4.88		
	03:30:00	18.06		1306.00	11.0	241.00	48.56	34.83	24.00	32.48	31.676													

2002/08/11 06:22:00 To 2002/08/12 06:00:00
 Gas 35.138 Cum. 35.138 10³m³
 Oil 29.890 Cum. 29.890 m³
 MUD 1.525 Cum. 1.525 m³

08/12/2002 06:54 16139864795 STAN PAGE 03

FieldNotes

Field Measurements

Date	Time	C Size	Pres	Pres	Temp	Pres	Pres	Orifice	Temp	Meter	Gas1	Cum	Measured	Oil	Cum	Gain	Mud	Cum	Gain	API	Salinity	pH	Mud	Cut	Calc	Calc
																									Inc	Inc
yyyy/mm/dd hh:mm:ss	mm	kPa(g)	kPa(g)	°C	kPa(g)	kPa	mm	°C	10 ⁻³ m ³ /d	10 ⁻³ m ³	m ³	m ³	m ³	m ³	m ³	m ³	m ³	m ³	* API	ppm		%				
2002/08/12	04:00:00	18.06		1200.00	11.0	241.00	62.29	34.83	24.00	33.470	32.203		27.400	1.100		1.473	0.036	60.00						2.83		
74	04:00:00	18.06		1200.00	11.0	241.00	62.29	34.83	24.00	33.470	32.203		27.400	1.100		1.473	0.036	60.00						2.83		
75	04:16:00	18.06	Noticing	1318.00	10.0	241.00	66.28	34.83	24.00	34.418	32.808		28.700	1.300		1.626	0.062							3.06		
76	04:30:00	18.06		1336.00	10.0	241.00	67.77	34.83	24.00	35.233	33.000															
77	05:00:00	18.06		1336.00	10.0	241.00	67.77	34.83	24.00	34.390	34.420															
78	06:30:00	18.06		1200.00	10.0	234.00	66.77	34.83	24.00																	

2002/08/11 06:22:00 To 2002/08/12 06:00:00

Gas	35.138	Cum.	35.138	10 ³ m ³
Oil	29.890	Cum.	29.890	m ³
MUD	1.525	Cum.	1.525	m ³

FieldNotes

Field Measurements

Date	Time	C	Size	Pres	Pres	Temp	Pres	Pres	Orifice1	Temp	Rate	Gas1	Cum. Gas1	Measured Oil1	Gain	Measured Mud1	Gain	API 1	Salinity	pH	Mud Cut	Calc	Calc
																						Inc	Inc
yyyy/mm/dd	hh:mm:ss	mm	kPa(g)	kPa(g)	°C	kPa(g)	kPa	mm	°C	10 ⁻³ m ³ /d	10 ³ m ³	m ³	m ³	m ³	m ³	m ³	* API	ppm	%				
2002/08/12	06:00:00	18.06		1320.00	10.0	234.00	66.77	34.93	26.00	34.600	36.138	29.890	1.108	1.626	0.000	60.70					0.00		
	06:30:00	18.06		1400.00	10.0	260.00	82.26	34.93	26.00	37.060	38.873												
	07:00:00	18.06		1366.00	10.0	236.00	69.00	34.93	26.00	36.173	40.640	30.910	1.020	1.626	0.000								
	07:30:00	18.06		1320.00	10.0	243.00	64.28	34.93	26.00	34.098	47.365												
	07:30:00	EMULSION IN SAMPLE																					
	08:00:00	18.06		1346.00	10.0	260.00	64.74	34.93	27.00	37.716	48.113	32.090	1.180	1.626	0.000	61.18							
	08:30:00	18.06		1364.00	10.0	234.00	64.78	34.93	26.00	33.796	48.888												
	09:00:00	18.06		1373.00	10.0	234.00	67.27	34.93	26.00	34.062	48.871	33.246	1.160	1.626	0.000								
	09:30:00	18.06		1420.00	10.0	227.00	68.72	34.93	24.00	38.180	40.338												
	10:00:00	18.06		1310.00	11.0	240.00	63.63	34.93	24.00	34.172	41.884	34.318	1.070	1.626	0.000	60.80							
	10:30:00	18.06		1375.00	11.0	234.00	60.80	34.93	24.00	36.761	41.812												
	11:00:00	18.06		1310.00	11.0	234.00	48.66	34.93	23.00	31.068	42.518	36.368	1.060	1.626	0.001								
	11:30:00	18.06		1348.00	12.0	241.00	67.76	34.93	22.00	36.362	43.217												
	12:00:00	18.06		1360.00	12.0	243.00	60.01	34.93	24.00	36.064	43.980	36.448	1.088	1.648	0.023	61.90							
	12:00:00	EMULSION STILL IN SAMPLE SINCE 7:30AM ABOUT 8%																					
	12:30:00	18.06		1296.00	12.0	241.00	68.76	34.93	26.00	36.760	44.708												
	13:00:00	18.06		1290.00	12.0	248.00	61.78	34.93	27.00	36.674	46.463	37.890	1.190	1.684	0.038								
	13:30:00	18.06		1320.00	12.0	241.00	68.81	34.93	26.00	36.670	48.216												
	14:00:00	18.06		1295.00	12.0	234.00	68.27	34.93	27.00	34.221	48.944	36.610	1.010	1.804	0.020	60.80							
	14:30:00	18.06		1328.00	12.0	234.00	67.82	34.93	27.00	34.623	47.882												
	15:00:00	18.06		1340.00	12.0	234.00	68.61	34.93	27.00	36.264	48.389	38.710	1.100	1.804	0.000								
	15:30:00	18.06		1310.00	12.0	228.00	67.62	34.93	26.00	34.381	49.118												
	16:00:00	18.06		1290.00	12.0	228.00	66.78	34.93	26.00	33.824	49.828	40.660	0.960	1.814	0.010	61.18							
	16:30:00	18.06		1320.00	11.0	234.00	61.06	34.93	26.00	32.664	49.617												
	17:00:00	18.06		1318.00	11.0	234.00	62.28	34.93	27.00	32.316	61.198	41.610	0.960	1.828	0.014								
	17:30:00	18.06		1198.00	11.0	234.00	61.64	34.93	27.00	32.668	61.082												
	18:00:00	SAMPLES TAKEN = 2 x HP GAS / 2 x STOCK OIL																					
	18:00:00	18.06		1328.00	11.0	234.00	67.27	34.93	26.00	34.602	62.603	42.600	0.960	1.638	0.010	61.30							
	18:30:00	18.06		1310.00	11.0	234.00	60.01	34.93	26.00	36.474	63.313	43.080	0.480	1.643	0.006								

2002/08/12 06:00:00 To 2002/08/12 18:30:00
 Gas 18.175 Cum 53.313 10³m³
 Oil 13.190 Cum 43.080 m³
 0.118 Cum 1.643 m³

FieldNotes Field Measurements

Date	Time	C Size	Pres	Pres	Temp	Pres	Pres	Orifice	Temp	Rate	Gas1	Cum.	Measured	Calc		Calc		API 1	Salinity	pH	Mud Cut
														Oil1	Measured	Mud1	Inc				
yyyy/mm/dd	hh:mm:ss	mm	kPa(g)	kPa(g)	°C	kPa(g)	kPa	mm	°C	10 ³ m ³ /d	10 ³ m ³	m ³	m ³	m ³	m ³	m ³	m ³	* API	ppm		%

108	2002/08/12	18:30:00	CLOSED DST / TUBING VENTING TO FLARE																		
-----	------------	----------	--------------------------------------	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--

2002/08/12 06:00:00 To 2002/08/12 18:30:00

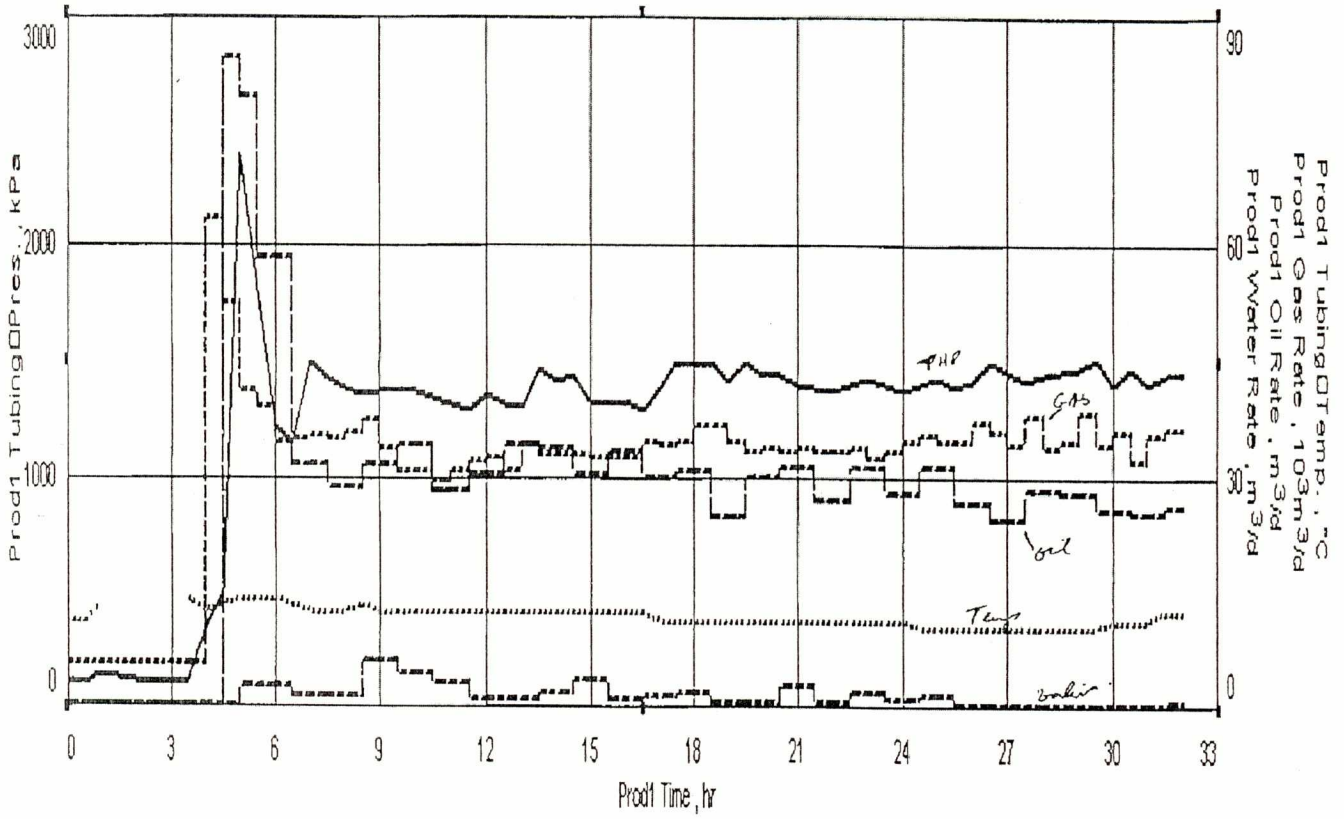
Gas	18.175	Cum.	53.313	10 ³ m ³
Oil	13.190	Cum.	43.080	m ³
MUD	0.118	Cum.	1.643	m ³

08/12/2002 06:54 16139864759 STAN PAGE 06

Attachment E: ST #2 Production Plot

Prod 2

Aug 13/02



**Attachment F: Drillstem Test
Report on Well Port au Port #1 –
ST #2 DST #2 (Fekete Associates
Inc.)**

DRILLSTEM TEST REPORT
ON WELL
PORT au PORT #1 – ST #2
DST #2: 3335.0 – 3482.0 mKB
Test Date: August 11 – 14, 2002

Prepared for:
Canadian Imperial Venture Corp.

Prepared by:
FEKETE ASSOCIATES INC.

REPORT DISTRIBUTION

"Four" (4) Copies of the Report to:

Canadian Imperial Venture Corp.
St. John's, Newfoundland

ATTENTION: Gerard Edwards

August 29, 2002

Canadian Imperial Venture Corp.
Suite 300, 16 Forest Road
St. John's, Newfoundland
A1C 6I9

ATTENTION: Gerard Edwards

RE: DRILLSTEM TEST REPORT
PORT au PORT #1 – ST #2
DST #2: 3335.0 – 3482.0 mKB
Test Date: August 11 – 14, 2002

The test data obtained from DST #2 have been analyzed to establish the formation characteristics, deliverability potential and reservoir pressure of the Table Point/Aguathuna formation. This report has been prepared to summarize the test results.

If you should have any further questions or concerns, please do not hesitate to contact the undersigned at (403) 213-4200.

Yours truly,
FEKETE ASSOCIATES INC.

M.S. Santo
Manager

L.Mattar, P.Eng.
President

MSS/mss

Background and Test Overview

Drillstem test #2 was performed over the interval 3335 – 3482 mKB. After performing the standard flow and shut-in periods (16 minute pre-flow/61 minute initial shut-in and 61 minute main flow/89 minute shut-in), an extended flow period of 36 hours was performed. During this flow period, the well produced gas at an average rate of $35 \times 10^3 \text{ m}^3/\text{d}$, and light oil (51° API) at a rate of 25 – 30 m^3/d . There was also 41.5 m^3 of mud recovered, indicating that the well was cleaning up. The extended flow was followed by a buildup period of 48 hours.

CONCLUSIONS

- The extrapolation of the initial shut-in indicates a reservoir pressure in the order of 32,900 kPaa.
- The conventional extrapolation of the final shut-in (Radial – Final Shut-in plot) implies a pressure loss in the order of 1900 kPa. However, geology indicates there is a reservoir boundary within 18 meters of the well. Consequently, a longer shut-in time is required to obtain a reliable extrapolation from conventional analysis. The model used to match the pressure data shows there is good potential for the pressure to fully recover.
- The test data are matched very well by simulating a two-layered reservoir, in which the layers are only communicating at the wellbore. This is consistent with geology and the results of DST #1.
- The model suggests one layer has extremely limited areal extent, which is suspected to be the gas zone. The areal extent of the other layer cannot be determined from the available data. A one-section drainage area has been assumed to extrapolate the pressure and forecast the deliverability. Further testing will be required to confirm the reservoir size.
- The permeability to oil is estimated to be in the order of 1.7 mD.
- A positive skin of +15 is calculated, indicating significant formation damage. This is consistent with the mud recovery observed during the extended flow period, and shows there is potential to improve the deliverability of this well.
- At a skin of +15, the stabilized oil rate is predicted to be 7.3 m^3/d . Under a stimulated condition ($s = -4$), a stabilized rate in the order of 17 m^3/d is predicted from the model.

TEST RESULTS

PRESSURE SUMMARY					
Extrapolated Reservoir Pressure	(p _i)	32,940	kPaa	4778	psia
Final Measured Pressure (@ hrs)		30,961	kPaa	4491	psia

RESERVOIR CHARACTERISTICS – Dominant Layer					
Flow Capacity to Oil	(kh)	9.9	mD.m	33	md.ft
Permeability to Oil	(k)	1.65	mD	1.67	md
Net Pay	(h)	6.0	m	20	ft
Skin	(s)	+15.5		+15.5	

A one-section drainage area is assumed

PRODUCTION AND DELIVERABILITY					
Final Gas Rate		35.5	10 ³ m ³ /d	1.26	MMcfd
Final Oil Rate		23.0	m ³ /d	145	bbi/d
Final Mud Rate		39	m ³ /d	245	bbi/d
Final GOR		1540	m ³ /m ³	8690	Scf/bbl

Fekete

Associates Inc.

Reservoir Engineering & Geology - Oil & Gas Property Evaluation - Well Test Interpretation - Software Development

November 9, 2001

HUNT OIL COMPANY OF CANADA INC.
3100, 450 – 1st Street SW
Calgary, Alberta
T2P 5H1

ATTENTION: Mr. Kevin Morrison
Senior Geologist, Frontier Exploration

Dear Sir;

RE: Garden Hill South Development
Port au Port #1 Well
May 20 to June 14, 2001 Production Test

To confirm last week's discussions, the May production test shows that the Port au Port #1 well encountered a much larger volume of oil than has historically been inferred from pressure buildup analysis.

The apparently obvious conclusion from initial pressure tests is that the well encountered about 25000 m³ (157,000 Bbls) of oil-in-place. From the production test, the oil-in-place cannot be less than 90,000 m³ (0.5 MMBbls) and is probably many times greater. A realistic oil-in-place cannot be estimated from the May test, since 1724 m³ (10,842 Bbls) of test production was insufficient to create any signs of depletion.

The interpretation of a limited oil volume has always been suspect, because it was inconsistent with the other information. In hindsight, the root cause was the assumption that the formation karsts are the oil reservoir. The conclusion from the May test is that the karsts contain essentially water, which leaves the surrounding matrix as the oil source.

By assuming water bearing karsts, the pressure test interpretation becomes consistent with the other information. The current model presents limited volume, water bearing karsts that are encapsulated by an extensive, much lower permeability oil matrix.

The above points are developed in the discussion section of this letter and the following attachments:

Figure 1 Daily Produced Oil and Water Volumes May 20 to June 14, 2001

Figure 2a Cumulative Production May 20 to June 1, 2001

Figure 2b Cumulative Production June 1 to June 14, 2001

Figure 3 Port au Port #1 Fluid Distribution Model

Figure 4 Port au Port Inversion Fairway

Appendix 1 Port au Port #1 Summary of Daily Produced Volumes

Appendix 2 Additional Observations for the Fluid Distribution Model

Appendix 3 Characterization of Reservoir/Trap Geometries in the Inversion
Fairway of the Round Head Thrust, Western Port au Port Peninsula

I look forward to further discussion on the topic. Please contact me directly at your convenience at 213-4235.

Yours truly,
FEKETE ASSOCIATES INC.

Ray Mireault, P. Eng.
Specialist, Reserves Development

RAM/
Attach.

Cc. S. Millan - CIVC
G. Edwards – CIVC
M. Cooper - PanCanadian

DISCUSSION

A non-conventional production test was performed on the Port au Port #1 well from May 20 to June 14, 2001. Salt deposition in the flowlines, wellhead and downhole tubing made it impossible to produce the well in a conventional fashion.

The procedure that evolved during testing was to flow the well on a fixed 19.5 mm (3/4") choke setting until salt deposition started to plug up the choke, which occurred after 4 to 6 hours. The well was then shut-in and about 5 m³ of hot (50°C) fresh water was pumped down the tubing string to dissolve the salt. The water was flowed back through the separator to dissolve surface deposits in the wellhead and flowlines, then shut in. A gauge cutter run followed, to confirm that the tubing was clear of salt. The well was then returned to production.

The entire flow and flush sequence was repeated between 2 and 3 times per 24 hour period. Cumulative production after 310.5 hours of flow with this cycling approach was:

Oil	1724 m ³	10,842 Bbls
Formation water	947 m ³	5,956 Bbls
Gas	820 E ³ m ³	29 MMSCF

A plot of daily produced volumes for the production period (Figure 1) shows a constant GOR and constant to slightly declining watercut. The stability of the daily values is remarkable, considering the wide fluctuations in hourly values (Figure 2a and b). Other noteworthy trends are:

- The hourly plots demonstrate that both water-cut and GOR started at high values and then declined monotonically during every 4 to 6 hour flow period. These trends are real and not a by-product of measurement uncertainty.
- Cumulative oil and water trend lines exhibit a constant slope using either hourly or daily production data. A constant slope indicates constant fluid production capability during the test period.

The test results challenge the hypothesis that the Port au Port #1 well encountered a limited volume of oil in the Upper Aguathuna formation, in the order of 25,000 m³ (157,000 Bbls). This early hypothesis was one possible explanation for the observed bottomhole pressure behavior

during previous, short-duration well tests. If the oil-in-place volume truly is 25,000 m³ there should have been a noticeable increase in GOR and a dramatic decrease in oil production rate, because 1724 m³ of produced oil represents 6.9% recovery.

A constant GOR suggests the converse. The reservoir did not experience any significant degree of depletion during the test. Volatile oil reservoirs experience dramatic GOR increases when reservoir pressure drops below bubble point, generally after less than 2% recovery under primary production. By analogy, one might conclude that the Port au Port #1 well has encountered an oil accumulation that exceeds 86,000 m³ (540,000 Bbls). The actual oil-in-place is likely many times greater than 86,000 m³, because this value is only an arithmetic minimum. For example, the test volume could just as easily represent 0.2, 0.02 or 0.002% recovery. The calculated oil-in-place then becomes 0.86, 8.6 or 86 E⁶ m³ (5.4, 54 or 540 MMBbls). The method does not assist us in determining which number is the better approximation.

An alternate approach that also provides only a minimum oil-in-place estimate is the single phase material balance equation ($C = dV/(VdP)$). Since GOR was constant during the test, it can be concluded that reservoir pressure did not fall below bubble point. Accordingly, the maximum pressure drop that could have occurred is about 4000 kPa, based on an initial reservoir pressure of about 37,000 kPa and a bubble point of 32,000 kPa.

Assuming a system compressibility $c_t = 2.0 \text{ E}^{-6}$ per kPa, the minimum calculated oil-in-place is 215 E³ m³ (1.4 MMBbls). Again, the true oil-in-place value is likely to be many times greater, since it is extremely unlikely that the test produced exactly the right amount of oil to deplete to just above the bubble point. For example, for reservoir pressure depletion of 400 or 40 or 4 kPa, the corresponding oil-in-place is 2.15, 21.5 or 215 E⁶ m³ (14, 140, 1400 MMBbls). This method also provides no assistance in determining a realistic oil-in-place value.

Port au Port Reservoir Geometry

A consistent explanation for the geological, pressure test and production test data is that Port au Port #1 has encountered an extensive but complicated reservoir geometry. An areally significant oil accumulation is consistent with discovering oil on the first drilling attempt, as was done in Port au Port #1.

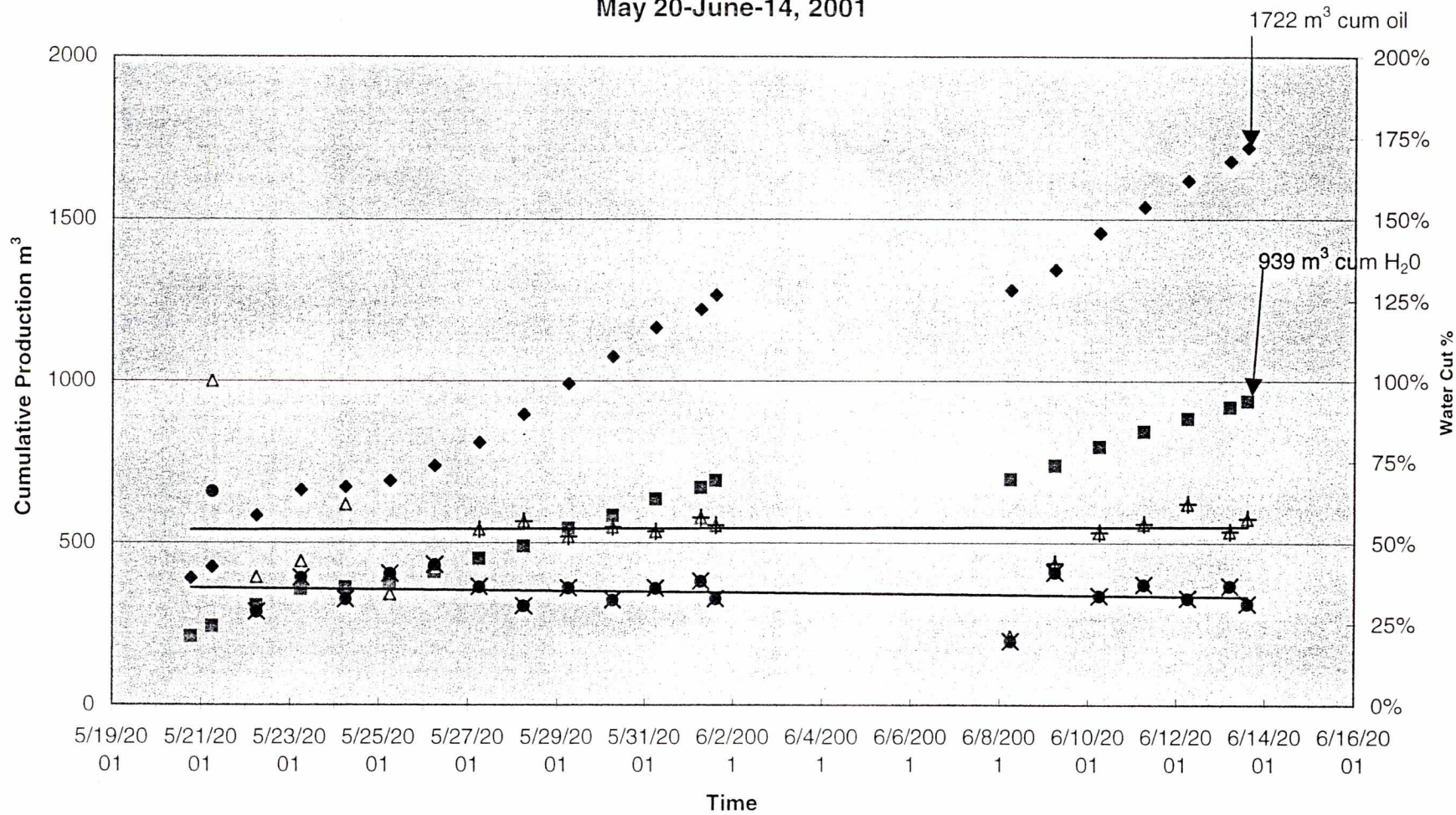
A simplified cross-sectional model presents a productive oil wet matrix and two volumetrically isolated water-bearing karsts (Figure 3). A 7 metre limestone barrier isolates the system from underlying water. One essential piece of data used to develop this model was the production log conducted during the May test. It indicated that the karst from 3472 to 3473 mKB produces essentially water. The other was the open hole resistivity log, which showed the lowest resistivity readings in the karsts. Other observations used to develop the model are presented in Appendix 2 and 3.

The reservoir geometry of the Upper Aguathuna formation near the Port au Port #1 well is further complicated in plan view by two boundaries (Figure 4). A shear fault zone between Port au Port #1 and the Talisman A-09 well identifies the southwest edge of the pool. Port au Port #1 is also less than 300 m from the western edge. This was proven by the currently drilling sidetrack well (ST 1), which did not encounter porosity in the Upper Aguathuna interval.

The presence of 2, approximately perpendicular boundaries does not infer a limited volume reservoir. At this time, the northern and eastern limits of the oil have not been delineated. Well ST 1, which found oil in the Lower Aguathuna, has disproved the assumption of a "regional" oil water contact at the highest water elevation in PaP #1. Accordingly, the oil accumulation could theoretically extend as far east as the Round Head Thrust; a distance of about 5 kilometers.

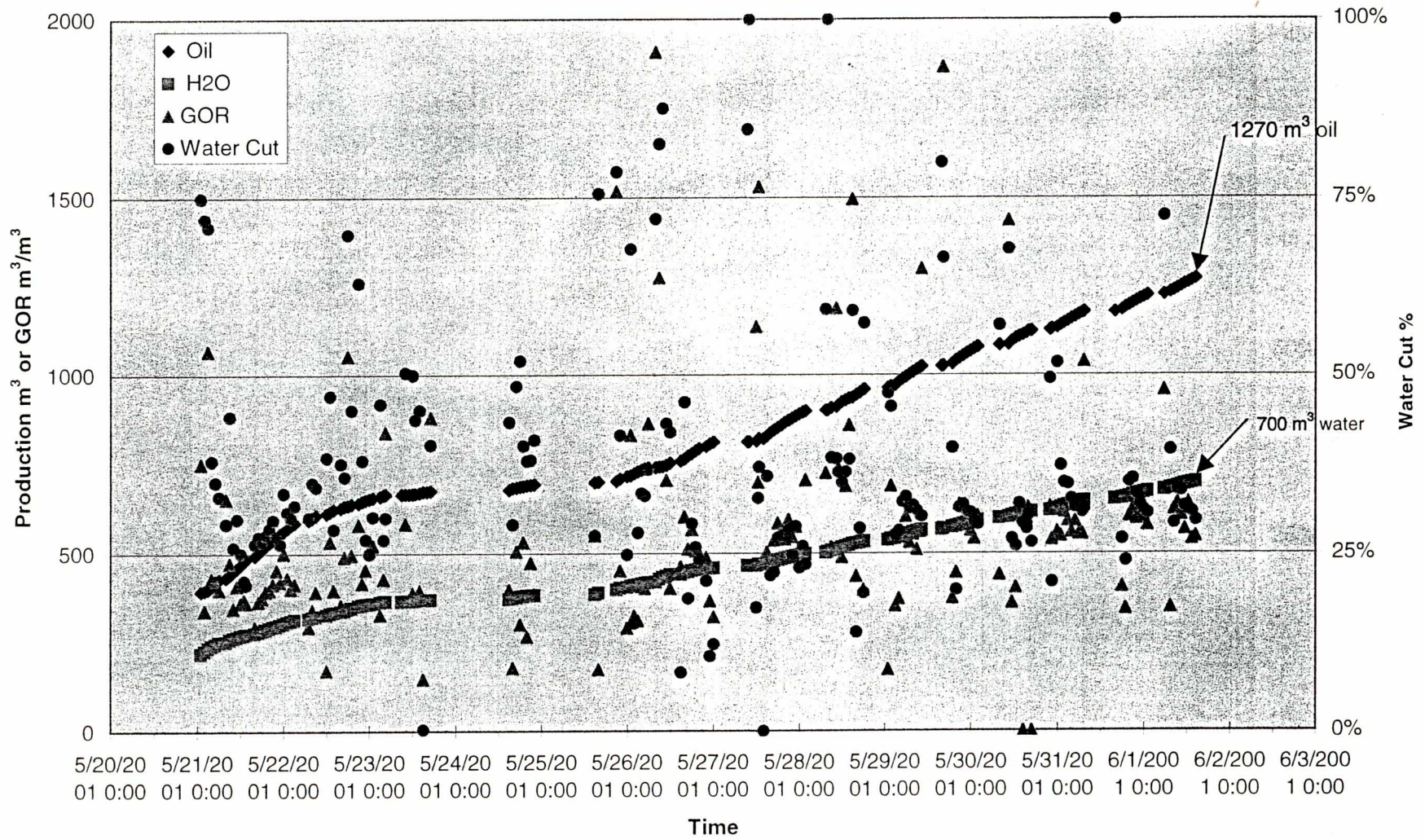
To the northeast, the maximum areal extent is at least as great. If the source rock for the PaP #1 oil is located 20 kilometers away at Shoal Point, then there must also be a continuous migration path from the source to PaP #1. The arguments for a continuous transmission path flow directly from Hunt and PanCanadian's work on the inversion fairway and are presented in an attached discussion paper (Appendix 2). For your information, the paper was originally prepared and submitted to the Nfld. Dept. of Mines and Energy.

Daily Produced Oil and Water Volumes May 20-June 14, 2001

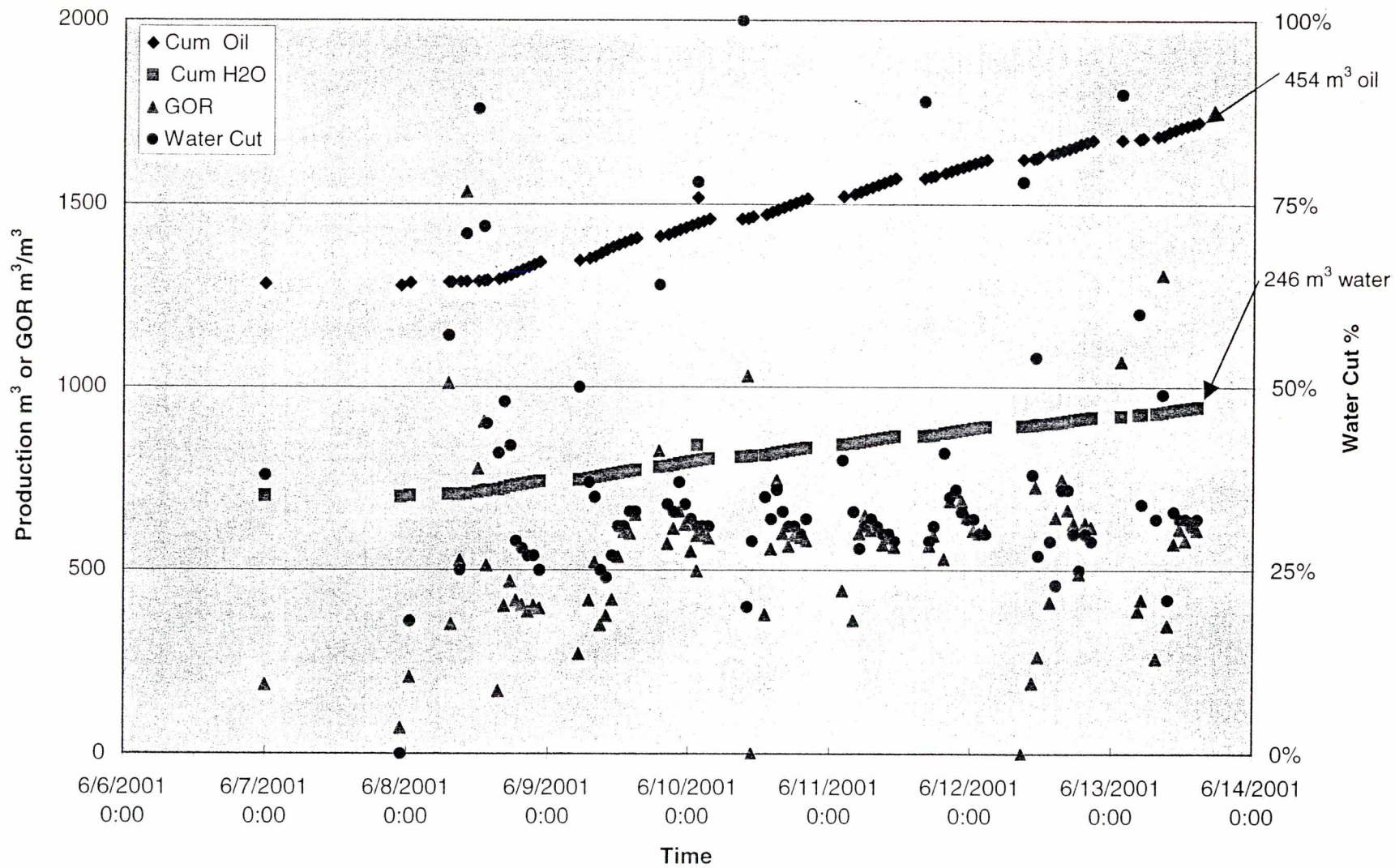


- ◆ Cum Oil
- Cum H₂O
- △ GOR
- + GOR - Selected Points
- Water Cut
- × Water Cut - Selected Points
- Linear (GOR - Selected Points)
- Linear (Water Cut - Selected Points)

Cumulative Production May 20-June 1, 2001

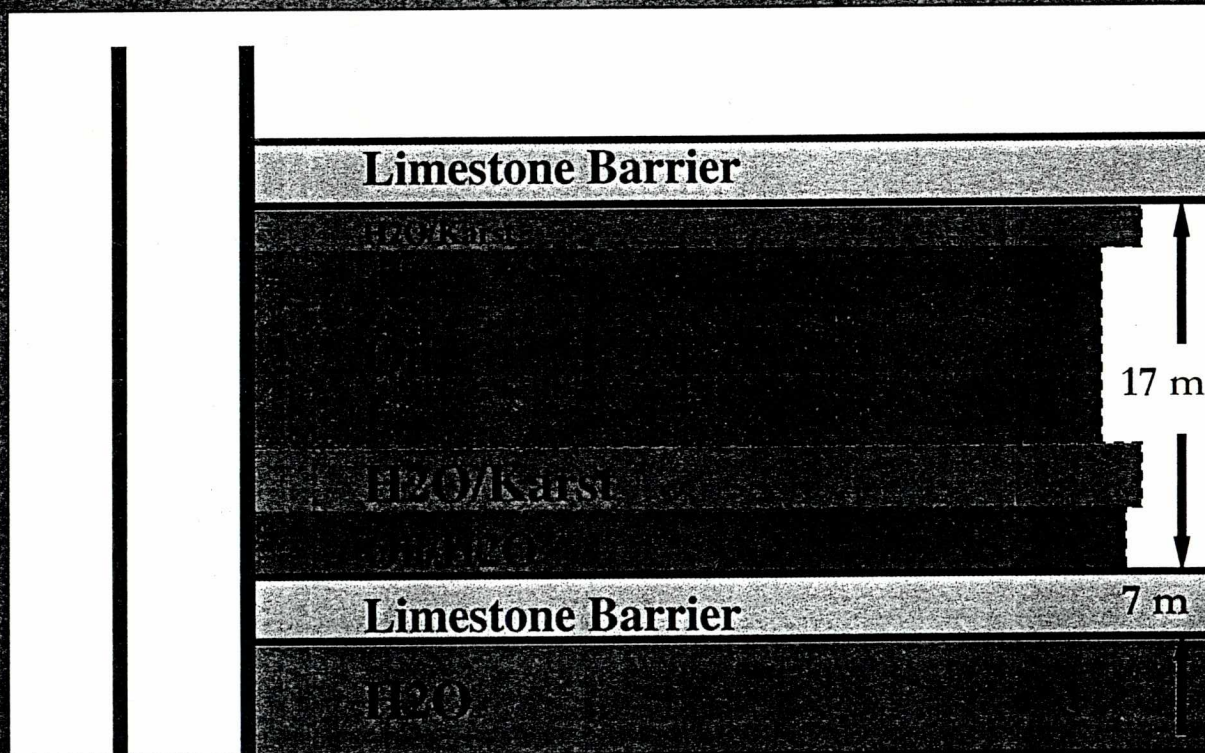


Cumulative Production June 8-14, 2001



Evolution: Port au Port Model

Port au Port #1 Fluid Distribution



Daily Production Summary

Company Canadian Imperial Venture Corporation
 LSD Newfoundland
 Zone Aguathuna
 Northland Job 201407A

Date	Daily Hours Flowed	Cumulative Flow Time	Daily Gas Volume	Cum Gas	Daily Cond/Oil Volume	Cum Cond/Oil	Daily Water Volume	Cum Water
(yyyy/mm/dd)	(hours)	(hours)	(E3m3)	(E3m3)	(m3)	(m3)	(m3)	(m3)
2001/05/05	1.00	1.00	0.00	0.00	0.00	0.00	8.10	8.10
2001/05/06	11.00	12.00	15.45	15.45	49.90	49.90	44.50	52.60
2001/05/07	7.30	19.30	5.57	21.02	6.48	56.38	7.97	60.57
2001/05/08	0.00	19.30	0.00	21.02	0.00	56.38	0.00	60.57
2001/05/09	14.50	33.80	55.66	76.68	161.90	218.28	71.00	131.57
2001/05/10	20.60	54.40	63.01	139.69	172.74	391.02	74.64	206.21
2001/05/11	0.00	54.40	0.00	139.69	0.00	391.02	0.00	206.21
2001/05/12	0.00	54.40	0.00	139.69	0.00	391.02	0.00	206.21
2001/05/13	0.00	54.40	0.00	139.69	0.00	391.02	0.00	206.21
2001/05/14	0.00	54.40	0.00	139.69	0.00	391.02	0.00	206.21
2001/05/15	0.00	54.40	0.00	139.69	0.00	391.02	0.00	206.21
2001/05/16	0.00	54.40	0.00	139.69	0.00	391.02	0.00	206.21
2001/05/17	0.00	54.40	0.00	139.69	0.00	391.02	0.00	206.21
2001/05/18	0.00	54.40	0.00	139.69	0.00	391.02	0.00	206.21
2001/05/19	0.00	54.40	0.00	139.69	0.00	391.02	0.00	206.21
2001/05/20	0.00	54.40	0.00	139.69	0.00	391.02	5.51	206.21
2001/05/21	21.00	75.40	70.83	210.52	171.97	562.99	92.65	304.37
2001/05/22	17.50	92.90	39.63	250.15	90.19	653.18	54.46	358.83

Confidential

2001/05/23	14.30	107.20	11.37	261.52	21.96	675.14	11.74	370.57
2001/05/24	8.50	115.70	6.48	268.00	18.91	694.05	12.91	383.48
2001/05/25	4.80	120.50	9.18	277.18	22.20	716.25	22.33	405.81
2001/05/26	19.50	140.00	48.84	326.03	95.28	811.53	53.89	459.70
2001/05/27	13.00	153.00	44.72	370.75	78.60	890.13	35.53	495.23
2001/05/28	12.00	165.00	39.24	409.98	68.95	959.08	38.22	533.45
2001/05/29	16.80	181.80	54.17	464.16	107.10	1066.18	54.14	587.59
2001/05/30	12.70	194.50	35.08	499.23	66.80	1132.98	37.64	625.23
2001/05/31	15.60	210.10	48.40	547.63	85.20	1218.18	45.94	671.17
2001/06/01	10.50	220.60	29.67	577.30	52.50	1270.68	29.68	700.85

Company Canadian Imperial Venture Corporation
 LSD Newfoundland
 Zone Aguathuna
 Northland Job 201407B

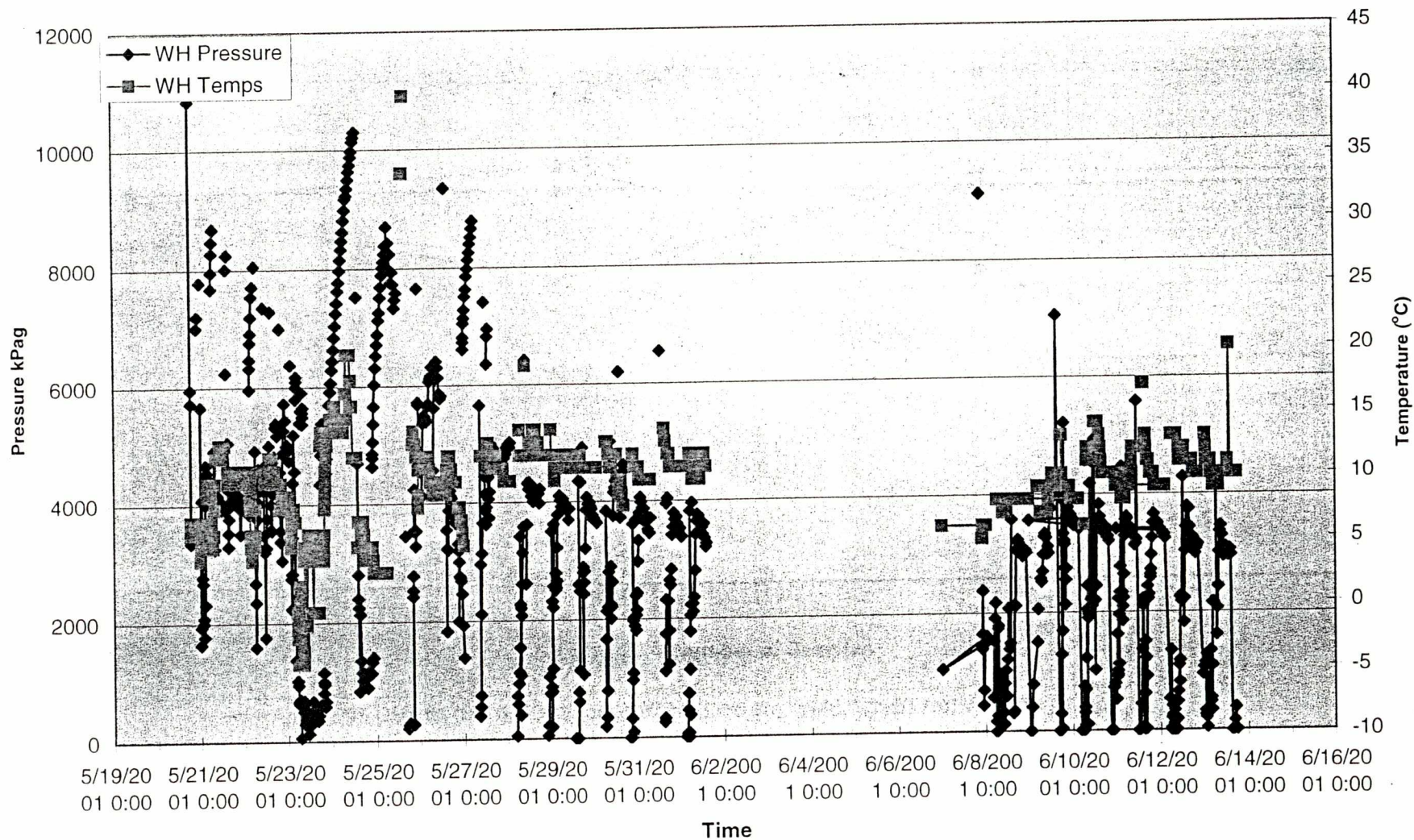
Date	Daily Hours Flowed	Cumulative Flow Time	Daily Gas Volume	Cum Gas	Daily Cond/Oil Volume	Cum Cond/Oil	Daily Water Volume	Cum Water
(yyyy/mm/dd)	(hours)	(hours)	(E3m3)	(E3m3)	(m3)	(m3)	(m3)	(m3)
2001/06/07	2.00	2.00	2.69	2.69	12.62	12.62	3.18	3.18
2001/06/08	14.40	16.40	26.20	28.89	60.28	72.90	39.43	42.61
2001/06/09	15.40	31.80	49.75	78.64	93.80	166.70	51.16	93.77
2001/06/11	15.30	47.10	43.52	122.16	78.80	245.50	40.54	134.31
2001/06/11	17.80	64.90	55.86	178.02	90.46	335.96	50.54	184.85
2001/06/12	13.70	78.60	36.59	214.61	68.91	404.87	32.45	217.30
2001/06/13	11.30	89.90	27.71	242.32	48.80	453.67	28.67	245.97
2001/06/14	0.00	89.90	0.00	242.32	0.00	453.67	0.00	245.97

**Port au Port #1 Fluid Distribution Model
Additional Observations**

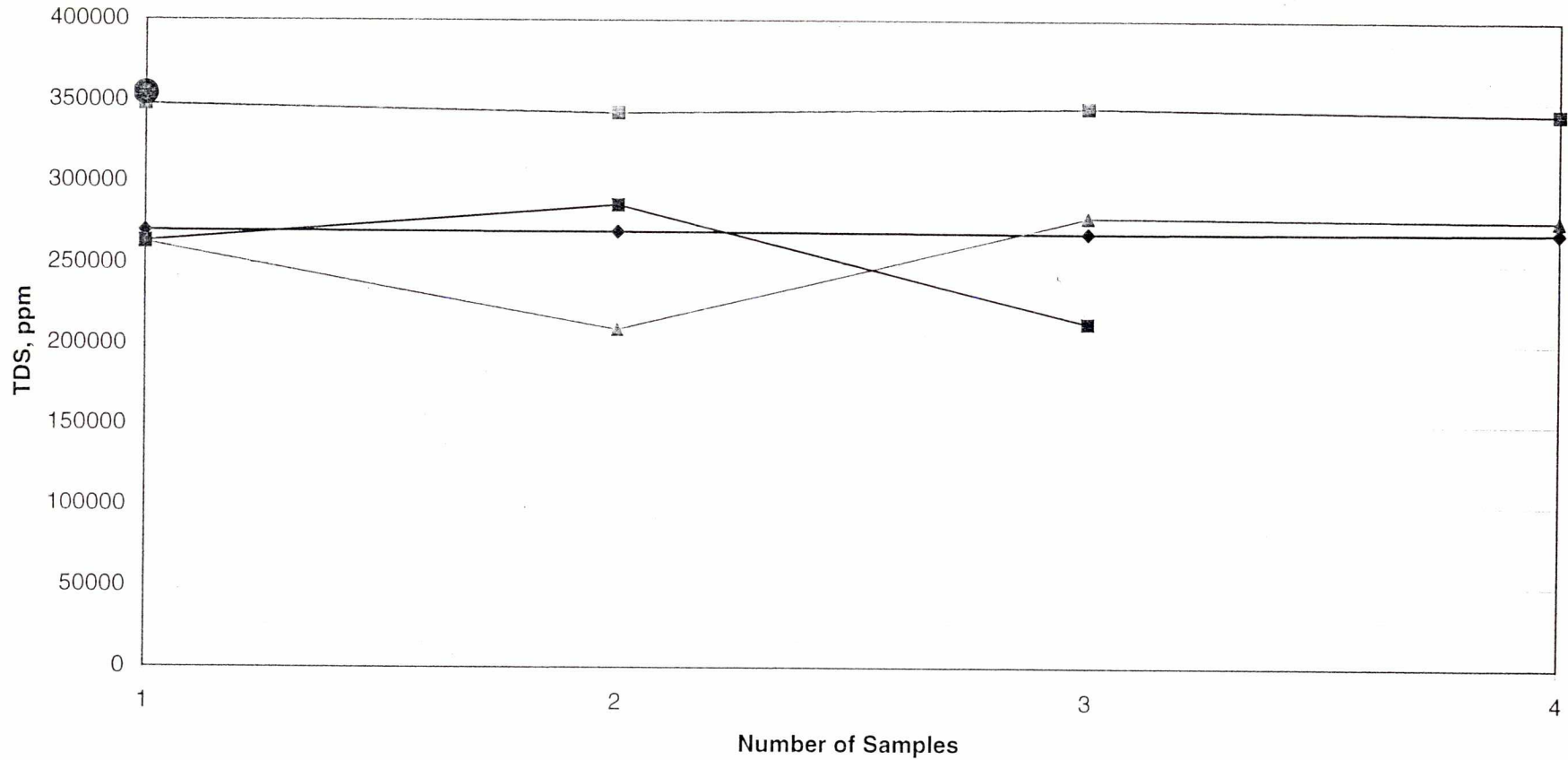
- Bottomhole pressure analysis consistently suggests a high permeability zone of limited volume and a much lower permeability zone, but cannot identify the type of fluid contained within each. Analysis of tests that produce significant volumes of more than one fluid (e.g. oil and water) are always problematic.
- The karsts are logically the high permeability zone while the low permeability profile identifies some combination of direct inflow into the wellbore from the matrix and slow recharge of the karsts. A physical explanation for a slow karst recharge rate is the calcium carbonate precipitate that typically lines cave interiors.
- A physical explanation for severely restricted inflow from the matrix into the wellbore comes from the well history. An unusually large amount of solid materials were pumped down the PaP #1 well and the Upper Aguathuna formation was exposed to an overbalanced condition for an unusually long time. The combination creates the potential for a very deep invasion depth that could be interpreted as altered permeability, rather than "skin", on well tests.
- Before the onset of testing in May, an additional 7 m of matrix was perforated. As the zone was already in communication with the wellbore, perforating should have had no observable effect, assuming a homogeneous reservoir. Instead, the wireline weight indicator immediately lost 150 lbs. then recovered. Wellhead pressure simultaneously increased 10 psi.
- Wellhead flowing pressures present a repeatable pattern that correlated with produced fluid composition (see page 3). Oil and gas rapidly displaced water out of the tubing when the well was shut-in, which increased the wellhead tubing pressure. In the first hour (approximate) of production, the well initially produced gas, followed by almost pure oil, followed by mostly water. As production continued, the water cut gradually decreased if the well was flowed at a high rate. At low rates, the well loaded up with water and died.

- Production at a 19 mm (3/4") choke gradually reduced the producing watercut to approximately 30%. Water production capability also tended to stabilize or decrease slightly with flow time. Both observations suggest the water production capability is limited. If the water resides in the karsts it is not limited by permeability, so it must be limited by expansion energy. Therefore, the volume of the karst (and the volume of water in it) is finite. Production capability is likely limited by the recharge rate through the cave interface to the matrix.
- The May test was initially plagued by a produced emulsion that prevented the formation of oil/water interfaces in the horizontal separator. The problem was so severe that it threatened further operation. However, the severity of the problem continually decreased as the well produced and was a non-issue by June. The decreasing trend and samples recovered from the well both suggest the emulsion was a man-made problem (e.g. lost circulation materials).
- It is difficult to explain how water resides in the upper karst at the top of the pay column, based on log resistivity and no obvious physical barrier, with a simple oil over water model. An additional complication is that the calculated water saturations are very low (8 to 10%) and indicate that the water content increases with elevation. These observations led to the conclusion that the matrix must be strongly oil wet and the more extensive phase of this two component reservoir system.
- A plot of Total Dissolved Solids (TDS) for formation waters that were recovered from DST's and production tests on PaP is non-linear with depth (page 4). This argues for segregation of the different porous intervals encountered by Port au Port #1.

Well Head Pressures & Temperatures May 20-June 14, 2001



Port au Port #1 DST Water Analysis



- ◆— April 1995 DST #1 (3916.1-3920.3m, 3932.3-3936.2m, 3946.7-3950.7m) Watts Bight
- April 1995 DST #2 (3515.0-3517.1, 3523.5-3526.5, 3533.5-3535.1, 3553.1-3555.2, 3556.4-3559.5) Aguathuna
- ▲— April 1995 DST #3 (3471.7 - 3476.2 m) Aguathuna
- April 1995 DST #4 (3459.2 - 3462.2 m) Aguathuna
- May 2000 CIVC Production Test (3459.2 - 3462.2 m) Aguathuna

**Characterization of Reservoir/Trap Geometries in the Inversion Fairway of
the Round Head Thrust, Western Port au Port Peninsula**

George S. Langdon, *P.Geol.*, Tectonics, Inc., Calgary
Ray Mireault, *P.Eng*, Fekete Associates Inc., Calgary

July 9, 2001

EXECUTIVE SUMMARY

Purpose:

1. To summarize what is known concerning the regional extent of the oil accumulation in the western Port au Port peninsula.
2. To develop an exploration drilling strategy from this knowledge.

Conclusions

Oil Distribution

1. Nature appears to have created a large, oil bearing, "sponge-like" matrix of dolomite rock that runs parallel to and extends continuously along the northwestern edge of the peninsula, from Shoal Point in the northeast to just before Cap St. George in the southwest. The area containing the matrix is known as the inversion fairway.
2. At this early stage of exploration, the width, thickness and internal geometry of the "sponge" are not known in detail. The general width of the fairway that contains the "sponge" is defined by two (2) structural features known as the Mainland Thrust and the Round Head Thrust. The length of the fairway is set by the source rock, which is primarily located at the northern Shoal Point end, and a wrench fault that defines the southern limit of the Garden Hill South field (Attachment 1).
3. Seismic interpretation suggests that structurally high spots (culminations) exist along the inversion fairway of the Round Head Thrust (e.g., Garden Hill South and Garden Hill North). These culminations are likely in hydrodynamic continuity owing to the preferential development of reservoir along a trend that closely parallels and is in proximity to, the Round Head Thrust.
4. The presence of a 17 m oil column above a 7 m aquitard (sealing zone) in the Port au Port #1 well provides the strongest evidence for the concept of a single, large oil accumulation within the fairway. Oil migration from the source rock at Shoal Point to the Port au Port #1 well at Garden Hill South required a continuous path (the matrix) along the length of the inversion fairway. The

dolomite matrix likely acted as a giant sponge, continuously imbibing and distributing oil from the source rock at the northern end until the oil reached the southern limits of the fairway (the Garden Hill South structure). An oil imbibing (oil-wet) matrix is the only consistent explanation for the observed distribution of oil and water encountered by the Port au Port #1 well.

5. The aquitard in Port au Port #1 separates the rock column into two vertically "stacked" compartments. The downdip extent of the oil above the aquitard is unknown at this time.
6. Since an oil-water contact cannot be defined in the Port au Port #1 well, the "saddles" between the structural high spots in the inversion fairway are also prospective for oil.
7. Possible trap configurations within the inversion fairway tend to support, rather than preclude, the potential for one continuous hydrocarbon accumulation from Shoal Point through the Garden Hill North and South structures.

Exploration Drilling

Commence by drilling the structural culminations (Garden Hill South, Garden Hill North). Follow with "step out" drilling from each structural culmination to determine the spill point for each structure. Drill "along trend" until each structure is fully delineated or the saddles between the structural highs are fully drilled.

Introduction

Oil has been discovered in the inversion fairway of the Round Head Thrust, on the western Port au Port Peninsula, Newfoundland. Fifty-one (51) degree gravity crude is presently being produced from the borehole of the Port au Port #1 well, which was originally drilled by Hunt/PanCanadian in 1995 and recompleted by Canadian Imperial Venture Corp. in May-June of 2001.

The oil is contained in highly karsted and dolomitized carbonates of the Middle Ordovician St. George Group, whose equivalents form reservoirs in the foreland of the Appalachian Mountain belt from Texas to Canada. Sourcing of the petroleum comes from organic rich shales of the Goose Tickle and Cow Head Groups which either stratigraphically or structurally overly the reservoir rocks in the Port au Port Peninsula, and indeed throughout western Newfoundland.

Reservoir development is focused on paleohighs along extensional fault blocks formed at the edge of the ancient Laurentian continental margin. These areas were susceptible to both early burial dolomitization and karsting, resulting in the development of conduits that later attracted dolomitizing fluids and enhanced the early porosity. The reservoir is heterogeneous and is recognized as a two-component system:

1. open, cavernous porosity zones which have a net thickness of several metres in the Port au Port #1 well, and;
2. matrix dolomites formed by extensive replacement of limestone protolith (largely mosaic and "crackle" breccias of the paleocavern roof facies) by burial and hydrothermal dolomitization.

Port au Port #1 drilled the eastern flank of a seismically mapped structural culmination, based on a limited amount of land-based seismic data. Complementary marine data in the near offshore is needed to fully define the nature of the culmination.

Because of this uncertainty and the presence of only one well, the extent and shape of the petroleum accumulation is not known. What is known is that there is a strong regional trend of reservoir and trap development parallel to and in front of the Round

Head Thrust, in an area known as the inversion fairway (Cooper et al., 2001)¹. The inversion fairway trends along the western Port au Port Peninsula between the coastline and the Round Head Thrust. Several possibilities for pool definition are here presented, based on the existing inversion fairway model.

The Inversion Fairway: Potential for Lateral Reservoir and Trap Continuity

The inversion fairway is proposed as a zone of continuous reservoir development and potential pool continuity immediately in front (west) and along the strike of the Round Head Fault. The structural and reservoir implications are described below.

a. **Structural considerations.** The structural situation of the play is dominated by a feature known as the Round Head Thrust, a large contractional fault that repeats both basement and platform rocks in the western Port au Port area (Attachment 1). During Acadian contraction, shortcut faults cut through the footwall blocks of the old extensional fault zone and created symmetrical rollover structures (anticlines) which are highly prospective for hydrocarbons. This structural style occurs in the immediate footwall of the Round Head Thrust and is known as the inversion fairway (Cooper et al., 2001)

A series of genetically and spatially related culminations are well-mapped on seismic along the length of the inversion fairway. These are from northeast to southwest; Shoal Point, Garden Hill North, Garden Hill South and St. George's Bay structures. The St. George's Bay A-36 and Talisman A-09 wells (St. George's Bay structure) are now considered to be separated from Garden Hill South by a wrench fault that trends along the south coast of the Port au Port Peninsula at Cap St. George, as seen on offshore seismic line CAH-92-5. This structure is waterbearing and lies updip of Garden Hill South. As there are plentiful signs of hydrocarbon charging in both wells, it appears that the structure may have been breached at its crest during Carboniferous exposure. Garden Hill South, possibly because of its lack of exhumation in the Carboniferous, experienced preservation of its accumulated oil. It is possible that the sealing fault system at Garden Hill South acted as a seal for hydrocarbons migrating from north to south.

¹ AAPG, March, 2001

The Shoal Point structure forms the high point of the inversion fairway north of Cap St. George. Prior to the drilling of the Shoal Point K-39 well, Hunt's exploration staff considered that the entire fairway as far south as Garden Hill South had the potential to be a continuous oil accumulation (as shown on Hunt maps obtained under terms of CIVC's farmout arrangement). In fact, a large upside was assigned to the Shoal Point prospect based on its possible extension onshore in Port au Port Bay and southwestward through the Garden Hill structures.

It is possible that, owing to operational difficulties, the Shoal Point well did not definitively test the apex of the structure offshore. Thus, a continuous hydrocarbon accumulation in this portion of the inversion fairway cannot be ruled out.

b. Reservoir considerations. Of equal importance is the observation that reservoir rock is best developed along the paleo-structural highs ("shoulders" of rotated extensional fault blocks). These areas now lie atop the structure in the inversion fairway (Attachment 3). This observation has been borne out by the fact that the Long Point M-16 well, drilled off-structure through the roof of the triangle zone, did not encounter significant reservoir rock. The development of porosity atop paleostructural highs occurred for two reasons:

1. Shallow water carbonates on highs were exposed to early and continuous dolomitization due to evaporative pumping of seawater.
2. Protracted exposure of highs led to karsting.

These early (Ordovician) porosity generation mechanisms then facilitated later (Devonian), tectonically-related dolomitization by hydrothermal brine circulation.

Apart from Long Point, all other of the 4 deep wells were drilled atop the inversion fairway and all encountered very thick sections of gross reservoir rock, as illustrated by Cooper et al. (2001) in their stratigraphic correlation section (their Figure 16). The inversion fairway, then, is clearly a zone of reservoir enhancement and continuity.

Port au Port #1

Recognition of Matrix Productivity and "Oil-Down-To" Point

Re-testing of the Port au Port well, in conjunction with log analysis, has led to the interpretation that the matrix is oil-bearing and productive, while the isolated pockets of cavernous porosity that exist within the matrix contain primarily water. A really extensive karst systems were not encountered in the Port au Port #1 well, but undoubtedly exist within the fairway and should contain primarily oil.

An oil-wet matrix is the only model that explains the different fluid compositions encountered within the different reservoir systems. As oil was imbibed into the matrix from the overlying source rocks, water in the matrix and in the areally extensive karsts was displaced downward until the structure was generally oil filled to the structural spill point. However, water in the limited volume karsts became trapped within the karsts as it was completely surrounded by the oil in the matrix.

The isolated karsts created localized pockets of "perched" water that can be well above the elevation of the structural spill point and the regional oil-water contact. Evidence for the model includes:

1. Water bearing karsts at the top and near the base of the oil column in the Port au Port #1 well (based on open hole and production logs; see Attachment 2).
2. An oil saturation that increases with depth on logs.
3. Very high salinities of produced water (in excess of 10 times sea water concentrations).
4. A watercut that decreases with increased fluid production rates (Attachment 5).
5. A stable to declining water cut trend during the May 20/01 to June 14/01 production test (Attachment 6).
6. A stable GOR trend over the entire test with a cumulative production of 1722 m³ oil (Attachment 6).

7. Analogous West Texas Ellenburger fields², where isolated, water-bearing karsts have been drilled at structurally high points within fields, well above regional or field-wide oil/water contacts.

Layers of non-porous limestone within the structure, such as the old cave floors, also became barriers to the downward displacement of water (aquifers). The barriers impeded oil imbibition into the areas of matrix rock that directly overlie and underlie the barriers, resulting in areas of higher water saturation within a regional matrix. The aquifer at 3476 m in the Port au Port #1 well appears to have focussed charging over a broad area into the 17 m thick reservoir section above it.

² University of Texas, Bureau of Economic Geology, Atlas of Major Texas Oil Fields, Austin, 1989

The Limited Oil Volume Hypothesis

The May to June 2001 test results disprove an early hypothesis: that the PaP#1 well encountered an oil bearing karst that was of limited areal extent and contained only a limited volume of oil, in the order of 25000 m³. A cumulative production of 1722 m³ oil with no GOR increase represents a 6.9% recovery factor on 25,000 m³ and directly contradicts the limited volume hypothesis. If the oil in place was truly limited, the well should have been producing at an elevated GOR by the end of the test, since reservoir pressure would have depleted below the fluid bubble point pressure (approximately 33000 kPa, from PVT analysis).

The consistency of the GOR and the production log instead suggests that the Port au Port #1 well has encountered an areally extensive matrix, the limits of which have not yet been determined. Production logging demonstrated that the lowermost karst produced most easily but contained 90 to 100% water.

The limited oil volume hypothesis was one of several early attempts at explaining the pressure performance observed during previous short-term DST and production tests. The simplicity of the hypothesis was appealing, despite being at odds with the geological evidence and the laws of probability³. It also did not consider that the "truckloads" of lost circulation material (LCM's) pumped down the well during the drilling operation, would detrimentally affect pressure performance during testing.

³ It is practically impossible for the first drilling attempt in a new basin to discover oil, unless the oil accumulation is so widespread and continuous that the location of the well is unimportant.

Oil Migration Process

The presence of limited volumes of “perched” water within an areally extensive matrix also disproves two (2) other early hypotheses:

1. That the water at the base of the oil column in Port au Port #1 is the oil-water contact for the Garden Hill South structure.
2. That buoyancy forces alone are responsible for the presence of oil in the South Structure. Oil imbibition, from the overlying source rocks through a continuous matrix from Shoal Point to Garden Hill South (the regional fairway), is now considered to be at least as important.

Port au Port #1’s limited water production capability clearly demonstrates that the interval 3471 – 3476.5 is not a true oil/water transition zone (Attachment 2). The conclusion is further supported by the relatively high oil saturations within the interval and the presence of a tight, non-dolomitized layer between 3476.5 m and 3483 m. Coincidentally, the non-dolomitized interval separates the oil-bearing zone above it from a porous zone of negligible oil saturation beneath.

The geometry encountered by the Port au Port #1 well infers that imbibition displaced oil areally and vertically throughout the porous, regional matrix. Vertical displacement continued at each location throughout the matrix until a barrier was encountered or the structure was filled to spill point. In Port au Port #1, oil above with water below suggests that the 7 m non-porous limestone unit at the base of the oil zone (3476 m – 3483 m) acted as a barrier (aquitarde) that separates the Aguathuna reservoir into two “stacked” compartments.

Based on this model, the oil column in Port au Port #1 is the furthest extension of one large oil pool. The pool originates with the Shoal Point structure, where most of the source rock is located and most of the oil originated. Imbibition transported this oil along the inversion fairway through Garden Hill North to Garden Hill South. Thus, the “saddles” between the Shoal Point and Garden Hill North Structures and between Garden Hill North and South are also prospective for oil.

The presence of oil in Port au Port #1 and the available seismic information further suggest that no tectonic events disrupted the fairway sufficiently to separate the trio, as happened with the St. George's Bay structure.

Possible Trap Configurations

At this early stage of development of the Garden Hill oil field(s), many questions remain as to the extent and geometry of the discovery. This is purely due to lack of extensive drilling, and to a lesser extent, lack of seismic data. Therefore, at this stage, geological models must be relied on to give approximations of the size and shape of the accumulation.

Based on the above considerations, the following trapping scenarios are possible. Any combination of the scenarios is also possible:

- a. Pure structural trapping, where the oil is trapped in an overall anticlinal trend, punctuated by culminations or highs, along the inversion fairway; because of the uncertainty regarding the position of the oil/water contact, these highs may be connected hydrodynamically along strike (Attachment 1).
- b. Hybrid (structural/stratigraphic) trapping, where updip seal is effected by a loss of porosity/permeability related to less karsting and dolomitization. This scenario is a possibility because such a diagenetic change would be related to the erosional geometry of the pre-inversion extensional fault blocks, and therefore, oriented parallel to the Round Head Thrust (Attachment 3e). Such a configuration could again allow for connection of culminations along strike.
- c. Paleogeomorphic trapping, where the culminations recognized on seismic are in part related to erosional relief on the unconformity. An example is the Casablanca Field, offshore Spain, which is a corroded carbonate ridge with five separate paleohills or erosional culminations (Watson, 1981⁴; Orlopp, 1990⁵).
- d. Fault-related diagenetic trapping, where reservoir created by hydrothermal dolomitization is distributed laterally from faults along vertical or sub-vertical

⁴ AAPG, v. 65, no. 5

⁵ AAPG, v. 74, no.5

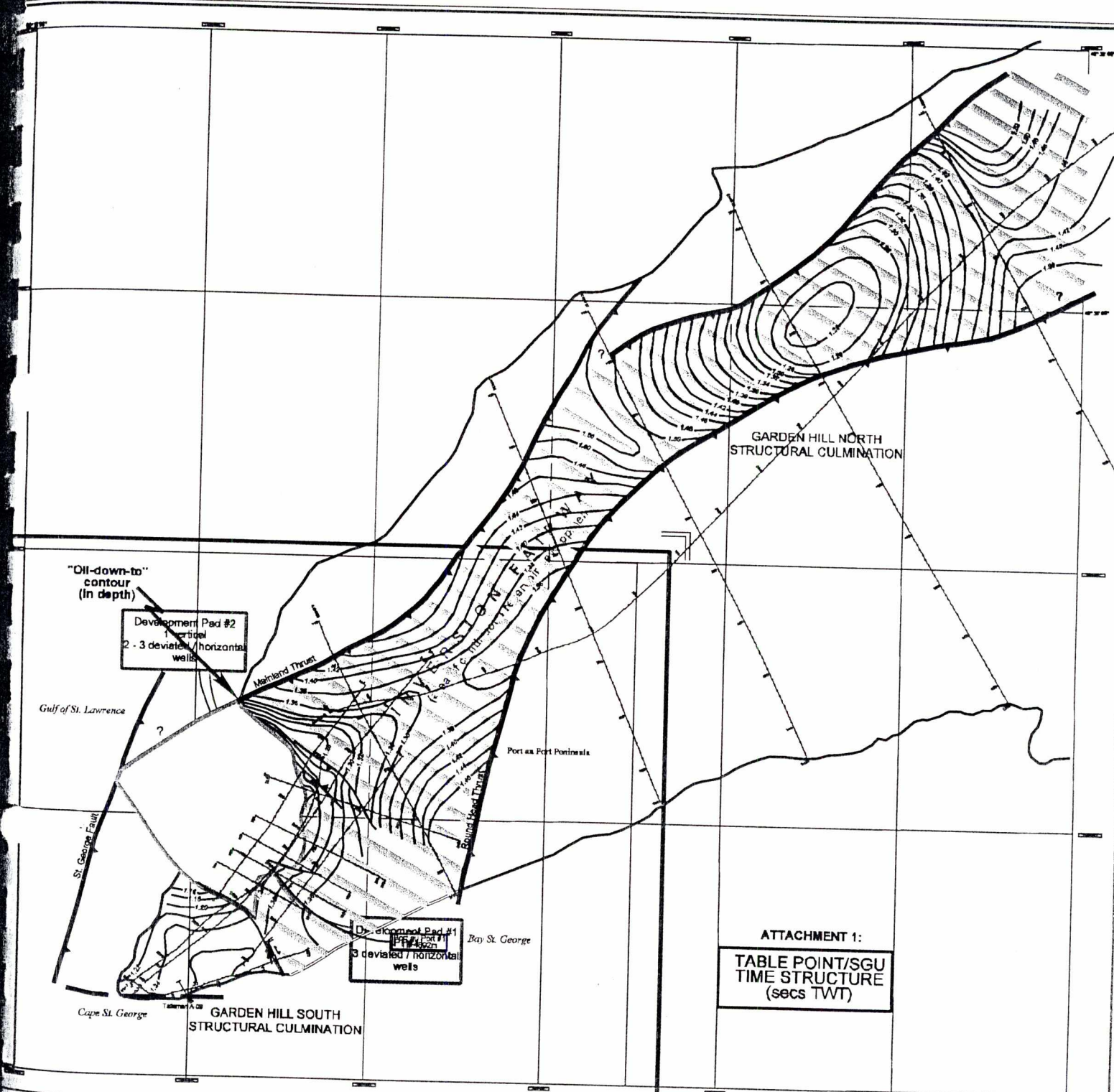
dolomitization fronts (Attachment 4). This situation is seen further north at the Daniel's Harbour zinc mine, and the best known petroleum-related example is the Albion-Scipio field in the Michigan Basin. More specifically, it is possible that some contribution to reservoir development was made by circulation of hot brines from the Round Head Thrust fault plane, which was active during the period of brine circulation, in the Acadian Orogeny.

Although the trap configurations do not give a unique solution to pool geometry along the inversion fairway, they tend to support, rather than preclude, the potential for a continuous hydrocarbon pool from Shoal Point to Garden Hill South.

Fairway Exploration

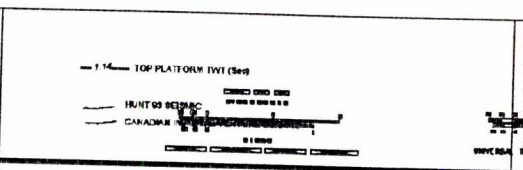
Since the entire fairway is prospective, the recommended approach to exploration of the fairway is to first drill the structural culminations, followed by step out drilling from each structure. Step out drilling should continue until the limits of each oil accumulation have been delineated or (more likely) the saddles between the accumulations have been fully developed.

- Attachment 1:** Map of the inversion fairway of the Port au Port Peninsula, showing wells drilled to date in this play, and depth structural contours atop the carbonate platform.
- Attachment 2:** Composite log over the reservoir section, Port au Port #1.
- Attachment 3:** Schematic profiles showing (a) reservoir enhancement atop rotated extensional fault blocks (after Hunt/PCP), (b) post-inversion hybrid trap formed by loss of reservoir updip to west by loss of karst/dolomitization intensity, and (c) map of hybrid trap configuration and possible distribution along inversion fairway.
- Attachment 4:** Schematic profile of reservoir created by fault-controlled hydrothermal dolomitization ("Albion-Scipio" model).
- Attachment 5:** Port au Port #1 Hourly Water Cuts and Cumulative Volumes; May 20 to June 1, 2001
- Attachment 6:** Port au Port #1 Daily Produced Oil and Water Volumes; May 20 to June 14, 2001



ATTACHMENT 1:
TABLE POINT/SGU
TIME STRUCTURE
(secs TWT)

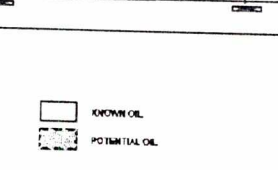
FORMATION	THICKNESS (m)	PERMEABILITY	POROSITY (%)
WELLS			
...



CANADIAN IMPERIAL VENTURE CORP.

GARDEN HILLS 2D SEISMIC
CORRELATION/STRATIGRAPHIC PLATFORM
DEPTH STRUCTURE (m)

WELLS PERMEABILITY AND
POROSITY ANALYSIS



CANADIAN IMPERIAL VENTURE CORP.

ATTACHMENT 1

TABLE POINT LIMESTONE

-10,579' TVSS

3450

ST. GEORGES UNCONFORMITY (AGUATHUNA)

"perched" water in karsts

new perf'd interval

#3

3475

"OIL DOWN TO POINT"

possible local aquitard

3500

WELL LEGEND

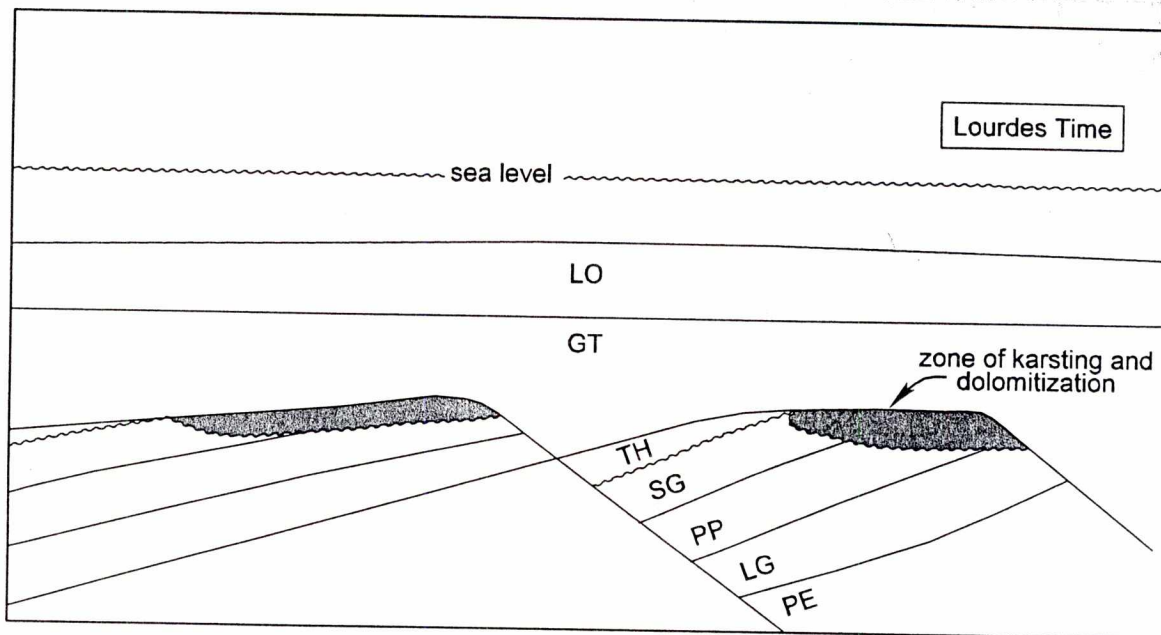
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2	Wellhead
3	Well casing
4	Well completion
5	Well perforation
6	Well cement
7	Well gravel
8	Well sand
9	Well silt
10	Well clay
11	Well shale
12	Well limestone
13	Well dolomite
14	Well sandstone
15	Well siltstone
16	Well claystone
17	Well shale
18	Well limestone
19	Well dolomite
20	Well sandstone
21	Well siltstone
22	Well claystone
23	Well shale
24	Well limestone
25	Well dolomite
26	Well sandstone
27	Well siltstone
28	Well claystone
29	Well shale
30	Well limestone
31	Well dolomite
32	Well sandstone
33	Well siltstone
34	Well claystone
35	Well shale
36	Well limestone
37	Well dolomite
38	Well sandstone
39	Well siltstone
40	Well claystone
41	Well shale
42	Well limestone
43	Well dolomite
44	Well sandstone
45	Well siltstone
46	Well claystone
47	Well shale
48	Well limestone
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87	Well siltstone
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90	Well limestone
91	Well dolomite
92	Well sandstone
93	Well siltstone
94	Well claystone
95	Well shale
96	Well limestone
97	Well dolomite
98	Well sandstone
99	Well siltstone
100	Well claystone

ATTACHMENT 2: Composite Log, PP#1

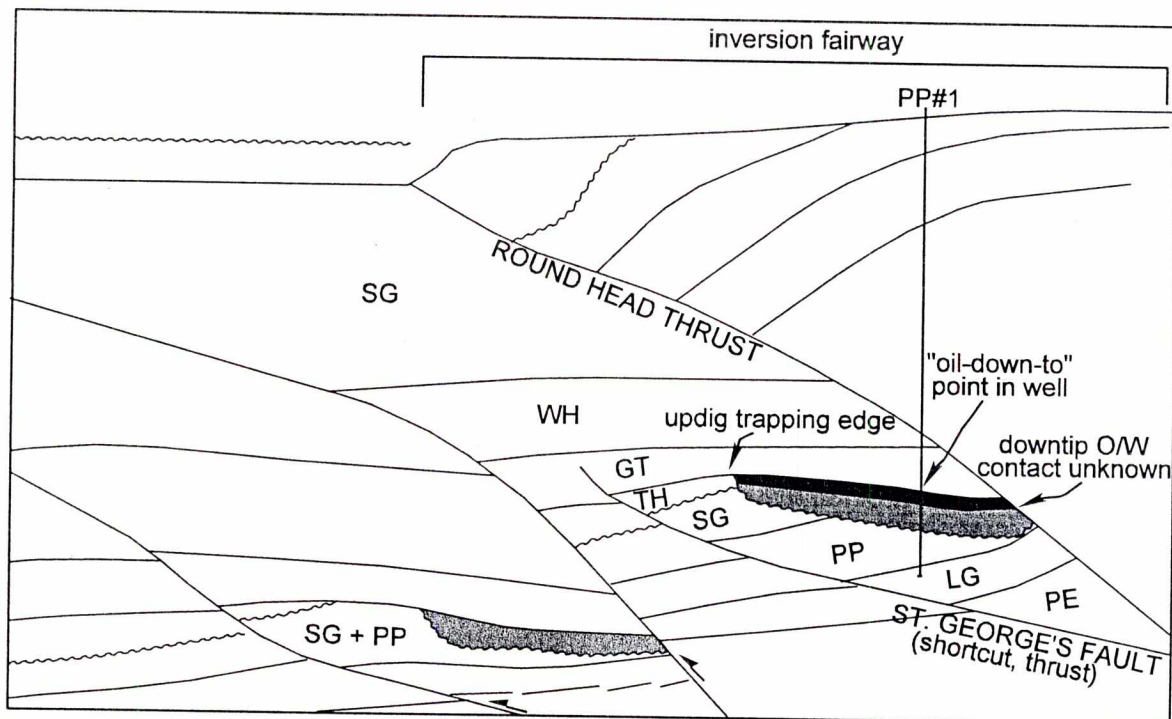
CANADIAN IMPERIAL VENTURE CORP.

COMPOSITE LOG PP#1

ATTACHMENT 3A.



ATTACHMENT 3B.

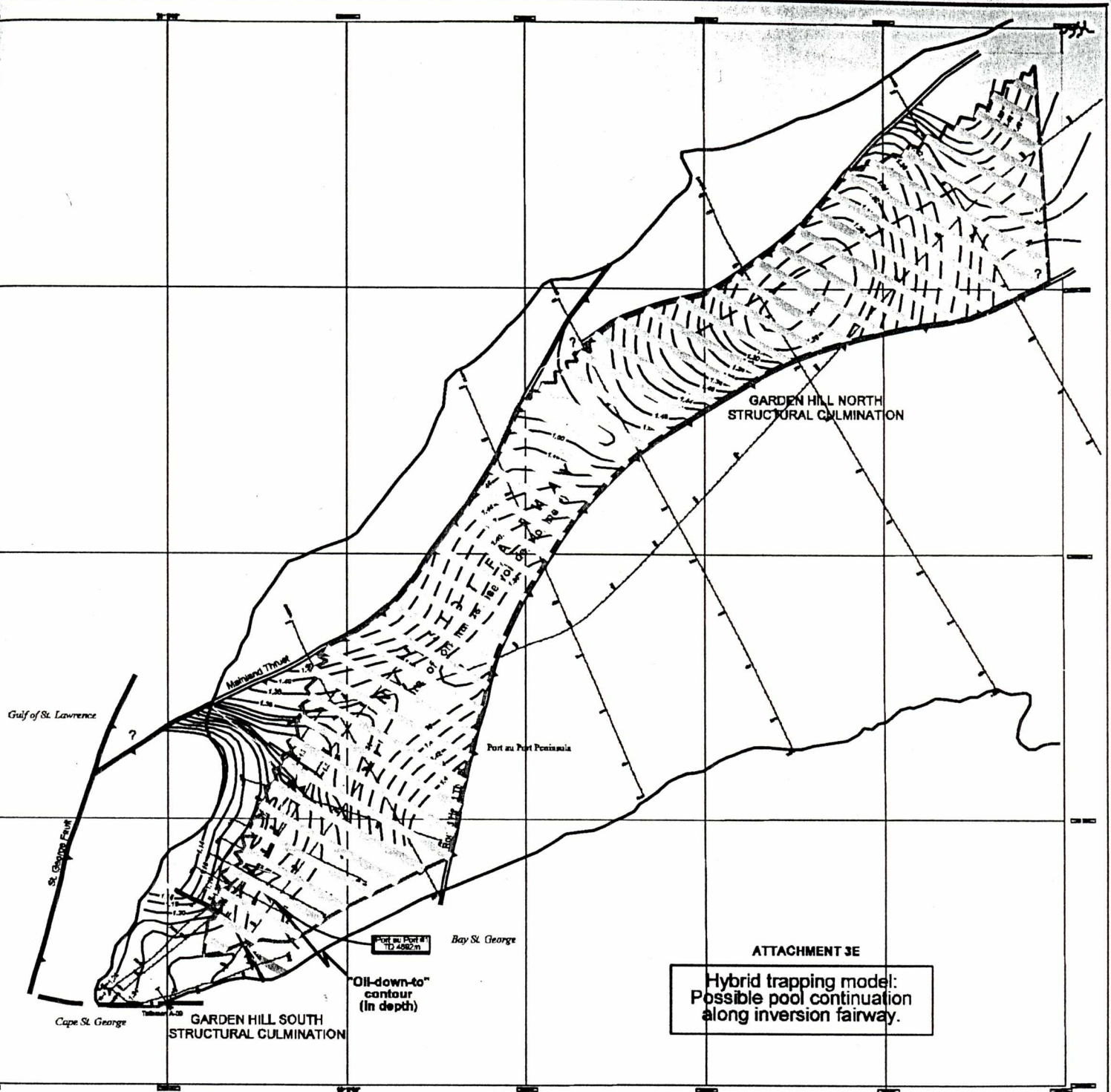


WELL LEGEND	
1	Wellbore
2	Wellhead
3	Well completion
4	Well casing
5	Well cement
6	Well annulus
7	Wellbore
8	Wellhead
9	Well completion
10	Well casing
11	Well cement
12	Well annulus
13	Wellbore
14	Wellhead
15	Well completion
16	Well casing
17	Well cement
18	Well annulus
19	Wellbore
20	Wellhead
21	Well completion
22	Well casing
23	Well cement
24	Well annulus
25	Wellbore
26	Wellhead
27	Well completion
28	Well casing
29	Well cement
30	Well annulus

ATTACHMENT 3A: Reservoir Enhancement atop extensional fault blocks
 ATTACHMENT 3B: Post-inversion hybrid trap (updip seal)

CANADIAN IMPERIAL VENTURE CORP.

ATTACHMENTS 3A & 3B



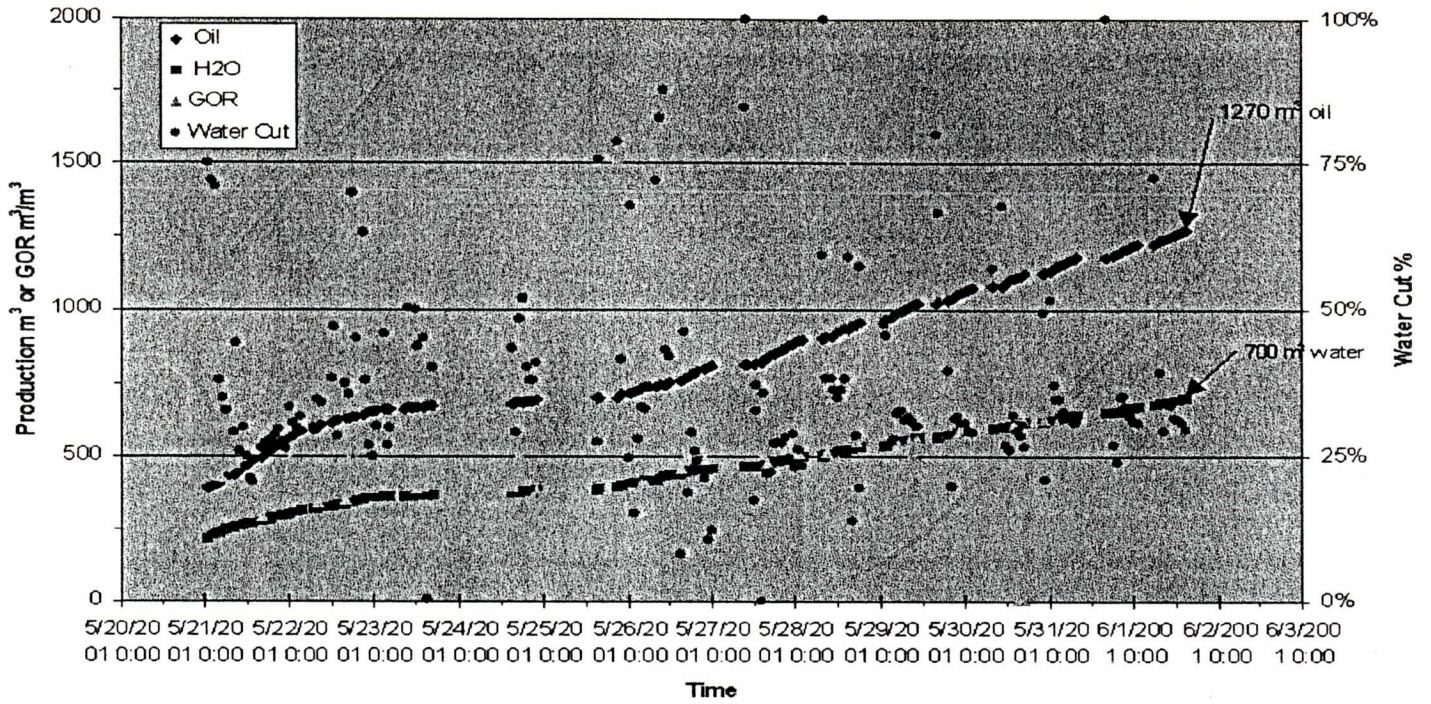
- 1.74 - TOP PLATFORM TWT (sec)
 - BENTONITE BOUNDARY
 - CANADIAN IMPERIAL VENTURES BOUNDARY



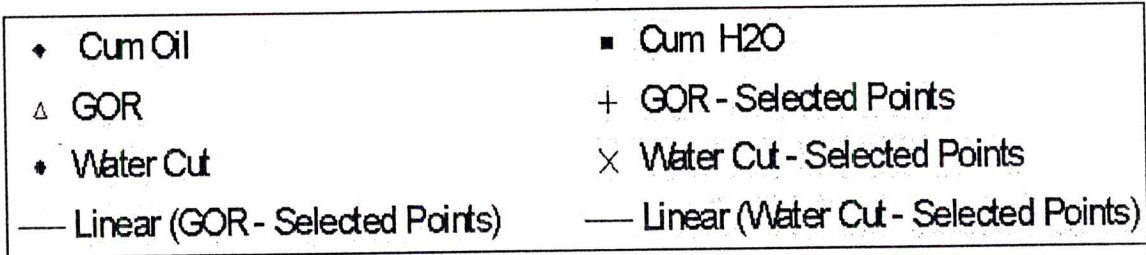
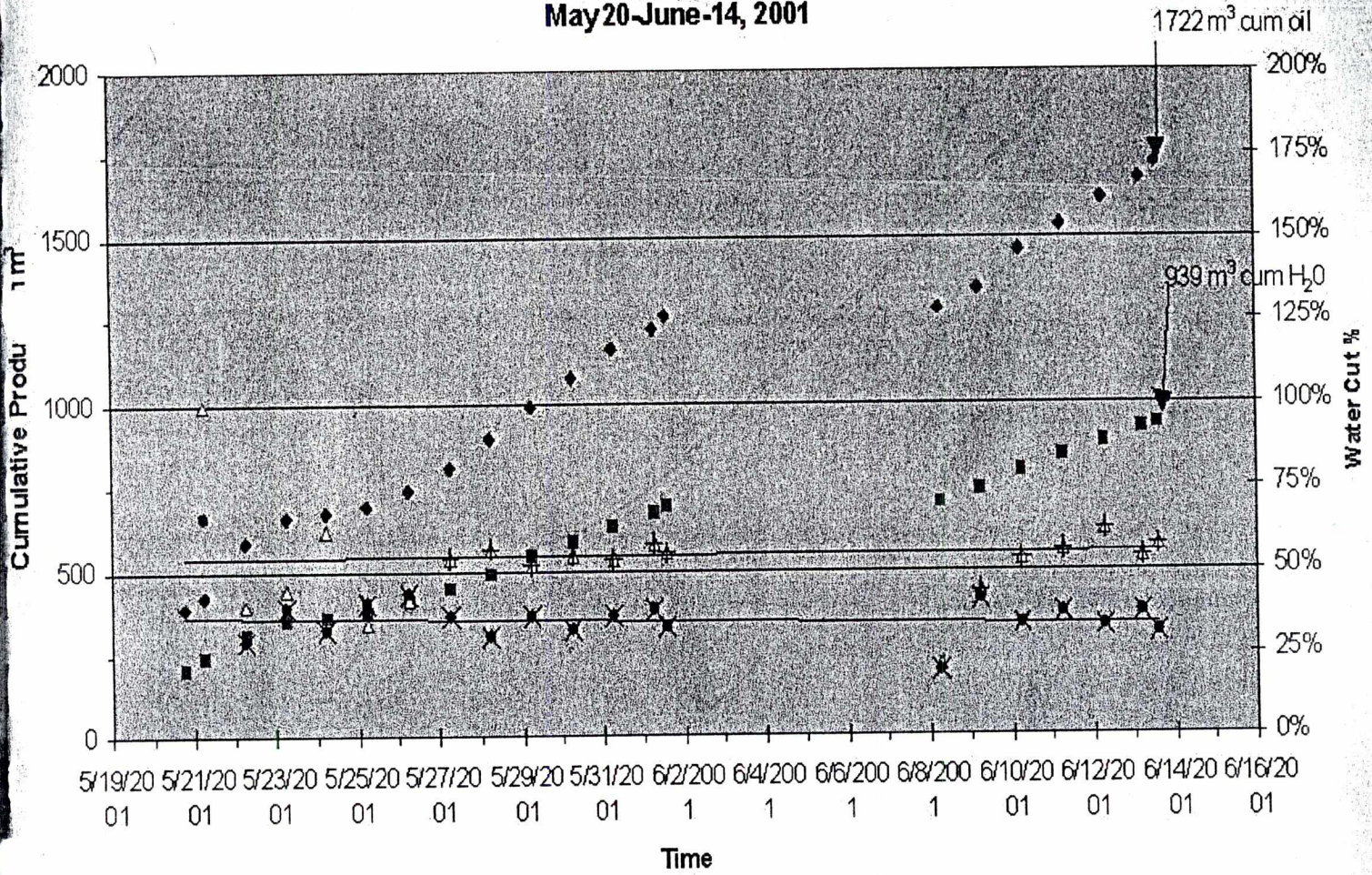
KNOWN AND POTENTIAL OIL

CANADIAN IMPERIAL VENTURE CORP.
 ATTACHMENT 3E

Cumulative Production
May 20-June 1, 2001



**Daily Produced Oil and Water Volumes
May 20 - June 14, 2001**



Fekete
Associates Inc.

Reservoir Engineering & Geology - Oil & Gas Property Evaluation - Well Test Interpretation - Software Development

June 11, 2001

CANADIAN IMPERIAL VENTURE CORP.
Suite 300, 3rd Floor, 16 Forest Road
P.O. Box 6232
St. John's, Newfoundland
A1C 6J9

ATTENTION: Mr. Steven Millan, P. Geol.
Chairman and CEO

Dear Sir;

RE: Garden Hill South Development
Port au Port #1 Well Test
Progress Report

Although testing of the Port au Port #1 well is still ongoing, well performance suggests that the formation matrix is oil bearing and productive, though it is either severely plugged around the well or of low permeability. A productive matrix at Port au Port #1 is consistent with the geological model and oil-in-place estimates for the Garden Hill South field. Severe plugging is plausible, given the unusually large volume of lost circulation material that was pumped down the wellbore during the drilling operation.

Another important finding is that wells drilled in Garden Hill South can be immediately placed on primary production following drilling and completion. Testing has demonstrated that wax and salt deposition can be economically dealt with in an ongoing operation and produced oil can be immediately trucked to local markets.

Trucking of primary production is an initial development step that was previously considered to be unavailable to Garden Hill South. The benefits of an early production system include significantly accelerating the onset of cash flow and acquiring additional data through production of the initial wells. This data can then be used to plan

subsequent development wells and facilities. Dry gas cycling remains the highly desirable end point for full field development.

Oil recovery under primary production is estimated to be 5 to 10% of the oil-in-place, or between 9 and 30 MMBbls for the Garden Hill South Field. Ultimate recovery for the combination of primary production and dry gas cycling remains at between 40 and 70% of the oil-in-place. These values are consistent with previous recoverable oil estimates for the field of 70 to 130 MMBbls, using a 40% recovery factor.

Performance to date suggests that daily oil production from Port au Port #1 may be stabilizing at about 80 m³/d (503 BOPD) but the test duration is insufficient to determine how long the well can sustain this rate. No treatment is recommended to try and increase the rate from Port au Port #1 at this time, other than to continue producing and allow the well to clean up on its own.

The significance to field development is that a rate of 80 m³/d from a massively damaged well indirectly supports previous productivity estimates of 300 to 1300 m³/d (1900 to 8200 BOPD) for new wells. Productivity estimates for new wells are based on producing karst analogies, such as the Ellenberger formation in West Texas.

A test duration of a few weeks is insufficient to provide any insight on well drainage area or the drilling density required for efficient oil recovery. A 16-hectare (40-acre) spacing pattern is prevalent in the Ellenberger formation, where matrix porosity averages between 1 and 3%. Since permeability is proportional to intergranular porosity in the dolomite matrix, and matrix porosity in the Port au Port #1 well averages 8 to 10%, one quarter section (64 ha) is recommended as an initial default well spacing. Production from the initial wells will provide additional information to either support or modify the spacing pattern.

In order to classify the oil in Garden Hill South as proven reserves, geological and engineering evidence must indicate, with a high degree of confidence, that the oil is economic to produce. Further production testing of Port au Port #1 will assist in this objective by:

1. refining operating practices
2. confirming revenue and operating costs
3. gaining additional reservoir information

The information is directly applicable in refining the economic projections for field development. In addition, a demonstrated positive cash flow will allow proven reserves to be assigned to the Port au Port #1 well.

Please contact me at your convenience with any questions or concerns. My direct number is 213-4235.

Yours truly,
FEKETE ASSOCIATES INC.



Ray Mireault, P. Eng.
Manager, Production Optimization
RAM/cf/jch
Attach.

Cc. G. Edwards - CIVC
K. Mercer - CIVC



**Attachment G: Geological Report
for CIVC Port au Port #1-ST2 well
Garden Hill Oilfield, Port au Port
Peninsula, Newfoundland
(Tectonics Inc.)**

***Geological Report for CIVC Port au Port #1-ST2 well
Garden Hill Oilfield, Port au Port Peninsula
Newfoundland***

by

**George S. Langdon, PhD, P.Geol.
Tectonics, Inc.
Calgary, Alberta**

August 26, 2002

Summary

The CIVC Port au Port#1-ST2 well tested gas from the Table Point Formation at 1.2 mmcfd and 51 degree oil from the Aguathuna Formation at 150 – 200 bopd. The entire Middle Ordovician carbonate platform section seen in the well is dolomitized, and appears to consist of interlayered crypto-crystalline, tight with fine- to medium crystalline dolomites containing intercrystalline and vuggy porosity. A gross reservoir rock interval of 36 m (vertical) was encountered, and net to gross ratio is estimated at 33%. The well has the potential to be stimulated and completed as an Aguathuna oil producer. All the data strengthen the technical merit of the proposed Port au Port #2 exploration well.

List of Figures

Figure 1: Stratigraphic column and summary diagram for the Port au Port #1-ST2 well.

Figure 2: Portion of the real-time gamma ray log, Port au Port #1-ST2.

Figure 3: Cross-section along seismic line CAH93-4A, showing geological interpretation of well results.

Appendices

Appendix I: Geolograph over key intervals, Port au Port #1-ST2.

Appendix II: Total gas log over key intervals, Port au Port #1-ST2.

Overview of Operations

The well was designed to effectively "twin" the PP#1 well by drilling virgin hole outside the radius of formation damage of the original borehole, and was directionally drilled toward Azimuth 010 to intersect the reservoir approximately 30 m away from Port au Port #1.

During the first attempt to drill out of the window in the casing (@3352 m) the inclination angle did not increase above about 6 degrees, and anomalously high drilling rates were being seen in the Goose Tickle Group shales. At the same time, a high proportion of old, hard cement was returning in the cuttings. It was subsequently realized that the well was drilling in the severely caved annulus of the original Port au Port #1 borehole. This hole was then cemented off back to the window and drilling recommenced with a second attempt to drill out through the window into formation. This time the bit was supported by the new cement and the kick-off operation was successful. This was recognized by the steadily building angle, the gradual decrease of fresh cement returns and replacement by formation cuttings, and a drilling rate of approximately 3 – 4 m/hr, more typical for the Goose Tickle.

A total gas detector was supplied by Datalog and set up in the doghouse during the operation. The results and interpretation of shows is summarized below. Key sections of the gas log are presented in Appendix II. All depths are measured depths (MD) unless otherwise noted.

Major total gas shows are associated with the entire section below the top of the Table Point Formation. Above this point, background gas liberated during drilling of the Goose Tickle typically ranged between 10 and 50 units, with occasional peaks up to 100 units. The Table Point Formation between 3443 m (MD) and 3454 m shows gas rapidly increasing and peaking at 1008 units. As illustrated in Appendix II, this corresponded to a increase in drilling rate from around 3 m/hour to about 10 m/hour in the upper 10 m of the Table Point. In the lower 3 metres of the Table Point, total gas ranges up to 512 units,

but as drilling rate jumped from 8.4 to 17.3 m/hr across the St. George Unconformity (top Aguathuna Fm.), gas increased rapidly to a peak at 2233 units and held at that level to 3465 m where DST #1 was called. In the interim, large amounts of trip and connection gas were seen, with peaks at 4478 units, 4826 units and 5942 units.

After DST #1 was completed the operation continued with conventional rotary drilling and significantly lower penetration rates (Appendices I and II). This apparently affected gas concentrations in the mud, as a peak of 2033 units corresponding to 3465 m is now shorter in wavelength and apparently concentrated at the top of the interval, as gas decreases throughout the remainder of the time interval to the 200 – 300 unit range. From 3470 – 3475 m the gas log is again characterized by a peak of 1982 units at the top of the interval (reflecting the shut-down time for the bottoms-up sample), which decreases to the 160 unit range for the remainder of the interval. Below about 3479, gas levels gradually decrease to the 100 unit level, commensurate with lower porosity suggested by gradually slowing penetration rate.

Sample Descriptions and Lithology Log (see Figure 1)

- 3350 m: cement (drilled out of window)
- 3352 m: mainly cement
- 3354 m: mainly cement
minor shale of Goose Tickle Group
- 3358 m large portion of cement
Lithology:
95% shale, med-dark grey
5% sandstone, very fine grained, NVP, no shows

The following samples showed regularly decreasing amounts of cement.

- 3360 m 95% shale a/a, non-calcareous
5% sandstone, very fine grained
- 3365 m 90% shale a/a
10% sandstone, a/a, highly calcareous cement
- 3370 m 90% shale, a/a, generally non-calcareous
10% sandstone, very fine to fine grained, generally immature, 80% quartz/20% lithic, very argillaceous in part, poorly sorted, with significant portions of chalky, calcareous matrix/cement, chips partially disaggregate when left in cold HCl
- 3375 m shale and sandstone, gen. a/a
- 3380 m 60% shale a/a

40% sandstone, very fine to fine grained, occasionally medium grained, mainly quartzose, about 20% lithic fragments, well sorted, scattered poor porosity, well rounded to sub-angular grains, no shows trace siltstone grading to very fine sandstone

- 3385 m 70% shale, non-calcareous, grading to slightly calcareous siltstone
25% sandstone, generally a/a, very well rounded but well cemented with apparent 3-point grain junctions, trace porosity, calcareous in part
5% limestone, white, interbedded with shale (bed boundary seen in composite grain)
- 3390 – 90% shale, a/a
- 3415 m 10% sandstone a/a, speckled, salt and pepper, containing a mixture of allochems, including quartz, mica, garnet, chlorite, pyrite, and shale, but no arkose
- 3420 m 80% shale a/a, slightly brown grey, non-calcareous
20% sandstone a/a
 trace dolomitic mudstone
 trace white limestone, microcrystalline to finely crystalline
- 3425 m 90% shale a/a
10% sandstone a/a
- 3430 - 90% shale a/a
- 3435 m 10% sandstone, trace porosity, no shows
 minor calcite veining with light brown stain (?) and bright yellow fluorescence
- 3440 m 90 % shale a/a
10% sandstone a/a

3445 m 70 % shale a/a
10% sandstone a/a
20% dolomite, brown to brown grey, crypto- to microcrystalline, faint oil stain, NVP, occasional rhombic form on edges of cuttings suggesting poor-fair (?) porosity.
 * fast drilling break at 3443 m corresponds to porosity in dolomites (see Appendix I)

Top Table Point Formation @ 3443 m.

3450 m 90% dolomite, medium to dark brown, microcrystalline, NVP, occasional dull patchy fluorescence
10% dolomite, finely crystalline, fair to good porosity, common bitumen in pore spaces, appears to partially plug pores, occasional very dull yellow fluorescence
 trace dolomite, white, coarsely crystalline to white

3453 m 70% dolomite, medium to dark brown, microcrystalline, mottled, NVP
 (bottoms 20% dolomite, brown, finely crystalline, fair intercrystalline and micro-
 up) vuggy porosity, common bitumen/dead oil residue visible in pore throats, common dull to medium yellow fluorescence. The two above lithologies are intergradational and are commonly seen on the same cutting.
10% dolomite, white, medium to coarse grained

N.B. By the presence of many composite grains with microcrystalline grading to very finely or finely crystalline dolomite at the edge of the grain, it is assumed that there is a fair amount of vuggy/micro-vuggy porosity scattered in patches throughout the rock. Most of this has bitumen associated with it. Based on this the overall porosity grade of the rock may reach fair, but most of it appears to have some bitumen plugging. The

presence of white sparry dolomite suggests that there may be small caverns or fracture-related voids present.

- 3455 m 80% dolomite, microcrystalline, a/a
 10% dolomite, finely crystalline, vuggy, a/a
 10% dolomite, white, sparry
- 3460 m 80% dolomite, tan to light brown to medium brown, very fine to finely crystalline, occasionally medium crystalline
 20% tan to brown dolomite a/a, grading to medium grained euhedral rhombic crystals, inferred fair porosity, patchy bitumen residue but not as prevalent as above with many open pore throats visible.

* This interval 3458 – 3465 m drilled at around 20 m/hr. while sliding with mud motor.

In general, the cuttings have begun to take on a more blocky, equant appearance in this sample.

Top Aguathuna Fm. @ 3458 m

- 3465 m 95% dolomite, microcrystalline to finely crystalline, NVP
 5 % dolomite, medium grained, rhombic, blocky chips, poor inferred porosity, trace bitumen residue.
 trace dolomite, sucrosic, excellent porosity
- 3470 m dolomite, generally a/a (very poor sample due to abundant shale cavings – returned to rotary drilling only below 3465 m.)
 * drilling rate slowed to around 6 m/hr in rotary drilling during this interval.

3475 m 80% dolomite, white and off-white, very fine to medium grained,
occasionally coarse grained, occasionally sparry, poor to fair porosity
inferred from occasional free crystal faces, no stain
20% dolomite, brown, bitumen residue (?)(cavings?)

* drilling rate slowed to 3 - 4 m/hr over this interval

3482 m 90% dolomite, white/off-white to tan to brown, occasional euhedral,
TD sample rhombic dolomite with good porosity, no show, minor bitumen
10% shale/limestone interbeds (cavings?)

* drilling rate slowed to 1 – 2 m/hr over this interval.

Logging

No conventional wireline logging was carried out in the well. A MWD gamma ray was run with the directional drilling assembly, located approximately 15 m behind the bit. This was very useful in correlating through the Goose Tickle section, as several gamma ray peaks are readily correlable with Port au Port #1 (Figure 2). In particular, the top Table Point Formation pick is very clear and enabled confident prediction of the Aguathuna top. It also correlated with a fast drilling break at 3443 m (MD).

Drill Stem Tests

DST #1 was carried out as a bottom-hole test at 3465 m MD, within the uppermost Aguathuna. The upper packer was set inside casing (PP#1) at 3335 m. The well flowed .230 to .300 mmcf/d over a 1-hour flow period. The main flow period was not carried out as the operation went back to drilling. A small amount of oil was recovered in the drilling mud (enough to cover the top of sample containers).

DST#2 was run as a bottom-hole test from TD at 3482 m MD. Over the main 36-hour flow period, the well flowed 49-51 deg API oil at rates of 150-200 bopd, and gas at 1.2 mmcf/d.

Detailed analysis of test data will be provided by Fekete Associates at a later date.

Interpretation of Geological Results of Port au Port #1-ST2

As mentioned previously, there was some initial difficulty in kicking off into the sloughing shales of the Goose Tickle Group, as the first attempt resulted in the bit tracking the annulus outside the PP#1 casing. Once the annulus was backfilled with cement and the area outside the window was supported with cement, the bit was able to cut cleanly into the formation, and inclination was built steadily from there on. The final Schlumberger directional survey (15 m behind bit at 3467.1 MD) showed an inclination of 32.6 degrees toward azimuth 003.9 degrees, with an implied horizontal offset of 24 m.

Tops from the well were picked on drilling rates, lithologies, gas log, and in the case of the Table Point, the MWD gamma log. Tops, thicknesses, and gross pay are compiled in Table 1.

The well showed two significant departures from prognosis, both of which may be considered positive from an exploration/production perspective. Firstly, the Table Point Formation appears to be thoroughly dolomitized, a situation which is not seen in any other well drilled in the area. In the shallow subsurface and at the surface on the northern peninsula (e.g., Daniel's Harbour/Port au Choix areas) the Table Point is commonly dolomitized. Conceptual dolomitization models for the western Port au Port area show dolomitization moving up into the Table Point strata as the Round Head Thrust is approached, thereby emphasizing the relationship between dolomitization and faulting, and suggesting that more intensive fracturing and faulting may be coming into play north-northeastward from Port au Port #1 toward the seismically-mapped tear fault (Figure 3).

Secondly, a structural gain of 10 m is seen at reservoir level. This suggests that a fault zone is present between the old and new boreholes. It is likely that this fault is a splay of the east-west reverse-transpressive ("tear fault") system which intersects seismic Line CAH93-4A at shotpoint 315, about 200 m northeast of Port au Port #1.

With the combination of 15 m additional dolomitization in the Table Point and 10 m structural gain, an additional gross reservoir rock of 25 m is seen in the well. This means that if the original base-known-oil is projected, than a minimum of 36 m gross reservoir rock occurs (top table Point at -3215 m to BKO at -3251 m: Figure 3). The well has drilled 36 m of this section as it stopped 3 m above the base-known-oil level (-3248 m).

Implications for Future Exploration

A significantly higher degree of dolomitization has been seen in the new well, although in general the reservoir appears to be one of interlayered porous and non-porous rock. In the absence of well logs, it is thought that the well may have penetrated a zone of “overdolomitization”, as suggested by the amounts of white, coarse, in part sparry dolomites in the Aguathuna section. This phenomenon may reflect proximity to a fault zone. As discussed above, the abrupt increase in structure also suggests that the well bore crossed a fault splay. Such a splay cannot be seen clearly on seismic line CAH93-4A (see Figure 4 from Langdon and Mireault, 2002¹), but the interpretation is consistent with the mapping of the east-west tear fault as a transpressive system, with a minimum 20 m structural gain seen on the north side of this fault (Figure 2, Langdon and Mireault, 2002¹). This is the proposed target area for the PP#2 exploration well. (*N.B.*, In Figure 3, the cross-section as a whole is oriented SSW-NNE, based upon the CAH93-4a seismic line, while the ST2 well was actually drilled toward azimuth 004).

Preliminary DST analysis and modelling suggest that the oil and gas legs are separate accumulations (perhaps separated by the St. George Unconformity at the top of the Aguathuna Formation), meaning that there may be an option to complete the well as an oil producer. Comparison between PP#1 and ST2 for the oil zone suggest that there is

¹ Langdon, George S., Tectonics, Inc. and Mireault, Ray, Fekete Associates, June 4, 2002: Revised Exploration Model for the Inversion Fairway, Western Port au Port Peninsula, Newfoundland, Internal report for Canadian Imperial Venture Corp.

pressure communication across the inferred fault. The occurrence of oil in the upper Aguathuna structurally higher than that in PP#1, and the absence of water through a section representing almost all the Aguathuna down to the base-known-oil (BKO) in PP#1, suggest that the BKO may be continuous across the inferred fault. Finally, the similarity of the oil gravity (~51 deg API) argues for lateral communication in the oil leg. These observations in general support the revised inversion fairway exploration model presented in Langdon and Mireault (2002) for PP#2, as illustrated in Figure 3.

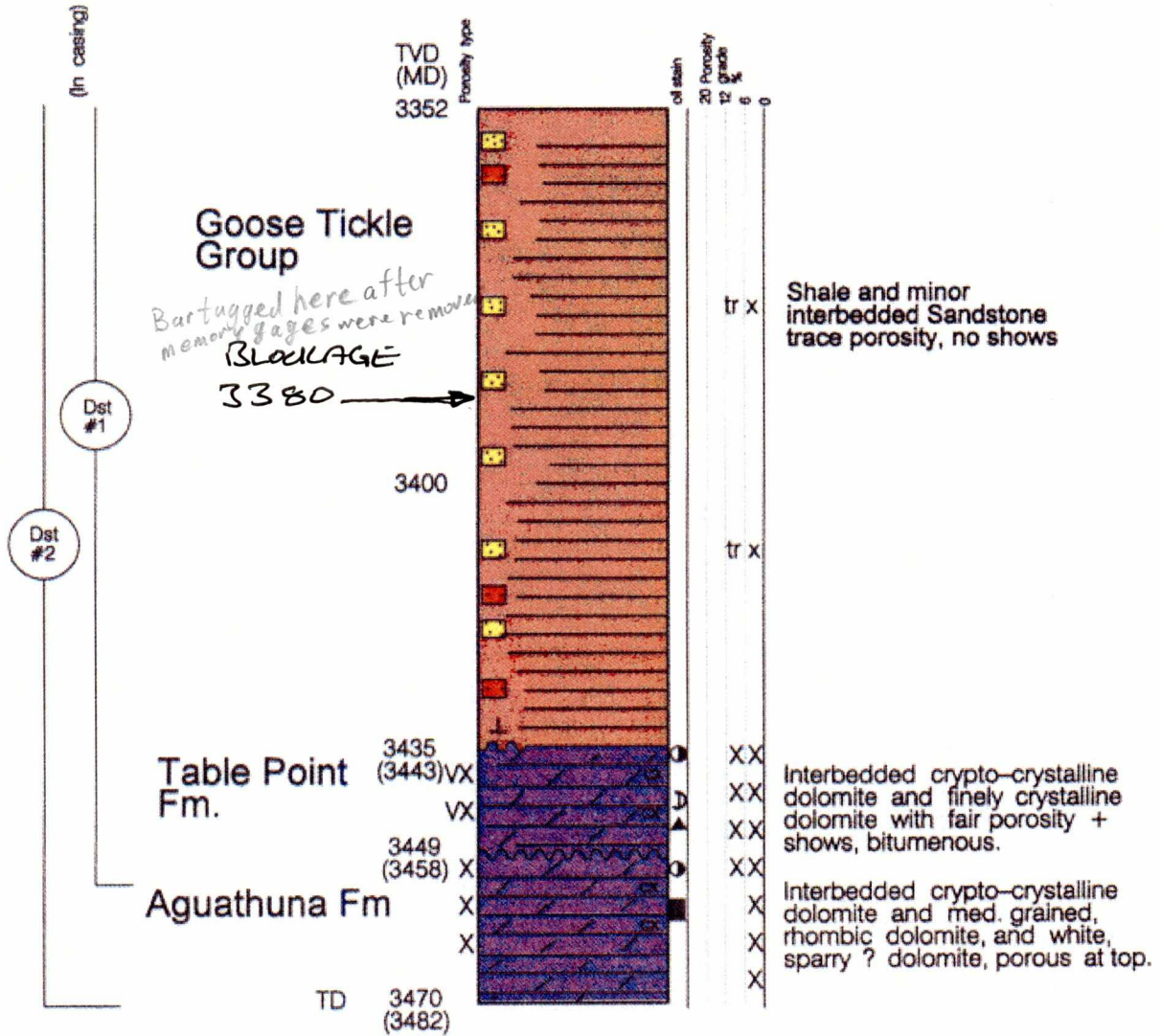
Port au Port #1-ST2: Geological Tops

Formation	MD (m)	TVD (m)	subsea	difference from prog	vertical thickness	"gross pay"
Tie-in (Goose Tickle Gp.)	3352	3352	-3132		83	
Table Point Fm.	3443	3435	-3215	10	14	15
Aguathuna Fm.	3458	3449	-3229	10	19	24
<i>Total depth</i>	3482	3468	-3248			

* equivalent to drilled thickness in gross reservoir

Table 1

CANADIAN IMPERIAL VENTURE CORP.
 PORT AU PORT #1 - ST2 (deviated)



DST #1: 0.230 - 0.300 mmcf/d gas

DST #2: 150 - 200 BOPD (49° - 51° API), 1.2 mmcf/d gas

Figure 1

Vertical Scale: 1cm per 2 meters Creation Date: Wed, Aug 07, 2002, 11:03:43 AM

CIVC PP#1-ST2

Gamma Ray,
Real-Time -
SLMPGR_RT_DEPTH,54

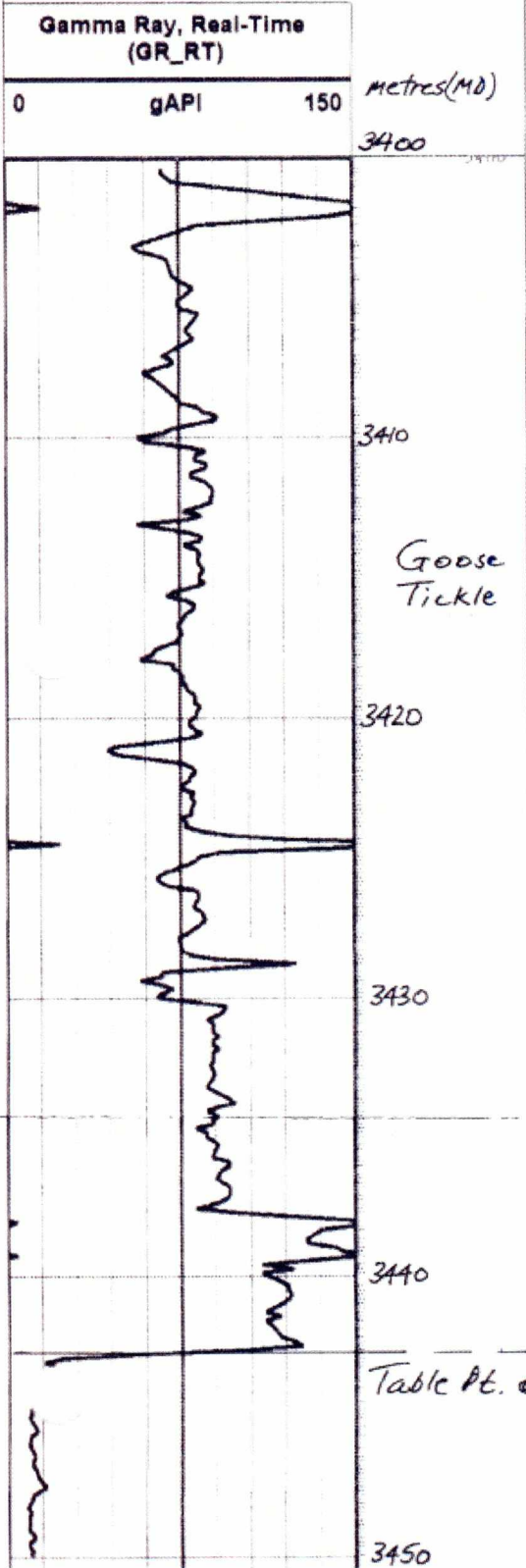


Figure 2

CROSS-SECTION ALONG SEISMIC LINE CAH93-4A

CANADIAN IMPERIAL VENTURE
GARDEN HILL FIELD
PORT AU PORT #1 / #2
KB 220m

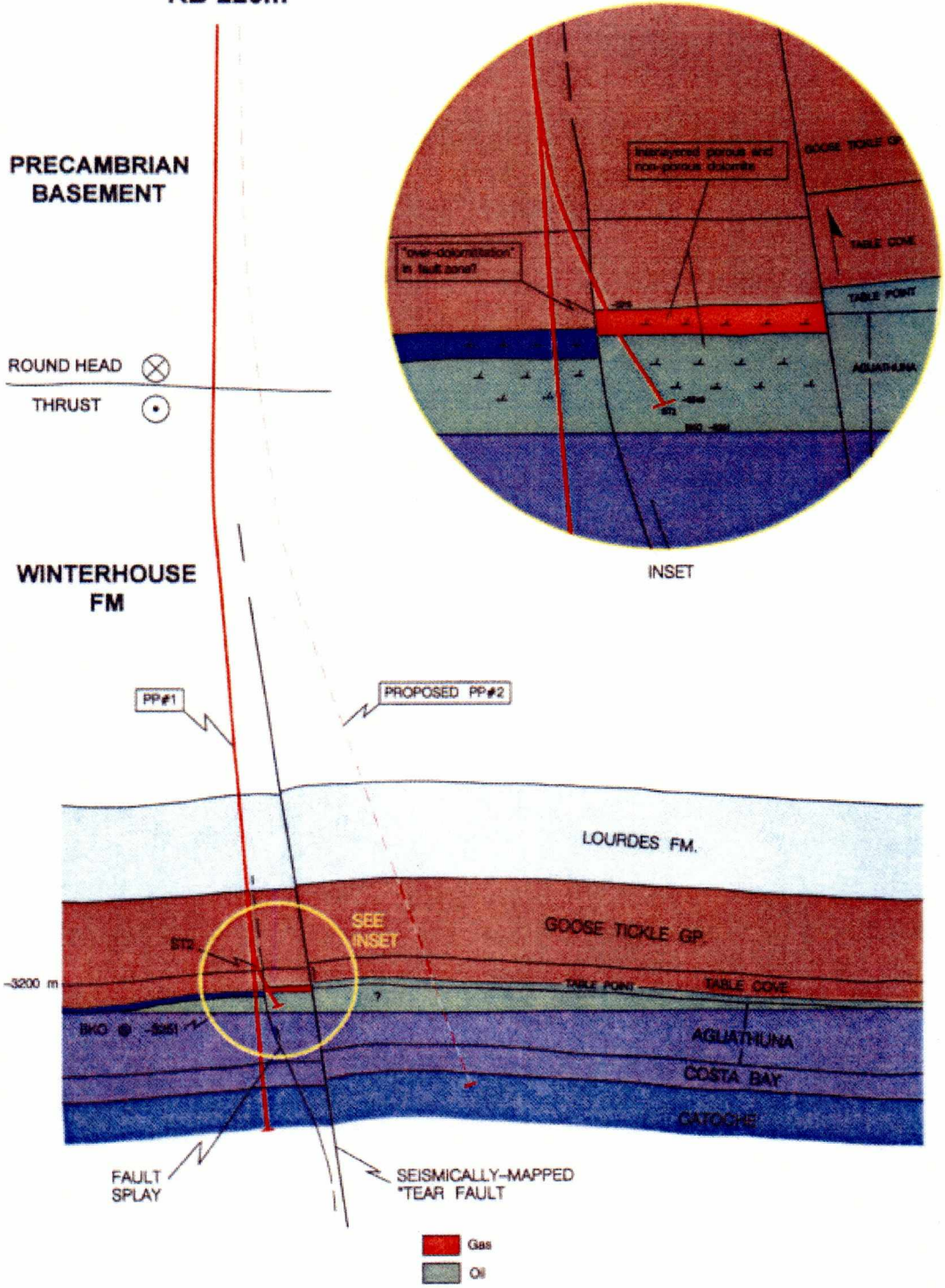
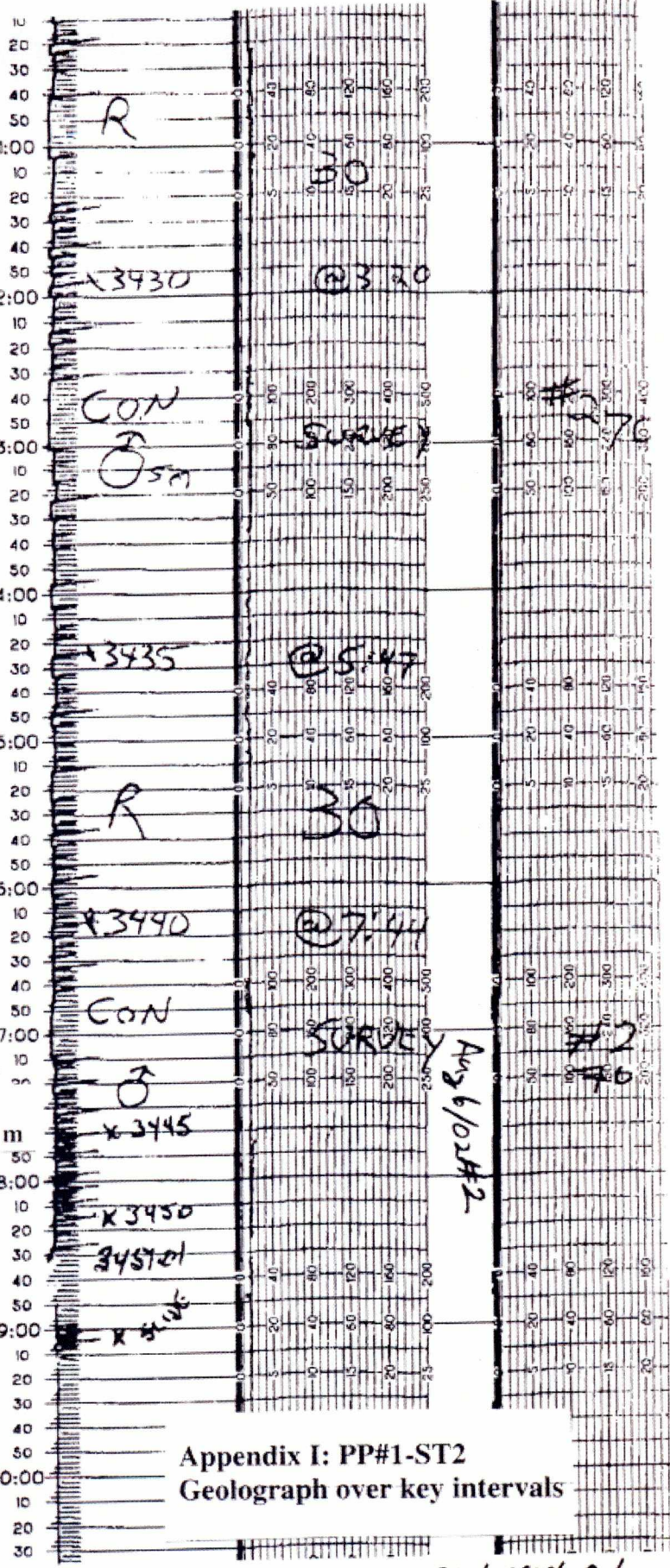
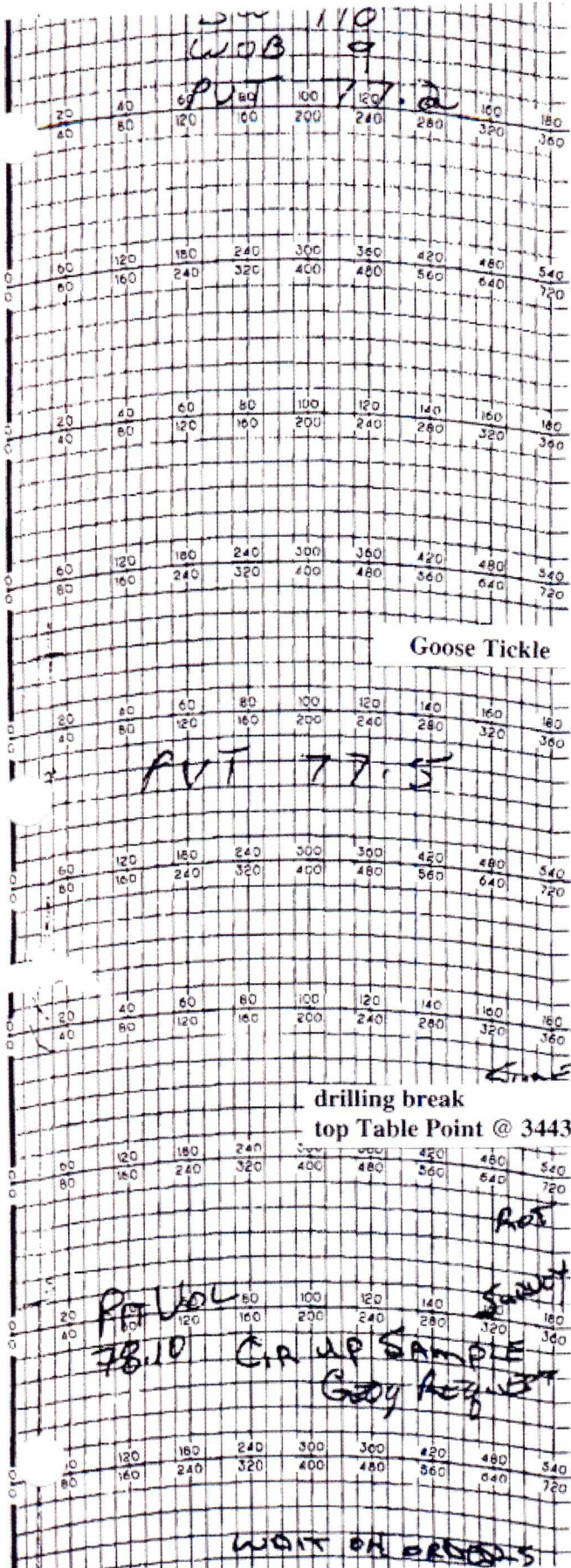


Figure 3



Appendix I: PP#1-ST2
Geologist over key intervals

METRIC SENSATOR

DRILLING RECORDER

CHANGE CHART AT 6 A.M.

PART NO. 263150

PRINTED



24
HOUR

24
HOUR



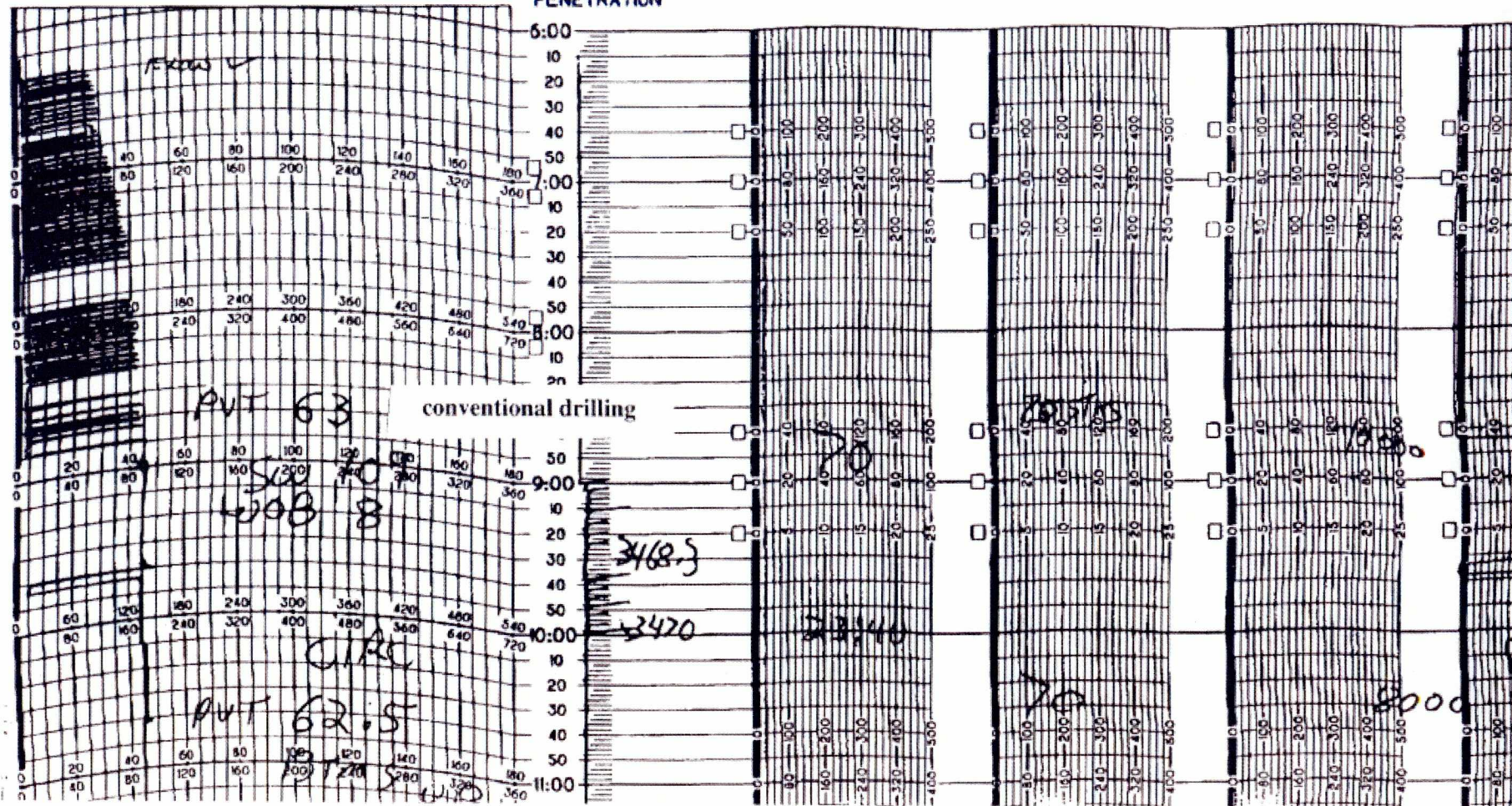
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 DISTRICT: PORT AU PORT T.D. OFF: _____
 DATE ON: Aug 09-02 T.D. ON: 3465m
 M. DRLD: _____

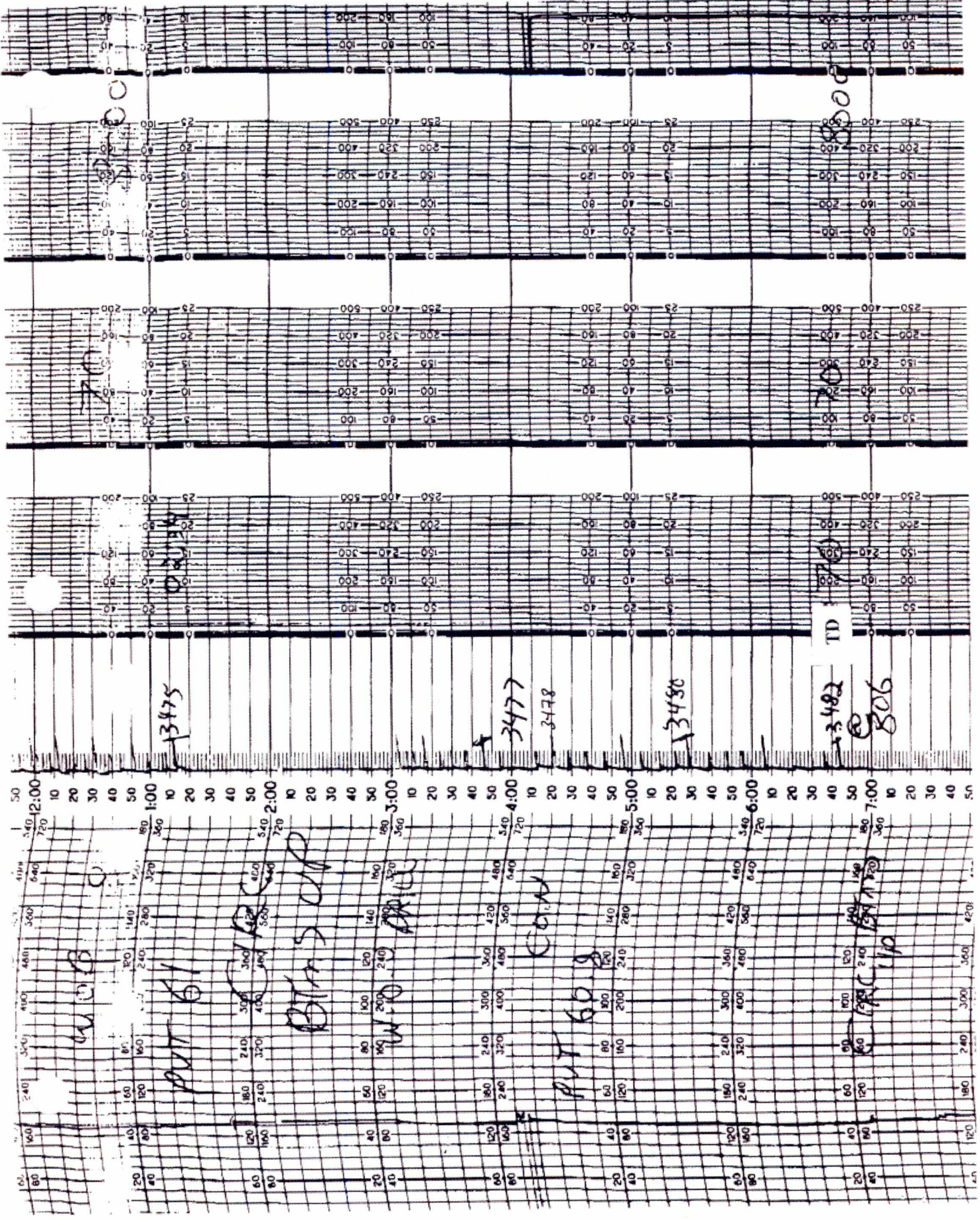
M/D TOTCO INSTRUMENTATION

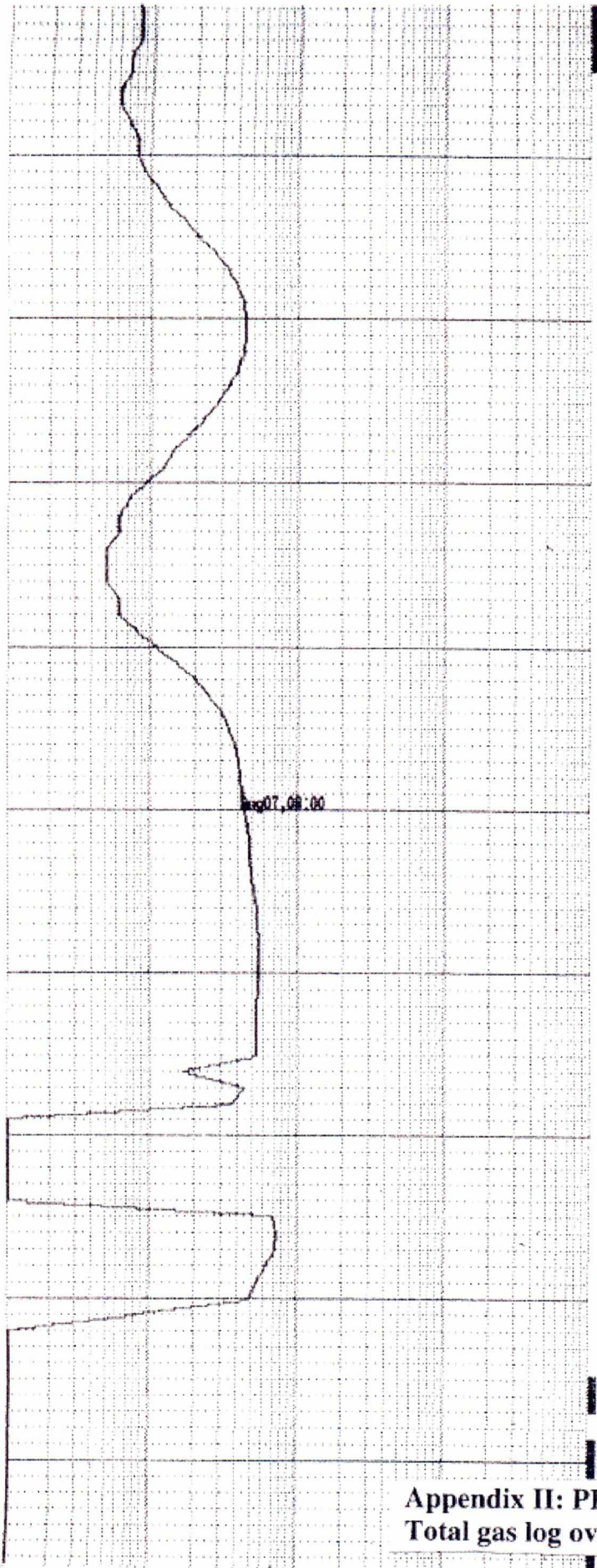
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| <input type="checkbox"/> TORQUE | <input type="checkbox"/> TORQUE | <input checked="" type="checkbox"/> TORQUE | <input type="checkbox"/> TOI |
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| <input type="checkbox"/> % MUD FLOW | <input type="checkbox"/> % MUD FLOW | <input type="checkbox"/> % MUD FLOW | <input type="checkbox"/> % |
| <input type="checkbox"/> % PIT LEVEL | <input type="checkbox"/> % PIT LEVEL | <input type="checkbox"/> % PIT LEVEL | <input type="checkbox"/> % |

WEIGHT IN 1000 KG

PENETRATION







3442 5.5

GOOSE TICKLE

3443 4.9

TABLE POINT

3444 4.6

3445 7.7

07:08:00

3446 7.5

3447 7.3

3448 10.3

3449 10.6

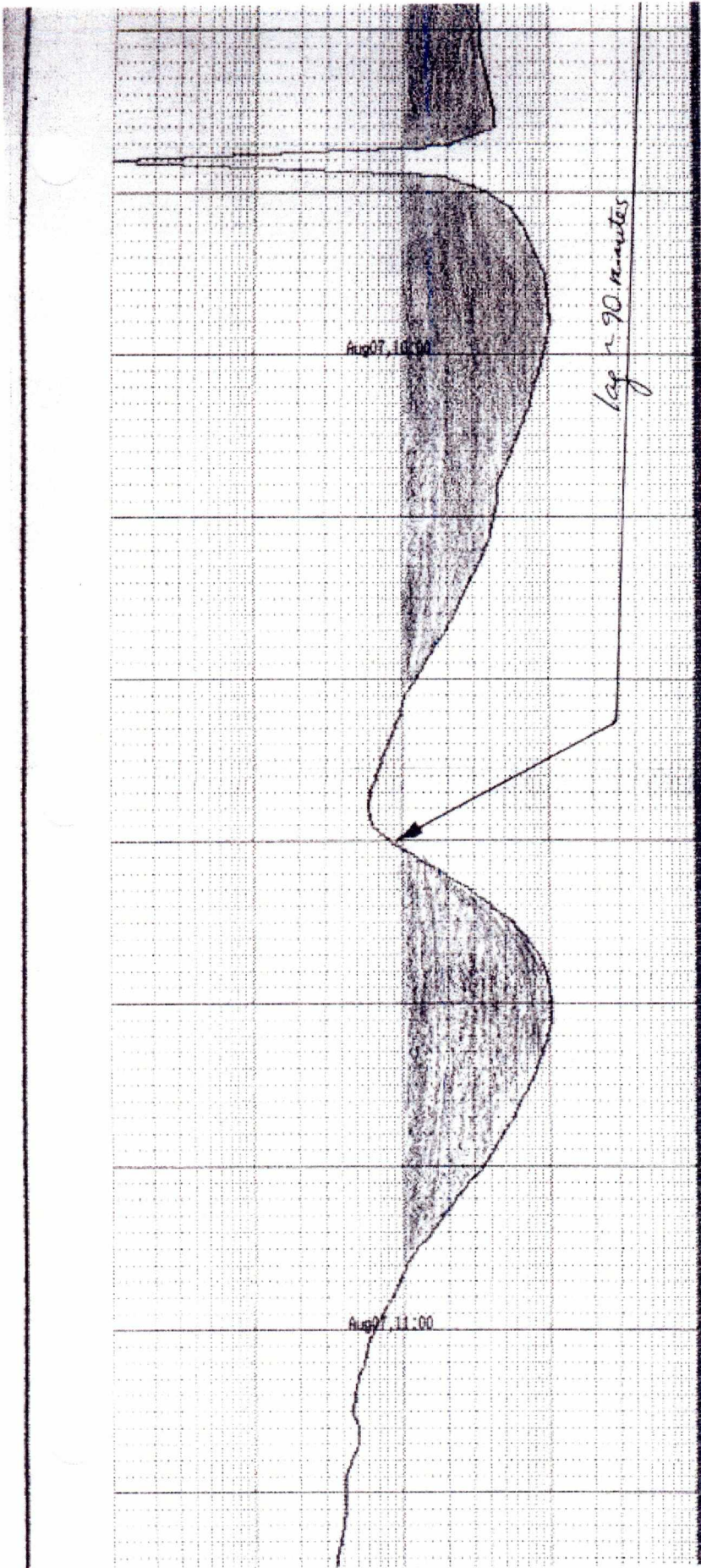
3450 7.1

log ~ 90 minutes

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Appendix II: PP#1-ST2
Total gas log over key intervals

Appendix II:
gas log
p.1



329u
 330u
 334u
 350u
 374u
 397u
 416u
 416u
 217u
 0u
 191u
 381u
 553u
 654u
 745u
 836u
 927u
 977u
 998u
 1008u
 977u
 917u
 866u
 796u
 735u
 674u
 614u
 553u
 492u
 442u
 444u
 422u
 397u
 363u
 326u
 283u
 254u
 221u
 193u
 166u
 143u
 123u
 108u
 97u
 88u
 79u
 72u
 66u
 61u
 58u
 62u
 82u
 123u
 195u
 290u
 397u
 552u
 692u
 823u
 923u
 993u
 1003u
 1003u
 953u
 873u
 803u
 712u
 632u
 552u
 472u
 402u
 340u
 278u
 226u
 187u
 154u
 127u
 108u
 94u
 82u
 71u
 53u
 57u
 54u
 50u
 47u
 45u
 49u
 49u
 44u
 40u
 40u
 40u
 39u
 37u
 35u

Gas maximum 1008 units

MAX 1003 u

gas log p.3

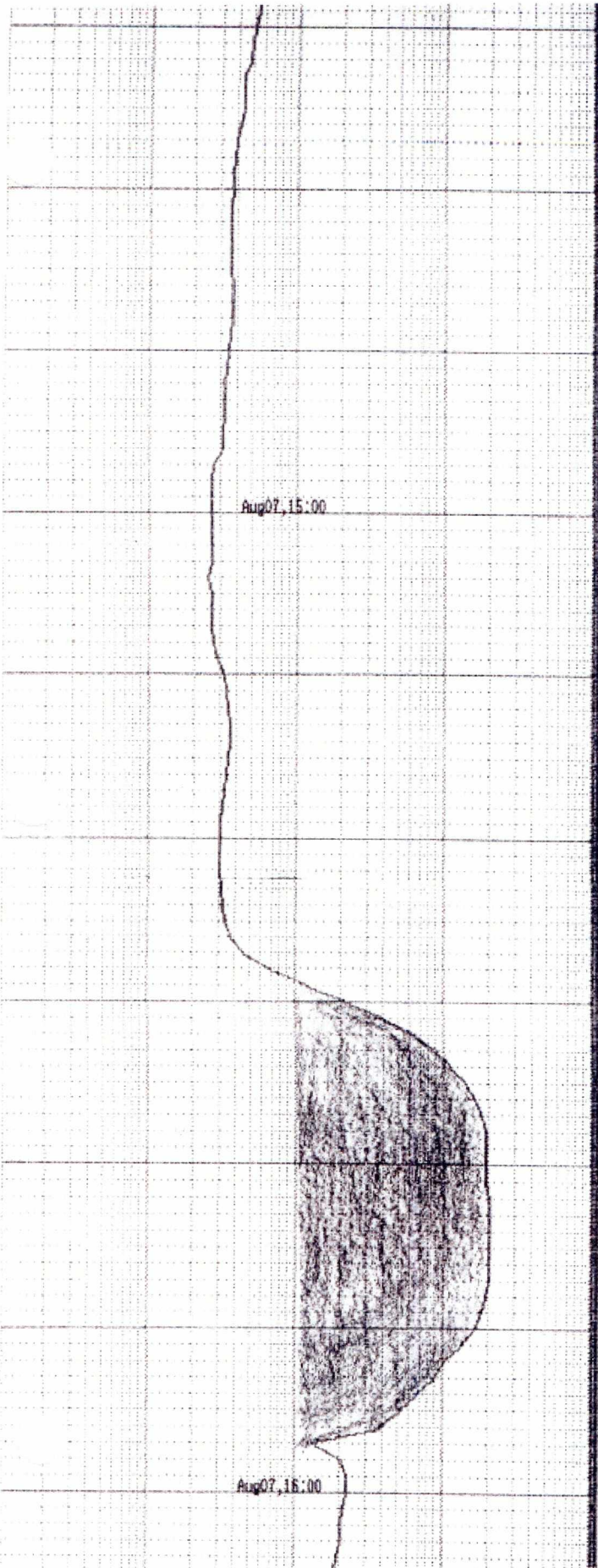


3454 10.6
 3455 8.8
 3456 8.4
 3457 12.3
 3458 17.3
 3459 16.0

~ ~ ~ SGU ~ ~ ~
 AGUATHUNA
 FM.

59u
58u
58u
60u
61u
63u
64u
65u
67u
69u
69u
71u
72u
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73u
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62u
49u
12u
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29u
32u
22u
49u
63u
63u
42u
41u
61u
67u
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53u
52u
51u
50u
49u
49u
47u
47u
46u
45u

gas log
 p. 9



Interval
3460 - 3465 m.

Max
2076 u

- 52u
- 49u
- 48u
- 47u
- 43u
- 43u
- 40u
- 38u
- 37u
- 36u
- 36u
- 35u
- 35u
- 35u
- 36u
- 36u
- 36u
- 35u
- 34u
- 33u
- 32u
- 32u
- 32u
- 31u
- 31u
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- 29u
- 32u
- 33u
- 34u
- 35u
- 35u
- 34u
- 33u
- 32u
- 31u
- 30u
- 30u
- 30u
- 30u
- 31u
- 32u
- 33u
- 36u
- 44u
- 66u
- 121u
- 228u
- 361u
- 622u
- 893u
- 1193u
- 1464u
- 1685u
- 1835u
- 1906u
- 1946u
- 1956u
- 1956u
- 2006u
- 2056u
- 2076u
- 2076u
- 2076u
- 2046u
- 1966u
- 1815u
- 1605u
- 1364u
- 1083u
- 852u
- 662u
- 511u
- 379u
- 135u
- 206u
- 225u
- 225u
- 218u
- 209u
- 201u
- 195u

gas log
p. 6